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1	Nitrate with benefits: optimizing radical production during	UV
2	water treatment	
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Fluence determination

36 Fluence was determined for MPUV and LPUV irradiation experiments following standardized methods where UV fluence is calculated by multiplying the average irradiance by 37 the exposure time in seconds.¹ The average irradiance was determined by correcting the incident 38 irradiance (radiometer reading) for sample depth, absorbance, sample reflectance, petri factor 39 and sensor factor (MPUV only). This method for MPUV fluence determination is herein defined 40as "unweighted." If the sample contained H₂O₂ and irradiated with MPUV, an H₂O₂-weighed 41 fluence method ² was applied, unless noted otherwise, which follows the method described 42 above ¹ and also weights each wavelength by the H₂O₂ molar absorption spectrum relative to its 43 value at 254 nm. 44

As noted in Bircher (2015)², H_2O_2 weighted fluence is similar to DNA weighted fluence. 45 46 The difference between the two methods is that H₂O₂ weighted fluence values are weighted by the H₂O₂ molar absorption spectrum (200 - 350 nm) (Figure S1) relative to its value at 254 nm, 47 48 whereas DNA weighted fluence values are weighted by the germicidal (DNA) absorption 49 spectrum or action spectra of a target microorganism relative to its value at 254 nm.



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50

52 Figure S1. Molar absorbance spectra of H₂O₂.

54	The selected fluence calculation method will influence sample irradiation times that are
55	needed to achieve a target fluence. For instance, irradiation times determined by H_2O_2 and DNA
56	weighted fluence methods will be relatively lower for a given fluence in waters with low
57	absorbance at $<\!240$ nm and 260 nm, respectively, since H_2O_2 and DNA absorb photons of light
58	efficiently at these wavelengths. Table S1 illustrates the different exposure times required to
59	achieve a fluence level of 1000 mJ/cm ² using unweighted, H_2O_2 weighted and DNA weighted
60	fluence determination methods for two different absorbing waters. As shown, the irradiation
61	times differ between the applied fluence determination methods and the two waters. Overall,
62	irradiation times for water 2 are lower than water 1 since it can be assumed that water 2 is a
63	lower absorbing water matrix (as indicated by its UV absorbance at 200 nm and 254 nm). In
64	comparing unweighted and H_2O_2 weighted irradiation times, the H_2O_2 weighted irradiation time
65	is 20% higher than the unweighted irradiation time for water 1. In contrast, the H_2O_2 weighted
66	irradiation time is 13% lower than the unweighted irradiation time for water 2. This is because
67	the absorbance at 200 nm of water 1 is relatively high compared to water 2.

69 Table S1. A relative comparison of MPUV irradiation times for two waters using unweighted,

70 H₂O₂ weighted and DNA weighted fluence determination methods. UV absorbance (UVA)

71 values are provided at 200 nm and 254 nm. Irradiation times reflect the exposure time needed to

72 achieve a fluence level of 1000 mJ/cm².

73

	Water 1	Water 2		
	UVA $200 = 0.094 \text{ cm}^{-1}$	UVA $200 = 0.007 \text{ cm}^{-1}$		
Fluence determination	UVA $254 = 3.2 \text{ cm}^{-1}$	UVA $254 = 1.2 \text{ cm}^{-1}$		
method	Irradiation time (sec)			
Unweighted	765	540		
H ₂ O ₂ weighted	931	475		
DNA weighted	1103	789		

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An advantage of applying H_2O_2 weighted fluence instead of unweighted fluence is that compound degradation rates achieved during MPUV experiments can be directly compared to those achieved during LPUV experiments, assuming water quality and experimental conditions remain constant. To validate this point, separate experiments were performed. Deionized water (0 mg-N/L of nitrate and nitrite) containing ~1 mg/L of pCBA and 10 mg/L H₂O₂ was irradiated with MPUV and LPUV (1000 mJ/cm²). MPUV exposure times were determined by H₂O₂ weighted and unweighted fluence methods. Hydroxyl radical steady concentrations ([·OH]_{ss}) were used as a metric to compare results, and [·OH]_{ss} calculations followed methods presented in Keen et al. (2012) ³.

