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Electronic Supplementary Information

Probing promotional effects of potassium and the nature of active chromium species in Cr/MCM-41 catalysts for methyl mercaptan abatement

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2 Experimental

2.1 Synthesis of support and catalysts

MCM-41 was synthesized via hydrothermal method by employing tetraethyl orthosilicate (TEOS) as silicon source and cetyltrimethyl ammonium bromide (CTAB) as the template. Ammonium solution (NH₄OH) was used to adjust the pH of synthesis solution. In a typical synthesis batch, 14 g of CTAB and 54 mL of NH₄OH were dissolved into 635 mL of deionized water under ambient temperature. Next to, 57.6 mL of TEOS was introduced by dripping in the above mixture solution under continuous stirring. Subsequently, the white solid was obtained after filtrated and dried 110 °C for 24 h. Finally, the sample was calcined under 550 °C for 5 h.

MCM-41 supported Cr-based catalysts were prepared via incipient wetness impregnation route, and the corresponding procedures were registered as follows: the calculated amount of Cr precursors ($H_8CrN_2O_4$, $K_2Cr_2O_7$ and K_2CrO_4) was added to hot deionized water to ensure that the precursor was completely dissolved so as to keep the same loading of Cr. Next to, 2 g of MCM-41 was rapidly added into the above mixture solution so as to make all the liquid to be totally adsorbed by MCM-41. Almost immediately, the resulted sample was placed under ambient temperature for one night, then dried at 110 °C for 6h. Finally, the dried material was calcined under 550 °C for 5h in air. The corresponding samples prepared with $H_8CrN_2O_4$, $K_2Cr_2O_7$ and K_2CrO_4 were denoted as Cr-N/MCM-41, Cr-K/MCM-41 and Cr-K₂/MCM-41, respectively.

To investigate and understand the roles of K addition, two other materials were also synthesized by using incipient wetness impregnation. The first one was named as K/MCM-41 that was prepared according to the above synthesis procedures by replacing Cr precursor with K_2CO_3 . The second one was labelled as Cr-N-K/MCM-41, in which Cr-N/MCM-41 rather than MCM-41 was impregnated with K_2CO_3 , and the mole ratio of Cr to K was kept at 1.0(Cr/K = 1.0). Moreover, to determine the optimum Cr content and K content on active Cr-N-K/MCM-41 sample, the different mole ratio of xCr-N-yK/MCM-41 catalysts (x=0.5, y=1; x=1.5, y=1; x=1, y=0.5; x=1, y=1.5) were also prepared at Cr/K =0.5, 1.5 and K/Cr=0.5, 1.5 by using incipient wetness impregnation.

The mechanically mixed catalysts (i.e. $CrO_3/MCM-41$, $Cr_2O_3/MCM-41$ and $CrO_3+Cr_2O_3/MCM-41$) containing 18 wt % Cr loading were synthesized. $CrO_3+Cr_2O_3/MCM-41$ catalyst was prepared by mixing equal masses of each component by means of grinding. Then, the obtained catalyst followed by calcination at 300 °C for 5h in N₂.

2.2 Catalyst characterization

X-ray diffraction (XRD) patterns of catalyst samples were recorded on a Rigaku D/max - 1200 diffractometer by using Cu K α radiation (λ =1.5406 Å) within the scattering angle (2 θ) range of 20-80°. The spectra of Ultraviolet-visible (UV-vis) diffuse reflectance were obtained from a PERSEE TU-1901 and tested in the region of 250-800 nm at room temperature. X-ray photoelectron spectroscopy (XPS) was implemented on a PHI 5000 Versa Probe II spectrometer by using non-monochromatic Al K α radiation (1486.6 eV) as X-ray source and photoelectron peak of C1s (284.6 eV) was employed to adjust binding energy for reference. Thermogravimetric (TG) analysis was carried out on a Mettler-Toledo TGA/DSC (STA449F3) instrument, and the sample was heated from 50 to 800 °C (10 °C/min) within nitrogen (N₂) flow. Chromium and potassium content of the samples were determined by ICP-OES.

The profiles of temperature-programmed reduction of hydrogen (H₂-TPR) were recorded on a fixed-bed reactor at temperature range from 200 °C to 700 °C. Firstly, 50 mg of catalyst was pre-treated at 400 °C for 1h by using the flow of 5 vol% O₂ in argon (Ar) to eliminate some physisorbed species on the surface of sample so as to keep the same conditions. After that, the obtained material were cooled to 200 °C within the ultra-pure argon (Ar) flow. Subsequently, H₂-TPR test was performed under the 10% H₂/Ar (30 cm³/min) with the heating rate of 10 °C/min from 200 °C to 700 °C, and hydrogen (H₂) consumption during the reduction reaction process was monitored by an on-line thermal conductivity detector (TCD).

