# **Electronic Supplementary Information (ESI)**

## Catalytic transformation of 2,5-furandicarboxylic acid to adipic acid over

### niobic acid-supported Pt nanoparticles

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#### **Experimental details**

#### 1. Materials and catalyst preparation

Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, CeO<sub>2</sub>, MgO, ZrO<sub>2</sub>, NbCl<sub>5</sub>, NH<sub>3</sub>·H<sub>2</sub>O, H<sub>2</sub>PtCl<sub>6</sub>·6H<sub>2</sub>O, RuCl<sub>3</sub>·3H<sub>2</sub>O, RhCl<sub>3</sub>·3H<sub>2</sub>O, IrCl<sub>3</sub>·3H<sub>2</sub>O, NaBH<sub>4</sub>, dimethyl sulfoxide (DMSO), ethanol and ethylene glycol were purchased from Sinopharm Chemical Reagent Co., Ltd. TiO<sub>2</sub> was obtained from Degussa, and HZSM-5 was purchased from Nankai University Catalyst Co. 2,5-furandicarboxylic acid (FDCA) was purchased from Aladdin. Tetrahydrofuran-2,5-dicarboxylic acid (THFDCA) was purchased from Jiangsu Aikang Biomedical Research and Development Co., Ltd. 2-hydroxyadipic acid (HAA) was purchased from Shanghai Shaoyuan Co. Ltd. Adipic acid (AA) was purchased from Alfa Aesar (China) Chemicals Co., Ltd. Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O was synthesized by a simple hydrothermal method.<sup>1</sup> Typically, 1.0 g NbCl<sub>5</sub> was dissolved in 10 mL ethanol under continuous stirring to obtain a settled solution. Then, a 4 wt% NH<sub>3</sub>·H<sub>2</sub>O aqueous solution (50 mL) was added to the above solution with stirring for 2 h. After filtration and washing, the solid was dispersed in 50 mL ultrapure water and the pH of mixture was adjusted to 6 by NH<sub>3</sub>·H<sub>2</sub>O aqueous solution. Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O was finally obtained after hydrothermal reaction at 513 K for 24 h, followed by filtration, washing and drying at 333 K under vacuum for 12 h.

Supported Pt or other noble metal catalysts were prepared by a chemical reduction method using NaBH<sub>4</sub> as a reductant. As an example, the preparation of Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O was described as follows. 0.30 g Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O was dispersed into 30 mL ultra-pure water. After stirring for 30 min, an aqueous solution of H<sub>2</sub>PtCl<sub>6</sub> (1.2 mL) with a concentration of 12.55 mg mL<sup>-1</sup> was added into the above suspension under stirring. The mixture was further stirred for another 30 min. Then, a fresh NaBH<sub>4</sub> (0.150 mol L<sup>-1</sup>) aqueous solution (5 mL) was added into the above mixture at 298 K. After stirring for 4 h, the solid catalyst was recovered by filtration, followed by washing and drying. The Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O catalyst thus obtained has a mean Pt particle size of 4.2 nm.

The series of Pt/Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O catalysts with different mean sizes of Pt NPs (denoted as Ptd/Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O, where d was the mean Pt particle size in nm) were prepared by choosing different reductants and different reduction conditions (temperatures and reduction times). For the preparation of catalysts with mean Pt sizes of 4.2, 7.2 and 9.3 nm, the Pt precursor (H<sub>2</sub>PtCl<sub>6</sub> aqueous solution) was mixed with Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O and then underwent reduction by NaBH<sub>4</sub> at temperatures of 298, 323 and 348 K for 4 h, respectively. For the preparation of catalyst with a mean Pt size of 5.2 nm, the reduction temperature was 273 K and reduction time 8 h. The catalyst with a mean Pt size of 3.8 nm was obtained by reduction of H<sub>2</sub>PtCl<sub>6</sub>·6H<sub>2</sub>O at 433 K for 4 h using ethylene glycol as a reductant. The catalyst with a mean Pt size of 1.8 nm was prepared by calcination of Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O-impregnated Pt precursor (H<sub>2</sub>PtCl<sub>6</sub>) at 773 K for 4 h in air, followed by reduction at 673 K for 4 h under 5% H<sub>2</sub>/N<sub>2</sub> gas flow(flow rate, 60 mL min<sup>-1</sup>).

