

Efficient Ammonia Synthesis over a Core-shell Ru/CeO₂ Catalyst with Tunable CeO₂ Size: DFT Calculation and XAS Spectroscopy Studies

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Figure S1 SEM images of (A) CSs-7, (E) CSs-9, and (I) CSs-11; (B) CSs-7@CeO₂, (F) CSs-9@CeO₂ and (J) CSs-11@CeO₂; (C) CSs-7@Ru-CeO₂, (G) CSs-9@Ru-CeO₂ and (K) CSs-11@Ru-CeO₂; (D) Ru@CeO₂-7; (H) Ru@CeO₂-9 and (L) Ru@CeO₂-11 of core-shell structure. (Page 2)

Figure S2 TEM images of (A) Ru@CeO₂-7, (B) Ru@CeO₂-9 and (C) Ru@CeO₂-11. Particle distribution of Ru nanoparticles over (A) Ru@CeO₂-7, (B) Ru@CeO₂-9 and (C) Ru@CeO₂-11.

Figure S3 Raman spectra of (A) CeO₂ supports and (B) Ru@CeO₂ catalysts after activity test. (Page 2)

Figure S4 H₂-TPR profiles of (A) CeO₂ supports and (B) Ru@CeO₂ catalysts. (Page 3)

Figure S5 SEM images of Ru@CeO₂-9 after activity and thermal stability test of 72 h. (Page3)

Figure S6 XPS spectra: (A) Ce3d of CeO₂ supports, (B) Ru3d and (C) Ru3p of H₂-reduced Ru@CeO₂ catalysts. (Page4)

Figure S7 in situ DRIFTS experiment of Ru@CeO₂-9 at 400 °C with different time (test condition: 10%CO+Ar)

Mass Transfer Calculation for ammonia synthesis over the Ru@CeO₂-9 catalyst
(Page5)

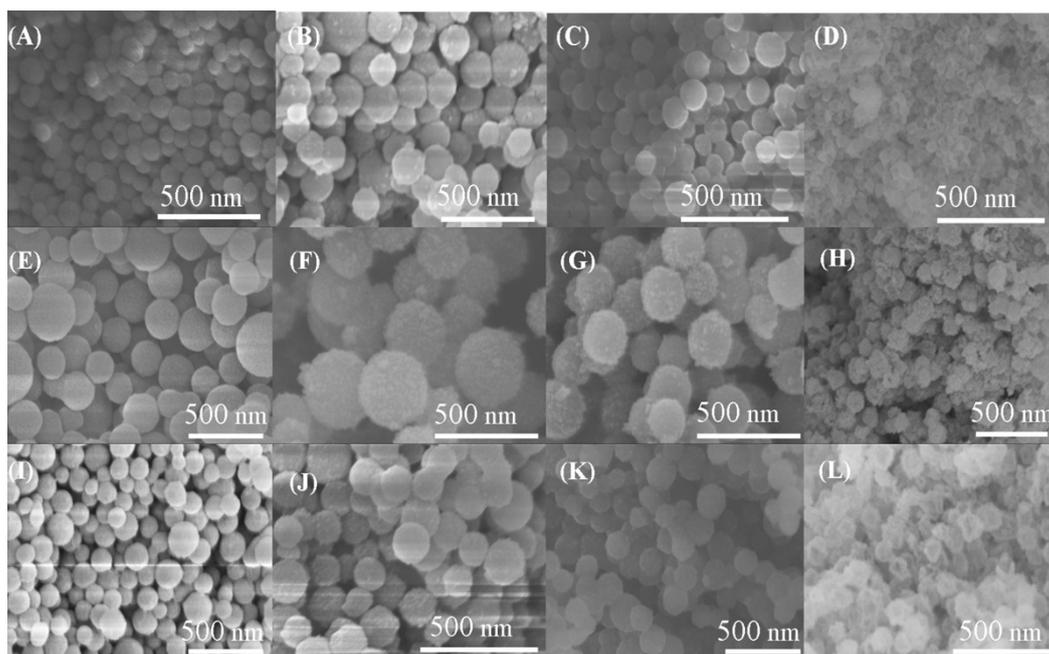


Figure S1 SEM images of (A) CSs-7, (E) CSs-9, and (I) CSs-11; (B) CSs-7@CeO₂, (F) CSs-9@CeO₂ and (J) CSs-11@CeO₂; (C) CSs-7@Ru-CeO₂, (G) CSs-9@Ru-CeO₂ and (K) CSs-11@Ru-CeO₂; (D) Ru@CeO₂-7; (H) Ru@CeO₂-9 and (L) Ru@CeO₂-11 of core-shell structure.