Base properties of catalyst samples were characterized by CO_2 -TPD, in which a TCD was used to on-line detect the concentration of the desorbed carbon dioxide (CO_2). Before CO_2 -TPD experiment, the catalyst (100 mg) was treated with helium (He, 30 cm³/min) flow at 500 °C for 2 h, then the obtained catalyst was cooled to room temperature. After that, the catalyst was saturated by 10% CO_2 within He (30 cm³/min) under room temperature. Then, the saturated catalyst were purified at 100 °C with ultra-pure helium (He) gas for 1 h to remove weak CO_2 and/or physically adsorbed CO_2 . CO_2 -TPD profile was recorded by heating cell temperature from 100 to 800 °C in ramp rate of 10 °C/min within ultra-pure He (30 cm³/min). O_2 -TPD were tested by similar experimental method on the same apparatus equipped with TCD. The catalysts (100 mg) were first treated at 450 °C for 1h in He flow (30 cm³/min) and cooled to room temperature in the same atmosphere, then O_2 (oxygen) flow was continuously pass at 30 cm³/min though materials for 1h. Then the saturated sample were swept using flowing He. O_2 -TPD profile was carried out at a heating rate of 10 °C/min from 30 to 800 °C in flowing He.

2.3 Catalytic activity test

The catalytic activity tests for CH₃SH decomposition was measured in a fixed-bed micro-reactor under atmospheric pressure at temperature region between 250 °C and 500 °C. 0.2g of catalyst with 60-40 mesh size was placed in the reactor. Then, the reactant gas mixture (1% CH₃SH balanced with N₂) in total flow 30 cm³/min was introduced to the reaction system. The outlet gas from the reactor was analyzed by employing two sets of on-line GC equipped with a flame photometric detector (FPD), a thermal conductivity detector (TCD), two flame ionization detectors (FID) together with one methanation reactor.

The conversion of CH₃SH (%) is defined as:

 $CH_3SH \ conversion = \frac{C_{(CH_3SH)in} - C_{(CH_3SH)out}}{C_{(CH_3SH)in}} \times 100\%$

 $C_{(CH3SH)in}$ represents the CH₃SH initial concentration, and $C_{(CH3SH)out}$ denotes the CH₃SH residual concentration after reaction.

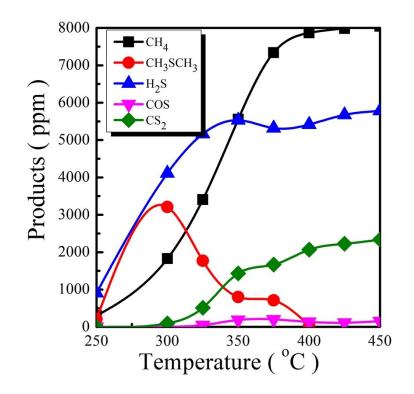


Figure S1. Decomposition products as a function of reaction temperature on Cr-N/MCM-41.

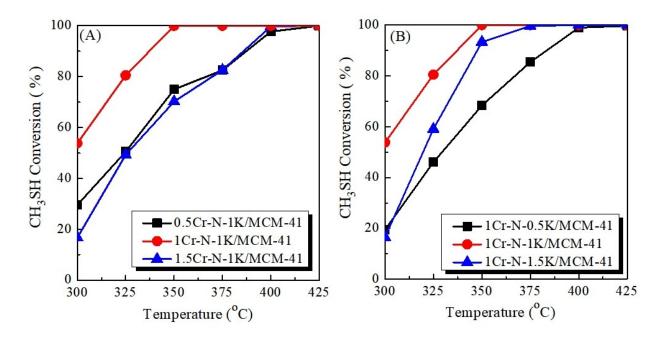


Figure S2. Conversion of CH₃SH as a function of reaction temperature on different Cr to K molar ratio of Cr-N-K/MCM-41 catalysts

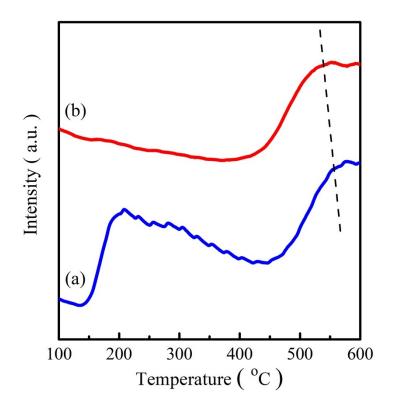


Figure S3. NH₃-TPD profiles of (a) Cr-N/MCM-41 and (b) Cr-N-K/MCM-41 catalysts.

