Electronic Supporting Information

Hierarchical Porous Metallized Poly-melamine-formaldehyde(PMF) as

Low-Cost and High-Efficiency Catalyst for Cyclic Carbonate Synthesis

from CO₂ and Epoxide

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General experimental methods.

Materials

Melamine (99%) was purchased from J&K Scientifics Ltd. (Beijing, China). Pluronic F127 was purchased from Sigma-Aldrich Co., LLC. (Shanghai, China). Isopar M was purchased from Exxon Mobil Co., Ltd. Paraformaldehyde (AR), propylene oxide (99%), tetrabutylammonium bromide (AR, 99%), Zinc chloride (AR), Epichlorohydrin (AR). Styrene oxide (AR), Allyl glycidyl ether (AR) and Chloroform-d (D,99.8%) with 0.03% v/v TMS were purchased from Aladdin Bio-Chem Techno. Co., Ltd. Ethylenediaminetetraacetic acid disodium salt dihydrate (EDTA-2Na, AR), Ammonium chloride (AR), Hydrochloric Acid(AR), Eriochrome Black T (AR), Methyl Alcohol (AR) and other chemicals were purchased from Tianjin Kermel Chemical Reagent Co., Ltd. Deionized water (DI water, 18.2 MΩ cm at 25 °C, 1.2 μg/L TOC) was obtained from a Millipore Milli-Q Advantage A10 water purification system (Billerica, MA, USA). All the chemicals were used without further purification.

Instrumentation

FT-IR spectra were recorded on a Thermo Scientific Nicolet iS50 FT-IR spectrometer at the resolution of 0.09 cm⁻¹. X-ray photoelectron spectroscopy (XPS) spectra were collected on a Thermo Scientific K-Alpha XPS spectrometer. Liquid ¹H NMR spectra were recorded on a Bruker 400 spectrometer. Solid ¹³C NMR spectra were recorded on a 500 MHz Avance Solids NMR. The CDCl₃ with TMS was used as an internal reference, and the residue H peaks of CHCl₃ were at 7.26 ppm. The N₂ adsorption and desorption isotherms were measured by a Micromeritics ASAP 2020M system at 77 K. The samples were deaerated at 120 °C for 8 h before measurements. The specific surface area was calculated by the Langmuir and the Brunaner-Emmett-Teller (BET) methods. The pore size distribution curve was calculated by using the non-local density functional theory (NLDFT) method. The XRD pattern was measured by a BRUKER D8 DISCOVER X-ray Powder Diffractometer. The field emission scanning electron microscopy (FE-SEM) measurement was carried out on a Zeiss Gemini SEM 500 microscope. The high-resolution transmission electron microscopy (HR-TEM) images were obtained by a JEOL JEM-2100F. The TGA measurement was carried out on a Q600 Simultaneous DSC-TGA over the temperature range of 25 °C to 800 °C under a N₂ atmosphere. The catalytic reaction was conducted in a stainless-steel autoclave (SLM Micro-Reactor, Beijing Century Senlong Co., Ltd.) with a 25 mL Teflon tube.

Fabrication of ah-PMF particles

Firstly, Pluronic F127 (4.62 g) and DMSO (12 mL) were placed in a three-neck flask (250 mL) and dissolved at 70 °C for 1 hour. Then, melamine (MA, 1.134g, 9 mmol) and paraformaldehyde (PF, 0.486 g, 16.2mmol) were added and dissolved at 95 °C for another 2 hours. Subsequently, Isopar M (40 mL) was added dropwise into the resulting solution with constant mechanical stirring at the speed of 120-150 rpm at 45 °C, until no phase separation was observed. The resulting creamy emulsion was poured into a hydrothermal reactor and heated at 170 °C for 3 days in an oven. After polymerization, the solid sample was stirred and washed using the solvents acetone, THF, and water successively. Finally, the solid powder was dried in a vacuum oven at 120 °C for 24 h. The yield of PMF product was 91.6%.