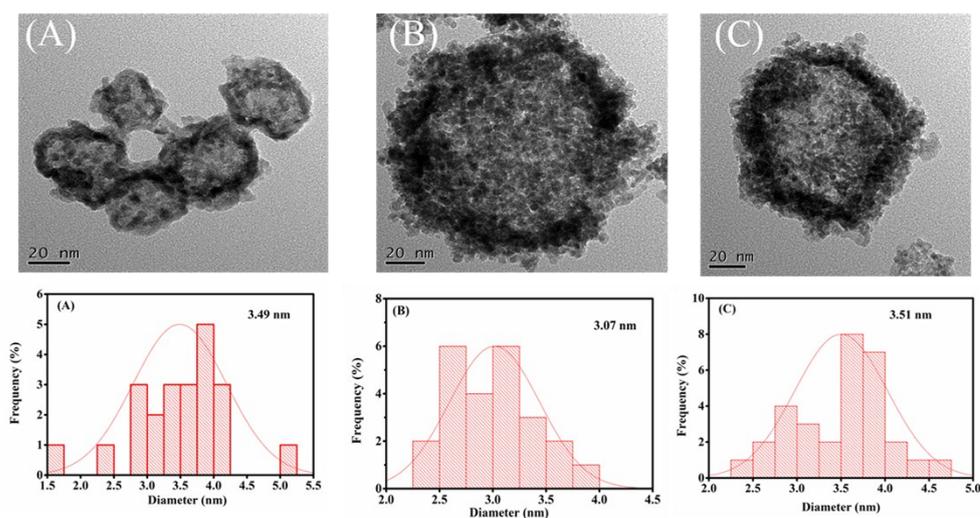


Figure S2 TEM images of (A) Ru@CeO₂-7, (B) Ru@CeO₂-9 and (C) Ru@CeO₂-11. Particle distribution of Ru nanoparticles over (A) Ru@CeO₂-7, (B) Ru@CeO₂-9 and (C) Ru@CeO₂-11.

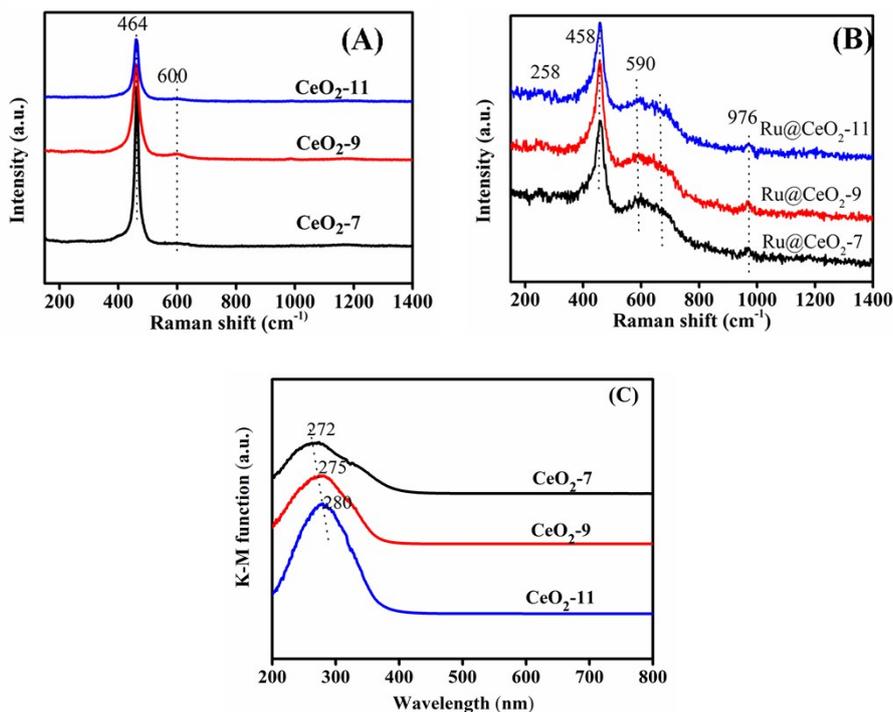


Figure S3 Raman spectra of (A) CeO₂ supports; (B) Ru@CeO₂ catalysts after activity test and (C) Uv-vis spectra of CeO₂ supports.

