Supporting Information for

Intensified Ozonolysis of Lignins in a Spray Reactor:

Insights into Product Yields and Lignin Structure

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The following contents are arranged in the order they appear in the manuscript.
Table S1: Comparison of continuous stirred tank and spray reactor operating conditions
Calc S1: Estimation of ozone permeation time in droplets4
Equation S1: Determination of liquid phase residence time in the spray reactor
Figure S1: Spray reactor temperature profiles during continuous ozonolysis of grass and
hardwood lignins6
Calc S2: Comparison of aldehyde production rates from CSTR and spray reactor7
Figure S2 and Table S2: Gas chromatograms showing aromatic aldehyde and acid concentrations
before ozonolysis and after ozonolysis following product fractionation
Figure S3: Full ¹ H NMR spectra of lignin before ozonolysis and after ozonolysis following product
workup9
Figure S4 and Table S4: 2D NMR of grass lignin before ozonolysis and after ozonolysis following
fractionation, and gravimetric analysis of product fractions10
Figure S5: Closeup ¹ H-NMR spectra of aromatic and aldehyde regions of lignin and product
fractions shown in Figure S311
Figure S6: ¹³ C NMR spectra of lignins before and after ozonolysis

Calc S3: Value of ozonolysis products in a cellulosic ethanol biorefinery context
Figure S7 and Table S4: 2D NMR of ozonized grass lignin with labeled peaks and integration
parameters14
Figure S8 and Table S5: GPC spectra and GC-FID chromatograms showing the effect of ozone
concentration on product yields from grass lignin15
Figure S9 and Table S6: GPC spectra and GC-FID yields showing the effect of liquid flow rate on
product yields from grass lignin16
Figure S10: SEM images of grass lignin before and after ozonation17
Table S7: Major GPC peaks before and after ozonation and their mass change
SI Methods: Chromatographic, Spectroscopic and Data Processing Methods
SI References

	CSTR	Operating Variable	Spray	
	70°C	Temperature (°C)	20°C	
	Ambient	Pressure	Ambient	
	2.5	[O ₃] _{in air} (vol. %)	2.5	
mm scale	0.71 - 14.2	Sol'n Flow Rate (mL/min)	50 - 125	μm scale
	1-5 minutes	O ₃ Contact Time	~10 seconds	
	Lignin in Acid	Bulk Phase	Ozone	
CSTR	Ozone	Dispersed Phase	Lignin Solution	Spray

Table S1: Comparison of continuous stirred tank and spray reactor operating conditions

Symbol	Value	Units	Description
$k_{ m b}$	1.38 x 10 ⁻²³	J/K	Boltzmann Constant
Т	293.15	К	Temperature
n	1.391 x 10 ⁻³	kg/ms	Dynamic viscosity of 3:1 v:v acetic: formic acid solution at
'1	1.001 × 10	16/113	20°C ¹
r _{oz}	1.40 x 10 ⁻¹⁰	m	Calculated radius of molecular ozone ²
D _{oz}	1.10 x 10 ⁻⁹	m²/s	Calculated diffusion constant for ozone
<i>r</i> d	3.5 x 10⁻⁵	m	Estimated droplet radius ³
tp	1.11	S	Calculated permeation time

Calc S1: Estimation of ozone permeation time in droplets

The diffusion coefficient for ozone in acid solution (D_{oz}) at room temperature is determined using the following Stokes-Einstein equation.²

$$D_{oz} = \frac{k_b * T}{6\pi * \eta * r_{oz}}$$

The various physical and transport parameters in the foregoing equation are tabulated in the Table above. Based on the calculated diffusivity of ozone in acetic acid (1.10 x 10^{-9} m²/s), it is estimated that for spherical liquid droplets with a radius of 35 µm, complete droplet permeation of the ozone will occur in approximately 1.11 seconds (t_p), based on the following equation.

$$t_p = \frac{r_d^2}{D_{oz}}$$

Equation S1: Determination of liquid phase residence time in the spray reactor

The spray reactor is operated such that there is no pooling (i.e., holdup) of the reaction mixture at the reactor bottom. Hence, the residence time is estimated based on the time a liquid stream enters the reactor via the spray and the time it exits the reactor as follows.

