Supplementary Information

Facile synthesis of "digestible", rigid-and-flexible, and bio-based building block for high-performance degradable thermosetting plastics

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Fig. S1 DSC curves of HMDO and DGHMDO.



Fig. S2 Hydrolysis of HMDO in 0.1 M hydrochloric acid solution (DMSO-d⁶/H₂O=9/1, v/v), ^a the ratio is the percentage of HMDO in the undegraded acetals.



Fig. S3 Hydrolysis of HMDO in 0.01M hydrochloric acid solution (DMSO-d⁶/H₂O=9/1, v/v), ^a the ratio is the percentage of HMDO in the undegraded acetals.



Fig. S4 Real-time ¹H NMR spectra of HMDO degradation in 0.001M HCl solution (DMSO- $d^6/H_2O=9/1$, v/v) at 23 °C.



Fig. S5 Real-time ¹H NMR spectra of HMDO degradation in 0.01M HCl solution (DMSO- $d^6/H_2O=9/1$, v/v) at 23 °C.



Fig. S6 Real-time ¹H NMR spectra of HMDO degradation in 0.1M HCl solution (DMSO-d⁶/H₂O=9/1, v/v) at 23 °C.



Fig. S7 Non-isothermal DSC curves of DGHMDO and DDM mixtures at different heating rates (5 °C min⁻¹, 10 °C min⁻¹, 15 °C min⁻¹ and 20 °C min⁻¹).



Fig. S8 ln (q/T_p^2) as a function of $1/T_p$ based on Kissinger's theory.



Fig. S9 ln q as a function of $1/T_p$ based on Ozawa's method.



Fig. S10 Contact angle of different solvents on DGHMDO-DDM.



Fig. S11 Appearance of DGHMDO-DDM before and after immersing in 0.1 M NaOH aqueous solution, water, 0.1 M HCl aqueous solution at 25 °C and 50 °C for 48 h.



Fig. S12 TGA curves of HMDO and DGHMDO.

Supplementary Tables

HMI	00	BP	A
C(1)-O(2)	1.41326	C(1)-C(4)	1.3883
O(2)-C(3)	1.36895	C(4)-C(5)	1.39854
C(3)-C(8)	1.4015	C(5)-C(6)	1.38029
C(3)-C(4)	1.38023	C(6)-C(7)	1.39159
C(4)-C(5)	1.39574	C(7)-C(9)	1.38508
C(5)-C(6)	1.384	C(9)-C(1)	1.39161
C(6)-C(7)	1.3907	C(7)-O(8)	1.36157
C(7)-C(8)	1.38009	C(4)-C(3)	1.53433
C(8)-O(9)	1.3548	C(2)-C(3)	1.53859
C(5)-C(10)	1.50377	O(8)-H	0.96084
C(10)-0(11)	1.40625		
O(11)-C(12)	1.41658		
C(12)-C(13)	1.52029		
C)13)-O(14)	1.41391		
О(9)-Н	0.96518		
O(14)-H	0.95993		

Table S1 Selected Bond Lengths (Å) in HMDO and BPA

Sample	DGHMDO-DDM	DGEBA-DDM
Pencil hardness	5H	6Н
Crosshatch adhesion	3B	2B
Reverse impact strength	45 cmkg	35 cmkg

Table S2 Coating performance of the thermosetting plastics

Table S3 Analyzed data for the positron lifetime of thethermosetting plastics

Sample	$\tau_3(ns)$	$I_{3}(\%)$	r_{PLAS}^{a} (Å)	V_{PLAS}^{b} (Å ³)	f_v^c (%)
DGHMDO-DDM	1.55	26.04	2.394	57.47	2.69
DGEBA-DDM	1.77	29.80	2.628	76.03	4.08