Fabrication of CE-1 and CE-2 particles

For the CE-1 sample, melamine (MA, 1.134g, 9 mmol), paraformaldehyde (PF, 0.486 g, 16.2mmol) and DMSO (12 mL) were placed in a three-neck flask (250 mL) and dissolved at 70 °C for 1 hour. The mixed solution was poured into a hydrothermal reactor and heated at 170 °C for 3 days in an oven. For the CE-2 sample, Pluronic F127 (4.62 g) and DMSO (12 mL) were placed in a three-neck flask (250 mL) and dissolved at 70°C for 1 hour. Melamine(MA, 1.134g, 9 mmol) and paraformaldehyde (PF, 0.486 g, 16.2mmol) were added and dissolved into the mixed solution. The resulting solution was poured into a hydrothermal reactor and heated into a hydrothermal reactor and heated into a hydrothermal reactor and heated into the mixed solution. The resulting solution was poured into a hydrothermal reactor and heated at 170 °C for 3 days in an

oven. After polymerization, the washing processes for these two samples was the same as the washing process used for the ah-PMF particles.

Metallization of ah-PMF particles

The metallization of ah-PMF particles was carried out via stirring in a 0.1 M ZnCl₂ solution for 24 h, followed by filtration and drying in a vacuum oven at 120 °C for 12 h. The Zn ion uptake was characterized by the titration method using EDTA as the titrant. Specifically, 3 mL of ammonium chloride buffer solution (pH=10) and one drop of Eriochrome Black T solution (0.5 g EBT in 75 mL of triethanolamine and 25 mL of ethanol) were mixed into 9 mL of filtrate. Then, 0.1 M EDTA solution was added dropwise into the mixed solution until the color of solution changed from purple to blue. The concentration of Zn ions was calculated via Eq. (1):

$$c_{Zn^{2+}} = \frac{c_{EDTA} \cdot (V_1 - V_2)}{V}$$
(1)

where c_{EDTA} is the concentration of EDTA solution, V is the volume of the filtrate, V₁ is the volume of EDTA solution used to titrate the filtrate, and V₂ is the volume of EDTA solution used for titrating the same volume of control solution, which is usually water. The Zn ions uptake was calculated via Eq. (2):

$$m_{Zn^{2+}} = \frac{\Delta c_{Zn^{2+}} \cdot V_0 \cdot M_{Zn}}{m_{PMF}}$$
(2)

where $\Delta c_{Zn^{2+}} = c_{Zn_1^{2+}} - c_{Zn_2^{2+}}$ is the change of the concentration of Zn ions, V₀ is the initial volume of ZnCl₂

solution, $\,M_{_{Z\!n}}\,$ is the molecular weight of Zn, and $\,m_{_{P\!M\!F}}\,$ is the mass of PMF particles.

Cycloaddition of CO₂ with epoxide catalyzed by Zn@ah-PMF.

First, the autoclave was purged with CO₂ to evacuate air for 10 min. Then, Zn@ah-PMF particles (16 mg, 0.0085 mol%), propylene oxide (15 mL, 214.3 mmol), and TBAB (464 mg) were added into the reactor. After charging CO₂ up to 2 MPa, the reactor was stirred at 100 °C for 0.5 h. When the reaction was finished, the resident CO₂ was vented at room temperature. The product yield was calculated by ¹H NMR (CDCl₃) with 1,1,2,2-tetrachloroethane as an internal standard. For the recyclability test, the catalyst was filtrated, washed with methanol for 4 times, and then vacuum dried at 120 °C for 24 h for the next recycling use.

Prediction of the selectivity of CO₂/N₂ mixtures by IAST

IAST (ideal adsorption solution theory) is a widely used method to predict binary mixture adsorption from the experimental results of pure-gas isotherms.⁴¹⁻⁴³ Firstly, the pure-gas isotherms should be well fitted by a proper adsorption model. Here, we used the following adsorption models to fit the isotherms of CO_2 and N_2 .

1) Single-site Langmuir equation (SSL)

$$q = \frac{q_m bp}{1 + bp} \quad (3)$$

where p is the pressure of the bulk gas at equilibrium (MPa), q is the adsorbed amount per mass of adsorbent (mmol/g), q_m is the saturation capacity of adsorbent, and b is the affinity coefficient.

