

Graphene Size-dependent Modulation of Graphene Framework Contributing to Superior Thermal Conductivity of Epoxy Composite

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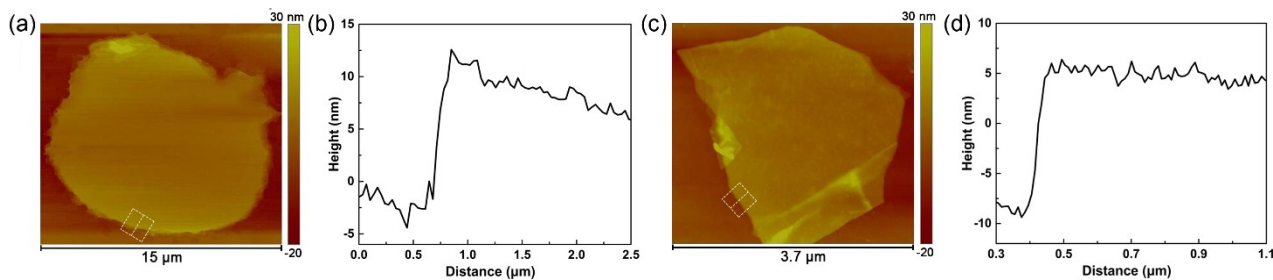


Figure S1 AFM images and thickness of (a-b) large and (c-d) small graphene sheets, respectively.

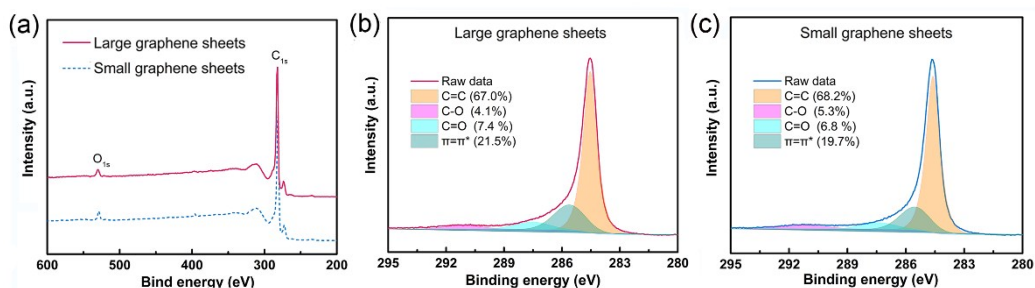


Figure S2 (a) XPS survey spectra of large and small graphene sheets. XPS-C1s spectrum of (b) large and (c) small graphene sheets.

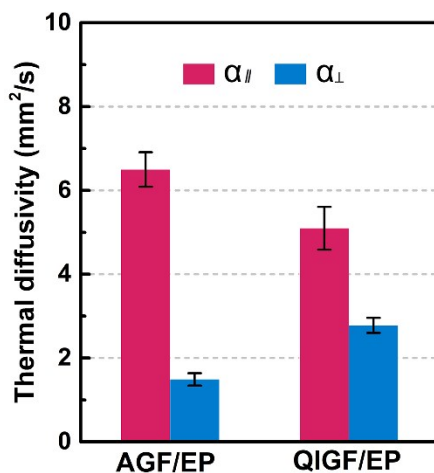


Figure S3 In- and through-plane thermal diffusivities of AGF/EP and QIGF/EP.

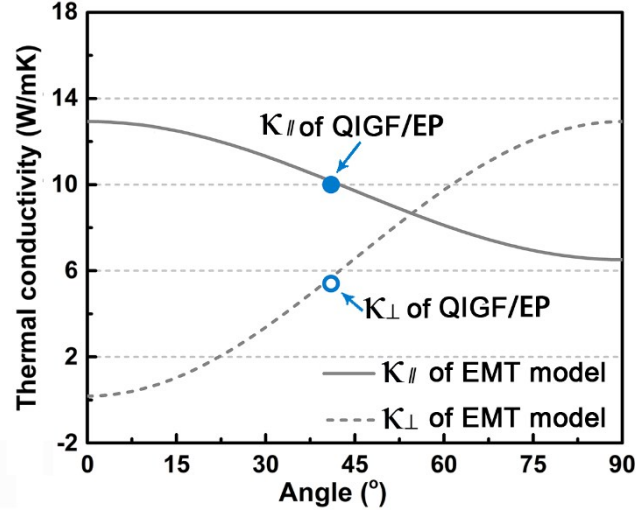


Figure S4 Deflection angle-dependent thermal conductivities of QIGF/EP composites calculated based on EMT model.

In order to explain the anisotropic ratio of QIGF/EP in theory, the thermal conductivity along in- and through-plane direction can be calculated by the effective medium theory (EMT) model, which is usually used to predict the thermal conductivity of laminate fillers/polymer system.¹ As the model describes, κ_{\parallel} and κ_{\perp} as the function of deflection angles of laminate fillers can be estimated based on the equation (1) and (2), respectively:

$$\kappa_{\parallel} = \kappa_m \left\{ \frac{2 + V_f \left[\frac{\kappa_p}{\kappa_m} (1 + \langle \cos^2 \theta \rangle) \right]}{2 - V_f \left[\frac{\kappa_p h - \kappa_m h - R_{bd} \kappa_p \kappa_m}{\kappa_p h} (1 - \langle \cos^2 \theta \rangle) \right]} \right\} \quad (1)$$

$$\kappa_{\perp} = \kappa_m \left\{ \frac{1 + V_f \left[\frac{\kappa_p}{\kappa_m} (1 - \langle \cos^2 \theta \rangle) \right]}{1 - V_f \left[\frac{\kappa_p h}{h + R_{bd} \kappa_p} \langle \cos^2 \theta \rangle \right]} \right\} \quad (2)$$

