

Electronic Supplementary Material (ESI) for Nanoscale.

Reprogrammable Multifunctional Chalcogenide Guided-wave Lens

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Section 1. Derivation of the refractive index profile of the curvature

As can be observed in the right column of Fig.1b, the curved surface S is produced by rotating a curve C symmetrically about the z -axis. The other two cylindrical coordinates are ρ and ϑ . Herein, we specify the curve C and thus the surface S by providing $\rho(s)$ or $s(\rho)$ where s is the arc distance measured along the C . One could use as the surface coordinates either s and ϑ or, on occasions, ρ and ϑ . The surface metric that gives the distance dL between the neighboring points is shown by

$$dL^2 = ds^2 + \rho^2 d\theta^2 \quad \backslash^*$$

MERGEFORMAT (S1)

If we multiply the dL by n , the refractive index and optical distance $d\zeta$ between the neighboring points can be expressed by

$$d\zeta^2 = n^2 (ds^2 + \rho^2 d\theta^2) \quad \backslash^*$$

MERGEFORMAT (S2)

If s and ϑ are treated as the independent variables, Eq. (S2) may be rewritten as

$$d\zeta^2 = n(s)^2 (ds^2 + \rho(s)^2 d\theta^2) \quad \backslash^*$$

MERGEFORMAT (S3)

However, if ρ and ϑ are chosen, it can be alternatively written as

$$d\zeta^2 = N(\rho)^2 (s'(\rho)^2 d\rho^2 + \rho^2 d\theta^2) \quad \backslash^*$$

MERGEFORMAT (S4)

where $N(\rho)=n(s)$. If we employ the bars over the quantities to present those relating to a particular structure and unbarred quantities for those associated with other equivalent structure³⁴, the equivalence of the optical metrics, by Eq.(S2), requires

$$n^2 (ds^2 + \rho^2 d\theta^2) = \bar{n}^2 (\bar{d}\bar{s}^2 + \bar{\rho}^2 \bar{d}\bar{\theta}^2) \quad \backslash^*$$

MERGEFORMAT (S5)

where $nds = \bar{n}\bar{d}\bar{s}$, $n\rho = \bar{n}\bar{\rho}$, and $\theta = \bar{\theta}$. It thus results in the behind set of integral relationships,

$$\int_a^s nds = \int_a^{\bar{s}} \bar{n}\bar{d}\bar{s} \quad \backslash^*$$

MERGEFORMAT (S6)

$$n\rho = \bar{n}\bar{\rho} \quad \backslash^*$$

MERGEFORMAT (S7)

$$\int_b^s ds/\rho = \int_b^{\bar{s}} \bar{d}\bar{s}/\bar{\rho} \quad \backslash^*$$

MERGEFORMAT (S8)

where a and \bar{a} , b and \bar{b} show the values of s and \bar{s} corresponding to the equal points in the two guides³⁴. We can then determine $\bar{n}(\bar{s})$ and $\bar{\rho}(\bar{s})$ when they correspond to the given guide. The mapping function $\bar{s} = f(s)$ can be achieved by solving Eq. (S8) for \bar{s} . By setting $\bar{s} = \bar{\rho} = r$ for a flat guide, Eqs. (S7) and (S8) are derived as following Eqs. (S9) and (S10), respectively.

$$N\rho = n(r)r \quad \backslash^*$$

MERGEFORMAT (S9)

$$\int_b^s ds/\rho = \int_1^r dr/r = \ln r \quad \backslash^*$$

MERGEFORMAT (S10)

Thus the mapping function is

$$r = f(s) = \exp \int_b^s ds/\rho \quad \backslash^*$$

MERGEFORMAT (S11)

where $s=b$ corresponds to $r=1$. One can derive below Eq. (S12) using Eqs. (S9) and (S11).

$$N(s) = n[f(s)]f(s)/\rho(s) \quad \backslash^*$$

MERGEFORMAT (S12)

If one employs ρ as the independent variable in place of s in Eq. (S11), we can then have

$$F(\rho) = \exp \int_1^\rho [s'(\rho)/\rho] d\rho \quad \backslash^*$$

MERGEFORMAT (S13)

By replacing $f(s)$ in Eq. (S12) with Eq.(S13), the refractive index of the curved surface can be derived as

$$N(\rho) = n[F(\rho)]F(\rho)/\rho \quad \backslash^*$$

MERGEFORMAT (S14)

The left-hand side of Eq. (S14) can be applied to the arbitrary rotationally symmetric curved surface on which light can propagate. We take an example of a Rinehart-shaped surface of which the arc distance s can be expressed as $s = \frac{1}{2}\rho + \frac{1}{2}\sin^{-1}\rho$.

An analytical solution of Eq. (S14) regarding the Rinehart-shaped surface can be expressed as

$$N(\rho) = \frac{2}{\left(1 + \sqrt{1 - \rho^2}\right)^{\frac{1}{2}} \left(e^{\frac{\rho}{\left(1 + \sqrt{1 - \rho^2}\right)^{\frac{1}{2}}}} + e^{\frac{-\rho}{\left(1 + \sqrt{1 - \rho^2}\right)^{\frac{1}{2}}}} \right)} \quad \backslash^*$$

MERGEFORMAT (S15)

The proposed approach allows gradient index lenses to be mapped onto arbitrary rotationally symmetric curved surfaces to manipulate the wavefront of the guided-wave and thus enabling various singular phenomenon. Examples of Einstein's ring, invisible cloak, Maxwell fish-eye, and Luneburg lenses are demonstrated, for Rinehart-shaped surfaces, always leading to the requirements of isotropic permittivity. The structure is simulated by a commercial software COMSOL based on the finite element method. The computational domain has a perfect electric conductor (PEC) boundary for the top and bottom surfaces of the curvature and scattering boundary conditions around the edge. The cylindrical wave is excited by a point source, propagating from left to right with the E -field polarized along the z -axis.