2) Dual-site Langmuir equation (DSL)

$$q = \frac{q_{m,1}b_1p}{1+b_1p} + \frac{q_{m,2}b_2p}{1+b_2p} \quad (4)$$

where the parameters are the same as in the SSL equation. The subscript 1 and 2 stand for sites 1 and 2, respectively.

3) Single-site Langmuir-Freundlich equation (SSLF)

$$q = \frac{q_m b p^{1/n}}{1 + b p^{1/n}}$$
 (5)

where n is the deviation from an ideal homogenous surface. Other parameters are the same as in the SSL equation.

4) Dual-site Langmuir-Freundlich equation (DSLF)

$$q = \frac{q_{m,1}b_1p^{1/n_1}}{1+b_1p^{1/n_1}} + \frac{q_{m,2}b_2p^{1/n_2}}{1+b_2p^{1/n_2}} \quad (6)$$

where the parameters used are the same as in the SSLF equation, and the subscript 1 and 2 stand for sites 1 and 2, respectively.

The results shown in Fig. S10 indicate that the dual-sites Langmuir-Freundlich (DSLF) equation is the most suitable model (R^2 =0.99998), which was then used to predict the selectivity of mixtures based on IAST. The selectivity of mixtures is defined as:

$$S_{A/B} = \left(\frac{x_A}{x_B}\right) \left(\frac{y_B}{y_A}\right) \quad (7)$$

where x and y are the mole fractions of the components in the adsorbed and bulk phases, respectively. The subscript A and B represent the components of the mixtures, which stand for CO_2 and N_2 here. We utilized Fortran language to calculate selectivity and the program code is shown in Appendix I.

DFT calculations:

The Density functional theory (DFT) calculations of the molecular structure of ah-PMF polymer were performed by using Materials Studio software with DMol3 DFT module at the B3LYP level.^{81,82}

General Characterization of Zn@ah-PMF



Fig S1 Photographs of non-aqueous HIPE with different preservation times at room temperature (a-c) and its structure diagram (d).



Fig. S2 Photograph of the ah-PMF monolith.



Fig. S3 FT-IR spectrum of Zn@ah-PMF.



Fig. S4 Solid ¹³C NMR spectra of Zn@ah-PMF



Fig.S5 XPS spectra of ah-PMF and Zn@ah-PMF.



Scheme S1 (a) The repeating unit of the ah-PMF polymer. (b) The ideal molecular structure diagram of Zn@ah-

PMF



Fig. S6 EDX mapping of Zn@ah-PMF: (a) SEM image and (b) EDS layered image of Zn@ah-PMF, in which the colors purple, brown, and green represent elements C, N and Zn, respectively. (c)-

(e) The images of element mapping of C, N and Zn.

Element	Weight %	Atomic %	Error %
СК	37.88	45.29	6.49
NK	50.97	52.26	10.34
ZnK	11.15	2.45	3.32

Table S1 The EDX elemental quantitative analysis of Zn@ah-PMF



Fig. S7 Thermal gravimetric analysis (TGA) on Zn@ah-PMF under nitrogen atmosphere



Fig. S8 (a) Adsorption and desorption isotherms of N2 at 77 K of Zn@CE-1; (b) Pore size distribution curve of Zn@CE-1; (c) Adsorption and desorption isotherms of N2 at 77 K of Zn@CE-2; (d) ore size distribution curve of Zn@CE-2



Fig.S9 SEM and TEM images of Zn@CE-1 (a-d) and Zn@CE-2 (e-h).



Fig. S10 The XRD patterns of Zn@CE-1, Zn@CE-2, and Zn@ah-PMF samples.



Fig. S11 SEM image of Zn@ah-PMF with a particle size of 400 mesh.



Fig. S12 BET plot (P/P₀=0.06-0.2) from N₂ isotherms at 77 K of Zn@ah-PMF.

Table S2 The stability of HIPEs at different conditions.

