

Supporting Information

Investigation of the deactivation behavior of Co catalysts in Fischer-Tropsch synthesis by using encapsulated Co nanoparticles with controlled SiO₂ shell layer thickness

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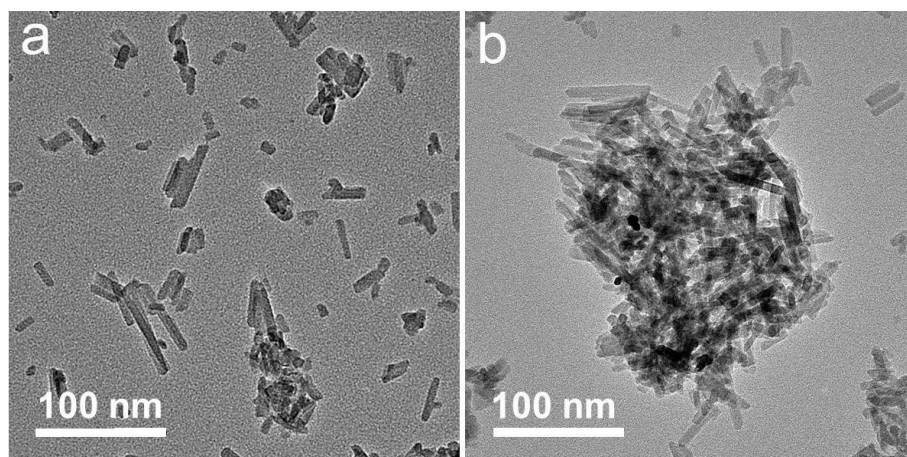


Fig. S1 TEM images of the Co_3O_4 nanorod precursors without calcination.

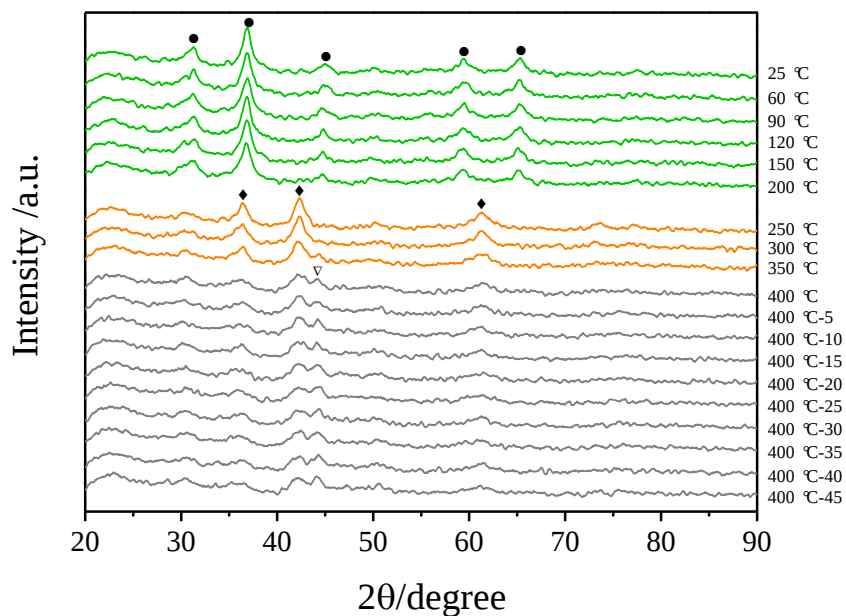


Fig. S2 In situ XRD patterns of 15Co10Zr/SiO₂ (Q50) catalyst. Note that: when conducting the in situ XRD experiment, the sample was in situ heated to 400 °C in a pure H₂ flow of 40 mL/min with a rate of 2 °C min⁻¹. It took about 7.5 min for each scanning. The x number in 400 °C-x represents the scanning times when the reduction temperature reached to 400 °C. ● Co₃O₄; ◆ CoO; ▽ Co.