where κ_m is the thermal conductivity of the matrix material; κ_p is the thermal conductivity of laminate fillers in parallel direction; R_{bd} is the thermal boundary resistance between fillers and matrix; θ is the

deflection angles of laminate fillers; V_f is the volume fraction of fillers; h is the average thickness of laminate fillers. According to the previous reports,^{2,3} the thermal conductivity of exfoliated graphene is ranged from 250 to 600 W/mK, and an average value (425 W/mK) was employed for this calculation. R_{bd} was taken to be 7.7×10^{-8} Km²/W, which were derived from literature.⁴ κ_m for the epoxy matrix (0.18 W/mK) was obtained by direct measurement of an epoxy. V_f was 3.1 vol% by conversion from the mass fraction of 5.5 wt%. h was around 15 nm by a statistical analysis of graphene sheets using AFM.

As a result, the evolution of theoretical thermal conductivity as a function of deflection angles of graphene sheets along in- and through-plane directions is presented in Figure S4, which is predicted from EMT model. In our work, the average angle of graphene sheets in QIGF/EP was $\approx 41^\circ$. Based on this, Figure S4 indicates a good agreement between theoretical and measured thermal conductivities (both of $\kappa_{//}$ and κ_{\perp}) of QIGF/EP. Moreover, the anisotropic ratio of theoretical value (1.88) is also close to the measured one.

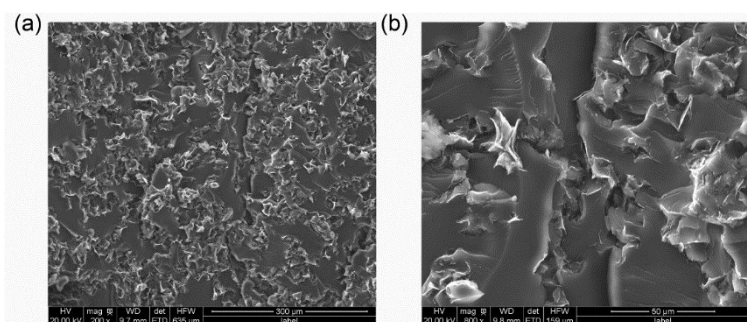


Figure S5 (a-b) SEM images of DG/EP.

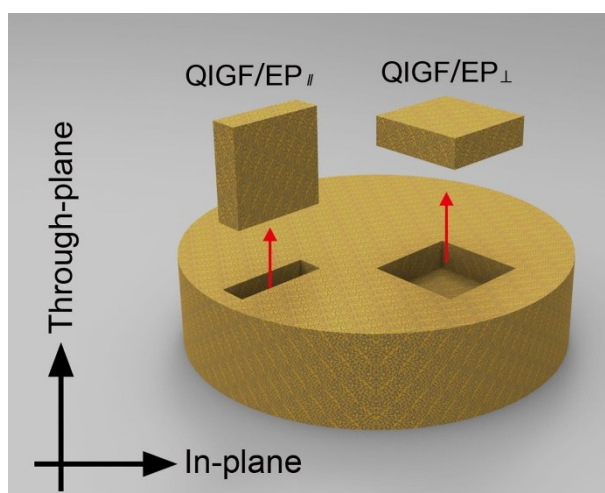


Figure S6 Schematic of the preparation of QIGF/EP_⊥ and QIGF/EP_{//}.

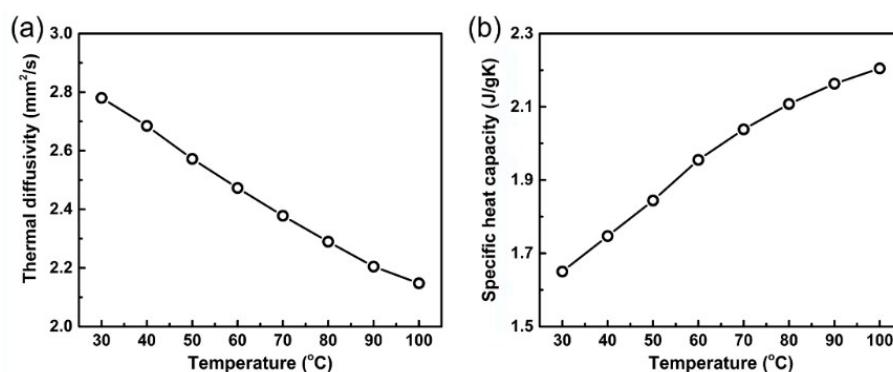


Figure S7 The variation of (a) α_{\perp} and (b) C_p of QIGF/EP as a function of environmental temperature.

Table S1 Comparison of thermal conductivity of our QIGF/EP composite with reported graphene/epoxy composites.

Filler	Tc (W/mK)	Fraction (wt%)	Direction	Reference
Graphene oxide sheets	0.85	5	Isotropic	5
Multilayer Graphene	1.5	5.7	Isotropic	6
Functionalize graphene nanosheets	1.91	4	Isotropic	7
Functionalized Graphene Flakes	1.53	10	Isotropic	8
Graphene-CNT	0.321	1	Isotropic	9
Graphene-Silica	0.29	1.5	Isotropic	10
Graphene coated PMMA balls	1.41	1	Isotropic	11
Pu foam templated graphene framework	1.51	5	Isotropic	12
Ni templated 3D graphene framework	2	8.3	Through-plane	13
	8.8		In-plane	
Hydrothermal graphene framework	2.13	1.9	Through-plane	14
	0.63		In-plane	
QIGF	5.4	5.5	Through-plane	This work
	10		In-plane	

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