

Electronic Supplementary Information

Realization of High-Quality Optical Nanoporous Gradient-Index Filters by Optimal Combination of Anodization Conditions

**Cheryl Suwen Law^{a,b,c}, Siew Yee Lim^{a,b,c}, Lina Liu^{a,d,e}, Andrew D. Abell^{*b,c,f}, Lluís F. Marsal^{*g} and
Abel Santos^{*a,b,c}**

^aSchool of Chemical Engineering and Advanced Materials, The University of Adelaide, Adelaide, South Australia 5005, Australia.

^bInstitute for Photonics and Advanced Sensing, The University of Adelaide, Adelaide, South Australia 5005, Australia.

^cARC Centre of Excellence for Nanoscale BioPhotonics, The University of Adelaide, Adelaide, South Australia 5005, Australia.

^dState key Laboratory of High-Efficiency Utilization of Coal and Green Chemical Engineering, Ningxia University, Yinchuan 750021, P. R. China.

^eCollege of Chemistry and Chemical Engineering, Ningxia University, Yinchuan 750021, P. R. China.

^fDepartment of Chemistry, The University of Adelaide, Adelaide, South Australia 5005 Adelaide, Australia.

^gDepartment of Electronic, Electric, and Automatics Engineering, University Rovira i Virgili, Tarragona, Tarragona 43007, Spain.

***E-Mails:** andrew.abell@adelaide.edu.au ; lluis.marsal@urv.cat ; abel.santos@adelaide.edu.au

Table of Contents

Fig. S1: Effective medium assessment of NAA-GIFs as a function of J and t_{an}	S-3
Fig. S2: Transmission spectra of NAA-GIFs produced by SPA under various T_{an} and $[H_2SO_4]$ for $t_{an} = 10$ h.....	S-4
Fig. S3: Transmission spectra of NAA-GIFs produced by SPA under various T_{an} and $[H_2SO_4]$ for $t_{an} = 15$ h.....	S-4
Fig. S4: Transmission spectra of NAA-GIFs produced by SPA under various T_{an} and $[H_2SO_4]$ for $t_{an} = 20$ h.....	S-5
Fig. S5: FEG-SEM images of NAA films produced with varying anodization current density (J) and anodization time (t_{an}).....	S-9
Table S1: Equations of different parameters for ANOVA table.....	S-7

