## **Supporting Information**

## A microporous zinc–organic framework with Lewis basic pyridyl sites for highly selective $C_2H_2/CH_4$ and $C_2H_2/CO_2$ gas separation

Peng Yan<sup>a,b</sup>, Jucai Yang<sup>a,\*</sup>, Xiangying Hao<sup>b</sup>, Zhisheng Chen<sup>b</sup>, Guanhua Shen<sup>b</sup>, Yanhua Zhao<sup>b</sup>, Deyun Ma<sup>c,\*</sup>and Jiaxin Zhu<sup>d</sup>

<sup>a</sup>School of Chemical Engineering, Inner Mongolia University of Technology and Inner Mongolia Key Laboratory of Theoretical and Computational Chemistry Simulation, Hohhot 010051, P. R. China. E-mail:yangjc@imut.edu.cn.

<sup>b</sup>School of Environmental and Chemical Engi-neering, Zhaoqing University, Zhaoqing 526061, P. R. China.

<sup>c</sup>School of Food and Pharmaceutical Engineering, Zhaoqing University, Zhaoqing 526061, P. R. China. E-mail: <u>mady@zqu.edu.cn</u>

<sup>d</sup>Department of Chemistry, Fudan University, Shanghai 200433, P. R. China.



Figure S1. Themogravimetric curves for 1 and 1a.



Figure S2. C<sub>2</sub>H<sub>2</sub>, CO<sub>2</sub>, CH<sub>4</sub>, CO and N<sub>2</sub> isotherms of 1a fitted by LF model at 273 K.



Figure S3.  $C_2H_2$ ,  $CO_2$ ,  $CH_4$ , CO and  $N_2$  isotherms of 1a fitted by LF model at 298 K.



Fig. S4. IAST-predicted selectivities for  $C_2H_2/CH_4(50:50)$ ,  $C_2H_2/CO_2(50:50)$ ,  $CO_2/N_2$  (15:85),  $CO_2/CO(1:2)$  and  $CO_2/CH_4$  (50:50) mixtures on 1a at 273 K.



Figure S5. IR spectra of 1.

Figure S6. The reusability of 1a for CO<sub>2</sub> adsorption.

1

2

3

Frequency of use

5

4

6

1.0

0.5

0.0



Figure S7. Variable-temperature PXRD patterns for 1.



Figure S8. PXRD patterns for 1 exposed to humid air for 1, 2, and 5 days.



Figure S9. The BET surface area plot of 1a.



**Figure S10.** The DFT-calculated adsorption configurations of  $C_2H_2$  in the channel. (Zinc, carbon, oxygen, nitrogen, and hydrogen atoms are in slateblue, gray, red, blue, and white, respectively.)

1				
Zn(1)-O(1)	1.939(3)	Zn(1)-N(1)	2.045(3)	
Zn(1)-O(6) <sup>ii</sup>	1.940(3)	$Zn(1)-O(5)^{i}$	1.982(3)	
$Zn(2)-O(2)^{i}$	2.110(6)	Zn(2)-O(3) <sup>iii</sup>	2.058(6	
Zn(2)-O(4) <sup>iii</sup>	2.134(6)	$N(1)$ - $Zn(1)$ - $O(5)^{i}$	104.37(13)	

Table S1 Selected bond lengths (Å) and bond angles (°) for 1.

$O(6)^{ii}$ -Zn(1)-O(5) <sup>i</sup>	123.65(15)	O(1)-Zn(1)-N(1)	99.21(13)	
O(1)-Zn(1)-O(5) <sup>i</sup>	111.99(15)	O(1)-Zn(1)-O(6) <sup>ii</sup>	115.15(12)	
$O(6)^{ii}$ -Zn(1)-N(1)	96.87(13)	$O(3)^{iii}$ -Zn(2)-O(2) <sup>ii</sup>	151.0(3)	
$O(2)^{ii}$ -Zn(2)-O(2) <sup>i</sup>	112.8(4)	$O(2)^{i}$ -Zn(2)-O(4) <sup>iii</sup>	91.3(2)	
$O(3)^{iii}$ -Zn(2)-O(2) <sup>i</sup>	93.3(3)	O(3) <sup>iii</sup> -Zn(2)-O(3)	65.2(4)	
O(3) -Zn(2)-O(4)	86.2(3)	O(4) <sup>iii</sup> -Zn(2)-O(4)	150.9(4)	
Symmetry codes: i = x, 1-y, 1.5+z; ii = 0.5-x, 0.5+y, z; iii = 1.5-x, 0.5-y, 1.5+z.				

