

Boosting biomass valorisation. Synergistic design of continuous flow reactors and water-tolerant polystyrene acid catalysts for a non-stopping production of esters

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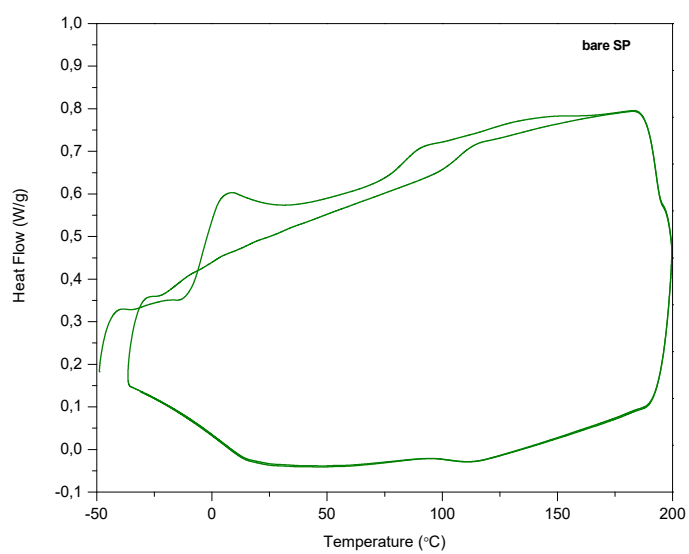


Figure S1. DSC plot for bare SP resin.

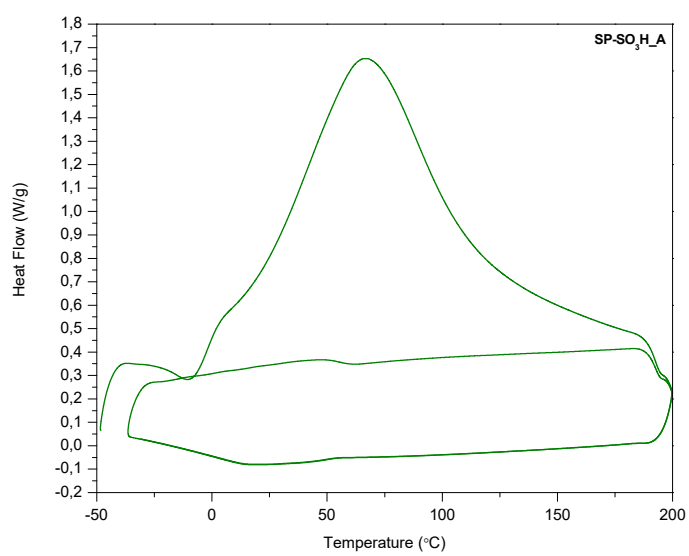


Figure S2. DSC plot for SP-SO₃H_A.

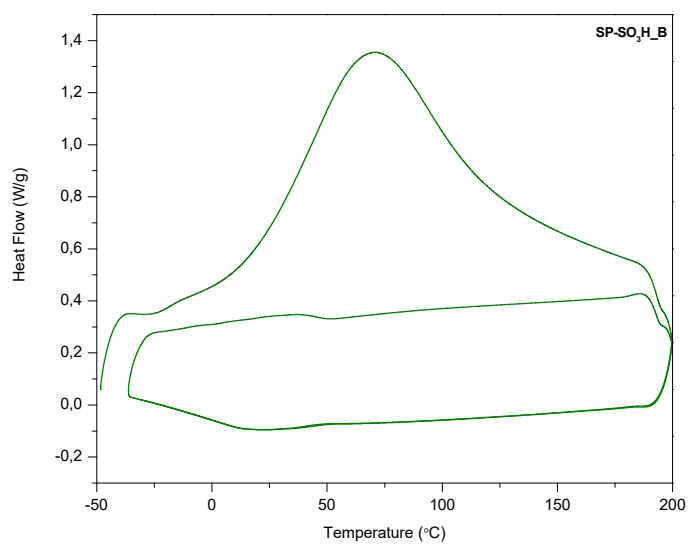


Figure S3. DSC plot for SP-SO₃H_B.