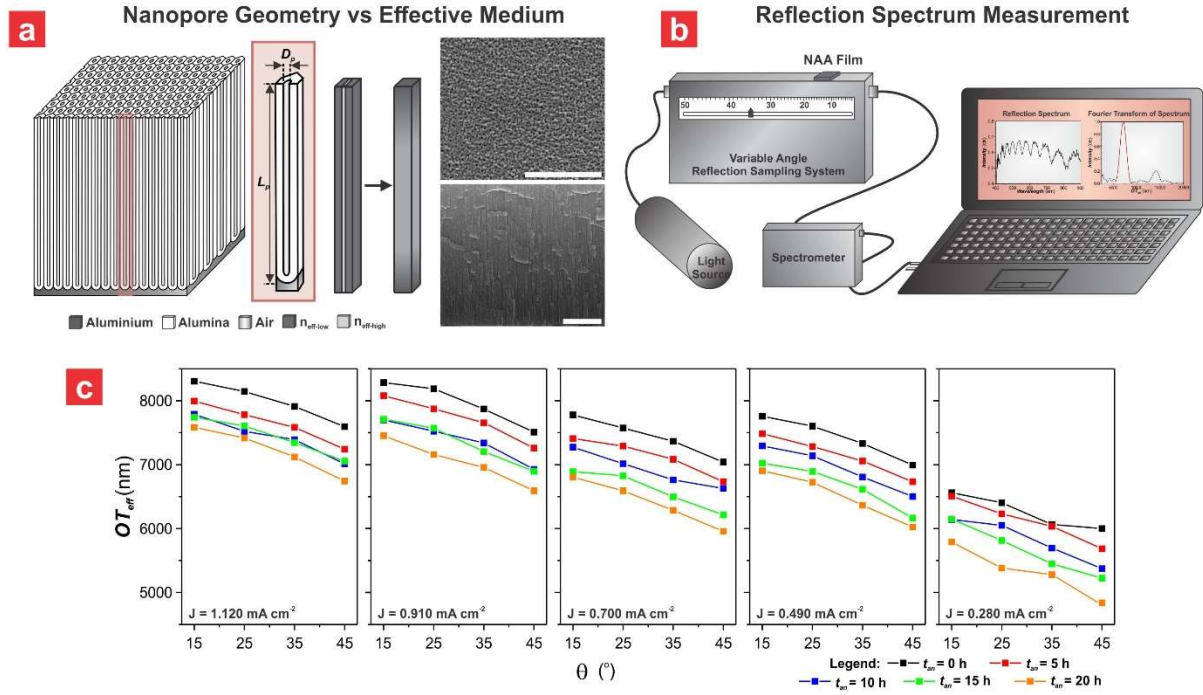


Fig. S1. Assessment of effective medium of NAA films produced with varying J and t_{an} . (a) Schematic illustration showing the correlation between nanopore geometry and effective medium in NAA films, with FEG-SEM images showing top and cross-sectional views of a representative NAA film (scale bar = 500 nm – top and scale bar = 1 μ m – cross-section). (b) Schematic of set-up used to acquire the reflection spectrum of NAA films. (c) Effective optical thickness (OT_{eff}) of NAA films produced with varying $J = 0.280$ – 1.120 mA cm^{-2} and $t_{an} = 0$ – 20 h at varying angle of incidence ($\theta = 15^\circ$, 25° , 35° and 45°).