With the addition of K, the intensity of weak acid sites decreased and the temperature of strong acid peak shift to the lower temperature. This phenomenon proves that alkali metal potassium significantly reduces the acidity of Cr-N/MCM-41 sample, which is beneficial to the catalytic conversion CH_3SH

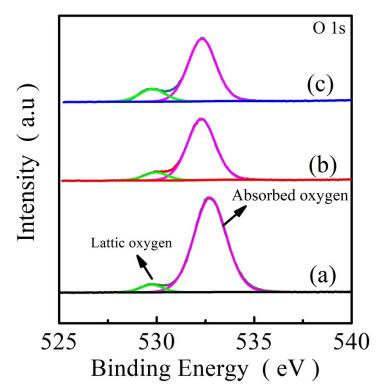


Figure S4. XPS of O 1s of (a) Cr-N/MCM-41, (b) Cr-K/MCM-41 and (c) Cr-N-K/MCM-41.

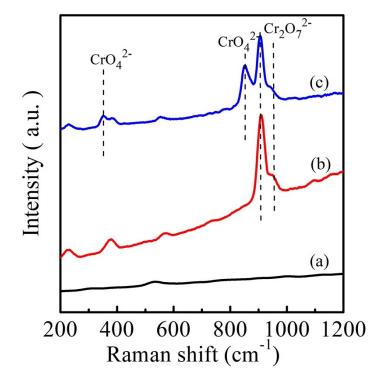


Figure S5. Raman spectra of (a) Cr-N/MCM-41, (b) Cr-K/MCM-41 and (c) Cr-N-K/MCM-41.

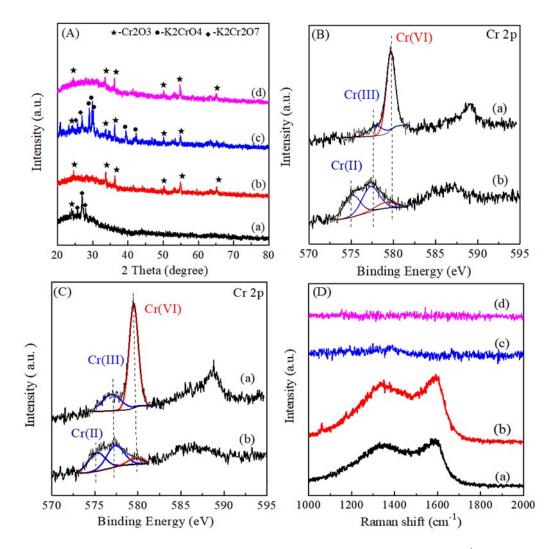


Figure S6. (A) XRD patterns of K-containing catalysts: (a) Fresh Cr-K/MCM-41; (b) Spent Cr-K/MCM-41; (c) Fresh Cr-N-K/MCM-41; (d) Spent Cr-N-K/MCM-41. (B) XPS spectra of fresh (a) and spent (b) Cr-K/MCM-41 catalyst. (C) XPS spectra of fresh (a) and spent (b) Cr-N-K/MCM-41 catalyst. (D) Raman spectra of spent and regenerated catalysts: (a) Spent Cr-K/MCM-41; (b) Spent Cr-N-K/MCM-41; (c) Regenerated Cr-K/MCM-41; (d) Regenerated Cr-N-K/MCM-41.

Sample	Cr/K	ICP-OES								
		K content (%)	Cr content (%)	Cr/K (ICP)						
0.5Cr-N-1K/MCM-41	0.5	11.9	6.4	0.54						
1Cr-N-1K/MCM-41	1	11.9	10.7	0.90						
1.5Cr-N-1K/MCM-41	1.5	11.9	14.1	1.18						

Table S1 ICP-OES results on different Cr to K molar ratio of Cr-N-K/MCM-41 samples.

Table S2 ICP-OES results on different K to Cr molar ratio of Cr-N-K/MCM-41 samples.