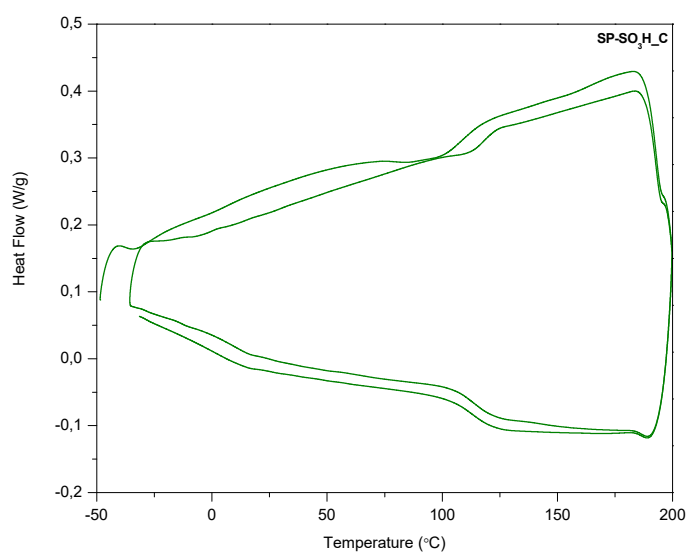


Figure S4. DSC plot for SP-SO₃H_C.

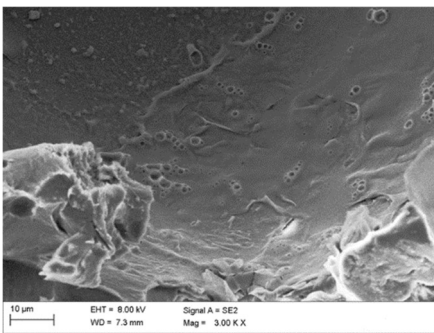
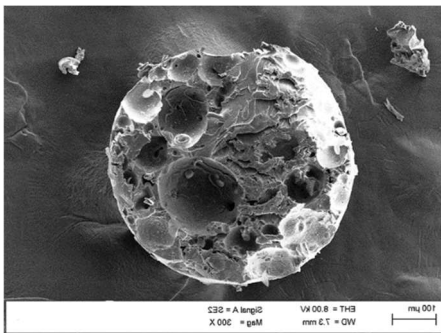
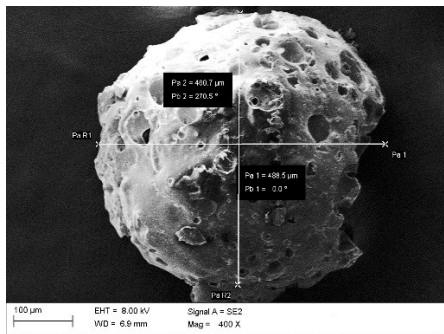


Figure S5. Representative SEM images of external (upper panel) and internal (lower panel) surface of bare SP resin

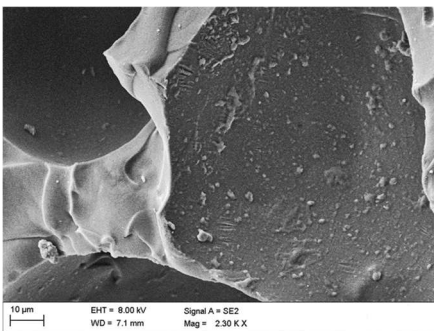
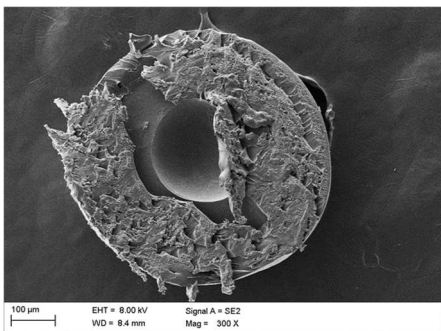
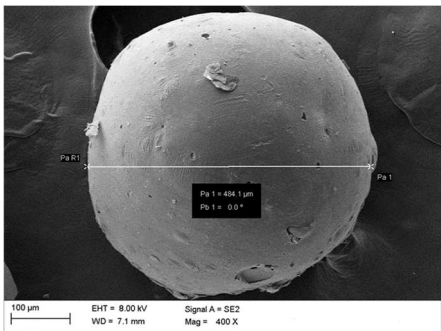