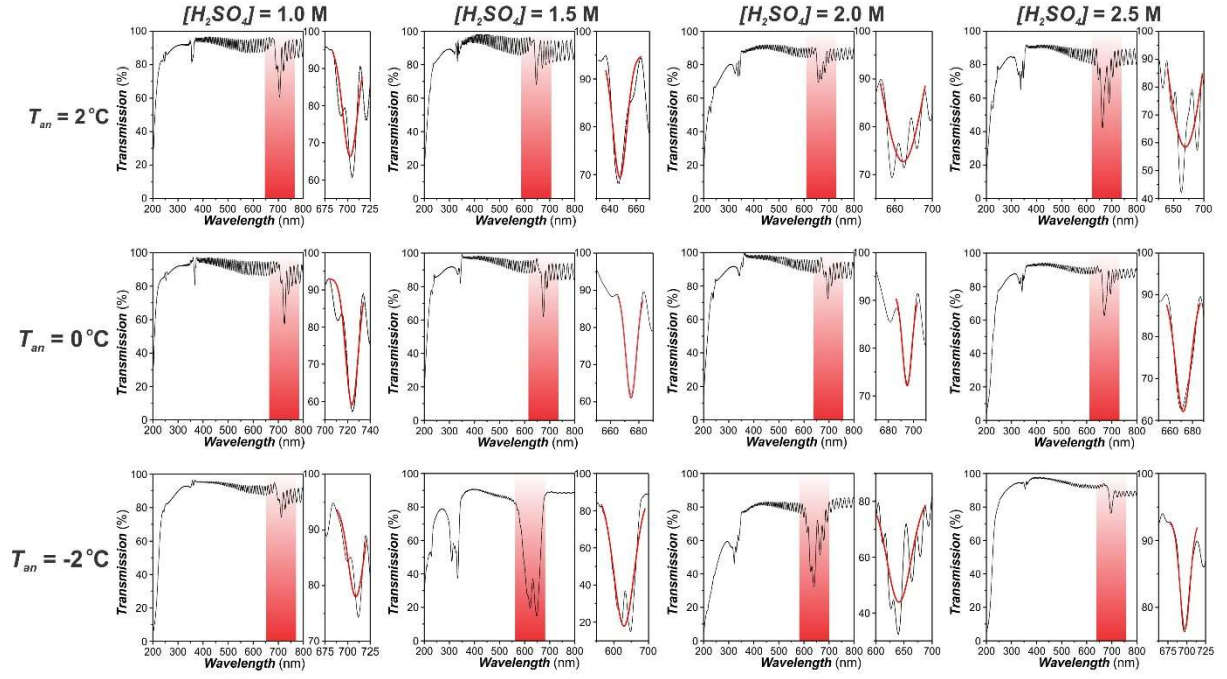


Fig. S2. Full transmission spectra and magnified views of the characteristic photonic stopband (PSB) of NAA-GIFs produced by SPA with varying $T_{an} = -2$ – 2°C and $[\text{H}_2\text{SO}_4] = 1.0$ – 2.5 M for $t_{an} = 10\text{ h}$.

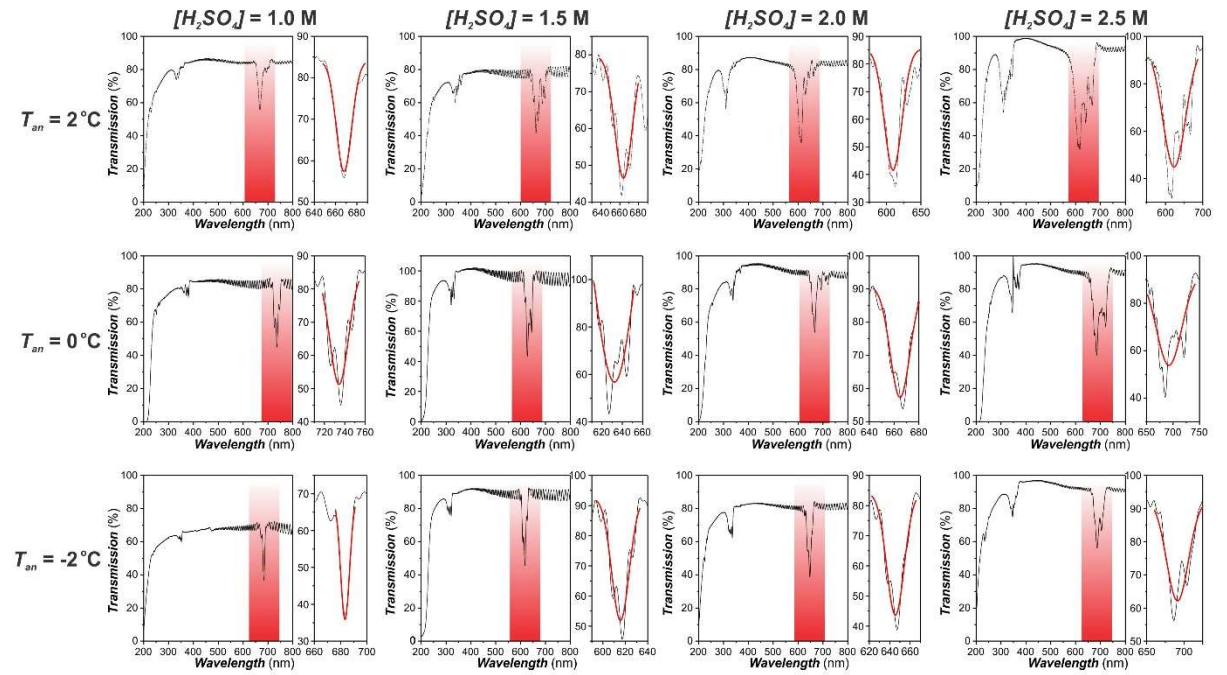


Fig. S3. Full transmission spectra and magnified views of the characteristic photonic stopband (PSB) of NAA-GIFs produced by SPA with varying $T_{an} = -2$ – 2°C and $[\text{H}_2\text{SO}_4] = 1.0$ – 2.5 M for $t_{an} = 15\text{ h}$.