Sample	K/Cr	ICP-OES							
		K content (%)	Cr content (%)	Cr/K (ICP)					
1Cr-N-0.5K/MCM-41	0.5	6.08	10.5	0.58					
1Cr-N-1K/MCM-41	1	11.9	10.7	1.11					
1Cr-N-1.5K/MCM-41	1.5	17.3	10.1	1.71					

Table S3 Catalytic activity comparison of K-containing with other reported catalyst

Catalyst	Temperature(°C) ^a	Refs.
CeO ₂	450	[1]
$Ce_{0.75}Y_{0.25}O_2$	450	[2]

HZSM-5	550	[3]
Cr/ZSM-5	450	[4]
Nd/ZSM-5	500	[5]
Sm/ZSM-5	500	[6]
La/ZSM-5	500	[3]
Reused Cr adsorbent	400	[7]
Cr-N/MCM-41	450	Present work
Cr-K/MCM-41	375	Present work
Cr-N-K/MCM-41	350	Present work

Table S4 Thermodynamic data (Δ H, S, G, K_p and Log₁₀(K_p)) of equation (1) obtainedfrom HSC Chemistry software under various temperature.

Reactions		$4(NH_4)_2CrO_4 = 2CrO_3 + Cr_2O_3 + N_2(g) + 6NH_3(g) + 7H_2O(g) $ (1)													
	0°C	50°C	100 °C	150°C	200 °C	250°C	300 °C	350 °C	400 °C	450°C	500 °C	550°C	600 °C	650°C	700°C
ΔH _r (T) (kJ/mol)	111.4	120.8	130.6	140.7	158.3	169.3	180.5	191.8	203.4	215.1	227.1	239.2	251.4	263.9	276.5
	15	45	38	35	09	14	15	94	53	93	13	10	83	29	48
ΔS _r (T) (J/K/mol)	535.4	567.1	595.2	620.6	659.1	681.2	701.7	720.7	738.5	755.3	771.3	786.4	800.9	814.8	828.1
	33	03	73	57	49	55	01	34	75	97	34	94	67	28	39
ΔG _r (T) (kJ/mol)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	34.83	62.41	91.48	121.8	153.5	187.0	221.6	257.2	293.7	331.0	369.2	408.1	447.8	488.2	529.3
	9	5	8	96	67	85	65	31	19	72	44	92	82	79	55
Kp	4.601	1.229	6.424	1.118	9.013	4.801	1.597	3.663	6.218	8.242	8.881	8.032	6.251	4.272	2.606
	E+006	E+010	E+012	E+015	E+016	E+018	E+020	E+021	E+022	E+023	E+024	E+025	E+026	E+027	E+028
Log ₁₀ (K _p)	6.663	10.09	12.80	15.04	16.95	18.68	20.20	21.56	22.79	23.91	24.94	25.90	26.79	27.63	28.41
		0	8	8	5	1	3	4	4	6	8	5	6	1	6

Table S5 Thermodynamic data (Δ H, S, G, K_p and Log₁₀(K_p)) of equation (2) obtained from HSC Chemistry software under various temperature.

Reactions		$2K_2Cr_2O_7 = 2K_2O + 2Cr_2O_3 + 3O_2(g)$ (2)													
Redectoris	0°C	50 °C	100 °C	150°C	200 °C	250 °C	300 °C	350 °C	400 °C	450°C	500 °C	550 °C	600 °C	650°C	700°C
ΔH _r (T) (kJ/mol)	527.9	539.6	551.4	563.2	575.4	587.9	600.7	614.7	632.2	645.8	659.5	673.3	687.1	700.9	714.8
	71	12	14	66	13	26	70	75	95	97	73	16	20	81	96
ΔS _r (T) (J/K/mol)	174.1	213.2	247.2	277.0	304.1	329.2	352.7	376.1	403.2	422.7	440.9	458.2	474.4	489.9	504.6
	78	46	09	08	36	69	13	48	19	10	96	19	99	36	15
ΔG _r (T) (kJ/mol)	480.3	470.7	459.1	446.0	431.5	415.6	398.6	380.3	360.8	340.2	318.6	296.1	272.8	248.6	223.8
	95	02	68	50	12	69	13	78	68	15	17	33	11	97	30
Kp	1.337E	8.099E	5.235E	8.590E	2.281E	3.115E	4.666E	1.296E	9.891E	2.652E	2.966E	1.610E	4.767E	8.449E	9.655E
	-092	-077	-065	-056	-048	-042	-037	-032	-029	-025	-022	-019	-017	-015	-013
Log ₁₀ (K _p)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	91.87	76.09	64.28	55.06	47.64	41.50	36.33	31.88	28.00	24.57	21.52	18.79	16.32	14.07	12.01
	4	2	1	6	2	7	1	7	5	6	8	3	2	3	5

Table S6 Thermodynamic data (ΔH , S, G, K _p and Log ₁₀ (K _p)) of equation (3) obtained
from HSC Chemistry software under various temperature.