Figure S6. Representative SEM images of external (upper panel) and internal (lower panel) surface of bare SP-SO₃H_B

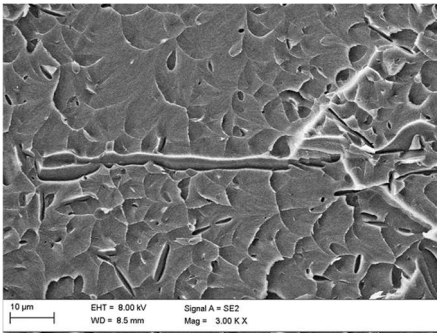
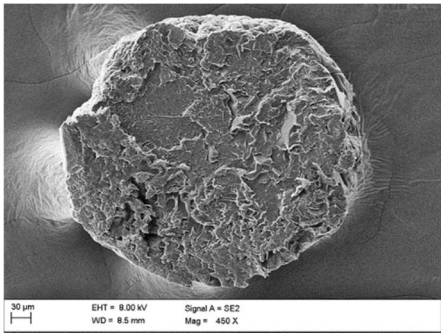
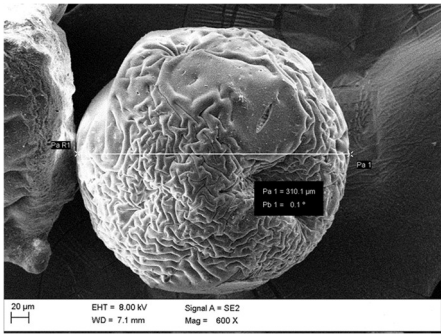


Figure S7. Representative SEM images of external (upper panel) and internal (lower panel) surface of bare SP-SO₃H_C

Table S1. Esterification¹ reaction of LA **5** with 1-pentanol (**6a**) catalyzed by SP-SO₃H_B-C

Entry	Catalyst	t (h)	C (%) ²
1		1	81
2	SP-SO ₃ H_B	2	88
3		5	>99
4		1	70
5	SP-SO ₃ H_C	2	72
6		5	85

¹Reaction conditions: LA/1-pentanol = 1:10 molar ratio; T=70°C; catalyst amount: 10 mol% (referred to the amount of immobilized -SO₃H moieties). ² Determined by GLC analysis, by methylating residual LA with diazomethane; remaining material was the unreacted mixture of LA and 1-pentanol.

Table S2. Esterification reaction of LA **5** with 1-pentanol (**6a**) catalyzed by SP-SO₃H_A

Entry	Catalyst (mol%) ¹	LA/ 1-pentanol	T (°C)	t (h)	C (%) ²
1	4.3	1:5	50	1	63
2	8			78	
3	10			76	
4	4.3			2	54
5	8			78	
6	10			79	
7	4.3			5	75
8	8			85	
9	10			83	
10	4.3		1	82	
11	8		86		
12	10		79		
13	4.3		2	86	
14	8		70	93	
15	10		80		
16	4.3		5	90	
17	8		95		
18	10		85		
19	4.3	1:10	50	1	45
20	8			73	
21	10			64	
22	4.3			2	46
23	8			73	
24	10			72	
25	4.3			5	60
26	8			82	
27	10			82	
28	4.3		1	58	
29	8		77		
30	10		85		
31	4.3		2	83	
32	8		70	93	
33	10		94		
34	4.3		5	90	
35	8		>99		
36	10		>99		
		>99 ³			

¹Referred to the amount of immobilized -SO₃H moieties. ² Determined by GLC analysis, by methylating residual LA with diazomethane; remaining material was the unreacted mixture of LA and 1-pentanol; ³Molecular sieves (1:1 wt/wt_{LA}).