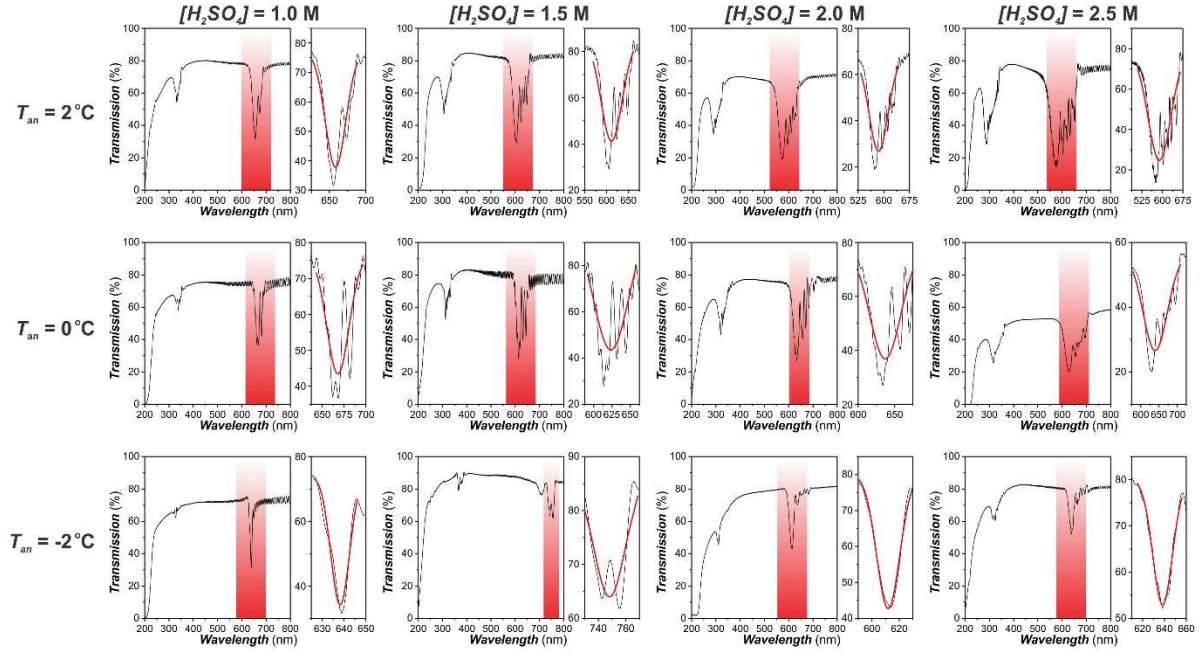


Fig. S4. Full transmission spectra and magnified views of the characteristic photonic stop band (PSB) of NAA-GIFs produced by SPA with varying $T_{an} = -2$ – 2°C and $[\text{H}_2\text{SO}_4] = 1.0$ – 2.5 M for $t_{an} = 20\text{ h}$.