84 The results are presented in Figure S2. When H_2O_2 weighted fluence was used to

85 determine MPUV irradiation times, the [·OH]_{ss} were comparable between MPUV and LPUV.

86 However, MPUV irradiation times determined using unweighted fluence yielded [·OH]_{ss} values

87 that were approximately two times lower than LPUV [·OH]_{ss} values.

88



89

- 90 Figure S2. Comparison of hydroxyl radical steady state concentrations ([·OH]_{ss}) determined for
- 91 MPUV and LPUV irradiation (1000 mJ/cm²) of deionized water containing pCBA (1 mg/L) and
- 92 10 mg/L of H_2O_2 . For MPUV, [·OH]_{ss} values were determined using H_2O_2 weighted fluence (left
- side) and unweighted fluence (right side). LPUV $[\cdot OH]_{ss}$ values are the same on both sides of the graph. Error bars represent the standard deviation between duplicate experiments.

95

97 2 Central composite design

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99 A central composite design (CCD) was utilized to systematically evaluate the significance of nitrate, H₂O₂ and alkalinity concentration (Tables S2) on radical production during MPUV and 100 LPUV irradiation experiments (1000 mJ/cm²). pCBA degradation rates (k'_{pCBA}) were used to 101 indirectly measure the production of radicals in irradiated synthetic water that contained 102 103 Suwannee River Fulvic Acid (SRFA) as the dissolved organic carbon (DOC) source (Table 2 in the manuscript). Pseudo first order degradation plots of pCBA were found to exhibit first order 104 105 behavior (Figure S3). The central composite design experimental matrix was comprised of a total 106 of 38 experiments (19 experiments and 5 center points per lamp type, Table S2). k'_{pCBA} values are provided in Table S2. 107



108

109 Figure S3. MPUV (top row) and LPUV (bottom row) pseudo first order pCBA degradation plots

- 110 of measured pCBA in SRFA synthetic water (Table 2 within the manuscript) containing low (90
- 111 mg/L as CaCO₃, plots a and c) and high (290 mg/L as CaCO₃, plots b and d) alkalinity. Nitrate

112 (10 mg-N/L) and H_2O_2 (3 mg/L) concentrations remained constant.

114 2.1 Central composite design analysis

116 Minitab Software, version 17 (Minitab LLC, PA) was used to evaluate the effect of the

117 independent factors (i.e., nitrate, H₂O₂ and alkalinity concentration) and the response (k'_{pCBA} and

118 nitrite). The response was transformed using a power transformation (i.e., (k'_{pCBA})^{1/2}) to stabilize

- 119 the variance and improve model fit⁴. All experiments (Table S2 and S6) were performed in
- 120 random order. MPUV and LPUV transformed k'_{pCBA} values were found to be normally
- 121 distributed (p values > 0.05) (Figure S4), therefore, the null hypothesis that the data is not
- 122 normally distributed cannot be rejected.
- 123

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124



- 126 Figure S4. Probability plots generated in Minitab illustrating normal distribution of transformed
- 127 pCBA degradation rates, $(k'_{pCBA})^{1/2}$, obtained for MPUV (left plot) and LPUV (right plot)
- 128 irradiation experiments (Table S2).
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- Table S2. Experimental central composite design (CCD) and corresponding pCBA pseudo first order degradation results (k'_{pCBA}) for MPUV and LPUV. k'_{pCBA} values were determined for a UV fluence up to 1000 mJ/cm². Experiments were run in random order and in SRFA synthetic water (Table 2 within the manuscript). Transformed data, i.e. (k'_{pCBA})^{1/2}, were used for CCD
- analysis.