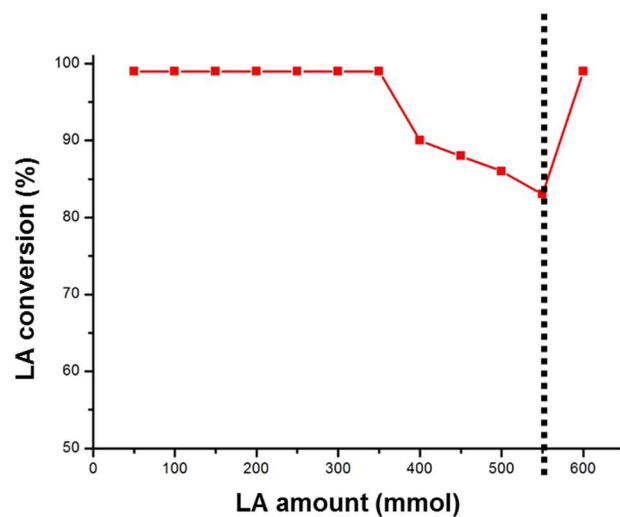


Figure S8. Graphic chart of continuous flow levulinic acid (LA, **5**) feeding (X-axis) and corresponding conversion to **7a** (Y-axis).

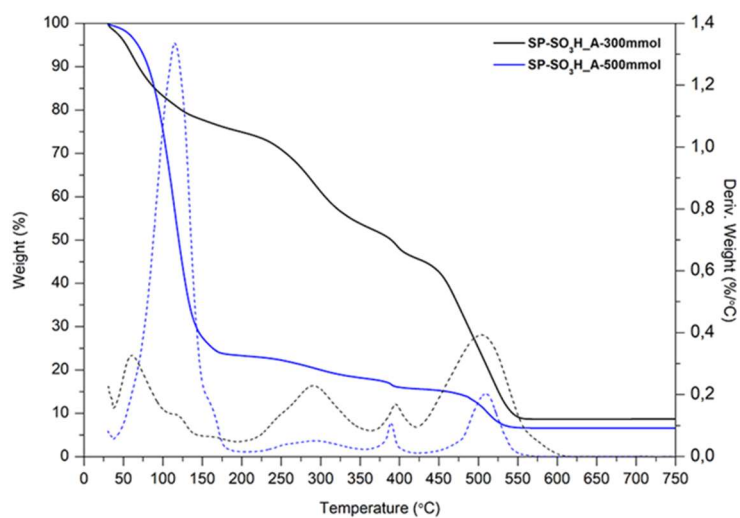


Figure S9. TGA and DTG curves of SP-SO₃H_A samples; Weight loss curves (solid lines) and their respective 1st derivatives (dashed lines) for sample withdrawn at 300 (blue curves) and 500 mmol (black curves) LA conversion.