Section 2. Refractive index of the $\text{Ge}_2\text{Sb}_2\text{Te}_5$ at the different structural phase

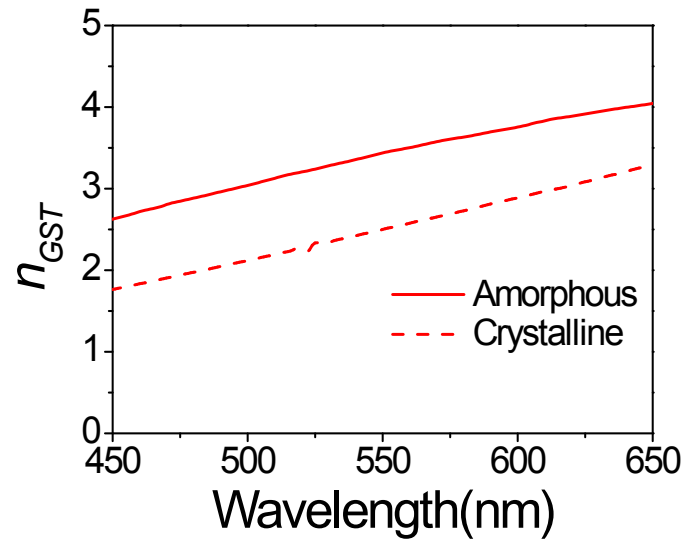


Figure S1. Refractive index n_{GST} vs wavelength for both amorphous and crystalline phases of $Ge_2Sb_2Te_5$ ²⁷.