#### 2. Catalyst characterization

The transmission electron microscopy (TEM) and high-resolution transmission electron microscopy (HRTEM) measurements were performed using a Tecnai F20 electron microscope operated at an acceleration voltage of 200 kV. The N<sub>2</sub> physisorption was performed on a Micromeritics Tristar 3020 surface area to measure the specific surface area, pore volume and pore size of the catalysts. X-ray photoelectron spectroscopy (XPS) measurements were performed on an ESCALAB 250Xi using Al-K $\alpha$  radiation. The binding energy was calibrated using the C 1s photoelectron peak at 284.6 eV as a reference. Inductively coupled plasma (ICP) optical emission spectrometry was performed by using an Agilent 700 ICP-OES instrument to measure the actual loading amounts of Pt. The diffuse reflectance Fourier-transform infrared (FT-IR) spectroscopy was carried out with a Nicolet 6700 spectrometer. For the CO-adsorbed FT-IR, the catalyst sample was loaded into an IR cell and calcined at 473 K for 1 h with Ar flow. After cooling to 303 K in Ar, a spectrum was collected as the background. Subsequently, CO was introduced into the IR cell and the adsorption of CO was conducted at 303 K for 30 min, and then another spectrum was recorded after fluxing the IR cell with Ar flow. The spectrum of CO adsorbed on the surface of catalysts was obtained by subtracting these spectra.

#### 3. Catalytic reaction

The catalytic transformation of FDCA to AA was performed in a batch-type Teflon-lined stainless-steel autoclave (30 mL). The temperature of the reactor was controlled by an oil bath with a magnetic stirring. Typically, the catalyst (0.020 g) and 0.10 mmol FDCA (0.0156 g) were added into the reactor that was precharged with ultrapure water (5 mL). Then the reactor was sealed and purged ten times with  $H_2$  at a fixed pressure (typically 3 MPa). The reaction was

started by vigorous stirring when the temperature reached 433 K. After a fixed reaction time, the reactor was quickly cooled by ice water to room temperature to terminate the reaction. For the recycling uses, the catalyst was recovered by centrifugation, washing with deionized water and drying at 333 K for 12 h. Then, the recovered catalyst was used for the next reaction. After reaction, gaseous products were collected in a gas bag. The gaseous products were analysed by a gas chromatograph (GC 2060) equipped with an RT-Plot-Q capillary column, and a thermal conductivity detector (TCD) and a flame ionization detector (FID) to detect  $CO_2$  and alkanes. Possible furan chemicals in the gas phase were also identified by the GC-MS (GC-2010 SHIMADZU, GCMS-QP2010 Plus) equipped with total ions chromatograph (TIC). Liquid products were analysed by electrospray ionization mass spectrometry (ESI-MS) (AmaZon SL, Bruker Daltonics Inc.) and quantified by a high-performance liquid chromatography (HPLC) with an instrument (Shimazu LC-20A) equipped with a refractive index (RI) detector and a Shodex SUGARSH-1011 column (8 mm  $\times$  300 mm) using a dilute H<sub>2</sub>SO<sub>4</sub> aqueous solution as a mobile phase. FDCA was analysed by the nuclear magnetic resonance (NMR) (Ascend III 500), in which 0.6 mL solution was mixed with 0.1 mL D<sub>2</sub>O and 0.1 mL DMSO (diluted to 100 ppm by ultrapure water) as an internal standard. The one-dimensional <sup>1</sup>H spectrum was measured by the water suppression method.<sup>2</sup>

The conversion of FDCA was calculated by the following equation.<sup>3</sup>

Conversion (%) =  $(C_{i,0} - C_{i,final}) / C_{i,0} \times 100\%$ 

The yield, selectivity and carbon balance (denoted as C balance) were calculated on a molar carbon basis by the following equations:

Yield (%) = (Number of carbon atom in product  $j \times C_{j,\text{final}}$ ) /(Number of carbon atom in  $i \times C_{i,0}$ ) × 100%

Selectivity (%) = (Number of carbon atom in product  $j \times C_{j,\text{final}}$ ) /(Number of carbon atom in  $i \times (C_{i,0}-C_{i,\text{final}})) \times 100\%$ 

C balance (%) =  $\sum$  (Number of carbon atom in product  $j \times C_{j,\text{final}}$ ) /(Number of carbon atom in  $i \times (C_{i,0}$ -  $C_{i,\text{final}})$ ) × 100%

 $C_{i,0}$  was the initial concentration of the substrate (FDCA, 20 mmol/L).  $C_{i,\text{final}}$  was the final concentration of the substrate (FDCA).  $C_{j,\text{final}}$  was the final concentration of liquid product (e.g., THFDCA, HAA and AA).