Dispersed phase/Temp. (°C)	75	85	120	140	160
Petroleum ether (b.p. 60-90	hoiling	_	_	_	_
°C) at 1 atm	Donnig				
Petroleum ether (b.p. 90-120	phase	hoiling			
°C) at 1 atm	separation	DOIIIIB	-	-	-
Isopar Mat 1 atm	stable	stable	stable	phase	hoiling
	stable	Stable	Stable	separation	bolling
Isopar M in hydrothermal	stable	stable	stable	stable	stable
reactor	stable	SIGNIE	stable	Stable	STUDIE



Fig. S13 The fitted adsorption isotherms of CO₂ (blue triangles) and N₂ (red dots) via (a) SSL, (b) DSL, (c) SSLF and (d) DSLF models.

Catalyst	Temp.[°C]	CO2 capacity (mg/g)	BET surface area (S _{BET})	Ref.
Co-CMP	25	79.3	965	11
Zn-CMP	25	58.4	791	52
PPh ₃ -ILBr-ZnBr ₂ @POPs	25	31.5	482	13
AI-HCP	0	93.3	400	78
AI-CMP	0	43.1	1278	80
HUST-1-Co	0	213.9	1360	15
Py-Zn@MA	0	58.1	207	22
Bp-Zn@MA	0	52.37	445	21
Zn/HAzo-POP-2	0	53.3	593.48	18
Cu/POP-Bpy	0	129	683	20
ah-PMF	0	38.3	497	This work

Table S3 A summary of CO_2 capacities and BET surface areas of other catalysts reported in literature.

Catalytic results.



Scheme S2 The proposed reaction mechanism of PO with CO_2 catalyzed by Zn@ah-PMF.



Fig. S14 The TOF (a), TON (a) and conversion (b) of the cycloaddition reaction of PO and CO₂ at 25 °C and 0.1 MPa.



Fig. S15 The SEM image of Zn@ah-PMF sample after 55 h catalytic reaction.



Fig. S16 The recyclability tests of Zn@ah-PMF.

Table S4 Cycloaddition reaction of epoxides with CO₂^[a].

$$\bigcap_{R}^{O} + CO_2 \xrightarrow{Cat.} \bigcap_{R}^{O}$$



[a] Reaction conditions: Epoxides, Zn@ah-PMF (16 mg), TBAB (0.414 g), the initial pressure of CO₂ is 2 MPa, 100 °C and 0.5 h. [b] Determined by ¹H NMR spectroscopy (CDCl₃, 400 MHz) using 1,1,2,2-tetrachloroethaneas as an internal standard. [c] TOF=[moles of product]/[(total moles of metal ions)*(reaction time)]. [d] Epichlorohydrin (18.3 mL, 233 mmol). [e] Allyl glycidyl ether (25.3 mL, 213.4 mmol). [f] 1,2-Epoxyethylbenzene (24.5 ml, 214 mmol).



Fig. S17 Typical ¹H NMR method used to calculate the yield of PO.