Section 3. "On/Off" state of the multi-functions in the Rinehart-shaped surface

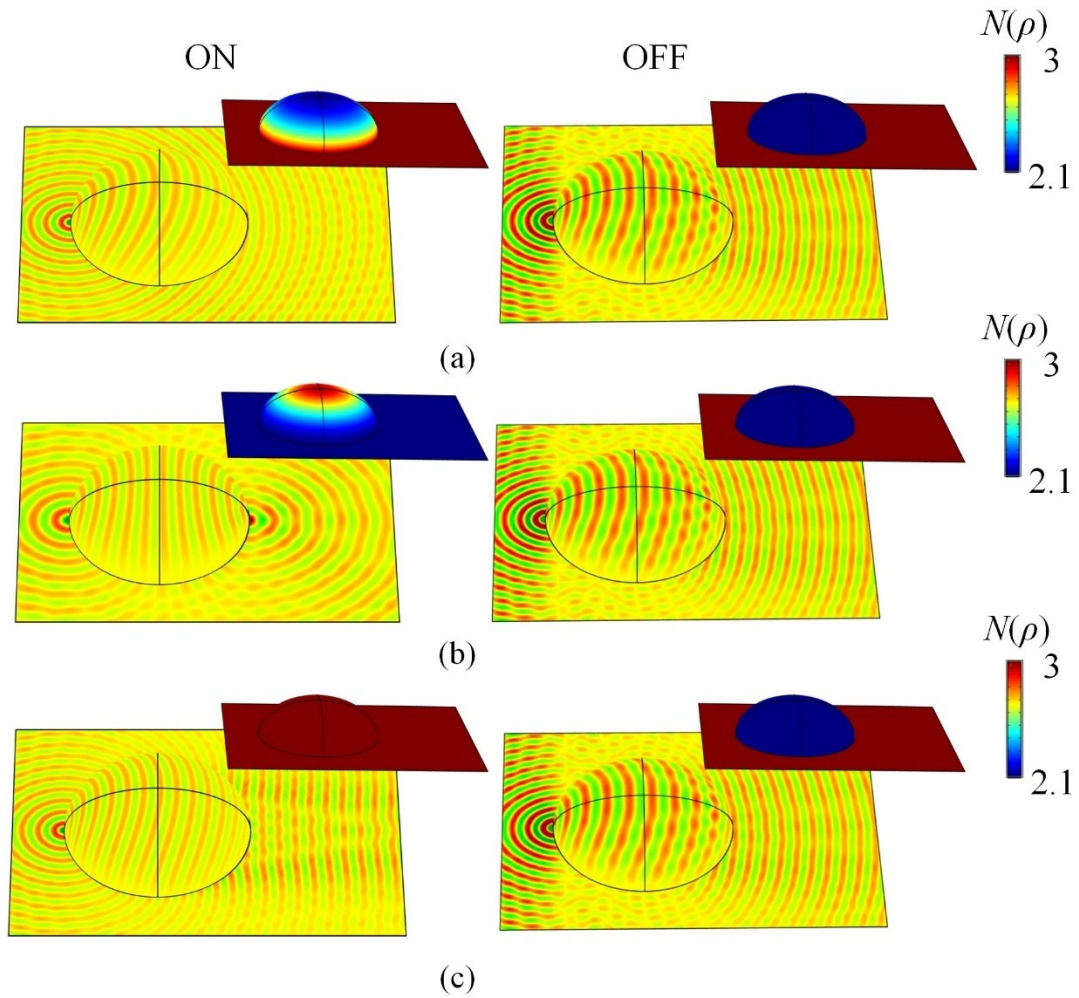


Figure S2. The left (right) columns show "on (off)" state of the functions of (a) invisible cloaking, (b) Maxwell fish-eye lens, and (c) Luneburg lens achieved by the Rinehart-shaped surface consisting of the $\text{Ge}_2\text{Sb}_2\text{Te}_5$ dielectric with the refractive index distributions presented in the insets accordingly. The right columns show that the guided-wave fronts are severely distorted once the $\text{Ge}_2\text{Sb}_2\text{Te}_5$ curvature is homogenously crystallized thus switches off the functionalities accordingly.

Section 4. The multi-functions in the Rinehart-shaped surface with the different discretization process

To explore the effect of the number of $\text{Ge}_2\text{Sb}_2\text{Te}_5$ segments on the phenomenon of Einstein ring, Figure S3 illustrates the propagation of the incident wave ($\lambda=500$ nm) across the curvatures that are divided into 6, 9, 12 and 15 slabs respectively. As can be observed, even the basic discretization of the required index profile (6-layered structure) can collimate the guided-wave. Thus, our design demonstrates an excellent tolerance of fabrication. The effect of the number of the $\text{Ge}_2\text{Sb}_2\text{Te}_5$ segments on the other functions can be found in Figs.S4-S6.

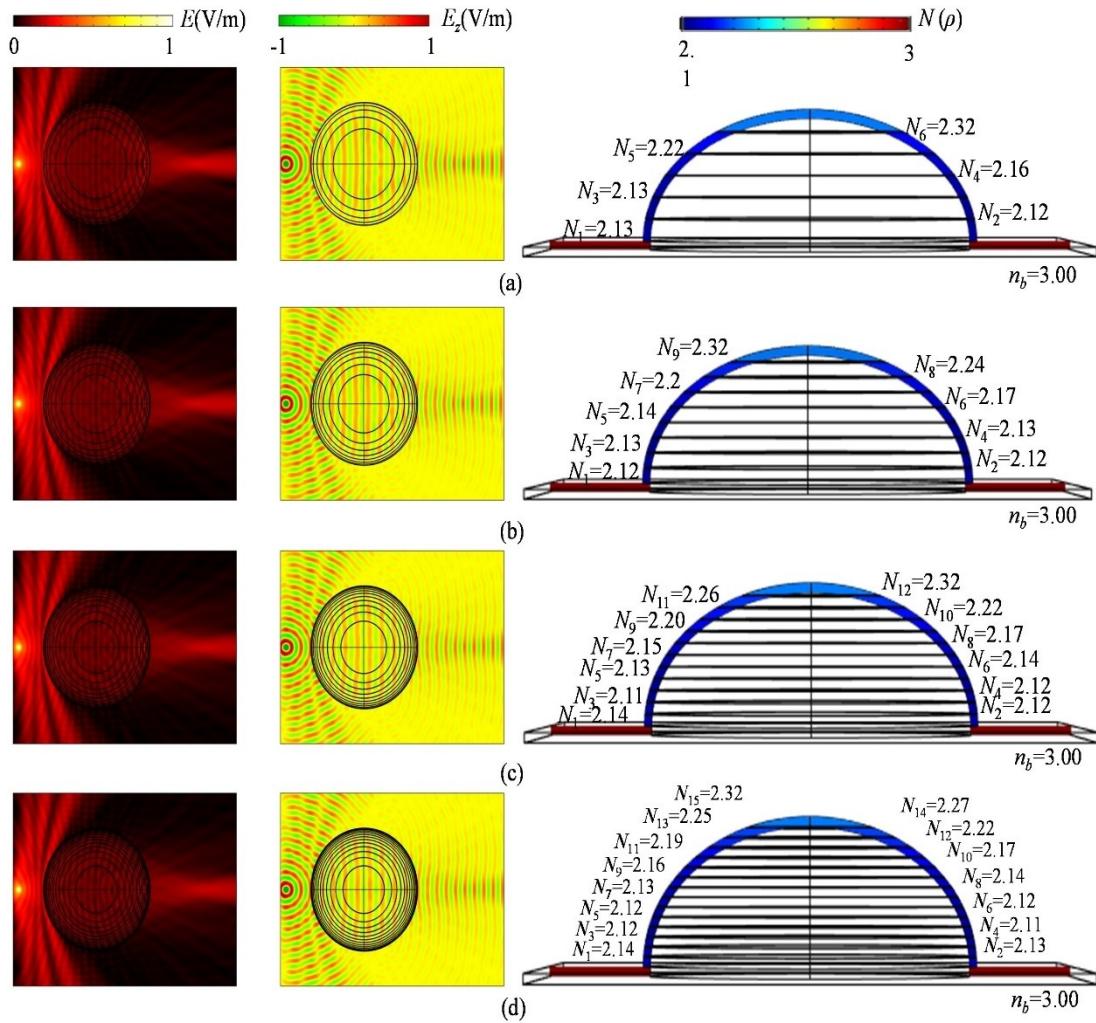


Figure S3. The propagation of E (left column) and E_z (central column) through the surface of (a) 6-layered, (b) 9-layered, (c) 12-layered, and (d) 15-layered Rinehart-shaped curvature at $\lambda = 500$ nm, where the Einstein's ring phenomenon is imitated. The radial cross sections of the different discretization process are illustrated in the right columns.

