Screen versus cyclone for improved capacity and robustness for sidestream and mainstream deammonification

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Figure E1. (A/B) Ratio of intrinsic AerAOB over NOB removal rates as a function of the average concentrations in the reactor's aerobic zones of ammonium and nitrite (A; $DO = 1.5 \text{ mg } O_2/L$) and DO and nitrite (B; ammonium = 2 mg N/L) without bioaugmentation from sidestream to mainstream. (C) The net growth rate of AnAOB given an AnAOB-specific SRT of 30 days without bioaugmentation. (D) Relationship between the percentage of TIN removed through deammonification and the AerAOB/NOB rates ratio in the system. (E) Minimum net AnAOB growth rate required for adequate deammonification given a certain TIN removal for three different AnAOB specific SRT. (F) Maximum aerobic SRT where the ratio of AerAOB over NOB removal rates equaled 2 in function of the average nitrite and ammonium in the aerobic zone.



Figure E2. (A/C/E) Minimum anoxic SRT required to meet the minimum 0.04 d⁻¹ AnAOB net growth rate criterion in function of the AnAOB retention efficiency for an average nitrite residual of 0.75 (A), 1 (C), and 2 (E) mg N/L in the anoxic zone without bioaugmentation from sidestream to mainstream. (B/D/F) The spread of aerobic SRT where can be operated given an AerAOB/NOB ratio above or equal 2 as a function of the NOB retention efficiency for an

average nitrite residual of 0.75 (**B**), 1 (**D**), and 2 (**F**) mg N/L in the anoxic zone. The upper boundary of the zone was given by the aerobic SRT where the rate ratio is 2, while the lower boundary is given by the washout SRT of NOB.