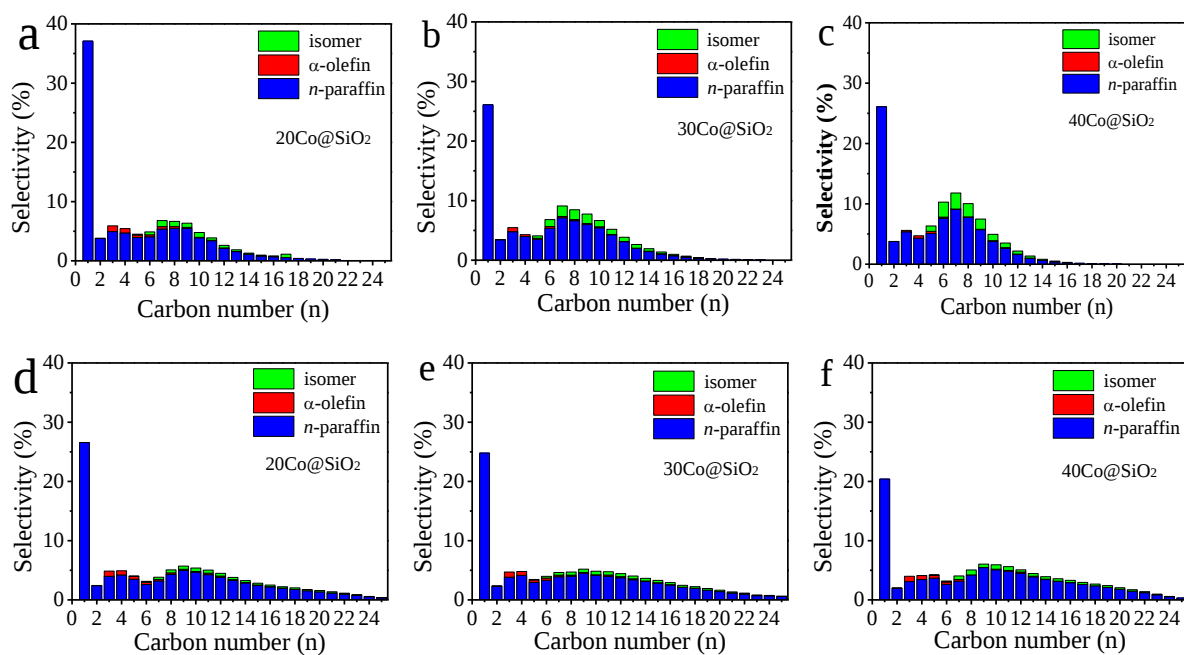


Fig. S3 Carbon number distributions of the FTS reactions over as-prepared catalysts at different reaction temperatures: (a-c) 240 °C; (d-f) 220 °C.

