# **Electronic Supplementary Information**

# Composition and morphology tuning during hydrothermal synthesis of Sr<sub>x</sub>Ba<sub>1-</sub> <sub>x</sub>Nb<sub>2</sub>O<sub>6</sub> tetragonal tungsten bronzes studied by in situ X-ray diffraction

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# Selected temperature profiles

Temperature profiles during heating of the capillary were measured with a thermocouple placed inside the sapphire capillary, while the capillary was filled with water and pressurized to 100 bar. Temperature profiles were measured in 50 °C intervals from 100 to 400 °C (referring to the set-point temperature of the heat blower). The measured values were then used to calibrate the set-point temperature of the heat blower with the actual temperature inside the capillary.



**Figure S1:** Heating profiles for various set-point temperatures (100 – 450 °C). For all set-point temperatures a steady state is reached after about 20 s.

# Typical input file used for the sequential Rietveld refinement in TOPAS

For the sequential refinements the following parameters where refined for SBN: scale factor, two lattice parameters (a and c in the tetragonal cell), Lorentzian and Gaussian strain parameter, isotropic atomic displacement parameter (APD, Biso) for both the niobium and the alkaline earth sites (4 in total), Sr fraction, Sr occupancy on the A1-site and 3 atomic position parameters (in total 14 structural parameters). The 3 atomic position parameters were the x and y positions for the B2- and A1-site respectively (only one parameter is needed for the A1-site due to symmetry constraints). Sr was allowed to occupy the A1- and A2-sites, while Ba was locked to the A2-sites while keeping the stoichiometry (the sum of Ba and Sr equal to 5 plus 1 vacancy) and having physically meaningful occupancies (non-negative and not higher than 1). Ba was locked to the A2-site to avoid parameter correlation during refinement. The background was fitted with a 35th order Chebyshev polynomial to account for the broad background peak of water and solutes for each frame. Zero-shift error was refined for the last frame for each experiment, and then kept fixed for the sequential refinement. Atomic positions and B<sub>iso</sub> values for all oxygen atoms were kept fixed to RT neutron data from Carrio et al. [1]. Because of the temperature being higher than, or close to the reported T<sub>c</sub> for SBN for all experiments, the centrosymmetric space group (no. 127, *P4/mbm*) was used for all refinements instead of the reported non-centrosymmetric space group (no. 100, *P4bm*) stable at RT.

Below is a typical input-file for *TOPAS* used in this work, showing what equations and constraints are used for the different parameters. A "summarized" version of the input-file is presented in Table S1, and a typical graphical representation of a Rietveld refinement is presented in Figure S2.

r\_exp 0.0255204487 r\_exp\_dash 0.127019401 r\_wp 1.96483467 r\_wp\_dash 9.77929996 r\_p 0.943879931 r\_p\_dash 9.91316111 weighted\_Durbin\_Watson 0.267602062 gof 76.9906006

iters 100000

xdd "IN FILE.xye"

r\_exp 0.0255204487 r\_exp\_dash 0.127019401 r\_wp 1.96483467 r\_wp\_dash 9.77929996 r\_p 0.943879931 r\_p\_dash 9.91316111 weighted\_Durbin\_Watson 0.267602062 gof 76.9906006

x\_calculation\_step 0.01

'35th order Chebychev

bkg @ 22599.4817`\_28.5226096 -20712.2473`\_53.3728287 1593.86128`\_51.3664193 -233.598229`\_49.7733623 251.054531`\_48.0132791 -1755.78153`\_46.9298452 2685.7828`\_46.1299153 -898.431397`\_45.0653321 -683.825704`\_44.2134599 1284.87657`\_43.7297047 -409.724229`\_43.2107424 -555.518095`\_42.4263143 589.952675`\_42.0875049 -144.851875`\_41.3547231 -225.389735`\_40.8036582 317.795294`\_40.4192511 -107.279117`\_39.9558045 76.0631089`\_39.3158164 142.786448`\_39.0693042 12.5318361`\_38.460597 18.3369476`\_38.1103801 78.7237282`\_37.559452 48.0405916`\_37.1906964 -3.35622708`\_36.2257427 -17.0849808`\_35.9528332 95.0641312`\_35.110942 -24.0283942`\_34.7009036 6.4279789`\_33.1029892 -32.3078696`\_32.356327 4.36366726`\_30.2236073 -22.5049771`\_29.6072912 -14.1927031`\_26.7415948 8.22815171`\_25.0805855 21.8396967`\_19.287633 -20.3509081`\_15.112047

