## **Electronic Supplementary Information**

## Effect of Donor Units in Methylated DPP-Based Polymers on Performance of Organic Field-Effect Transistors

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Fig. S1 The TGA of the synthesized polymers.



Fig. S2 Cyclic voltammograms of the polymers (reduction part).



**Fig. S3** The transfer and output characteristics of the OFETs based on PMDPP- BT, PMDPP-TVT, and PMDPP-TAT with and without the FeCl<sub>3</sub> interlayer at their optimized thermal annealing temperatures.

Polymer	Annealing Temperature (°C)	Lamellar Stacking		π-π Stacking		FWHM
		PMDPP50- BT	200	0.2413	26.03	1.689
PMDPP50- TVT	250	0.2591	24.25	1.759	3.57	17.4
PMDPP66- TAT	150	0.2254	27.87	1.740	3.61	17.4

 Table S1 Solid-state packing parameters for the polymer thin films.



**Fig. S4** AFM height images of the (a) PMDPP50-BT, (b) PMDPP50-TVT, and c) PMDPP66-TAT films deposited at their optimal annealing temperatures. The scale bar is 500 nm.

The method to evaluate OFET parameters: field-effect mobility,  $\mu$ , and threshold voltage,  $V_{\text{th}}$ , is the classical metal-oxide-semiconductor field-effect transistor (MOSFET) model. This method is described for the two extreme modes of operation above threshold,  $|V_{\text{GS}}| > V_{\text{th}}|$ , in equations (1) and (2). For linear mode,  $|V_{\text{DS}}| < |V_{\text{GS}} - V_{\text{th}}|$ ,

$$I_{\rm D} = \mu_{\rm lin} c_{\rm ox} \frac{W}{L} \left[ (V_{\rm GS} - V_{\rm th}) V_{\rm DS} - \frac{V_{\rm DS}^2}{2} \right], \tag{1}$$

and for saturation mode  $|V_{\text{DS}}| > |V_{\text{GS}} - V_{\text{th}}|$ ,

$$I_{\rm D} = \mu_{\rm sat} c_{\rm ox} \frac{W}{2L} (V_{\rm GS} - V_{\rm th})^2, \qquad (2)$$

where  $V_{GS}$  is the gate voltage,  $V_{th}$  is the threshold voltage,  $I_D$  is the drain current,  $V_{DS}$  is the drain voltage,  $\mu_{lin}$  and  $\mu_{sat}$  are the linear and saturation mobility, respectively, W and L are the width and length of the transistor channel and  $c_{ox}$  is the capacitance per unit area.

 $I_{\rm D}$  shows an abrupt change in slope as a function of  $V_{\rm GS}$ ,  $I_{\rm D}$  ( $I_{\rm D}^{1/2}$ ) is linear with  $V_{\rm GS}$  in the linear (saturation) regime as defined in equations (1) and (2). This slope is used to calculate mobility and extrapolate the threshold voltage.



*Y-function method (YFM):* Y-function method (YFM) is considered as a fast and precise alternative method for obtaining Rc comparing with the traditional transmission line method (TLM). From the transfer characteristics of the OFETs,  $I_d$  in the linear regime can be described as in following equation:

$$I_d = \frac{W}{L} C_i (V_g - V_{Th}) \frac{\mu_0}{1 + \theta (V_g - V_{Th})} \times V_d \tag{1}$$

where  $C_i$  is the dielectric capacitance per unit area, and  $\mu_o$  is the low-field mobility.  $\theta$  is the mobility attenuation factor, which consists of the extrinsic factors caused by the surface roughness and phonon scattering ( $\theta_o$ ) and contact resistance [ $\theta^* = (W/L)\mu_o C_i R_c$ ]. Assuming a constant  $R_c$ , the transconductance ( $g_m$ ) can be expressed as

$$g_m = \frac{\delta I_d}{\delta V_g} = \frac{W}{L} C_i \frac{\mu_0}{\left[1 + \theta (V_g - V_{Th})\right]^2} \times V_d$$
<sup>(2)</sup>

 $\theta$  can be obtained by plotting  $1/g_m^{1/2}$  versus  $V_g$  at a strong charge accumulation, where a linear behavior is obtained. Assuming that  $\theta_o$  is negligible,  $R_c$  can be calculated, as summarized in Table. Note that the negative value of  $\theta$ , is presumably due to the gate-field enhanced mobility, which is compensated for by the conventional mobility attenuation.