$$t_R = \frac{[(t_1 - t_2) + (t_3 - t_4)]}{2}$$

 $t_{R} = \text{residence time in reactor (s)}$ $t_{1} = \text{time at which liquid first exits reactor (s)}$ $t_{2} = \text{time at which liquid first enters reactor (s)}$ $t_{3} = \text{time at which liquid stream exiting reactor breaks (s)}$ $t_{4} = \text{time at which liquid stream stops spraying into reactor following cessation of spraying (s)}$



Figure S1: Spray reactor temperature profiles during continuous ozonolysis of grass and hardwood lignins. Temporal temperature profiles during the ozonolysis of G1 grass (top and bottom image) and H1 hardwood (middle image) lignins were measured with a 4-point thermocouple. In the 45 cm tall cylindrical reactor (Figure 2), the thermocouple (24 cm in length) has probes at the center of the reactor ("bottom probe"), 6 cm above that towards the gas stream inlet ("middle bottom"), a further 6 cm above that ("middle top probe") and at the top of the reactor next to the gas stream inlet (top probe). The volume in the legends represents the total amount of sprayed solution. After 1 minute, the variation in temperature between the four probes is less than \pm 0.1 °C. As shown in the adjoining table above, temporal vanillin yields [defined as mass of vanillin produced (estimated from GC-FID data)/mass of lignin fed*100] show that the vanillin yield reaches a steady state after approximately 2 minutes.

Calc S2: Comparison of aldehyde production rates from CSTR and spray reactor

Assuming (i) constant density (ρ) of the reaction mixture which is dominated by acetic acid (99 wt.%) (ii) negligible concentration of aldehydes in the feedstock, and (iii) fixed aldehydes yield (*Y*) from both CSTR and spray reactor, the production rate (*P* mol/min) of aldehydes can be calculated as follows:

$$P\left(\frac{mol}{\min}\right) = C\left(\frac{g_{lignin}}{g_{solution}}\right) \rho\left(\frac{g_{solution}}{mL_{solution}}\right) Q\left(\frac{mL_{solution}}{min}\right) Y\left(\frac{g_{aldehydes}}{g_{lignin}}\right) M\left(\frac{mol_{aldehydes}}{g_{aldehydes}}\right)$$

The range of values used in the CSTR and spray experiments are provided in the Table below.

Symbol	Value	Measure	Description
С	1.0	wt. % (g/g)	Feed concentration
ρ	1.05	g/mL	Density of acetic acid
0	0.71-14.2	nol (min	Range of flow rates for CSTR ⁷
ų	50 – 125	mL/min	Range of flow rates for spray reactor
Y	0.05	g/g	Aldehyde yields
			Average molar mass of a 3:1 w:w 4-
Μ	129.6	g/mol	hydroxybenzaldehyde (122.1 g/mol) and vanillin
			(152.1 g/mol) mixture

For the range of flow rates (*Q*) shown in the table above, the calculated production rates (*P*) for CSTR and spray reactor are shown in the following table. Clearly, the production rates in the spray reactor are between one to two orders of magnitude greater than in a CSTR.

Reactor	<i>P</i> (mol/min) corresponding to lowest flow rate used in the reactor	<i>P</i> (mol/min) corresponding to highest flow rate used in the reactor
CSTR	2.89 (10-6)	5.77 (10 ⁻⁵)
Spray	2.03 (10-4)	5.08 (10-4)



Figure S2: GC/FID chromatograms of lignin solutions before ozonolysis and after ozonolysis following product fractionation. Figure (A) shows byproducts vanillic acid (18.17 minutes) and 4-hydroxybenzoic acid (19.5 minutes) in low concentrations, while Figure (B) shows vanillin (24.6 minutes) and 4-hydroxybenzaldehyde (31.3 minutes) as major products. Reaction run at 20°C with 2.5 mol. % ozone in air flowing at 180 std L/h and 1.0 wt. % lignin feed solution in acetic acid flowing at 75 mL/min.

The quantitative aldehyde and acid yields obtained from the GC/FID chromatograms above are shown in the following table.

Table S2: Aldehyde and acid yields from G1 lignin before ozonolysis and after ozonolysi	S
following fractionation.	