start\_X 3

finish\_X 51

no\_LIMIT\_warnings

do\_errors

Zero\_Error(!zero ,-0.00549`\_0.00032)

lam ymin\_on\_ymax 0.001 la 1.0 lo 0.77445 lh 0.1

LP\_Factor(90) 'change the LP correction or lh value if required

 $e0\_from\_Strain(\ 0.00063`\_0.00001,\ sgc,\ 0.23848`\_0.00481,\ slc,\ 0.08791`\_0.00518) \ 'defines \ and \ refines \ the \ values \ e0,\ name \ for \ Strain\_G,\ value,\ name \ for \ Strain\_L,\ value$ 

 $prm \ !e0\_SBN = Voigt\_FWHM\_GL(CeV\_or\_0(sgc, sgv), CeV\_or\_0(slc, slv)) \ .25 \ Pi/360; : \ 0.00063`\_0.00001 \ 'calculates \ the \ e0 \ using a \ macro \ in \ topas.inc$ 

r bragg r b SBN 1.11129852 phase\_MAC 22.296247`\_0.0920996971 phase\_name "SBN" MVW(1995.992<sup>2</sup>\_2.409, 626.224<sup>2</sup>\_0.024, 100.000<sup>2</sup>\_0.000) scale scale SBN 0.000309860911` 1.918e-006 space group P4/mbm Phase\_LAC\_1\_on\_cm( 118.00760`\_0.62990) Phase\_Density\_g\_on\_cm3( 5.29271`\_0.00639) Tetragonal(a SBN 12.564880` 0.000213 min=12.45; max=12.60;, c SBN 3.966552` 0.000076 min=3.955; max=3.98;) site Nb1 num posns 2 occ Nb 1 beq b Nb1 3.12544` 0.08979 min 0 max 7 x 0 y 0.5 z 0 site Nb2 num\_posns 8 occ Nb 1 beq b\_Nb2 2.21513`\_0.04540 min 0 max 7 x = 0.07529+xNb2; y = 0.21097+yNb2; z 0 site A1 num\_posns 2 x 0 y 0 z 0.5 occ Sr SrA1 0.92471`\_0.01099 min = 1/2; max = Sr/2; beq b\_A1 2.30362`\_0.15923 min 0 max 7 site A2 num\_posns 4 x xA2 = 0.17097 + disp;y yA2 = 0.67097 + disp;z 0.5 occ Sr SrA2 = (Sr-2\*SrA1)/4; : 0.03903`\_0.01330 beq b\_A2\_4.38415`\_0.10159 min 0 max 7 Ba/4; : 0.74862`\_0.01212 occ Ba BaA2 = beq b Ba2 = b A2; x 0.3413 y 0.0055 z 0.0 site O1 num posns 8 occ O 1 beq 1.90 x 0.1413 y 0.0647 z 0.0 site O2 num posns 8 occ O 1 beq 1.93 x 0.2817 y 0.7817 z 0.0 site O3 num\_posns 4 occ O 1 beq 0.13 site O4 num posns 2 occ O 1 beq 3.85 z 0.5 x 0 y 0.5 site O5 num\_posns 8 occ O 1 beq 2.88 x 0.2965 y 0.4175 z 0.5 prm Sr 2.00554`\_0.04846 min 1 max 4 prm Ba = 5-Sr; : 2.99446`\_0.04846 prm disp 0.00229' 0.00017 min -0.01 max 0.01 prm xNb2 -0.00090`\_0.00014 min -0.01 max 0.01 'Dispplacment in x-direction for Nb2-site prm yNb2 0.00254'\_0.00015 min -0.01 max 0.01 'Displcament in y-direction for Nb2-siter prm !sumA1 = SrA1; : 0.92471`\_0.01099 'Total occupancy on A1 site prm !sumA2 = BaA2+SrA2; : 0.78765`\_0.00549 'Total occupancy on A2 site prm !vac\_A1 = (1-sumA1)\*2; : 0.15059`\_0.02197 'Fraction vacancy on A1 prm !vac A2 = (1-sumA2)\*4; : 0.84941` 0.02197 'Fraction vacancy on A2 prm !sum\_vac = vac\_A1+vac\_A2; : 1.00000`\_0.00000 'Total vacancy prm !sum Ba = 4\*BaA2; : 2.99446` 0.04846 'Total Ba