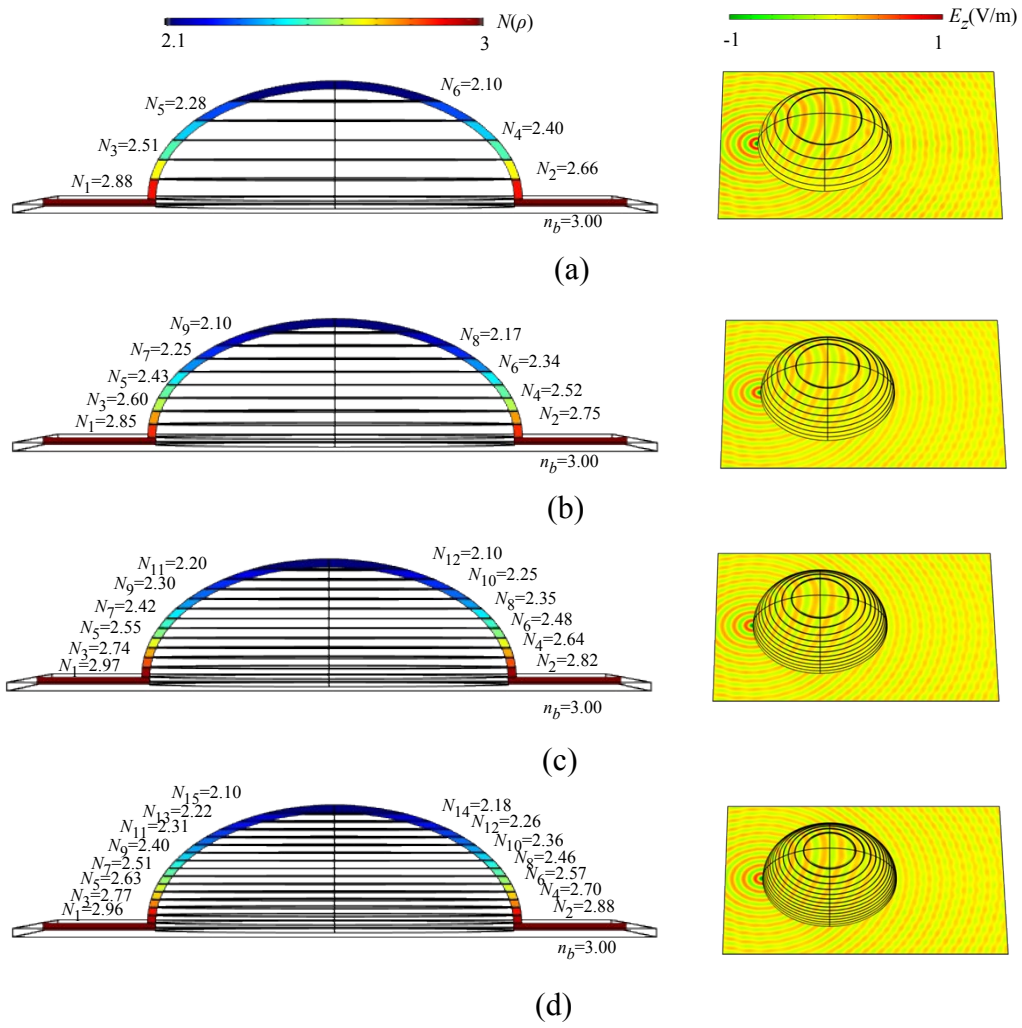


Figure S4. The propagation of E_z (right column) through the surfaces of (a) 6-layered, (b) 9-layered, (c) 12-layered, and (d) 15-layered Rinehart-shaped curvature at $\lambda= 500$ nm, where the optical invisibility phenomenon is imitated. The radial cross sections of the different discretization process are shown in the left columns.