The site time yield for the formation of AA was calculated by the following equation:

Site time yield = Molar amount of AA formed/(Molar amount of Pt in the catalyst  $\times$  Pt dispersion  $\times$  reaction time)

The Pt dispersion was calculated by the following equation:<sup>4</sup>

Pt dispersion = 1.13/d (diameter, unit: nm)

In the above equation, d was the mean diameter of Pt NPs.

### **Supplementary Tables and Figures**

Catalyst	Conversion	Selectivity (%)			AA yield	C balance
	(%)	AA	THFDCA	HAA	(%)	(%)
Pt/HZSM-5	96	8	7	76	7.4	91
Pt/HZSM-5 <sup>a</sup>	98	10	8	26	10	44
Pt/CeO <sub>2</sub>	71	12	58	14	8.5	84
$Pt/CeO_2^a$	98	2	42	8	1.6	52

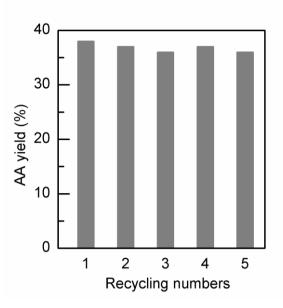
Table S1 Conversion of FDCA over Pt/HZSM-5 and Pt/CeO<sub>2</sub> catalysts.

Reaction conditions: FDCA 0.10 mmol, catalyst (Pt loadings 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K, 4 h. <sup>*a*</sup> 10 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.

Table S2 Conversion of FDCA over Pt-MoO<sub>x</sub>/TiO<sub>2</sub> catalyst.

Reaction cycle	Conversion	Selectivity (%)			AA yield	C balance
	(%)	AA	THFDCA	HAA	(%)	(%)
1 <sup>st</sup> use	>99	22	1	9	22	32
2 <sup>nd</sup> use	>99	18	1	7	18	26

Reaction conditions: FDCA 0.10 mmol, catalyst 0.020 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K, 8 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.



**Fig. S1** Recycling uses of Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O catalyst. Reaction conditions: FDCA 0.10 mmol, catalyst (Pt loadings 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K, 8 h.

Catalyst	Conversion	Selectivity (%)			AA Yield	C balance
	(%)	AA	THFDCA	HAA	(%)	(%)
Pt/Nb <sub>2</sub> O <sub>5</sub> ·xH <sub>2</sub> O	>99	38	7	1	38	46
Pd/Nb <sub>2</sub> O <sub>5</sub> · <i>x</i> H <sub>2</sub> O	>99	2	77	3	2.2	82
$Ru/Nb_2O_5 \cdot xH_2O$	>99	5	0.3	0.4	5.2	5.7
Rh/Nb <sub>2</sub> O <sub>5</sub> ·xH <sub>2</sub> O	>99	4	0.4	1	3.6	5.4
Ir/Nb <sub>2</sub> O <sub>5</sub> ·xH <sub>2</sub> O	>99	4	3	0.5	4.2	7.5

**Table S3** Conversion of FDCA over  $Nb_2O_5 \cdot xH_2O$ -supported noble metal catalysts.

Reaction conditions: FDCA 0.10 mmol, catalyst (metal loadings 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K, 8 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.

Pt loadings	Conversion	Selectivity (%)			AA yield	C balance
(wt%)	(%)	AA	THFDCA	HAA	(%)	(%)
0	1.0	0	0	0	0	0
1	34	17	17	37	5.7	71
2.5	76	23	22	50	18	95
5	>99	30	21	32	30	83

**Table S4** Effect of Pt loading amounts on catalytic behaviours of  $Pt/Nb_2O_5 \cdot xH_2O$  catalyst for the conversion of FDCA.

Reaction conditions: FDCA 0.10 mmol, Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O 0.030 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 433 K, 8 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.