	Variables		MDUV	I DUV	Trans	formed	
Exp. ID	NO ₃ - (mg-N/L)	H ₂ O ₂ (mg/L)	Alkalinity (mg/L as CaCO ₃)	k' _{pCBA} (cm ² /mJ)	k' _{pCBA} (cm ² /mJ)	MPUV k' _{pCBA}	LPUV k' _{pCBA}
1	3	3	90	1.09E-03	8.24E-04	3.30E-02	2.87E-02
2	10	3	90	1.16E-03	5.45E-04	3.40E-02	2.33E-02
3	3	8	90	1.66E-03	1.59E-03	4.08E-02	3.98E-02
4	10	8	90	1.79E-03	1.44E-03	4.23E-02	3.80E-02
5	3	3	290	7.46E-04	5.36E-04	2.73E-02	2.32E-02
6	10	3	290	9.43E-04	5.09E-04	3.07E-02	2.26E-02
7	3	8	290	1.20E-03	1.00E-03	3.46E-02	3.17E-02
8	10	8	290	1.47E-03	9.96E-04	3.84E-02	3.16E-02
9	0.6	5.5	190	9.60E-04	9.02E-04	3.10E-02	3.00E-02
10	12.4	5.5	190	1.31E-03	8.97E-04	3.62E-02	3.00E-02
11	6.5	1.3	190	8.27E-04	3.68E-04	2.88E-02	1.92E-02
12	6.5	9.7	190	1.64E-03	1.48E-03	4.05E-02	3.85E-02
13	6.5	5.5	22	1.66E-03	1.33E-03	4.08E-02	3.64E-02
14	6.5	5.5	358	9.47E-04	7.46E-04	3.08E-02	2.73E-02
15	6.5	5.5	190	1.21E-03	9.08E-04	3.48E-02	3.01E-02
16	6.5	5.5	190	1.21E-03	8.78E-04	3.48E-02	2.96E-02
17	6.5	5.5	190	1.28E-03	8.68E-04	3.58E-02	2.95E-02
18	6.5	5.5	190	1.30E-03	9.38E-04	3.61E-02	3.06E-02
19	6.5	5.5	190	1.27E-03	9.64E-04	3.56E-02	3.10E-02

		Variab	oles	MP	UV	LPU	UV
Exp.	p. $NO_3^ H_2O_2$ Alkalinity		Alkalinity		pН	(SU)	
ID	(mg-N/L)	(mg/L)	(mg/L as CaCO ₃)	Initial	Final	Initial	Final
1	3	3	90	8.5	8.7	8.5	8.7
2	10	3	90	8.5	8.7	8.5	8.5
3	3	8	90	8.5	8.5	8.5	8.6
4	10	8	90	8.5	8.6	8.5	8.6
5	3	3	290	8.5	8.7	8.5	8.4
6	10	3	290	8.5	8.6	8.5	8.7
7	3	8	290	8.5	8.6	8.5	8.7
8	10	8	290	8.5	8.4	8.5	8.5
9	0.6	5.5	190	8.6	8.4	8.6	8.3
10	12.4	5.5	190	8.6	8.5	8.6	8.4
11	6.5	1.3	190	8.6	9.1	8.6	8.7
12	6.5	9.7	190	8.6	8.7	8.6	9
13	6.5	5.5	22	8.6	8.6	8.6	8.3
14	6.5	5.5	358	8.6	8.7	8.6	8.7
15	6.5	5.5	190	8.6	8.6	8.6	8.6
16	6.5	5.5	190	8.6	9.1	8.6	8.6
17	6.5	5.5	190	8.6	8.8	8.6	8.5
18	6.5	5.5	190	8.6	8.5	8.6	8.5
19	6.5	5.5	190	8.7	8.6	8.7	8.4

161 Table S3. Corresponding pH values for the central composite design (CCD) results (Table S2).

164 2.2 Model adequacy

165

The significance of model terms on the response was evaluated at a 90% confidence level using analysis of variance (ANOVA). For ANOVA, significant terms exhibited an F-value that was higher than the critical F-values for a given degrees of freedom and a p-value < 0.1. A stepwise backwards elimination approach was applied to remove the least significant terms from the quadratic model until all variables in the model had a p-value less than or equal to the alpha value set at 0.1. The ANOVA results are presented in Table S3.