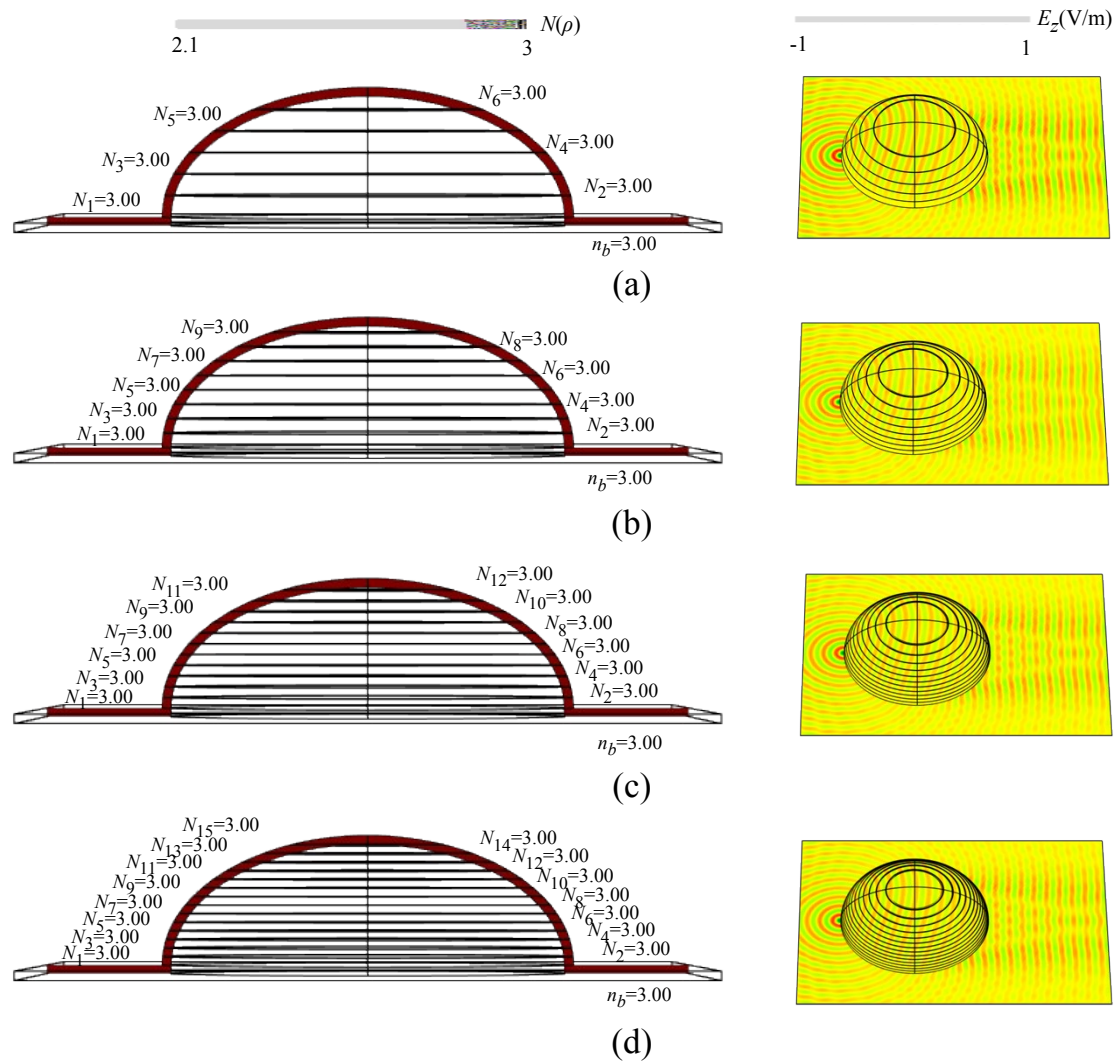


Figure S5. The propagation of E_z (right column) through the surfaces of (a) 6-layered, (b) 9-layered, (c) 12-layered, and (d) 15-layered Rinehart-shaped curvature at $\lambda = 500$ nm, where the Luneburg lens is imitated. The radial cross sections of the different discretization process are illustrated in the left columns.