str

#### prm !sum\_Sr = 2\*SrA1+4\*SrA2; : 2.00554`\_0.04846 'Total Sr

prm !ratio\_Sr = sum\_Sr/(sum\_Sr+sum\_Ba); : 0.40111`\_0.00969 'Amount of Sr in formula SrxBa1-xNb2O6

TCHZ\_Peak\_Type(, -0.45497, ,-0.01050, , -0.45190, , 0.45791, , 0.00012, , 0.00182)

#### Out\_X\_Yobs\_Ycalc\_Difference("IN\_FILE.txt")

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Out(Get (gof), "%15.5e")

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Out(scale\_pyro, "%15.5e")

Out(zero, "%15.5e\n")



**Figure S2:** Representative graphical representation of a Rietveld refinement, presented with SBN50\_T300 at the end of experiment.

Parameter	Prep refinement	<b>Batch refinement</b>	Comment					
Zero error	Refined	Fixed	Fixed to value at end of experiment					
Scale factor	Refined	Refined						
a [Å]	Refined	Refined						
c [Å]	Refined	Refined						
Gaussian and Lorentzian strain	Refined	Refined						
Sr fraction [a.u.]	Refined	Refined						
Sr occupancy A1 [a.u.]	Refined	Refined						
Sr occupancy A2 [a.u.]	Calculated	Calculated	Assuming unfilled TTB					
Ba fraction [a.u.]	Calculated		Assuming Ba = 1 - Sr					
Ba occupancy A1	Locked to 0							
Ba occupancy A2	Calculated		Assuming unfilled TTB					
Nb2 atomic positions (x and y)	Refined	Refined	2 parameters					
A1 atomic positions (x and y)	Refined	Refined	1 parameter (symmetry constraint)					
O positions	Fixed	Fixed	Fixed to neutron data					
O thermal parameters	Fixed Fixed Fixed to neutron da							
Total parameters refined	15	14						

**Table S1.** Overview of refined parameters from the Rietveld batch refinements and as preparation for the batch refinements respectively. Also included is a comment on what constraints or restrictions have been used for the different refinements.

### Validation of the Rietveld refinement model

 $Sr_xBa_{1-x}Nb_2O_6$  (SBN100\*x) was prepared by Aamlid et al. [2] by solid-state synthesis at 1400 °C with four different nominal compositions (SBN25\_T800, SBN33\_T800, SBN50\_T800 and SBN61\_T800) and synchrotron X-ray powder diffraction data was collected at SNBL, ESRF ( $\lambda = 0.77624$  Å). Details of synthesis and X-ray diffraction measurements conditions are found in [2]. The same Rietveld refinement model as previously described was used on this data set to verify that especially the refined Sr fraction values can be trusted. Figure S3 shows the Rietveld refinements, and in Figure S4 the refined lattice parameters (a and c) are plotted as a function of refined Sr fraction (diamonds) and nominal Sr fraction (upside down triangle) and compared to literature values. The results show that the refined Sr fraction definitely can be trusted (refined lattice parameters as a function of refined Sr fraction fits well with literature). It is also observed that the refined Sr fraction, since the samples are made by solid-state synthesis), as is seen by the better fit of the lattice parameters with literature when plotted versus the nominal Sr fraction.