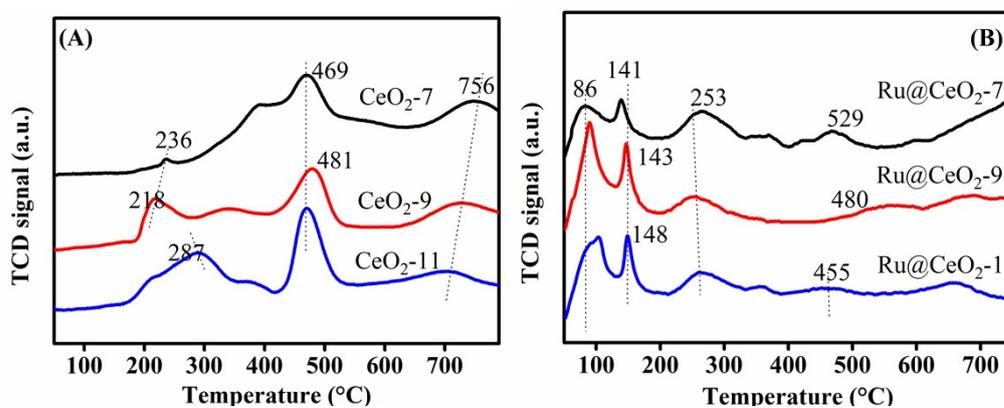


Figure S4 H₂-TPR profiles of (A) CeO₂ supports and (B) Ru@CeO₂ catalysts.

H₂-TPR profiles of CeO₂ and Ru@CeO₂ are shown in Figure 7. For pure CeO₂-7, the peaks located at 236 °C and 469 °C are related to the reduction of surface oxygen, while the peak above 700 °C is associated with the reduction of lattice oxygen species. Unlike CeO₂-7, CeO₂-9 and CeO₂-11 show low-temperature reduction peaks at 218 and 209 °C, indicating that the surface oxygen species on CeO₂-9 and CeO₂-11 are more easily reduced. For all the Ru@CeO₂ catalysts generated using the CeO₂

supports, RuO₂ can be reduced below 150 °C. It is deduced that with the weakening of Ce–O bond by the strongly bound Ru species, the reduction of surface oxygen species on CeO₂-9 and CeO₂-11 becomes more facile. Furthermore, the strong Ce–O–Ru bonding causes electron transfer from Ru to the CeO₂ support, thus forming Ru^{δ+}. We roughly estimated the relative number of Ru^{δ+} and Ce–O–Ru bonds based on the area of the corresponding reduction peaks. It is observed that the relative number of Ru–O–Ce and Ru^{δ+} follows the order of Ru@CeO₂-9 > Ru@CeO₂-11 > Ru@CeO₂-7.

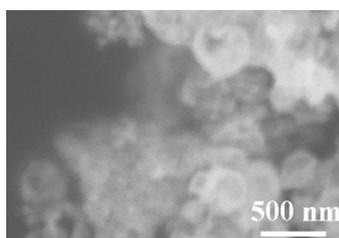


Figure S5 SEM images of Ru@CeO₂-9 after activity and thermal stability test of 72 h.

