## **Supporting Information**

## Synergistic Effect of Mo-W Carbides on Selective Hydrodeoxygenation of Guaiacol to Oxygen-Free Aromatic Hydrocarbons

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## External and internal mass transfer evaluation via Mears' criteria and Thiele module.

The Mears' criterion,  $C_m$ , is the ratio of the rate of reaction to the external diffusion rate [1]. The effect of external mass transfers can be neglected if the Mears' criterion calculated to be below than 0.15:

$$C_m = \frac{-r_{A(obs)} \times \rho_b \times R \times n}{k_c \times C_{Ab}} < 0.15$$

where  $r_{A(obs)}$  is the observed reaction rate per unit mass of catalyst (kmol kg<sup>-1</sup> s<sup>-1</sup>);  $p_b$  is catalyst bed density (kg m<sup>-3</sup>) calculated as  $p_b = (1-\varepsilon) p_c$  ( $\varepsilon$  is catalyst bed porosity,  $p_c$  catalyst density); R is catalyst particle radius (m); n is the reaction order;  $k_c$  is mass transfer coefficient for reactant (m s<sup>-1</sup>);  $C_{Ab}$  is the concentration of reactant (kmol m<sup>-3</sup>).

The  $\varepsilon$  porosity of catalyst bed is estimated as 0.3 and  $p_c$  catalyst density is reported to be  $\Box$ 760 kg m<sup>-3</sup>. In order to calculate the Mears' criterion, determination of  $k_c$  is required. Mass transfer coefficient ( $k_c$ ) is estimated via the equation of Sherwood number (Sh): Sh = ( $k_c \times 2R$ )/D<sub>e</sub> (where D<sub>e</sub> is the estimated diffusivity of reactant and is calculated as 7.6 × 10<sup>-6</sup> cm<sup>2</sup> s<sup>-1</sup> by using Wilke-Lee equation [2]). The influence of external mass transfer can be neglected due to the calculated Mears' criterion lower than 0.15 (Table S1)

**Table S1**. Parameters and data for calculating the Mears' criterion to estimate the external mass transfer limitation in guaiacol HDO reaction.

Parameters	
$r_{A(obs)}$ (kmol kg <sup>-1</sup> s <sup>-1</sup> )	$\Box 2.06 \times 10^{-6}$
$p_b$ (kg m <sup>-3</sup> )	□532
<i>R</i> (m)	$\Box 1.0 \times 10^{-4}$
n	□0.99
$k_c (\mathrm{m}\mathrm{s}^{-1})$	0.076
$C_{Ab}$ (kmol m <sup>-3</sup> )	0.45
Estimated Mears' criterion	$3.17 \times 10^{-6}$

Thiele module,  $\phi$ , is the ratio of reaction rate to diffusion rate inside the catalyst and is calculated below:

$$\Phi = \frac{-r_{A(obs)} \times \rho_c \times R^2}{D_e \times C_{As}} = \eta \phi^2$$

where  $r_{A(obs)}$  is the observed reaction rate per unit mass of catalyst (kmol kg<sup>-1</sup> s<sup>-1</sup>);  $p_c$  is the catalyst density (kg m<sup>-3</sup>); R is catalyst particle radius (m);  $D_e$  is the estimated diffusivity of reactant at 623K (m<sup>2</sup> s<sup>-1</sup>);  $C_{As}$  is the reactant concentration at the catalyst surface (kmol m<sup>-3</sup>);  $\eta$  is the internal effectiveness factor and  $\phi$  is the Thiele module. If  $\eta \rightarrow 1$ , the internal mass transfer inside the catalyst pellet has no resistance and in contrast, if  $\eta \rightarrow 0$ , the internal mass diffusion is the rate limiting step. Due to the negligible external mass transfer,  $C_{Ab}$  supposes to be equal to  $C_{As}$ . Based on the date in Table S1 and the calculated  $D_e$  earlier, Thiele module  $\phi$  is calculated to be 0.0021. Small value of the Thiele module indicates the rate of the internal mass transfer is faster than the reaction rate, thus the effect of internal mass diffusion can be neglected.



Figure S1. Continuous flow process diagram of HDO system



Figure S2. XPS survey spectrum of Mo<sub>2</sub>C.



Figure S3. XPS survey spectrum of MoWC



Figure S4. XPS survey spectrum of WC-700



Figure S5. Mo 3d and W 4f XPS spectra of mechanically mixed Mo<sub>2</sub>C+WC sample.



Figure S6. Intrinsic rates of guaiacol conversion over metal carbides at 350°C and 400 psig.

Catalyst	Reactor	Temperature (°C)	P (psig)	Major product	Conversion (%)	Deoxygenation (%) <sup>a</sup>	Ref
Ru/C	Fixed-bed	350	580	benzene	34.2	39.6	3
Pd/C	Fixed-bed	350	580	methoxy- cyclohexane	15	23.3	3
Pt/MgO	Fixed-bed	300	20	phenol	9	□0.3	9
$Pt/AL_2O_3$	Fixed-bed	300	20	Catechol	6	$\Box 0.1$	9
PtRh/ZrO <sub>2</sub>	Batch reactor	300-400	725	methoxy- cyclohexanol	100	40	7
Pt/Mo <sub>2</sub> C	Fixed-bed	350	70	benzene	98	99	8
Pd/Mo <sub>2</sub> C	Fixed-bed	350	70	benzene	99	81	8
$\alpha$ -MoC <sub>1-x</sub> /AC <sup>b</sup>	Batch reactor	340	ambient	phenol	87	-	4
Mo <sub>2</sub> C/CNF <sup>d</sup>	Batch reactor	350	725	phenol	99	3	5
Mo <sub>2</sub> C/CNT <sup>c</sup>	Batch reactor	350	580	catechol	91	-	6
Mo <sub>2</sub> C/CNF	Batch reactor	300	290	phenol	67		10
СоМо	Batch reactor	400	725	phenol	< 15	-	7
NiMo	Batch reactor	400	725	cyclohexane	< 15	-	7
W <sub>2</sub> C/CNF	Batch reactor	350	725	phenol	66	4	5
NiMoW sulfide	Fixed-bed	350	400	phenol	99	28	11
MoWC	Fixed-bed	350	400	benzene	93	92	This report

Table S2. Comparison of deoxygenation activity of guaiacol over various catalysts

<sup>a</sup> Total selectivity of non-oxygen containing compounds (i.e. benzene, toluene, hexane, hexene) <sup>b</sup> Activated carbon; <sup>c</sup> Carbon nanotube; <sup>d</sup> Carbon nanofiber

Table S3	. Conversion of guaiacol at various	temperatures over n	netal carbides and t	he intrinsic reaction
rate at 35	0°C and 400 psig, 1 hour on stream			

Catalyst		Conversion (%)		
	250°C	300°C	350°C	$(10^{-4} \text{ mole}_{\text{Guai}} \text{ atom}_{(\text{Mo+W})^{-1}} \text{ s}^{-1})$
Mo <sub>2</sub> C	35.1	72.4	78.1	3.6
WC	12.1	14.8	27.2	2.6
MoWC	52.9	77.6	93.3	4.7
Mo <sub>2</sub> C+WC	25.5	27.6	38.9	2.1

\* Average rate over the first 60 mins

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