**Figure S3:** Rietveld refinement of SBN25\_T800, SBN33\_T800, SBN50\_T800 and SBN61\_T800 showing data (blue circles), calculated (red) and the difference between data and calculated (grey). Grey bars show theoretical hkl positions of the SBN diffraction lines.



**Figure S4:** Refined lattice parameters for SBN (a and c) plotted versus refined Sr fraction (diamonds) and nominal Sr fraction (triangles). Indicated with open symbols are literature values for the a and c parameters at room temperature obtained from Podlozhenov et al. [3].

# TEM study of observed rods and bipyramids from hydrothermal synthesis of SBN

A hydrothermal reaction was done in a conventional steel autoclave with a PTFE liner with a filling factor of 70 %. The reaction was performed at 250 °C for 48 h and a Sr fraction of 0.5 in the precursor. The X-ray diffraction pattern showed SBN as the main phase with traces of the Pyro phase. By scanning electron microscopy (SEM) a mixture of rods and bipyramids were observed. It was assumed that SBN had formed rods, while the Pyro phase formed bipyramids. To verify this transmission electron microscopy (TEM) with a combination of imaging, electron diffraction and energy-dispersive X-ray spectroscopy (EDX) were used.

A JEOL JEM-2100 TEM equipped with an Oxford X-max80 EDX-detector was used, with an acceleration voltage of 200 kV. The sample was prepared by dropping a diluted acetone-dispersion of the sample on a carbon coated copper TEM grid and let dry it dry for approximately 10 min.

The results show that the rods are in fact SBN, and that the bipyramids are Pyro. Also, it shows that the Pyro phase is Sr rich compared with the SBN rods.



**Figure S5:** TEM images, electron diffraction and EDX for the observed rods (top row) and bipyramids (bottom row). EDX data are normalized to the most intense Cu-peak which is coming from the sample holder and is thus assumed to be comparable for the two EDX patterns.

# Lattice parameters (a and c) from Rietveld refinement

Figure S6 shows lattice parameters *a* (a and b) and *c* (c and d) obtained from Rietveld refinement at the of the experiments plotted versus reaction temperature (a and c) and Sr fraction *x* in the precursor (b and d). For details about the Rietveld refinement, and discussions about the results, see the main text.



**Figure S6:** Lattice parameters *a* (Figure a and b) and *c* (Figure c and d) from Rietveld refinement at the end of the experiments as a function of reaction temperature (Figure a and c) and Sr fraction x in precursor (Figure b and d)

# Morphology development as a function of temperature and Sr fraction

Decreasing reaction time gives in general an increase in aspect ratio. At lower temperatures more compositions show signs of hollow cubes or rods, while SBN have tube shaped particles for all temperatures.



Figure S7: SEM images of all compositions (SBN20-60) with reaction temperatures of 200, 225 and 300 °C.

# Summary of the final refined values for all experiments

Scale factor, isotropic Lorentzian and Guassian strain, lattice parameter, Sr fraction, Sr occupancy on A1site, B<sub>iso</sub> for the Nb1-, Nb2-, A1- and A2-site, and two atomic position parameters for the Nb2-site (x and y) and one for the A1-site for SBN were refined. Scale factor was refined for Pyro (with Pawley fit) and Uknw (with single peak phases) when present for the batch refinement, keeping lattice parameters (Pyro) and peak positions (Uknw) fixed to the values refined in the last frame.

**Table S2:** Refined values (strain, lattice parameter a and c, Sr fraction, Sr occupancy on A1-site, atomic displacement parameters for Nb1, Nb2, A1 and A2, atomic position parameters,  $R_{wp}$  and  $R_{bragg}$ ) for the last frame from each experiment. Estimated standard deviations from *TOPAS* are given, where for example 1.5(1) equals  $1.5 \pm 0.1$ .