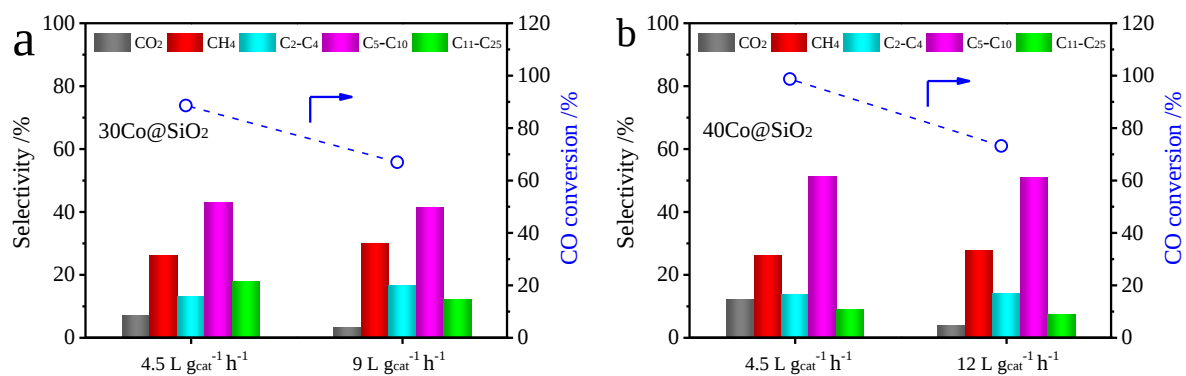


Fig. S4 Effects of GHSV on FTS activity and product distribution over as-prepared catalysts. Reaction conditions: 0.5 g of catalyst, 1 MPa, $\text{H}_2/\text{CO}/\text{N}_2 = 63.3/31.7/5$, 240 °C, 30Co@SiO₂ (a) and 40Co@SiO₂ (b). The values of CO conversion and selectivity were obtained as the average of last 5 h (46-50 h) in 50 h run stream.

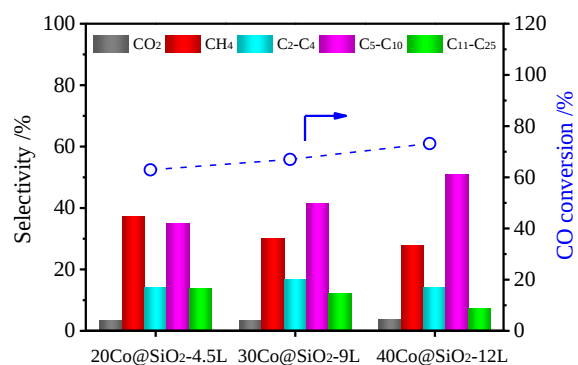


Fig. S5 Comparison of the FTS activity and product distribution over as-prepared catalysts with adjusted GHSV in order to obtain similar initial CO conversion. Reaction conditions: 0.5 g of catalyst, 1 MPa, H₂/CO/N₂ = 63.3/31.7/5, and 240 °C. The values of CO conversion and selectivity were obtained as the average of last 5 h (46-50 h) in 50 h run stream.

The calculation method of the water partial pressure can be described as below:

We can set the initial molar number of feeding gas $H_2 = 63.3$ mol, $CO = 31.7$ mol, and $N_2 = 5$ mol. And the CO conversion = x%, CO_2 selectivity = y%, CH_4 selectivity = z1%, $(C_2^{\bar{}}+C_2^o)$ selectivity = z2%, $(C_3^{\bar{}}+C_3^o)$ selectivity = z3%, $(C_4^{\bar{}}+C_4^o)$ selectivity = z4%. Then, the molar number of gas in the reactor can be calculated according to the following equations:

- 1) $Molar_{H_2} = 63.3 - 2 \times 31.7 \times x\% + 31.7 \times x\% \times y\%$;
- 2) $Molar_{CO} = 31.7 - 31.7 \times x\%$;
- 3) $Molar_{N_2} = 5$;
- 4) $Molar_{CO_2} = 31.7 \times x\% \times y\%$;
- 5) $Molar_{CH_4} = 31.7 \times x\% \times (1-y\%) \times z1\%$;
- 6) $Molar(C_2^{\bar{}}+C_2^o) = \{31.7 \times x\% \times (1-y\%) \times z2\% \} / 2$;
- 7) $Molar(C_3^{\bar{}}+C_3^o) = \{31.7 \times x\% \times (1-y\%) \times z3\% \} / 3$;
- 8) $Molar(C_4^{\bar{}}+C_4^o) = \{31.7 \times x\% \times (1-y\%) \times z4\% \} / 4$;
- 9) $Molar_{H_2O} = 31.7 \times x\% - 31.7 \times x\% \times y\% \times 2$

Based on the above obtained molar content of gas in the reactor, the partial pressure of water vapor can be calculated as following equation:

$$P_{H_2O} = 1.0 \times \frac{Molar_{H_2O}}{(Molar_{H_2} + Molar_{CO} + Molar_{N_2} + Molar_{CO_2} + Molar_{CH_4} + Molar_{C_2} + Molar_{C_3} + Molar_{C_4} + Molar_{H_2O})} \text{ (MPa)}$$