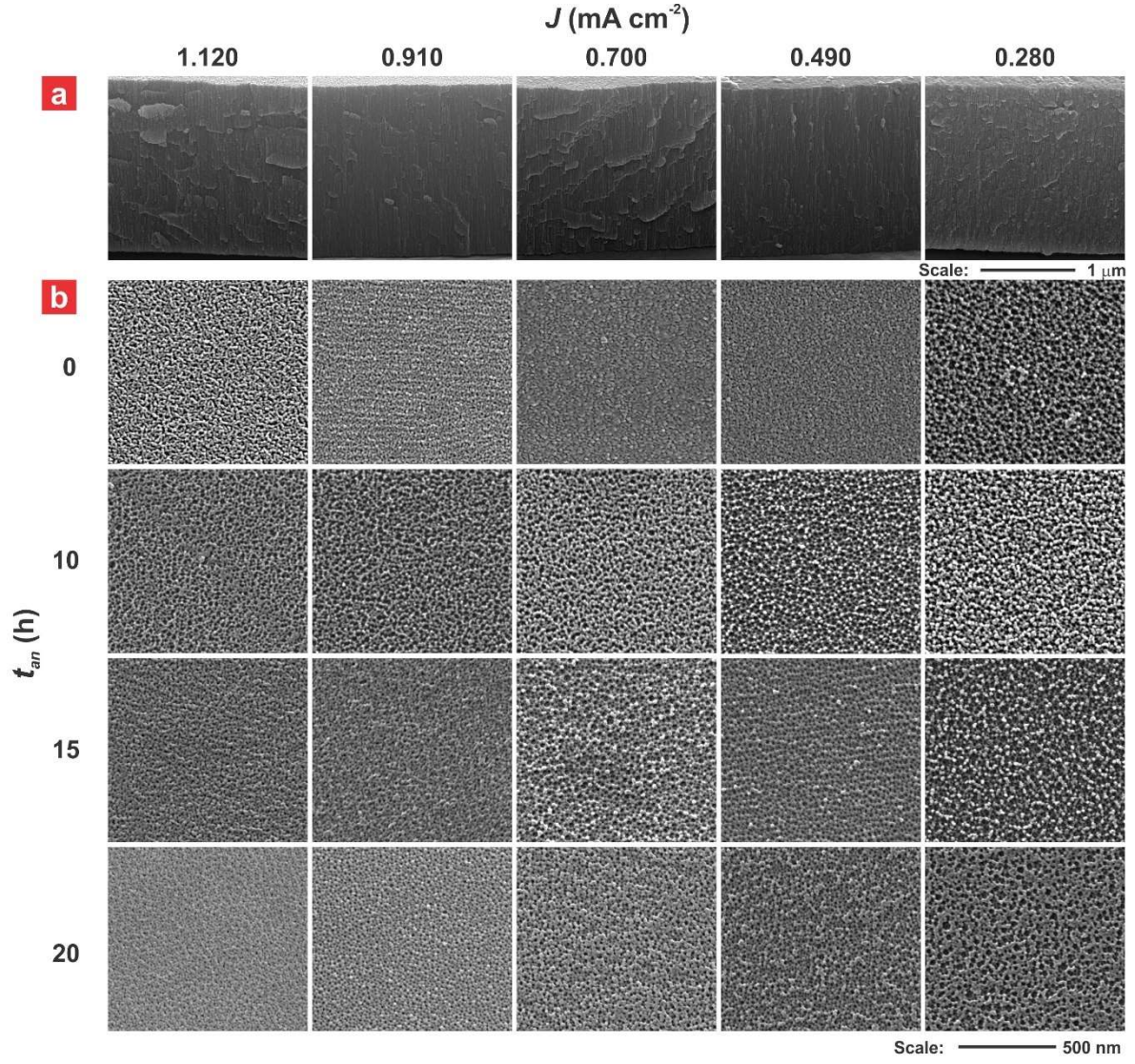


Fig. S5. SEM images of NAA films produced with varying anodization current density (J) and anodization time (t_{an}). (a) Cross-sectional view of NAA films showing the length of pore grown at different J (0.280–1.120 mA cm^{-2}) (scale bar = 1 μm) (b) Top view of NAA films produced as a function of J and t_{an} (0–20 h) (scale bar = 500 nm).

The ANOVA table (**Table 3**) was calculated using the equations outlined in **Table S1**, where *SS* is the sum of squares of the corresponding source, *DF* is the degree of freedom of such source, *MS* is the mean square of corresponding source, F_0 is the test statistic of that source, a, b and c are the total number of levels corresponding to t_{an} , T_{an} and $[H_2SO_4]$, respectively, and n is the total number of replications.