172 Model adequacy was further evaluated by performing a residual versus fits analysis

173 (Figure S5). As shown in Figure S5, data is randomly scattered about the 0 y-axis indicating the

174 model is a good fit.

MF	рСВА		LPUV k' _{pCBA}				
Source	DF	F-Value	P-Value	Source	DF	F-Value	P-Value
Model	5	138	0	Model	7	93	0
Linear	3	225	0	Linear	3	209	0
NO ₃ -	1	55	0	NO ₃ -	1	5.7	0.036
H ₂ O ₂	1	413	0	H_2O_2	1	505	0
Alkalinity	1	206	0	Alkalinity	1	116	0
Square	1	9.0	0.010	Square	2	5.5	0.022
$(NO_{3})^{2}$	1	9.0	0.010	$(H_2O_2)^2$	1	4.8	0.052
				(Alkalinity) ²	1	4.9	0.049
2-Way Interaction	1	5.9	0.030	2-Way Interaction	2	8.3	0.006
NO ₃ -	1	5.9	0.030	NO ₃ -	1	6.3	0.029
× Alkalinity			0.050	× Alkalinity			
				$H_2O_2 \times Alkalinit$	1	10	0.008
Error	13			y Error	11		
Lack-of-Fit	9	1.4	0.394	Lack-of-Fit	7	2.4	0.211
Pure Error	4			Pure Error	4		
Total	18			Total	18		

176 Table S4. ANOVA table for MPUV (left) and LPUV (right) k'_{pCBA} response surface quadratic 177 model.



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183

184 The significant model terms are presented in equations 1 and 2. The squared alkalinity 185 term, found to be significant via ANOVA analysis (Table S4, LPUV), was not included in 186 equation 2 because the value was an order of magnitude lower than other significant terms. With 187 the exception of the $(H_2O_2)^2$ term in eq. 2, all main and interaction terms (eq. 1 and 2) had a p-188 value < 0.05 (Table S4).

189

$$(k'_{pCBA} MPUV)^{\frac{1}{2}} = 2.99 \times 10^{-2} + (6.4 \times 10^{-4} NO_3) + (1.49 \times 10^{-3} H_2O_2) - (3.70 \times 10^{-5} alkalinity) - (4.40 \times 10^{-5} (NO_3)^2) + (2.00 \times 10^{-6} (NO_3 \times alkalinity)) (1)$$

192

 $(k'_{pCBA} LPUV)^{\frac{1}{2}} = 2.19 \times 10^{-2} - (6.10 \times 10^{-4} NO_3) + (3.94 \times 10^{-3} H_2O_2) - (3.90 \times 10^{-5} alkalinity)$ $- (8.50 \times 10^{-5} (H_2O_2)^2) + (2.00 \times 10^{-6} NO_3 \times alkalinity)$ $- (4.00 \times 10^{-6} (H_2O_2 \times alkalinity))$ (2)

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197 2.3 Validation of CCD results

199 To validate results found by CCD analysis, separate experiments were performed in SRFA

200 synthetic water (Table 2 within the manuscript) at a fixed H₂O₂ concentration (10 mg/L) with

201 high and low alkalinity (60 and 300 mg/L as CaCO₃) and nitrate (1 and 10 mg-N/L) (Table S5).

202

203 Table S5. MPUV and LPUV k'_{pCBA} values determined in SRFA synthetic water (Table 2 within

204 the manuscript) at high and low alkalinity and nitrate concentrations and set H₂O₂ concentration

205 (10 mg/L). Each k'_{pCBA} value is the average of duplicate experiments (coefficient of variation

206 was < 6%, n=2).