Strain		Lattice Lattice		Sr Sr occ		Biso	Biso		
Sample	[10 <sup>-3</sup> ]	parameter	parameter	fraction	A1	Nb1	Nb2	x Nb2-site	
		a [Å]	c [Å]	x [a.u.]	[a.u.]	[Ų]	[Ų]		
SBN60_T300	0.76(2)	12.5672(2)	3.9651(1)	0.30(1)	0.75(1)	2.9(1)	2.0(1)	0.0751(2)	
SBN60_T225	0.70(4)	12.5664(2)	3.9659(1)	0.38(2)	0.91(2)	3.3(2)	2.0(1)	0.0746(3)	
SBN60_T200	0.75(5)	12.5537(3)	3.9633(2)	0.37(2)	0.92(3)	2.9(2)	2.3(1)	0.0744(4)	
SBN50_T400	0.77(2)	12.5607(1)	3.9647(1)	0.34(1)	0.85(1)	2.4(1)	1.9(1)	0.0740(2)	
SBN50_T300	0.66(1)	12.5635(1)	3.9659(1)	0.32(1)	0.81(1)	3.0(1)	2.13(5)	0.0746(2)	
SBN50_T225	0.71(2)	12.5692(2)	3.9621(1)	0.33(1)	0.82(1)	3.4(1)	1.9(1)	0.0747(2)	
SBN50_T200	0.71(2)	12.5644(2)	3.9710(1)	0.46(1)	0.86(1)	3.6(1)	2.2(1)	0.0730(2)	
SBN50_T175	0.61(2)	12.5639(1)	3.9737(1)	0.41(1)	0.88(1)	3.7(1)	2.1(1)	0.0739(2)	
SBN40_T300	0.60(1)	12.5637(1)	3.9693(1)	0.31(1)	0.77(1)	3.2(1)	2.18(4)	0.0740(1)	
SBN40_T225	0.66(2)	12.5655(1)	3.9676(1)	0.37(1)	0.89(1)	3.4(1)	2.0(1)	0.0733(2)	
SBN40_T200	0.62(2)	12.5689(1)	3.9590(1)	0.27(1)	0.66(1)	3.5(1)	2.3(1)	0.0745(2)	
SBN30_T300	0.44(1)	12.5559(1)	3.9773(1)	0.24(1)	0.61(1)	3.3(1)	2.50(5)	0.0742(1)	
SBN30_T225	0.55(1)	12.5583(1)	3.9749(1)	0.29(1)	0.73(1)	3.3(1)	2.4(1)	0.0736(2)	
SBN30_T200	0.59(1)	12.5634(1)	3.9649(1)	0.26(1)	0.65(1)	3.4(1)	2.3(1)	0.0742(1)	
SBN20_T300	0.78(2)	12.5422(2)	3.9909(1)	0.23(1)	0.57(1)	2.9(1)	2.3(1)	0.0736(2)	
SBN20_T225	0.83(3)	12.5533(2)	3.9852(1)	0.24(2)	0.61(2)	3.0(2)	2.3(1)	0.0737(3)	
SBN20_T200	0.73(3)	12.5638(2)	3.9826(1)	0.25(2)	0.62(2)	2.8(2)	2.7(1)	0.0743(3)	
SBN50_supercrit	0.96(5)	12.5397(3)	3.9718(2)	0.60(2)	0.72(2)	3.1(2)	2.0(1)	0.0723(3)	

Table S2 continued:

		Biso	Biso			Occ			
Sample	y Nb-site2	A1-site	A2-site	x A1-site	y A1-site	vacancy	R <sub>wp</sub>	R <sub>bragg</sub>	Beam
		[Ų]	[Ų]			A1 [a.u.]	[%]	[%]	time
SBN60_T300	0.2139(2)	0.0(2)	4.3(1)	0.1728(2)	0.6728(2)	0.50(2)	1.29	0.93	Feb
SBN60_T225	0.2132(3)	1.9(3)	4.3(2)	0.1736(4)	0.6736(4)	0.19(4)	1.63	0.83	Feb
SBN60_T200	0.2147(4)	0.8(4)	3.2(2)	0.1725(4)	0.6725(4)	0.16(1)	4.16	2.13	Oct
SBN50_T400	0.2131(2)	1.9(2)	3.8(1)	0.1732(2)	0.6732(2)	0.29(2)	1.63	0.85	Feb
SBN50_T300	0.2135(2)	1.0(2)	4.3(1)	0.1730(2)	0.6730(2)	0.39(2)	1.66	1.09	Feb
SBN50_T225	0.2132(3)	0.7(2)	4.7(1)	0.1720(3)	0.6720(3)	0.35(3)	2.25	1.35	Feb
SBN50_T200	0.2128(2)	1.8(2)	4.3(1)	0.1744(2)	0.6744(2)	0.29(3)	2.14	1.89	Feb
SBN50_T175	0.2126(2)	1.4(2)	3.7(1)	0.1739(2)	0.6739(2)	0.23(2)	1.67	1.23	Feb
SBN40_T300	0.2133(1)	0.9(1)	4.3(1)	0.1731(1)	0.6731(1)	0.45(2)	1.94	1.61	Feb

SBN40_T225	0.2132(2)	2.1(2)	4.4(1)	0.1736(2)	0.6736(2)	0.23(3)	1.90	1.47	Feb
SBN40_T200	0.2144(2)	0.0(2)	4.7(1)	0.1725(2)	0.6725(2)	0.67(2)	3.12	3.05	Oct
SBN30_T300	0.2130(1)	0.0(2)	4.3(1)	0.1729(1)	0.6729(1)	0.79(2)	2.37	2.35	Oct
SBN30_T225	0.2132(2)	1.0(2)	4.3(1)	0.1735(2)	0.6735(2)	0.53(2)	2.43	1.75	Oct
SBN30_T200	0.2134(2)	0.0(2)	4.5(1)	0.1727(1)	0.6727(1)	0.70(2)	4.15	3.31	Oct
SBN20_T300	0.2109(2)	0.0(3)	3.9(1)	0.1734(2)	0.6734(1)	0.85(2)	2.95	1.80	Oct
SBN20_T225	0.2169(3)	0.0(3)	4.3(1)	0.1732(3)	0.6732(3)	0.78(3)	6.74	3.62	Oct
SBN20_T200	0.2130(3)	0.0(3)	4.0(1)	0.1730(3)	0.6730(3)	0.76(3)	5.77	3.63	Oct
SBN50_supercrit	0.2092(3)	1.7(4)	2.8(2)	0.1732(3)	0.6732(3)	0.57(4)	4.56	2.95	Feb

# Effect of changing the alkaline earth to niobium ratio in the Rietveld refinement

To determine the effect of non-stoichiometry (having the sum of alkaline earth higher or lower than the stoichiometric value of 5) on the Rietveld refinement, the last frame of SBN30\_T300 was refined with varying amounts of alkaline earth (4.5 - 5.6). No other changes were done compared to the other refinements explained in the main text.

The results show that the  $B_{iso}$  value of the A1-site is 0 (nonphysical) for a total sum of 5 and less, and flattens out at 2.3 Å<sup>2</sup> for values higher than 5.4. Both R-values,  $R_{wp}$  and  $R_{bragg}$  decrease (which indicates an improved fit to the experimental data) with an increasing amount of Sr plus Ba. These results point towards a higher amount of alkaline earth than the stoichiometric value of 5 for the formed SBN.

Hypothetical charge compensation for an alkaline earth amount > 5 could be oxygen interstitials or free/itinerant electrons. Interstitial oxygen is unlikely, just as for perovskites, since the anion sublattice is close packed. Itinerant electrons have been suggested at the charge compensation in  $Sr_{1.2-x}Ba_xNb_2O_6$  (filled SBN, with 6 alkali earth) made under reducing conditions [4].



**Figure S8:** Refined values for Sr occupancy on the A1- and A2-sites, Ba occupancy on the A2-site and  $B_{iso}$  value for the A1-site (left) and the corresponding  $R_{wp}$  and  $R_{bragg}$  values as a function of sum of amount of alkaline earth included in the Rietveld refinement. Grey line indicates the stoichiometric amount for the sum of alkaline earth.

# References

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