The hypotheses $H_0, H_1, H_2, H_3, H_4, H_5$ and H_6 were evaluated based on the comparison between F_0 value calculated from ANOVA table and the value of F-distribution for a significance level of 95% (i.e. 0.05) with the corresponding value of *DF* (Source) and *DF* (Error) (i.e. $F_{(0.05, DF (Source), DF (Error))}$). In this way, the tested null hypothesis (i.e. $H_0, H_1, H_2, H_3, H_4, H_5$ and H_6) associated with cases i–vii were rejected if:

- i) $H_0: F_{0-tan} \geq F_{(0.05, DF (tan), DF (Error))}$
- ii) $H_1: F_{0-Tan} \geq F_{(0.05, DF (Tan), DF (Error))}$
- iii) $H_2: F_{0-[H_2SO_4]} \geq F_{(0.05, DF ([H_2SO_4]), DF (Error))}$
- iv) $H_3: F_{0-tan.Tan} \geq F_{(0.05, DF (tan.Tan), DF (Error))}$
- v) $H_4: F_{0-tan.[H_2SO_4]} \geq F_{(0.05, DF (tan.[H_2SO_4]), DF (Error))}$
- vi) $H_5: F_{0-Tan.[H_2SO_4]} \geq F_{(0.05, DF (Tan.[H_2SO_4]), DF (Error))}$
- vii) $H_6: F_{0-tan.Tan.[H_2SO_4]} \geq F_{(0.05, DF (tan.Tan.[H_2SO_4]), DF (Error))}$

Considering three-factor analysis of variance model in general form:

$$y_{ijkl} = \mu + \alpha_i + \beta_j + \gamma_k + (\alpha\beta)_{ij} + (\alpha\gamma)_{ik} + (\beta\gamma)_{jk} + (\alpha\beta\gamma)_{ijk} + \epsilon_{ijkl} \quad \begin{cases} i = 1, 2, \dots, a \\ j = 1, 2, \dots, b \\ k = 1, 2, \dots, c \\ l = 1, 2, \dots, n \end{cases}$$

In this study, α , β and γ represent t_{an} , T_{an} , $[H_2SO_4]$, respectively.

Table S1. Equations of different parameters for ANOVA table.

Source	SS	DF	MS	F ₀
t_{an}	$SS_{t_{an}} = \frac{1}{bcn} \sum_{i=1}^a y_{i...}^2 - \frac{y_{...}^2}{abcn}$	$a - 1$	$MS_{t_{an}} = \frac{SS_{t_{an}}}{a - 1}$	$F_{0-t_{an}} = \frac{MS_{t_{an}}}{MS_E}$
T_{an}	$SS_{T_{an}} = \frac{1}{acn} \sum_{j=1}^b y_{.j..}^2 - \frac{y_{...}^2}{abcn}$	$b - 1$	$MS_{T_{an}} = \frac{SS_{T_{an}}}{b - 1}$	$F_{0-T_{an}} = \frac{MS_{T_{an}}}{MS_E}$
$[H_2SO_4]$	$SS_{[H_2SO_4]} = \frac{1}{abn} \sum_{k=1}^c y_{..k.}^2 - \frac{y_{...}^2}{abcn}$	$c - 1$	$MS_{[H_2SO_4]} = \frac{SS_{[H_2SO_4]}}{c - 1}$	$F_{0-[H_2SO_4]} = \frac{MS_{[H_2SO_4]}}{MS_E}$
$t_{an} \cdot T_{an}$	$SS_{t_{an} \cdot T_{an}}$ $= \frac{1}{cn} \sum_{i=1}^a \sum_{j=1}^b y_{ij...}^2 - \frac{y_{...}^2}{abcn} - SS_{t_{an}} - SS_{T_{an}}$ $= SS_{Subtotals(t_{an} \cdot T_{an})} - SS_{t_{an}} - SS_{T_{an}}$	$(a - 1)(b - 1)$	$MS_{t_{an} \cdot T_{an}} = \frac{SS_{t_{an} \cdot T_{an}}}{(a - 1)(b - 1)}$	$F_{0-t_{an} \cdot T_{an}} = \frac{MS_{t_{an} \cdot T_{an}}}{MS_E}$