	MP k' _{pCBA} (o	UV cm²/mJ)	LPUV k' _{pCBA} (cm ² /mJ)			
Alkalinity	Nitrate (mg-N/L)					
(mg/L as CaCO3)	1	10	1	10		
60	-1.74E-03	-1.83E-03	-2.20E-03	-2.08E-03		
300	-1.34E-03	-1.41E-03	-1.42E-03	-1.50E-03		

207

An increase in nitrate concentration from 1 to 10 mg-N/L at low alkalinity resulted in a \sim 5%

209 increase and decrease in k'pCBA values for MPUV and LPUV, respectively. At high alkalinity

210 conditions, the same increase in nitrate concentration led to a \sim 5% increase in k'_{pCBA} values for

both MPUV and LPUV, which aligns with the trends observed in Figure 3 of the manuscript and 211

212 further validates CCD findings.

Experimental matrix 213 **3**

214

215 The experimental matrix presented in Table S2 was supplemented with two additional

216 experiments, 20 and 21. Analysis of the data is discussed in section 4.2 of the manuscript. Table

S6 also reports the k'_d as a percent of the overall k'_{pCBA} value for a given test condition. 217

218

219 Table S6. Experimental matrix and corresponding pCBA pseudo first order degradation results

(k'_{pCBA}) for MPUV and LPUV. Experiments were run in random order and in SRFA synthetic 220

water (Table 2 within the manuscript). The contribution of direct photolysis (k'd) to the overall 221

222 k'_{pCBA} value is reported and was calculated using 1.37×10^{-4} cm²/mJ ± 3% (average followed by 223 the coefficient of variation, n=4) and 1.21×10^{-4} cm²/mJ ± 2% for MPUV and LPUV,

224 respectively.

Exp. ID	NO ₃ - (mg-N/L)	H ₂ O ₂ (mg/L)	Alkalinity (mg/L as CaCO ₃)	NO ₃ ⁻ /H ₂ O ₂	MPUV k' _{pCBA} (cm²/mJ)	Contribution of MPUV k' _d	LPUV k' _{pCBA} (cm²/mJ)	Contribution of LPUV k' _d
1	3	3	90	1.0	1.09E-03	13%	8.24E-04	15%
2	10	3	90	3.5	1.16E-03	12%	5.45E-04	22%
3	3	8	90	0.4	1.66E-03	8%	1.59E-03	8%
4	10	7	90	1.3	1.79E-03	8%	1.44E-03	8%
5	3	4	290	0.8	7.46E-04	18%	5.36E-04	23%
6	10	3	290	3.5	9.43E-04	15%	5.09E-04	24%
7	3	8	290	0.4	1.20E-03	11%	1.00E-03	12%
8	10	8	290	1.3	1.47E-03	9%	9.96E-04	12%
9	1	5	197	0.1	9.60E-04	14%	9.02E-04	13%
10	12	6	197	2.2	1.31E-03	10%	8.97E-04	13%
11	7	1	197	4.4	8.27E-04	17%	3.68E-04	33%
12	7	10	197	0.7	1.64E-03	8%	1.48E-03	8%
13	7	6	30	1.2	1.66E-03	8%	1.33E-03	9%
14	7	6	420	1.2	9.47E-04	15%	7.46E-04	16%
15	7	6	197	1.2	1.21E-03	11%	9.08E-04	13%
16	7	6	197	1.2	1.21E-03	11%	8.78E-04	14%
17	7	6	197	1.2	1.28E-03	11%	8.68E-04	14%
18	7	6	197	1.2	1.30E-03	11%	9.38E-04	13%
19	7	6	197	1.2	1.27E-03	11%	9.64E-04	13%
20	6	2	76	3.5	7.56E-04	18%	3.83E-04	32%

	21	6	1	76	4.5	8.90E-04	15%	3.53E-04	34%
225									

227 4 Nitrate and nitrite concentrations

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229 The initial nitrate and final nitrite concentrations after MPUV and LPUV irradiation

230 experiments (Table S2) are presented in Table S7.