Table S4 Degradation ratio of DGHMDO-DDM under different

conditions

Adjusted condition	Main solvent	Acid	Concentration (M)	Temperature (°C)	Volume ratio (water/main solvent)	Time (h)	Degradation ratio (%)
Tomporatura	Acetone	HCl	0.1	25	1/9	12	5.46
Temperature	Acetone	HCl	0.1	50	1/9	5.5	100
	THF	HCl	0.1	50	1/9	6	100
	Acetone	HCl	0.1	50	1/9	5.5	100
The type of	Ethanol	HCl	0.1	50	1/9	12	57.17
main solvent	Methanol	HCl	0.1	50	1/9	12	56.48
	DMF	HCl	0.1	50	1/9	12	3.92
	DMSO	HCl	0.1	50	1/9	12	-0.7
The type of acid	Acetone	HCl	0.1	50	1/9	5.5	100
	Acetone	H_2SO_4	0.1	50	1/9	12	42.65
	Acetone	H_3PO_4	0.1	50	1/9	12	93.34
	Acetone	Acetic acid	0.1	50	1/9	12	-0.24
The	Acetone	HCl	1	50	1/9	0.5	100
concentration of	Acetone	HCl	0.5	50	1/9	1	100
acid	Acetone	HCl	0.1	50	1/9	5.5	100
	Acetone	HCl	0.1	50	0.5/9.5	1.5	100
	Acetone	HCl	0.1	50	1/9	5.5	100
The ratio of	Acetone	HCl	0.1	50	2/8	12	84.33
water/main	Acetone	HCl	0.1	50	3/7	12	69.39
solvent	Acetone	HCl	0.1	50	4/6	12	68.61
	Acetone	HCl	0.1	50	5/5	12	69.02
	No	HCl	0.1	50	10/0	12	3.13

Table S5 Chemical stability of DGHMDO-DDM in deionizedwater, hydrochloric acid aqueous solution and sodium hydroxideaqueous solution

Solvent	Concentration (M)	Temperature (°C)	Time (h)	Degradation ratio (%)
Deionized water	-	25	48	0
Hydrochloric acid aqueous solution	0.1	25	48	6.4
Sodium hydroxide aqueous solution	0.1	25	48	0
Deionized water	-	50	48	0
Hydrochloric acid aqueous solution	0.1	50	48	32.1
Sodium hydroxide aqueous solution	0.1	50	48	0

Supplementary Methods

Thermal stability:

The thermal stability of polymers is often indicated by the statistic heat-resistant index (T_s) which is calculated through (equation 1) with $T_{d5\%}$ (degradation temperature of 5% weight loss) and $T_{d30\%}$ (degradation temperature of 30% weight loss).²

$$T_s = 0.49 \left[T_{d5\%} + 0.6 \left(T_{d30\%} - T_{d5\%} \right) \right] \tag{1}$$

Curing kinetics of DGHMDO and DDM:

The activation energy of the epoxy systems was determined by Kissinger's method (equation 2) and Ozawa's method (equation 3). ³

$$-\ln(q/T_{p}^{2}) = E_{a}/RT_{p} - \ln(AR/E_{a})$$
⁽²⁾

$$In \ q = -1.052 \times E_a / RT_p + In(AE_a / R) - InF(x) - 5.331$$
(3)

Where q is the heating rate, T_p is the peak exothermic temperature, E_a is an average activation energy of the curing reaction, A is the pre-exponential factor, R is the gas constant, and F(X) is a conversion dependent term. Table S3 summarizes the T_p and its corresponding heating rate. The E_{as} were calculated from the slope of the plots of $-In(q/T_p^2)$ versus $1/T_p$ based on Kissinger's theory or In(q) versus $1/T_p$ based on Ozawa's method, which are presented in Figure S15-S16.

The cross-link density of the thermosetting plastics was estimated by the average molecular weight between cross-link points (Mc) which was reckoned in terms of equation 4.

$$M_{c} = \frac{n_{epoxy} \cdot M_{epoxy} + n_{DDM} \cdot M_{DDM}}{n_{DDM}}$$
(4)

where n is the amount of the corresponding component of the epoxy resin and M is the molecular weight of the corresponding component of the epoxy resin. The calculation results are summarized in the Table S6.

Calculation of the free volume (f_{ν}) of the thermosetting plastics:

The long-lifetime component τ_3 is attributed to "pick-off" annihilation of o-Ps at holes in the amorphous phase and can be used to estimate the size of the free volumes in the amorphous

phases by equation 5.4

$$\tau_{0-Ps}^{-1} = 2 \left[1 - \frac{R}{R+\Delta R} + \frac{1}{2\pi} sin(\frac{2\pi R}{R+\Delta R}) \right]$$
(5)

Where R is the radius of free volume hole and $\Delta R = 0.1656$ nm is derived from fitting the observed o-Ps lifetimes in molecular solids with known hole sizes. The formation probability of o-Ps, I_3 , is correlated with the intensity of the free volume.

The free volume radius R is calculated by the formula (6), and the free volume size is calculated by equation 6.

$$V = 4\pi R^3/3 \tag{6}$$

The volume fraction of the free volume, which is the percentage of the total volume of the polymer, expressed in f_v , can be calculated using equation (7), where C is a constant 0.0018 Å⁻³.

$$f_v = C \times I_3 \times V_f \tag{7}$$

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