¹H NMR spectra of the products







homogeneous and heterogeneous catalysts.								
Catagory	Catalyct ^[a]	Temp.	Pressure ^[b]	Time	sic	Conv.	TOE[b-1]	Ref.
Category	Catalyst	[°C]	[MPa]	[h]	3/0	[%]	IOF[II]	
Homogeneous	S1	120	0.69	5.25	4000-6500	-	531	44
	S2	120	2	5	4000	66	528	45
SalenComplexs	\$3	75	1.3	2	1500	80	602	46
	S4	100	3.45	2	1000	90	451	47
	Co-CMP	100	3	1	205	98.1	201	11
	S5	100	2	16	500	89	20	48
Heterogeneous	DVB@ISA	60	1	24	400	99	16.5	49
SalenComplexs	Zn@SBMMP	80	2	4	250	97	50.8	50
	Co-MON	60	1	12	2000	75	125	51
	Zn-CMP	120	3	1	2000	55.3	1100	52
	[C8-mim] ⁺ [BF4] ⁻	100	14	5 min	60	98	516	53
	[HTEA]I	110	2	6	53	91	8.1	54
Homogeneous Ionic Liquid	[CBDMAPy]Br	130	2	20 min	100	92	276	55
	S6	110	1.5	2	690	96	331	56
	S7	90	0.5	2	50	92	23	57
	GO-[Smlm]I-40	140	2	4	32	93	7.4	58
	SBA-[V _{0.15} -OH _{0.6}]R ₂ 37	140	2	5	154	95	188	59
	PPh ₃ -ILBr-ZnBr ₂ @POPs	120	3	1	8000	44	3520	13
Heterogeneous	PS-MimFeCl ₄	100	8	6	100	77	12.8	60
Ionic Liquid	PSIL-4	110	6	7	148	97.4	20.6	61
	T-IM	150	1	10	1538	87	134	62
	PDMBr	110	1	4	77	98.7	19	63
	ZIF-95	80	1.2	2	250	83.2	104	64
	ZnGlu	80	1.2	6	213	99	35	65
	Cu(Hip)₂py	120	1.2	6	62	62	6.5	66
	Ni-Saldpen-MOF	80	2	4	143	86	31	67
	MOF-5	50	6	4	40	97.6	9.8	68
	UMCM-1-NH ₂	25	1.2	24	156.25	90	5.9	69
	gea-MOF-1	120	2	6	666.7	88	98	16
MOF	Meim-UiO-66	120	0.1	24	192	77	6.2	17
	Tmof-1	25	0.1	48	100	99	2.1	70
	Cu ₆ (µ ₄ -O) ₂ (SO ₄) ₄ (DMA) ₆	25	0.1	24	417	98.2	17.1	71
	In-MOF	80	2	4	769	57.2	110	72
	MIL-101-N(n-Bu)3Br	80	2	8	111	99.1	13.8	73
	Ni-1	40	0.1	40	333	98.4	8.2	74
	[Zn ₆ (TATAB) ₄ (DABCO) ₃ (H ₂ O) ₃] 12DMF 9H ₂ O	100	0.1	16	238	100	15.4	75

 $\textbf{Table S5}\ Comparison\ of\ the\ Zn@ah-PMF\ catalyst\ in\ the\ cycloaddition\ reaction\ of\ PO\ and\ CO_2\ with\ the\ reported$

(0011100100	1							
Category	Catalyst	Temp. [ºC]	Pressure [MPa]	Time [h]	s/C	Conv. [%]	TOF[h ⁻¹]	Ref.
Homogeneous	S8	90	2	1	100000	37.9	37900	76
omplexs	S9	25	0.1	8	2000	55	137	77
	Al-HCP	100	3	0.25	20000	18.6	14880	78
Heterogeneous	Al-iPOP-2	100	1	4	10000	98	2425	14
Metalloporphyri	Zn(Por)OP	120	3	2.5	1000	95	1628	79
nComplexs	AI-CMP	100	3	5	2000	91	364	80
	HUST-1-Co	25	0.1	30	3205	94.6	103	15
	Py-Zn@MA	150	2	6	360	96	260	22
	Bp-Zn@MA	100	1	1.5	1160	99	2252	21
Other POPs	Zn/HAzo-POP-2	100	3	0.5	1872	83	3330	18
	Cu/POP-Bpy	25	0.1	48	200	99	4.1	20
	Zn@AP/HMTA-0.20	100	1	1.5	232	98.6	168.6	19
This work	Zn@ah-PMF	100	2	0.5	11750	79.1	18388	-
	Zn@ah-PMF	25	0.1	55	73800	8.5	114.4	-

(Connected)

[a]The chemical formulas of some catalysts are listed as following.



[b] Pressure refers to the initial CO_2 pressure.

Reference (1-40: main text references, 41-82: electronic supporting information references)

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Appendix 1 The program code of IAST

PROGRAM IAST

IMPLICIT NONE REAL(8),DIMENSION(1:2) :: y, qm1, b1, n1, qm2, b2, n2 REAL(8) bisection INTEGER i, n REAL(8),DIMENSION(1:100) :: P, x1, x2, S

OPEN (UNIT=10,FILE="d:\INPUT.txt", STATUS="UNKNOWN") READ(10,*) n READ(10,*) (y(i),i=1,2) !for flue gas, y(1)=0.15,y(2)=0.85; for ideal gas, y(1)=y(2)=0.5 READ(10,*) (P(i),i=1,n) READ(10,*) (qm1(i),i=1,2) READ(10,*) (b1(i),i=1,2) READ(10,*) (n1(i),i=1,2) READ(10,*) (qm2(i),i=1,2) READ(10,*) (b2(i),i=1,2) READ(10,*) (n2(i),i=1,2) CLOSE(10)