231

- 232 Table S7. Nitrate and nitrite concentrations were measured using the cadmium reduction flow
- 233 injection method which is compliant with Standard Method 4500. The detection limit (DL) for
- 234 nitrate plus nitrite is 0.004 mg-N/L and nitrite is 0.005 mg-N/L. The initial nitrite concentration
- 235 for all experiments was 0 mg-N/L, and final nitrite concentrations were measured after MPUV
- and LPUV irradiation up to 1000 mJ/cm².

		MPUV,	LPUV,		
Exp.	Nitrate	Nitrite	Nitrite	MPUV,	LPUV,
ID	(mg-N/L)	(mg-N/L)	(mg-N/L)	NO ₂ ^{-/} NO ₃ ⁻	NO ₂ ^{-/} NO ₃ ⁻
1	3	0.22	1.3E-02	7.4%	0.33%
2	10	0.33	3.4E-02	3.2%	0.32%
3	3	0.21	1.1E-02	7.6%	0.37%
4	10	0.28	2.2E-02	2.8%	0.23%
5	3	0.22	9.0E-03	7.4%	0.30%
6	10	0.27	2.6E-02	2.5%	0.25%
7	3	0.22	1.2E-02	8.1%	0.41%
8	10	0.31	2.9E-02	2.7%	0.33%
9	0.6	0.10	DL	14.9%	0.00%
10	12.4	0.33	3.1E-02	2.6%	0.23%
11	6.5	0.29	1.4E-02	4.5%	0.21%
12	6.5	0.29	1.5E-02	4.3%	0.20%
13	6.5	0.26	1.2E-02	3.9%	0.18%
14	6.5	0.28	1.6E-02	4.1%	0.24%
15	6.5	0.23	2.0E-02	3.1%	0.31%
16	6.5	0.28	2.6E-02	4.3%	0.40%
17	6.5	0.24	2.2E-02	3.6%	0.34%
18	6.5	0.27	2.2E-02	4.2%	0.23%
19	6.5	0 25	2 1E-02	3.8%	0 32%

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246 5 Calculations

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248 5.1 **C3OH** scavenging calculation

- 250 The scavenging capacity of the water matrices evaluated in Figure 8 within the manuscript
- 251 was determined by multiplying the second order C3OH rate constant (k_{C3OH}, M⁻¹s⁻¹) of the
- 252 scavenger [S] by its measured molar concentration. Literature values of k_{c3OH} are provided in
- 253 Table S7.

254

- 255 Table S8. The C3OH scavengers evaluated for Figure 8 within the manuscript and their
- 256 corresponding second order rate constants with C3OH.

Scavenger	$k_{csOH}(M^{-1}s^{-1})$	Reference
SRFA DOC	2.06×10^{8}	McKay et al., 2011 ⁵
NO ₂ -	1.00×10^{10}	Buxton et al., 1988 ⁶
HCO ₃ -	8.5×10^{6}	Buxton et al., 1988 ⁶
CO ₃ ²⁻	3.9×10^{8}	Buxton et al., 1988 ⁶
H ₂ O ₂	2.70×10^{7}	Buxton et al., 1988 ⁶

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260 5.2 Molar absorption coefficient calculation

262 Molar absorption coefficient values of H₂O₂ and nitrate were experimentally calculated by

263 applying Beer-Lambert Law (equation 3), where ε (M⁻¹cm⁻¹) is the molar absorption coefficient,

264 A (cm⁻¹) is the sample absorbance at a specific wavelength, c is the molar concentration (M) and

265 *l* is the optical pathlength (1 cm) (Table S9). Absorbance values were measured using a Cary 100

- 266 Bio UV-Vis spectrophotometer (Agilent Technologies, CA). Since nitrate absorbs strongly at
- 267 wavelengths above > 220 nm and weakly at wavelengths < 250 nm, higher and lower nitrate
- 268 concentrations were used to measure the absorbance at 200 nm and 254 nm, respectively.

$$\varepsilon = \frac{A}{c \times b}$$

270

- 271
- 272
- 273 Table S9. Molar concentration (c), absorbance (A) and corresponding molar absorption
- 274 coefficient (ε) values for H₂O₂ and nitrate at 200 nm and 254 nm. Absorbance was measured 275 using a 1 cm cell pathlength.
- 276