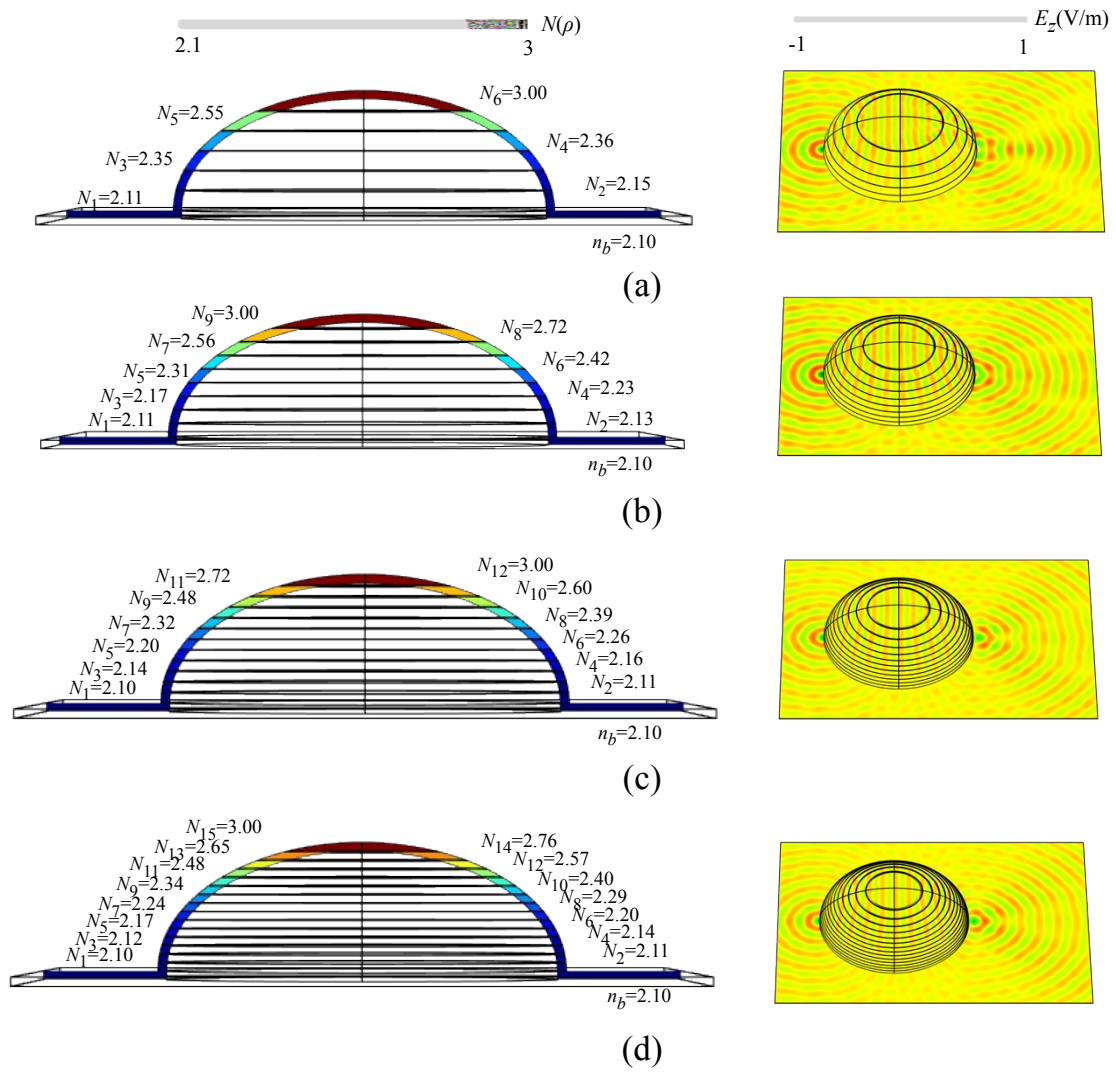


Figure S6. The propagation of E_z (right column) through the surfaces of (a) 6-layered, (b) 9-layered, (c) 12-layered, and (d) 15-layered Rinehart-shaped curvature at $\lambda= 500$ nm, where the Maxwell fish eyes lens is imitated. The radial cross sections of the different discretization process are illustrated in the left columns.

Section 5. The multi-functions in the Rinehart-shaped surface at the different wavelengths

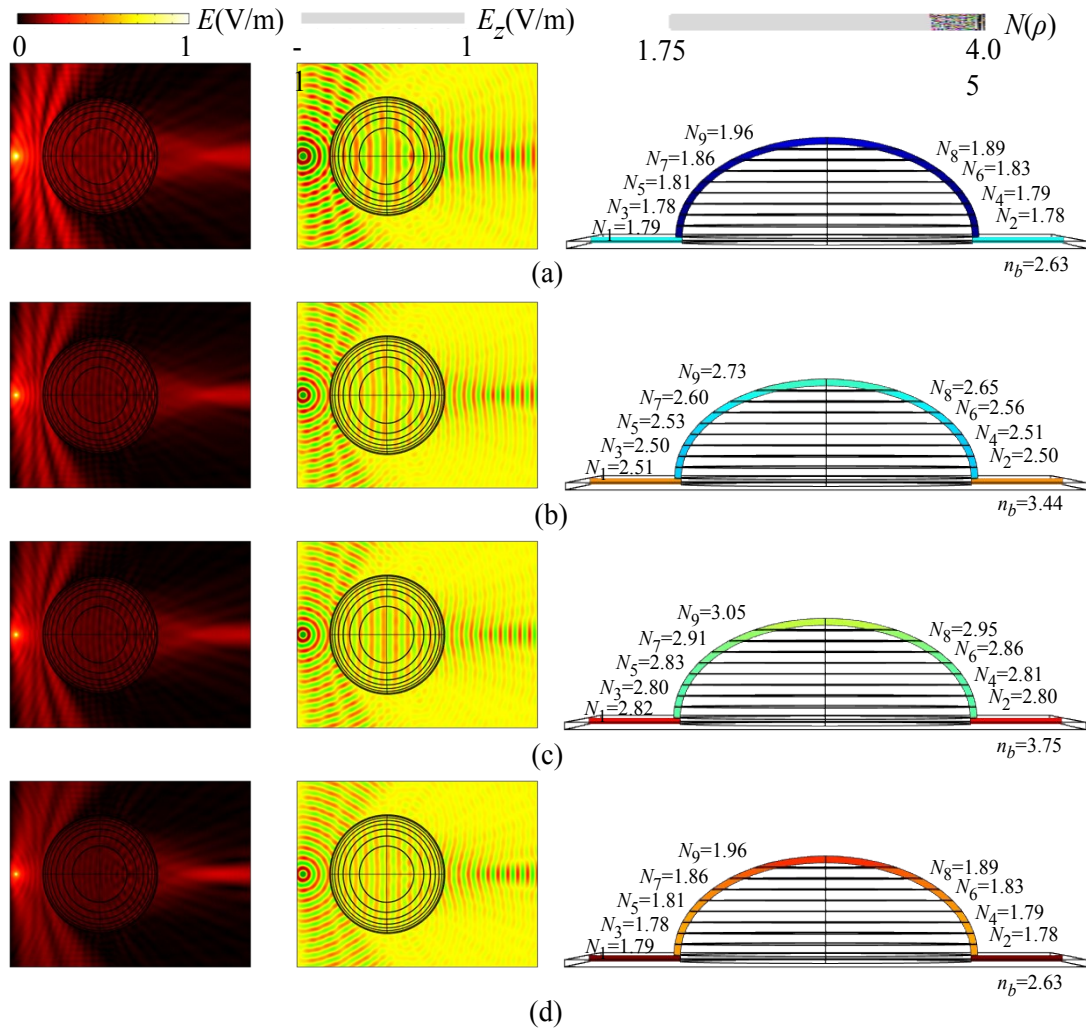
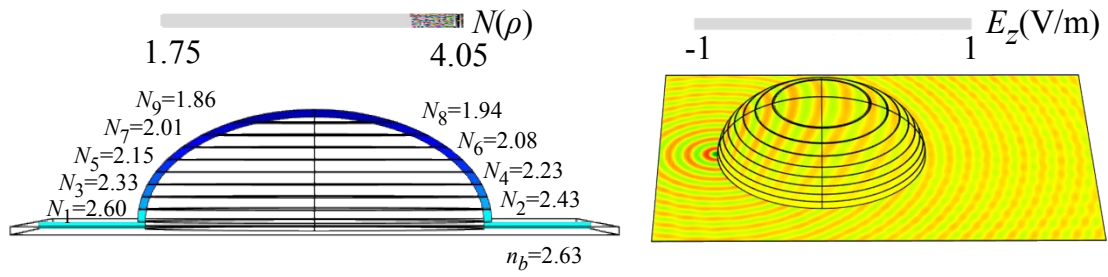
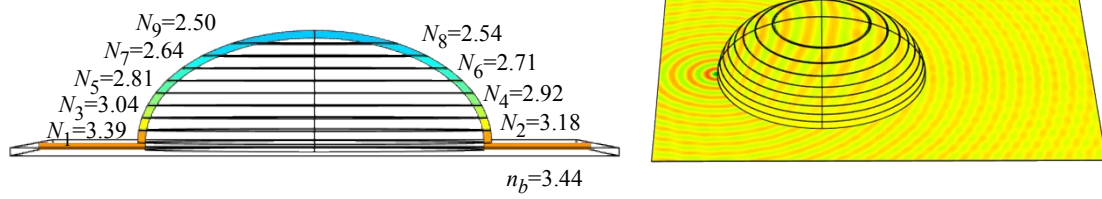