DO i=1,n x1(i)=bisection(P(i),qm1,b1,n1,qm2,b2,n2,y) x2(i)=1-x1(i) END DO

DO i=1,n

 $\label{eq:Si} S(i) = (x1(i)/y(1))/(x2(i)/y(2)) \ ! \mbox{To calculate the selectivity} \\ END \ DO$

OPEN (UNIT=20,FILE="d:\OUTPUT_DSLF.txt", STATUS="UNKNOWN") DO i=1,n WRITE(20,100) P(i), S(i), x1(i), x2(i), y(1), y(2) END DO 100 format(10f15.6) CLOSE(20) END ! This Section is used to calculate the root of equation "f" by the method

! of bisection and the function is named as "bisection"

FUNCTION bisection(P,qm1,b1,n1,qm2,b2,n2,y)

IMPLICIT NONE REAL(8), DIMENSION(1:2) :: qm1, b1, n1, qm2, b2, n2, y REAL(8) lt, rt, mi, f, P, bisection lt=0.0 rt=1.0 DO WHILE (ABS(rt-lt)>1E-10)

mi=(lt+rt)/2 IF (f(P,qm1,b1,n1,qm2,b2,n2,y,lt)*f(P,qm1,b1,n1,qm2,b2,n2,y,mi)<0) THEN

rt=mi

ELSE

lt=mi

END IF

END DO

bisection=mi

END FUNCTION bisection

! The Function is the equation from IAST theory, and the pure-gas ! isotherm is fitted with dual-site Langmuir-Freundlich model. FUNCTION f(P,qm1,b1,n1,qm2,b2,n2,y,x1) IMPLICIT NONE REAL(8), DIMENSION(1:2) :: qm1, b1, n1, qm2, b2, n2, y

f2=qm1(2)*n1(2)*LOG(1+b1(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*LOG(1+b2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*n2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*n2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(P*y(2)/(1-x1))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1/n1(2)))+qm2(2)*(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1/n1(2)))+qm2(2)*(1-x))**(1-x))**(1/n1(2)))+qm2(2)*(1-x))**

REAL(8) P, x1, f, f1, f2 f1=qm1(1)*n1(1)*LOG(1+b1(1)*(P*y(1)/x1)**(1/n1(1)))+qm2(1)*n2(1)*LOG(1+b2(1)*(P*y(1)/x1)**(1/n2(1)))+qm2(1)*n2(1)*n2(1)*LOG(1+b2(1)*(P*y(1)/x1)**(1/n2(1)))+qm2(1)*n2(

x1))**(1/n2(2)))

END FUNCTION f

f=f1-f2

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Appendix 2 The input value and the predicted results of ideal gas and flue gas via IAST

(1) The input value.

26#This is the number of pressure value.

0.15, 0.85# This is the molar fraction of CO_2 and N_2 in bulk phase. 0.15/0.85 is the ratio of flue gas, and 0.5/0.5 is the ratio of ideal gas.

3.05E-04, 5.08E-04, 7.11E-04, 9.13E-04, 0.00102, 0.00521, 0.01029, 0.01531, 0.01787, 0.02042, 0.02545, 0.03051, 0.03558, 0.04066, 0.04572, 0.05078, 0.05586, 0.06093, 0.06599, 0.07106, 0.07612, 0.08118, 0.08625, 0.09132, 0.09638, 0.10096# This is the selected pressure value, and the unit is MPa.

1.88361, 1.01283# This is the fitting parameter $q_{m,1}$ of CO₂ and N₂, respectively.

