## **Supplementary Information**

## Designable Dirac Point Voltage of Graphene by Mechanical Bending Ferroelectric gate of Graphene Field Effect Transistor and Its Multifunctional Application

Guangliang Hu<sup>ab</sup>, Jingying Wu<sup>b</sup>, Chunrui Ma<sup>\*a</sup>, Zhongshuai Liang<sup>b</sup>, Weihua Liu<sup>b</sup>, Ming Liu<sup>b</sup>,

Judy Z. Wu<sup>c</sup>, Chun-Lin Jia<sup>bd</sup>

- <sup>a</sup> State Key Laboratory for Mechanical Behavior of Materials, Xi'an Jiaotong University, Xi'an,
   710049, China
- <sup>b</sup> School of Electronic and Information Engineering, Xi'an Jiaotong University, Xi'an, 710049, China
- <sup>c</sup> Department of Physics and Astronomy, University of Kansas, Lawrence, Kansas, 66045, USA
- <sup>d</sup> Ernst Ruska Centre for Microscopy and Spectroscopy with Electrons, Forschungszentrum Jülich

<sup>\*</sup> Address correspondence to: <u>chunrui.ma@mail.xjtu.edu.cn</u>

## Mechanical model for strain gradient in the PLZT film.

The strain gradient formed in the PLZT film can be estimated using a mechanical model as below: A sample (films with substrate) with *L* for length, *W* for width and *h* for thickness was considered. Along the thickness direction, we assumed that the length at h/2 is not change when the sample was bent at a certain radius ( $r_0$ ). For the upward bending state, as shown in the Figure. S4 (a), the angle ( $\theta$ ) corresponding to the sample can be expressed as

$$\theta = \frac{180}{\pi} \cdot \frac{L}{r_0 + \frac{h}{2}} \tag{1}$$

Therefore, the length (L') of the sample at r can be expressed as

$$L' = \frac{\theta \cdot \pi}{180} \cdot r = L \cdot \frac{r}{r_0 + \frac{h}{2}}$$
(2)

The strain (u) at r can be expressed as

$$u = \frac{L - L}{L} = \frac{r}{r_0 + \frac{h}{2}} - 1$$
(3)

So, the strain gradient  $(\frac{\partial u}{\partial r})$  can be written as

$$\frac{\partial u}{\partial r} = \frac{1}{r_0 + \frac{h}{2}}$$
(4)

For downward bending state, as shown in the Figure. S4 (b), the strain gradient can be

$$\frac{\partial u}{\partial r} = \frac{1}{r_0 - \frac{h}{2}}$$
 estimated as similar mechanical model.



**Figure S1.** (a) A typical XRD  $\theta$ -2 $\theta$  scans for the PLZT/LSMO/STO multilayer on F-Mica. (b)  $\varphi$  scans taken around the (202) reflections of the F-Mica substrate (top), (002) reflections of the LSMO/STO layer (bottom).



**Figure S2.** (a)  $I_D$ - $V_G$  curves at different downward bending radius. (b)  $I_D$ - $V_G$  curves at different bending cycles under 6 mm downward bending radius.



**Figure S3.** (a)  $I_D$ - $V_G$  curves at different bending cycles under 6 mm upward bending radius ( $V_D$ =10 mV). (b)  $V_{Dirac}$  of curves in (a) at different bending cycles under 6 mm upward bending radius



Figure S4. Mechanical model for upward bending state (a) and downward bending state (b).



Figure S5. The capacitance of the PLZT under the voltage of 2 V.



Figure S6. (a) *P-E* loops at different bending cycles and at the voltage of 2 V after different downward bending cycles (6 mm bending radius). (b) and (c) are  $V_c$  and  $P_r$  after different bending cycles in (a), respectively.