**Table S2** Fitting parameters of the Langmuir-Freundlich modle at 273 K.

Parameters			1		
	$C_2H_2$	$CO_2$	CH <sub>4</sub>	СО	N <sub>2</sub>
q <sub>m</sub>	4.9159	5.2880	3.2623	2.4980	1.6150
k	0.1423	0.0199	0.0071	0.0019	0.0017
n	0.7072	1.0001	0.9929	1.0419	1.0868
R <sup>2</sup>	0.9995	0.9999	1	0.9999	0.9999

 Table S3 Fitting parameters of the Langmuir-Freundlich modle at 298 K.

Parameters	1				
	$C_2H_2$	$CO_2$	CH <sub>4</sub>	CO	N <sub>2</sub>
q <sub>m</sub>	4.4688	5.0619	3.0861	2.0099	1.2232
k	0.0585	0.0079	0.0030	0.0010	0.0011
n	0.8074	0.9967	1.0197	1.0792	1.1840
$\mathbb{R}^2$	0.9996	0.9999	0.9999	0.9999	0.9999

## The method for calculation of gas selectivity:

The ideal adsorbed solution theory (IAST) developed by Myers and Praunitz [1]. From the IAST, the spreading pressure  $\pi$  is expressed as follows:

$$\pi_{i}^{0}(p_{i}^{0}) = \frac{RT}{A} \int_{0}^{p_{i}^{0}} \frac{q_{i}}{p} dp \quad (1)$$
$$\pi_{i}^{*} = \frac{\pi_{i}^{0}A}{RT} = \int_{0}^{p_{i}^{0}} \frac{q_{i}}{p} dp \quad (2)$$

where  $\pi$  and  $\pi^*$  are the spreading pressure and the reduced spreading pressure, separately. A is the specific surface area of the adsorbent.  $p_i^0$  is the gas pressure of component *i* that corresponding to the spreading pressure  $\pi$  of the gas mixture.

At a constant temperature, the spreading pressure of single component is the same:

$$\pi_1^* = \pi_2^* = \dots = \pi_n^*$$
 (3)

For binary adsorption of component i, the IAST requires:

$$Py_i = p_i^0 x_i \quad (4)$$

where  $y_i$  and  $x_i$  are the molar fractions of component i in the gas phase and in the adsorbed phase, respectively. *P* is the total gas pressure,  $p_i^0$  is the pressures of component i at the same spreading pressure as that of the mixture.

The adsorption isotherm of the pure component was fitted with a certain adsorption model to obtain the corresponding parameters. Then use formula (2) to get the specific spreading pressure expression. Finally, the  $x_i$  corresponding to a given total pressure P and the composition of  $y_i$  in the gas mixture is obtained according to formula (3) and (4).

Thus, adsorption selectivity S of a binary mixture is defined as:

$$S = \frac{\frac{x_1}{y_1}}{\frac{x_2}{y_2}}$$
(5)

The method for calculation of isosteric heat of adsorption:

The relationship between adsorption heat and temperature and pressure can be obtained by integrating the Clausius-Clapeyron equation as follows:

$$\ln p = -\frac{Q_{st}}{RT} + C$$

Using the adsorption isotherm data at different temperatures to draw a graph, the isosteric heat of adsorption can be obtained according to the slope of the straight line.

## **Density-Functional Theory Calculations:**

To obtain the gas binding energies, we use the DMOL3 to calculate the energy for the system, framework and gas molecule. The static binding energy was then calculated by using:  $EB = (E_{(MOF)}+Eg_{(gas)})-E_{(MOF+gas)}$ .<sup>2,3</sup>

[1] A. Myers, J.M. Prausnitz, Thermodynamics of mixed-gas adsorption, *AIChE. J.*, 1965, **11**, 121-127.

[2] DMol3, v. Accelrys, Inc, San Diego, 2005.

[3] Babarao, R.; Jiang, J. J. Phys. Chem. C, 2009, 113, 18287-18291.