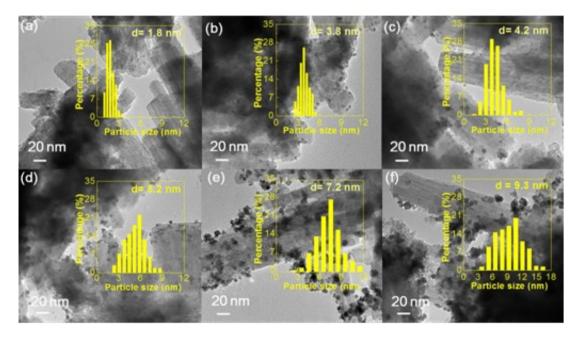
Catalyst	Temperature (K)	HAA conversion (%)	AA selectivity (%)	AA yield (%)
Pt/Nb <sub>2</sub> O <sub>5</sub> ·xH <sub>2</sub> O	433	57	61	35
	453	79	43	34
	473	>99	24	24
Pt/SiO <sub>2</sub>	433	16	22	3.4

Table S5 Conversion of HAA over the Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O and Pt/SiO<sub>2</sub>.

Reaction conditions: HAA 0.10 mmol, catalyst (Pt loading 5 wt%) 0.030 g, H<sub>2</sub>O 5 mL, 8 h. HAA and AA denote 2-hydroxyadipic acid andadipic acid, respectively.

Catalyst	Reductant	Reduction temperature (K)	Reduction time (h)
Pt-1.8/Nb <sub>2</sub> O <sub>5</sub> · <i>x</i> H <sub>2</sub> O	$H_2$	673	4
Pt-3.8/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	Ethylene glycol	433	4
Pt-4.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	NaBH <sub>4</sub>	298	4
Pt-5.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	NaBH <sub>4</sub>	273	8
Pt-7.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	NaBH <sub>4</sub>	323	4
$Pt-9.3/Nb_2O_5 \cdot xH_2O$	NaBH <sub>4</sub>	348	4

**Table S6** Synthetic conditions for the  $Pt-d/Nb_2O_5 \cdot xH_2O$  catalysts with different mean sizes of Pt particles.

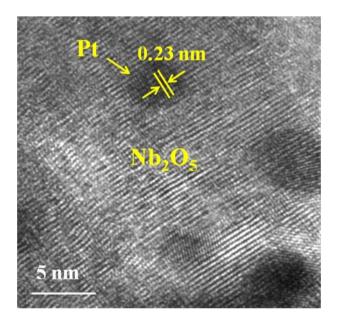


**Fig. S2** TEM images and the corresponding Pt particle size distributions for  $Pt-d/Nb_2O_5 \cdot xH_2O$ . Mean size of Pt particles: (a) 1.8 nm, (b) 3.8 nm, (c) 4.2 nm, (d) 5.2 nm, (e) 7.2 nm and (f) 9.3 nm.

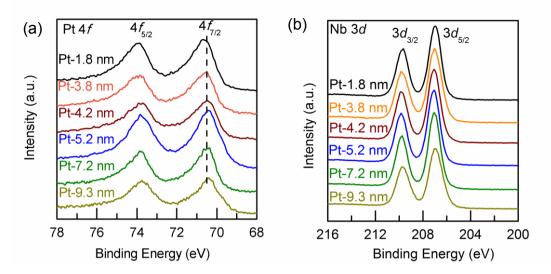
Catalyst	Pt loadings	Surface area	Pore volume	Pore size	Pt dispersion
	(wt%) <sup>a</sup>	$(m^2 g^{-1})$	$(cm^3 g^{-1})^b$	$(nm)^b$	(%) <sup>c</sup>
Pt-1.8/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.9	60	0.12	10	63
Pt-3.8/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.6	62	0.12	9.3	30
Pt-4.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.6	61	0.12	11	27
Pt-5.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.6	58	0.13	11	22
Pt-7.2/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.7	54	0.13	10	16
Pt-9.3/Nb <sub>2</sub> O <sub>5</sub> · $x$ H <sub>2</sub> O	4.8	53	0.11	11	12

**Table S7** Physical properties for  $Pt-d/Nb_2O_5 \cdot xH_2O$  catalysts with different mean sizes of Pt particles.

<sup>*a*</sup> Measured by ICP measurement. <sup>*b*</sup> Measured by N<sub>2</sub> physical adsorption; <sup>*c*</sup> Calculated by using the equation: Pt dispersion = 1.13/d, where *d* is the mean size of Pt nanoparticles.<sup>4</sup>



**Fig. S3** High-resolution TEM image for the Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O catalyst.



**Fig. S4** XPS spectra for  $Pt-d/Nb_2O_5 \cdot xH_2O$  catalysts with different mean sizes of Pt particles. (a) Pt 4f. (b) Nb 3d.