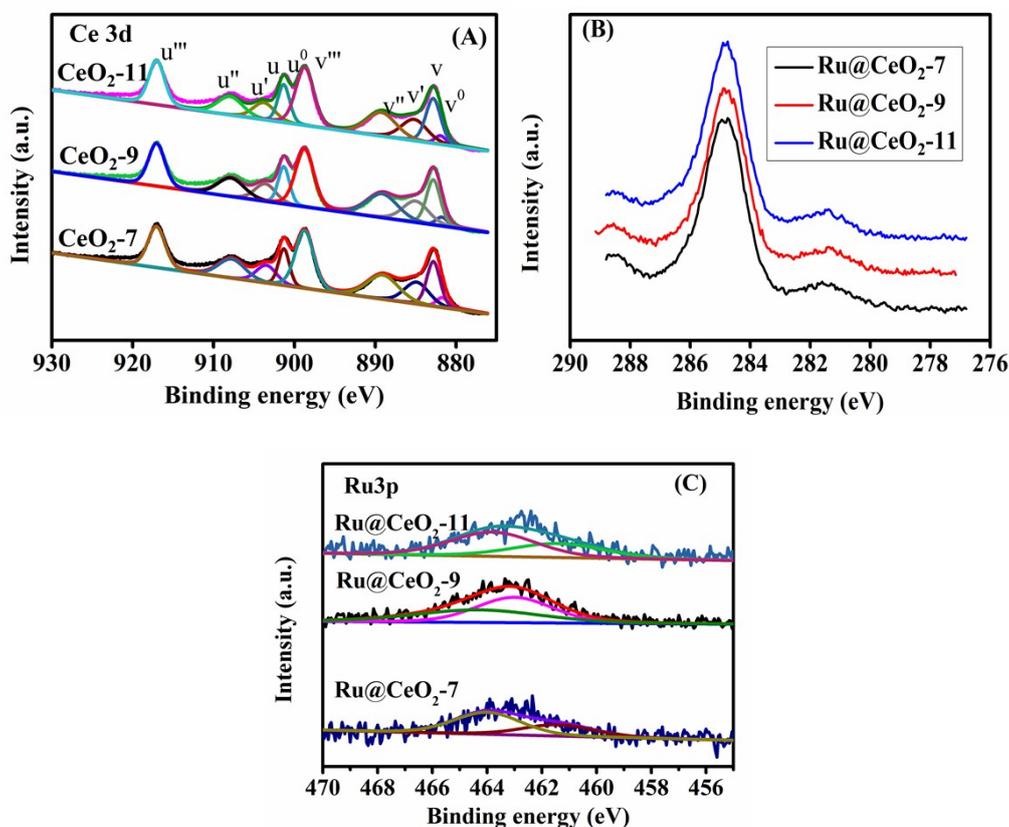


Figure S6 XPS spectra: (A) Ce_{3d} of CeO₂ supports, (B) Ru_{3d} and (C) Ru_{3p} of H₂-

reduced Ru@CeO₂ catalysts.

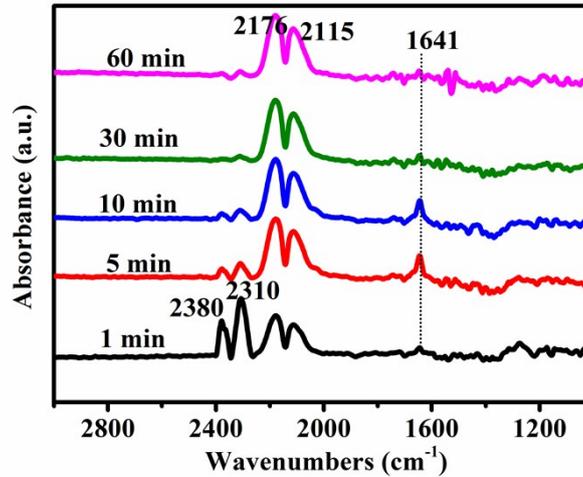


Figure S7 in situ DRIFTS experiment of Ru@CeO₂-9 at 400 °C with different time (test condition: 10%CO+Ar)

Mass Transfer Calculation for ammonia synthesis over the Ru@CeO₂-9 catalyst

Mears Criterion for External Diffusion (Fogler, p841; Mears, 1971)

If $\frac{-r_A' \rho_b R n}{k_c C_{Ab}} < 0.15$, the external mass transfer effects can be neglected.

$-r_A'$ = reaction rate of nitrogen, kmol/(kg·cat·s)

n = reaction order with respect to nitrogen gas.

R = average radius of catalyst particles, m

ρ_b = bulk density of catalyst bed, kg/m³

C_{Ab} = bulk gas concentration of nitrogen, kmol/m³

k_c = mass transfer coefficient, m/s

$$\frac{-r_A' \rho_b R n}{k_c C_{Ab}} = [2 \times 10^{-7} \text{ kmol-N}_2/(\text{kg}\cdot\text{cat}\cdot\text{s})] [910 \text{ kg/m}^3] [2.5 \times 10^{-4} \text{ m}] [1] / ([1.7 \text{ m/s}] * [0.04 \text{ kmol/m}^3]) = 0.67 \times 10^{-7} < 0.15 \quad \{\text{Mears for External Diffusion}\}$$

Weisz-Prater Criterion for Internal Diffusion (Fogler, p839)

If $C_{WP} = \frac{-r'_{A(obs)} \rho_c R^2}{D_e C_{As}} < 1$, the internal mass transfer effects can be neglected.

$-r'_{A(obs)}$ = reaction rate of nitrogen, kmol/(kg·cat·s)

ρ_c is solid catalyst density, kg/m³

R = average radius of catalyst particles, m

ρ_b = bulk density of catalyst bed, kg/m³

C_{Ab} = bulk gas concentration of nitrogen, kmol/m³

D_e = effective gas-phase diffusivity, m²/s [Fogler, p815]

C_{As} = gas concentration of A at the catalyst surface, kmol-A/m³

$$C_{WP} = \frac{-r'_{A(obs)} \rho_c R^2}{D_e C_{As}} = [2 \times 10^{-7} \text{ kmol-N}_2/(\text{kg}\cdot\text{cat}\cdot\text{s})] [2.8 \times 10^3 \text{ kg-cat/m}^3] * [2.5 \times 10^{-4} \text{ m}]^2 / ([3.3 \times 10^{-6} \text{ m}^2/\text{s}] * [0.04 \text{ kmol-N}_2/\text{m}^3]) = 2.65 \times 10^{-4} < 1$$

{Weisz-Prater Criterion for Internal Diffusion}