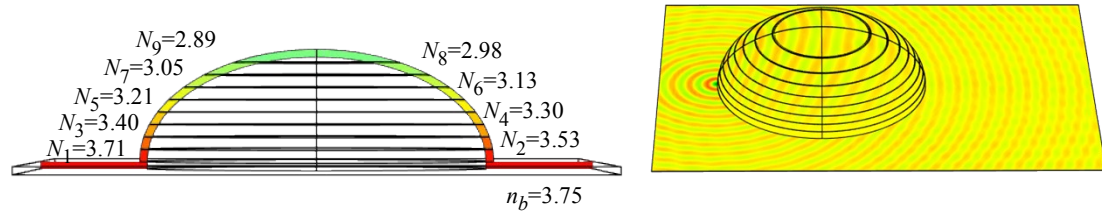
Figure S7. The propagation of E (left column) and E_z (central column) through the surface of 9-layered Rinehart-shaped curvature at (a) $\lambda = 450$ nm, (b) $\lambda = 550$ nm, (c) $\lambda = 600$ nm, and (d) $\lambda = 650$ nm, where the Einstein ring phenomenon is imitated.



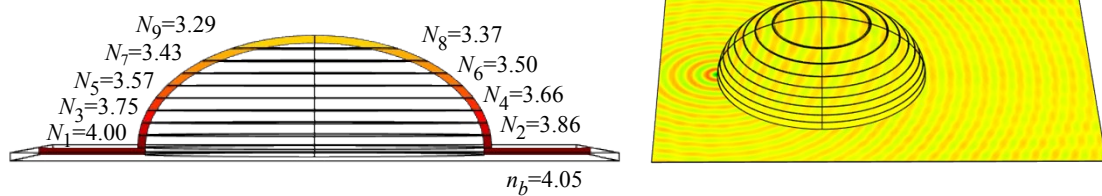
(a) $\lambda = 450$ nm



(b) $\lambda = 550$ nm



(c) $\lambda = 600$ nm



(d) $\lambda = 650$ nm

Figure S8. The propagation of E_z (left column) through the surface of 9-layered Rinehart-shaped curvature at (a) $\lambda = 450$ nm, (b) $\lambda = 550$ nm, (c) $\lambda = 600$ nm, and (d) $\lambda = 650$ nm, where the optical invisibility is imitated. The left column shows the radial cross sections of the discretized Rinehart-shaped surface at the different wavelengths.