Reactions		$2 \operatorname{Cr}_2 \operatorname{O}_3 + 4 \operatorname{K}_2 \operatorname{CO}_3 + 3 \operatorname{O}_2 (g) = 4 \operatorname{K}_2 \operatorname{CrO}_4 + 4 \operatorname{CO}_2 (g)$ (3)													
neactions	0°C	50°C	100 °C	150°C	200 °C	250 °C	300 °C	350 °C	400 °C	450 °C	500 °C	550 °C	600 °C	650 °C	700°C
ΔH _r (T) (kJ/mol)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	156.2	157.4	158.4	159.4	160.7	162.3	164.3	166.6	169.2	174.9	175.4	175.7	175.6	175.2	156.4
	46	44	86	63	20	66	79	69	21	49	92	47	68	09	59
ΔS _r (T) (J/K/mol)	129.5	125.5	122.5	120.0	117.2	113.9	110.2	106.4	102.5	94.25	93.53	93.20	93.30	93.80	113.8
	13	32	20	68	69	68	97	69	33	8	0	9	0	9	48
ΔG _r (T) (kJ/mol)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	191.6	198.0	204.2	210.2	216.2	221.9	227.5	233.0	238.2	243.1	247.8	252.4	257.1	261.8	267.2
	22	09	05	70	05	88	96	15	41	12	05	72	33	09	50
K _p	4.437	1.022	3.869	9.086	7.422	1.467	5.545	3.418	3.079	3.647	5.537	1.053	2.420	6.534	2.218
	E+036	E+032	E+028	E+025	E+023	E+022	E+020	E+019	E+018	E+017	E+016	E+016	E+015	E+014	E+014
Log ₁₀ (K _p)	36.64	32.00	28.58	25.95	23.87	22.16	20.74	19.53	18.48	17.56	16.74	16.02	15.38	14.81	14.34
	7	9	8	8	1	7	4	4	8	2	3	2	4	5	6

Table S7 Thermodynamic data (Δ H, S, G, K_p and Log₁₀(K_p)) of equation (4) obtained from HSC Chemistry software under various temperature.

Reactions		$4K_2CrO_4 + 2 Cr_2O_3 + 3O_2(g) = 4K_2Cr_2O_7 $ (4)													
	0°C	50 °C	100 °C	150°C	200 °C	250 °C	300 °C	350°C	400 °C	450°C	500 °C	550°C	600 °C	650°C	700°C
ΔH _r (T) (kJ/mol)	-	_	-	-	_	_	-	-	-	_	-	_	-	-	-
	53.43	64.74	76.38	88.23	100.3	112.8	125.5	138.5	151.8	165.4	179.3	193.5	208.1	223.1	247.4
	4	0	9	9	75	21	59	61	43	26	27	66	64	44	58
ΔS _r (T) (J/K/mol)	-	_	_	-		_	_	_	-	_	-	_	_	-	
	84.24	122.2	155.7	185.5	212.6	237.6	260.8	282.6	303.1	322.5	341.1	359.0	376.2	392.8	418.6
	7	08	20	15	18	17	68	14	14	76	61	04	19	99	77
ΔG _r (T) (kJ/mol)	-	-	-	-9.738	0.225	11.48	23.95	37.55	52.19	67.84	84.44	101.9	120.3	139.5	159.9
	30.42	25.24	18.28			9	8	0	8	4	1	48	31	61	78
	2	9	2												
κ _p	6.57	1.20	3.62	1.59	9.44	7.12	6.55	7.11	8.89	1.25	1.97	3.38	6.32	1.26	2.58
- .h	8E+	7E+	6E+	3E+	4E-	5E-	3E-	4E-	6E-	6E-	1E-	9E-	1E-	6E-	4E-
	005	004	002	001	001	002	003	004	005	005	006	007	008	008	009
Log ₁₀ (K _p)	5.818	4.082	2.559	1.202	-0.025	-1.147	-2.184	-3.148	-4.051	-4.901	-5.705	-6.470	-7.199	-7.897	-8.588

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