2.04164, 0.33765# This is the fitting parameter b_1 of CO_2 and $N_2,$ respectively

0.84167, 1.18592# This is the fitting parameter n_1 of CO_2 and $N_2,$ respectively

0.96608, 1.01266# This is the fitting parameter $q_{m,2}$ of CO_2 and $N_2,$ respectively

11.28204, 0.33652# This is the fitting parameter b_2 of CO_2 and N_2 , respectively

1.36777, 1.18589#This is the fitting parameter n₂ of CO₂ and N₂, respectively

Pressure	Coloctivity	r	r	1,	1,
(MPa)	Selectivity	λ_{CO_2}	λ_{N_2}	<i>Y</i> _{CO₂}	\mathcal{Y}_{N_2}
0.000305	101.6569	0.990259	0.009741	0.5	0.5
0.000508	94.89442	0.989572	0.010428	0.5	0.5
0.000711	90.65712	0.98909	0.01091	0.5	0.5
0.000913	87.60955	0.988715	0.011285	0.5	0.5
0.00102	86.28583	0.988543	0.011457	0.5	0.5
0.00521	68.40017	0.985591	0.014409	0.5	0.5
0.01029	61.61455	0.984029	0.015971	0.5	0.5
0.01531	57.79085	0.982991	0.017009	0.5	0.5
0.01787	56.32932	0.982557	0.017443	0.5	0.5
0.02042	55.08075	0.982169	0.017831	0.5	0.5
0.02545	53.04622	0.981497	0.018503	0.5	0.5
0.03051	51.39798	0.980915	0.019085	0.5	0.5
0.03558	50.02234	0.980401	0.019599	0.5	0.5
0.04066	48.84612	0.979938	0.020062	0.5	0.5
0.04572	47.82781	0.97952	0.02048	0.5	0.5
0.05078	46.92997	0.979136	0.020864	0.5	0.5
0.05586	46.12645	0.97878	0.02122	0.5	0.5
0.06093	45.40514	0.978451	0.021549	0.5	0.5
0.06599	44.75255	0.978143	0.021857	0.5	0.5
0.07106	44.15602	0.977855	0.022145	0.5	0.5
0.07612	43.60991	0.977583	0.022417	0.5	0.5
0.08118	43.10657	0.977328	0.022672	0.5	0.5
0.08625	42.63985	0.977085	0.022915	0.5	0.5
0.09132	42.20639	0.976855	0.023145	0.5	0.5
0.09638	41.80332	0.976637	0.023363	0.5	0.5
0.10096	41.46132	0.976449	0.023551	0.5	0.5

(2) The output results for ideal gas via IAST.

(3) The output results for flue gas.

Pressure	Selectivity	x_{CO_2}	x_{N_2}	\mathcal{Y}_{CO_2}	\mathcal{Y}_{N_2}
0.000305	118.821	0.95448	0.04552	0.15	0.85
0.000508	110.9571	0.951411	0.048589	0.15	0.85
0.000711	106.0476	0.949275	0.050725	0.15	0.85
0.000913	102.5279	0.947625	0.052375	0.15	0.85
0.00102	101.0025	0.946876	0.053124	0.15	0.85
0.00521	80.70337	0.934391	0.065609	0.15	0.85
0.01029	73.20708	0.928155	0.071845	0.15	0.85
0.01531	69.02988	0.924137	0.075863	0.15	0.85
0.01787	67.43834	0.922486	0.077514	0.15	0.85
0.02042	66.07929	0.921018	0.078982	0.15	0.85
0.02545	63.86251	0.918499	0.081501	0.15	0.85
0.03051	62.06058	0.916331	0.083669	0.15	0.85
0.03558	60.54894	0.914421	0.085579	0.15	0.85
0.04066	59.24819	0.912706	0.087294	0.15	0.85
0.04572	58.11387	0.911154	0.088846	0.15	0.85
0.05078	57.10579	0.909727	0.090273	0.15	0.85
0.05586	56.19599	0.908399	0.091601	0.15	0.85
0.06093	55.37199	0.907163	0.092837	0.15	0.85
0.06599	54.61965	0.906004	0.093996	0.15	0.85
0.07106	53.92544	0.904909	0.095091	0.15	0.85
0.07612	53.28377	0.903874	0.096126	0.15	0.85
0.08118	52.68652	0.90289	0.09711	0.15	0.85
0.08625	52.1272	0.90195	0.09805	0.15	0.85
0.09132	51.60248	0.901052	0.098948	0.15	0.85
0.09638	51.10955	0.900193	0.099807	0.15	0.85
0.10096	50.68719	0.899445	0.100555	0.15	0.85