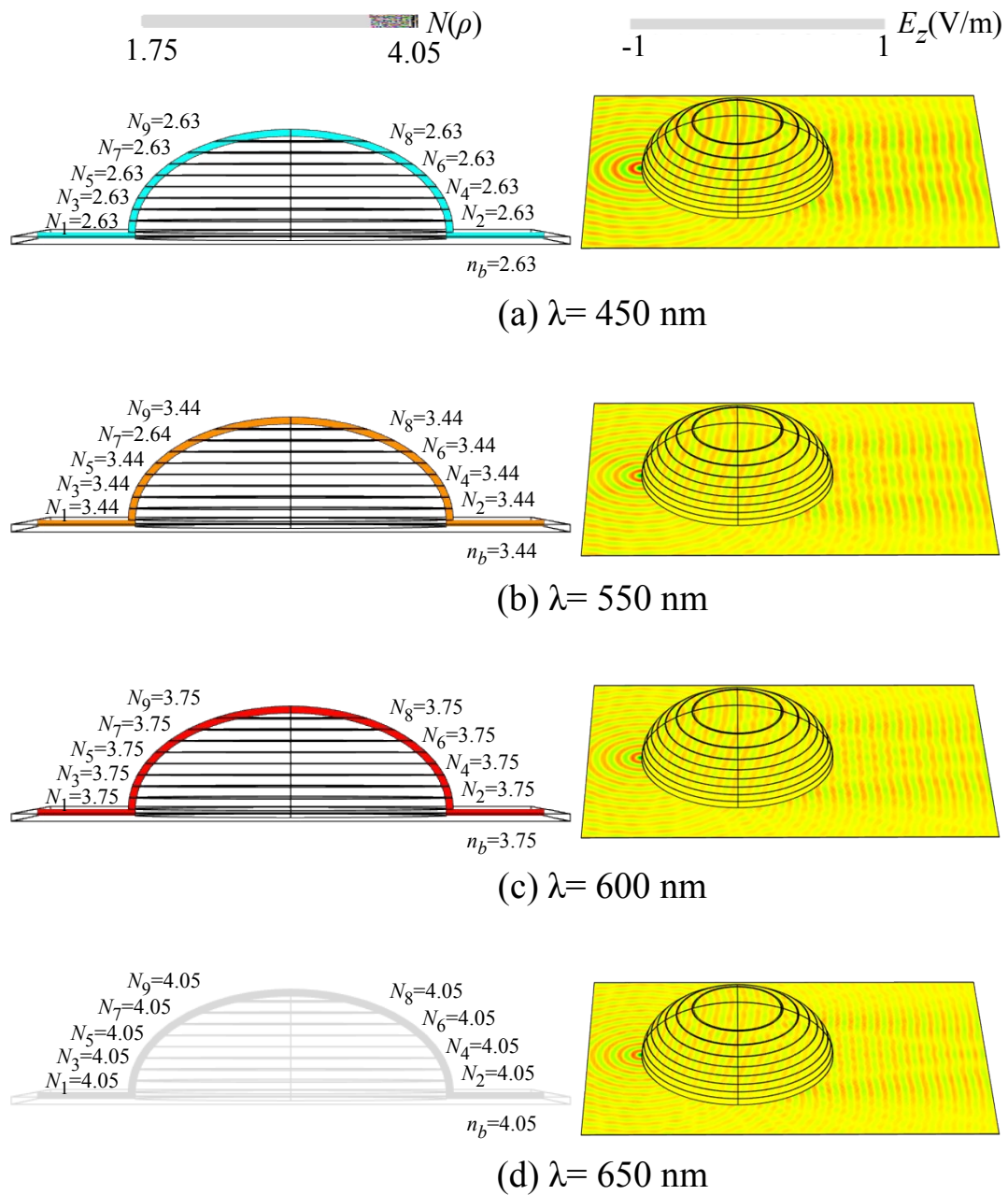


Figure S9. The propagation of E_z (left column) through the surface of 9-layered Luneburg-shaped curvature at (a) $\lambda = 450$ nm, (b) $\lambda = 550$ nm, (c) $\lambda = 600$ nm, and (d) $\lambda = 650$ nm, where the Luneburg lens is obtained. The left column shows the radial cross sections of the discretized Luneburg-shaped surface at the different wavelengths.

Section 6. The conditions of the Ge₂Sb₂Te₅ slabs for the various functions.

Table S1. The corresponding crystallization proportion, time durations, and refractive index of each Ge₂Sb₂Te₅ slab for the invisible cloaking at $\lambda = 500$ nm

Layer	Crystallization ratio	Time duration (ns)	Refractive index
#Ground	0	0	3
#1	16.7%	8	2.85
#2	27.8%	14	2.75
#3	44.4%	22	2.6
#4	53.3%	26	2.52
#5	63.3%	31	2.43
#6	73.3%	37	2.34
#7	83.3%	42	2.25
#8	92.2%	46	2.17
#9	100%	50	2.10

Table S2. The corresponding crystallization proportion, time durations, and refractive index of each Ge₂Sb₂Te₅ slab for the Maxwell fish-eye lens $\lambda = 500$ nm

Layer	Crystallization ratio	Time duration (ns)	Refractive index
#Ground	100%	50	2.1
#1	100%	50	2.1
#2	97.2%	48	2.13
#3	93.4%	46	2.17
#4	87.3%	43	2.23
#5	79.3%	39	2.31
#6	67.9%	33	2.42
#7	53.5%	26	2.56
#8	36.3%	18	2.72
#9	0	0	3.0

Table S3. The corresponding crystallization proportion, time durations, and refractive index of each Ge₂Sb₂Te₅ slab for the Einstein ring at $\lambda = 500$ nm

Layer	Crystallization ratio	Time duration (ns)	Refractive index
#Ground	0	0	3
#1	98%	49	2.12
#2	98%	49	2.12
#3	97%	48	2.13
#4	97%	48	2.13
#5	95%	47	2.14
#6	92%	46	2.17
#7	89%	44	2.2
#8	84%	42	2.24
#9	76%	38	2.32

Section 7. Description of the supporting movie.

It shows that the wavefront of a guided wave propagating across the layered curvature can be dynamically modulated via the stream of t_{bias} . Our device possesses an excellent performance of the continuous reconfigurability and versatile reprogrammable functions. The dynamic variations of the refractive index and temperature of each Ge₂Sb₂Te₅ layer for the different functionalities are presented simultaneously. However in order to simplify the movie, we only plot out the temperature distributions of the #Ground layer, layer #1 and #9.