	H_2O_2			Nitrate		
Wavelength (nm)	c (M)	A (cm ⁻¹)	ε (M ⁻¹ cm ⁻¹)	c (M)	A (cm ⁻¹)	ε (M ⁻¹ cm ⁻¹)
200	5.88E-04	0.121	205	7.13E-05	0.718	10066
254	5.88E-04	0.012	20	7.13E-04	0.005	6

(3)

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278 6 MPUV irradiation experiments with nitrified wastewater and groundwater

Photolysis of nitrate can generate GOH thereby creating a *de facto* advanced oxidation
process (AOP). GOH generation by MPUV photolysis of nitrate will occur more efficiently than
GOH generation by LPUV photolysis of nitrate because nitrate absorbs photons more strongly
at wavelengths < 250 nm. Therefore, a major advantage of MPUV photolysis of nitrate is the
generation of GOH without oxidant addition.

285 To demonstrate this point, groundwater (collected from a well in Los Angeles, CA) and nitrified wastewater effluent (Metro Wastewater Reclamation, Denver, CO) that contained native 286 287 nitrate concentrations (see Table S10 for water quality data) were spiked with pCBA (1 mg/L) and irradiated with MPUV (1000 mJ/cm²). The contribution of MPUV direct photolysis (k'_d) to 288 289 the total pCBA decay rate (k'_{pCBA}) was subtracted $(k'_{pCBA, indirect} = k'_{pCBA} - k'_{d})$ in order to isolate 290 pCBA degradation via radical oxidation (k'_{pCBA, indirect}). Values of MPUV k'_{pCBA, indirect} were then compared to the theoretical pCBA decay rates that would be achieved by LPUV/H₂O₂. LPUV 291 k'_{pCBA} values were attained by modeling pCBA degradation following methods presented by 292 293 Wols et al. (2013) ⁷.

As discussed in section 4 of the manuscript, the pCBA degradation rates (Table S11)

295 achieved in these systems after 1000 mJ/cm² were equivalent to LPUV irradiation (1000 mJ/cm²)

296 of the same experimental matrix containing ~ 1.5 mg/L and ~ 4 mg/L H₂O₂. It is important to note

297 that if a MPUV fluence other than 1000 mJ/cm² was applied, the corresponding equivalent H_2O_2

298 concentration for LPUV would change since nitrite levels after MPUV would be different.

299

- 300 Table S10. Water quality data for groundwater and nitrified wastewater effluent. Groundwater
- 301 samples were collected from a well site in Los Angeles, CA and wastewater effluent was
- 302 collected after biological aeration followed by filtration from Metro Wastewater Reclamation
- 303 (Denver, CO). The UV absorbance measured at 254 nm (UVA 254) represents the sample

304 absorbance with 1 mg/L pCBA addition.

Parameter	Units	Groundwater	Wastewater effluent
DOC	mg _c /L	0.50	8.5
pH	SU	8.1	7.6
NO ₃ -	mg-N/L	1.2	1.7
NO ₂ -	mg-N/L	0	0
Alkalinity	mg/L as CaCO ₃	150	70
UVA 254	cm ⁻¹	0.021	0.170

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308 Table S11. $k'_{pCBA, indirect} (k'_{pCBA, indirect} = k'_{pCBA} - k'_{d})$ values were experimentally determined for

309 MPUV/NO₃⁻ irradiation (1000 mJ/cm²) of groundwater and wastewater effluent (Table S8). The

310 equivalent H_2O_2 concentration needed to achieve the same k'_{pCBA, indirect} values during LPUV

311 exposure were theoretically determined using a steady-state kinetic model (Wols et al. 2013)⁷.

	k' _{pCBA, indirect} (cm ² /mJ)	MPUV/NO ₃ - (mg-N/L)	LPUV/H ₂ O ₂ (mg/L)
Groundwater	3.02E-04	1.2	1.30
Wastewater effluent	1.45E-04	1.7	3.80

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