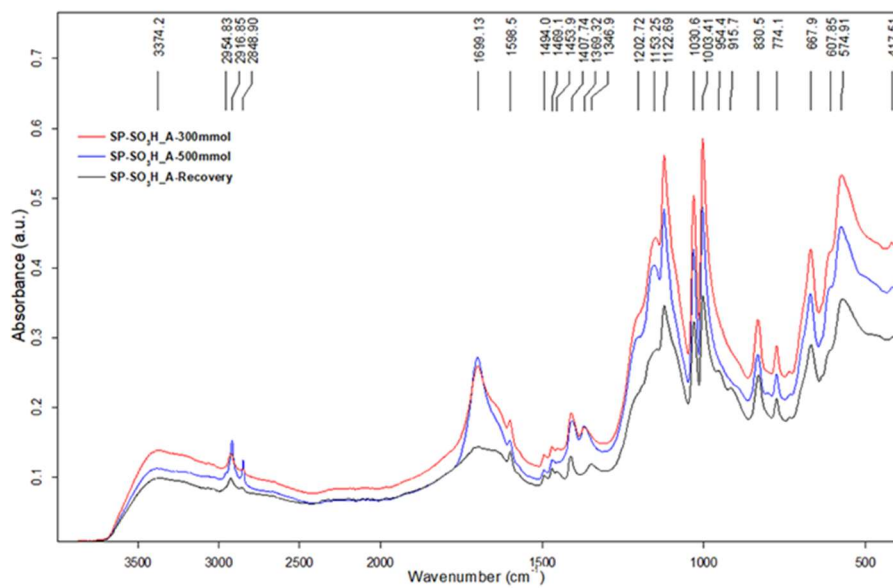


Figure S10. FTIR plots of SP-SO₃H_A samples withdrawn at 300 (red line) and 500 mmol (blue line) LA conversion. FTIR pattern of regenerated SP-SO₃H_A (black line) is also reported for comparison purposes.

E-factor calculation for the esterification reaction of LA (5) with 1-pentanol (6a) under flow conditions.

E-factor: $[58 \text{ g (LA)} + 440 \text{ g (1-pentanol)} - 91 \text{ g (pentyl levulinate 7a)} - 380 \text{ g (96\% recovered excess 1-pentanol)}] / 91 \text{ g (pentyl levulinate 7a)} = \underline{0.29}$

E-factor calculation for the esterification reaction of LA (5) with ethanol (6b) under flow conditions.

E-factor: $[11.6 \text{ g (LA)} + 46 \text{ g (ethanol)} - 13.4 \text{ g (ethyl levulinate 7b)} - 39.3 \text{ g (95\% recovered excess ethanol)}] / 13.4 \text{ g (ethyl levulinate 7b)} = \underline{0.36}$

The Al_2O_3 scavenger was not considered in the calculation due to its complete regeneration.

E-factor calculation for the esterification reaction of LA (5) with octanol (6e) under flow conditions.

E-factor: $[11.6 \text{ g (LA)} + 130 \text{ g (1-octanol)} - 20.06 \text{ g (octyl levulinate 7e)} - 105.3 \text{ g (90\% recovered excess 1-octanol)}] / 20.06 \text{ g (octyl levulinate 7e)} = \underline{0.81}$

The Al_2O_3 scavenger was not considered in the calculation due to its complete regeneration.

E-factor calculation for the esterification reaction of LA (5) with i-propanol (6g) under flow conditions.

E-factor: $[11.6 \text{ g (LA)} + 60 \text{ g (i-propanol)} - 14.22 \text{ g (i-propyl levulinate 7g)} - 48.6 \text{ g (90\% recovered excess i-propanol)}] / 14.22 \text{ g (i-propyl levulinate 7g)} = \underline{0.61}$

The Al_2O_3 scavenger was not considered in the calculation due to its complete regeneration.

E-factor calculation for the esterification reaction of LA (5) with sec-butanol (6h) under flow conditions.

E-factor: $[11.6 \text{ g (LA)} + 74 \text{ g (sec-butanol)} - 15.48 \text{ g (sec-butyl levulinate 7h)} - 58.6 \text{ g (88\% recovered excess sec-butanol)}] / 15.48 \text{ g (sec-butyl levulinate 7h)} = \underline{0.74}$

The Al_2O_3 scavenger was not considered in the calculation due to its complete regeneration.

E-factor calculation for the esterification reaction of 3-HB (8) with butanol (6d) under flow conditions.

E-factor: $[10.4 \text{ g (3-HBA)} + 74 \text{ g (1-butanol)} - 15.52 \text{ g (butyl-3-hydroxybutyrate 9)} - 61.3 \text{ g (92\% recovered excess 1-butanol)}] / 15.52 \text{ g (butyl-3-hydroxybutyrate 9)} = \underline{0.49}$