$t_{an} \cdot [H_2SO_4]$	$SS_{t_{an} \cdot [H_2SO_4]}$ $= \frac{1}{bn} \sum_{i=1}^a \sum_{k=1}^c y_{i.k.}^2 - \frac{y_{...}^2}{abcn} - SS_{t_{an}} - SS_{[H_2SO_4]}$ $= SS_{Subtotals(t_{an} \cdot [H_2SO_4])} - SS_{t_{an}} - SS_{[H_2SO_4]}$	$(a-1)(c-1)$	$MS_{t_{an} \cdot [H_2SO_4]}$ $= \frac{SS_{t_{an} \cdot [H_2SO_4]}}{(a-1)(c-1)}$	$F_{0-t_{an} \cdot [H_2SO_4]}$ $= \frac{MS_{t_{an} \cdot [H_2SO_4]}}{MS_E}$
$T_{an} \cdot [H_2SO_4]$	$SS_{T_{an} \cdot [H_2SO_4]}$ $= \frac{1}{an} \sum_{j=1}^b \sum_{k=1}^c y_{j.k.}^2 - \frac{y_{...}^2}{abcn} - SS_{T_{an}} - SS_{[H_2SO_4]}$ $= SS_{Subtotals(T_{an} \cdot [H_2SO_4])} - SS_{T_{an}} - SS_{[H_2SO_4]}$	$(b-1)(c-1)$	$MS_{T_{an} \cdot [H_2SO_4]}$ $= \frac{SS_{T_{an} \cdot [H_2SO_4]}}{(b-1)(c-1)}$	$F_{0-T_{an} \cdot [H_2SO_4]}$ $= \frac{MS_{T_{an} \cdot [H_2SO_4]}}{MS_E}$
$t_{an} \cdot T_{an} \cdot [H_2SO_4]$	$SS_{t_{an} \cdot T_{an} \cdot [H_2SO_4]}$ $= \frac{1}{n} \sum_{i=1}^a \sum_{j=1}^b \sum_{k=1}^c y_{ijk.}^2 - \frac{y_{...}^2}{abcn} - SS_{t_{an}} - SS_{T_{an}}$ $- SS_{[H_2SO_4]} - SS_{t_{an} \cdot T_{an}} - SS_{t_{an} \cdot [H_2SO_4]}$ $- SS_{T_{an} \cdot [H_2SO_4]}$ $= SS_{Subtotals(t_{an} \cdot T_{an} \cdot [H_2SO_4])} - SS_{t_{an}} - SS_{T_{an}}$ $- SS_{[H_2SO_4]} - SS_{t_{an} \cdot T_{an}} - SS_{t_{an} \cdot [H_2SO_4]}$ $- SS_{T_{an} \cdot [H_2SO_4]}$	$(a-1)(b-1)(c-1)$	$MS_{t_{an} \cdot T_{an} \cdot [H_2SO_4]}$ $= \frac{SS_{t_{an} \cdot T_{an} \cdot [H_2SO_4]}}{(a-1)(b-1)(c-1)}$	$F_{0-t_{an} \cdot T_{an} \cdot [H_2SO_4]}$ $= \frac{MS_{t_{an} \cdot T_{an} \cdot [H_2SO_4]}}{MS_E}$
<i>Total</i>	$SS_T = \sum_{i=1}^a \sum_{j=1}^b \sum_{k=1}^c \sum_{l=1}^n y_{ijkl}^2 - \frac{y_{...}^2}{abcn}$	$abcn - 1$		
<i>Error</i>	$SS_E = SS_T - SS_{Subtotals(t_{an} \cdot T_{an} \cdot [H_2SO_4])}$	$abc(n-1)$	$MS_E = \frac{SS_E}{abc(n-1)}$	