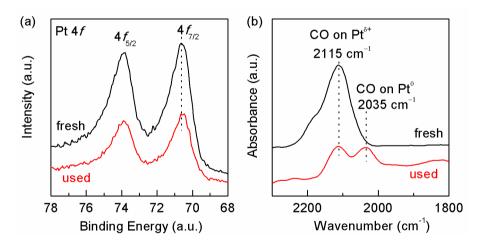


Fig. S5 (a) XPS spectra and (b) CO-adsorption IR spectra for Pt-1.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O catalysts.

Catalytic phase	Conversion	Selectivity (%)			AA yield	C balance
	(%)	AA	THFDCA	HAA	(%)	(%)
Liquid	28	0	2.0	0	0	2.0
Solid <sup>b</sup>	>99	37	6	1	37	44

**Table S8** Conversion of FDCA with the liquid and solid phases separated from the thermal treatment media for Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·xH<sub>2</sub>O via hot filtration.<sup>a</sup>

<sup>a</sup> Reaction conditions: FDCA 0.10 mmol, H<sub>2</sub> 3 MPa, 473 K, 8 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively. Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O was treated under the standard reaction conditions (H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K, 8 h) and then the mix was separated into liquid and solid phases via hot filtration. <sup>b</sup> H<sub>2</sub>O 5 mL.

H <sub>2</sub> pressure	Conversion	Selectivity (%)			AA yield	C balance
(MPa)	(%)	AA	THFDCA	HAA	(%)	(%)
0.5	99	21	13	28	21	62
1	>99	27	12	20	27	59
2	>99	31	10	8	31	49
3	>99	38	7	1	38	46

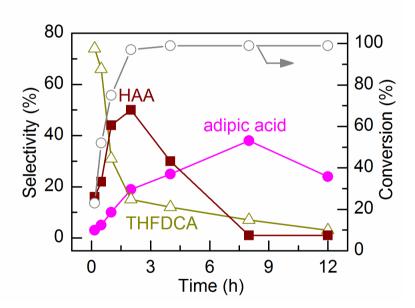
**Table S9** Conversion of FDCA over the  $Pt-3.8/Nb_2O_5 \cdot xH_2O$  catalyst under different  $H_2$  pressures.

Reaction conditions: FDCA 0.10 mmol, Pt/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O (Pt loading 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, 473 K, 8 h. FDCA, AA, THFDCA and HAA denote 2,5-furandicarboxylic acid, adipic acid, tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.

Temperature	Conversion	By-products Selectivity (%)					
(K)	(%)	$\rm CO_2$	C <sub>1</sub> -C <sub>6</sub> alkanes	HCA	DHHA	1,6-hexanediol	
433	99	3.5	1.1	0.5	0	0	
453	>99	6.5	0.6	2.5	0.2	0.14	
473	>99	12	1.1	3.7	4	0.23	

**Table S10** By-products during the conversion of FDCA over Pt- $3.8/Nb_2O_5$ ·*x*H<sub>2</sub>O catalyst at different reaction temperatures.

Reaction conditions: FDCA 0.10 mmol,Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O (Pt loading 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, 8 h. FDCA, HCA and DHHA denote 2,5-furandicarboxylic acid, hydroxycaproic acid, and 5,6-dihydroxyhexanoic acid, respectively.



**Fig. S6** Time-course result for Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O-catalyzed conversion of FDCA. Reaction conditions: FDCA 0.10 mmol, catalyst 0.020 g, H<sub>2</sub>O 5 mL, H<sub>2</sub> 3 MPa, 473 K. THFDCA and HAA denote tetrahydrofuran-2,5-dicarboxylic acid and 2-hydroxyadipic acid, respectively.

Temperatur	e AA conv. (%)	Yield (%)					
(K)	_	CO <sub>2</sub>	C <sub>1</sub> -C <sub>6</sub> alkanes	HCA	1,2-hexanediol		
433	6.9	2.4	1.4	2.9	0		
473	35	2.7	10	17.5	4.2		

**Table S11** Conversion of AA over Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O catalyst.

Reaction conditions: AA 0.10 mmol,Pt-3.8/Nb<sub>2</sub>O<sub>5</sub>·*x*H<sub>2</sub>O (Pt loading 5 wt%) 0.020 g, H<sub>2</sub>O 5 mL, 8 h. AA and HCA denote adipic acid and hydroxycaproic acid, respectively.

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