Component	Vanillic Acid	4HBA	Vanillin	4HB	Total Aromatics
component	wt. %				
Unreacted Lignin	0.16 ± 0.01	0.07 ± 0.02	0.16 ± 0.04	0.06 ± 0.02	0.45 ± 0.05
Ozonized Lignin	0.07 ± 0.02	0.10 ± 0.05	1.1 ± 0.1	4.0 ± 0.1	5.2 ± 0.1
LMW Extract	0.03 ± 0.01	0.06 ± 0.05	0.73 ± 0.02	3.9 ± 0.1	4.7 ± 0.1
HWM Solids	0.10 ± 0.05	0.09 ± 0.02	0.21 ± 0.03	0.12 ± 0.02	0.57 ± 0.06



Figure S3: Full ¹H-NMR of Lignins before ozonolysis and after ozonolysis following product workup (Experimental conditions are identical to those shown in Figure S2 caption).



Figure S4: ¹H (f2) and ¹³C (f1) 2D-HSQC NMR analyses of grass lignin (G1) before ozonolysis and after ozonolysis following product workup corresponding to samples shown in Figure S3.

Table S3: Effect of ozone concentration on the yields of low molecular weight (LMW) and high molecular weight (HMW) fractions along with mass balance closure (Experimental conditions are identical to those shown in Figure S2 caption).

[O₃] in Air (Mol. %)	LMW Extract (wt. %)	HMW Solids Fraction (wt. %)	Mass Balance Closure (%)
2.5	37 ± 1	59 ± 1	96 ± 1
5.0	45 ± 1	48 ± 1	93 ± 1
7.5	53 ± 1	38 ± 1	91 ± 1

Here, low molecular weight (LMW) fraction refers to the extracted fraction with peaks between ~150 Da and 22 kDa.



Figure S5: Closeup ¹H-NMR spectra of aromatic and aldehyde regions of lignin and product fractions shown in Figure S3.



Figure S6: DEPT ¹³C-NMR of lignins before ozonolysis and after ozonolysis following product workup (Experimental conditions are identical to those shown in Figure S2 caption).

SI Calc 3: Potential value of the aromatic aldehydes relative to lignocellulosic ethanol

It is assumed that the lignin content generated by one dry metric ton of corn stover is 18.5%.⁴ Based on our experimental findings, the aromatic aldehydes (vanillin and 4-hydroxybenzaldehyde) recovered from the pendant aromatic groups constitute approximately 5 wt. % of the lignin content. Further, the ethanol production per dry metric ton of corn stover is reported to range from 47 to 76 gallons.⁵ If one assumes that the average cost of the aromatic aldehydes is 12 US \$/kg,⁶ then the potential additional value created by these products per gallon of ethanol produced is estimated as follows:

5 kg aldehydes	185 kg lignin	1000 kg corn stover	12 US \$	2.56 US \$
100 kg lignin	× 1000 kg corn stover	× 76 gal.ethanol	× 1 kg aldehyde	=



Figure S7: Labeled ¹H (f2) and ¹³C (f1) HSQC NMR peaks of ozonized grass lignin (G1) from Figure S4. Relevant parameters are given in Table S4 below.

Peak #	f2 (¹H) ppm	f1 (¹³ C) ppm	Width	Height	Normalized Peak Intensities	Absolute Peak Intensities
1	7.75	132.48	68.36	462.28	2.00	729.65
2	7.51	130.43	58.59	317.82	0.38	139.47
3	7.42	126.43	19.53	231.14	0.09	31.19
4	7.38	111.04	19.53	288.92	0.12	44.76
5	7.14	128.84	115.87	288.92	0.51	185.17
6	6.95	116.06	78.12	491.17	2.56	933.45
7	6.94	111.86	53.18	490.87	0.34	123.75
8	6.74	115.75	126.95	462.28	2.49	908.38
9	6.56	115.75	58.59	462.28	1.21	439.76

Table 34. Integration parameters and uata for Figure 37 noni 2D Nivik of Ozonizeu grass lightin



Figure S8: Effect of ozone concentration on molecular weight distribution of product mixture obtained from G1 lignin (Other experimental conditions are identical to those shown in Figure S2 caption).

Table S5: Effect of ozone concentration on aromatic yields from G1 Lignin (Other experimental conditions are identical to those shown in Figure S2 caption)

Mol. % O₃	Vanillic Acid	4HBA	Vanillin	4HB	Total
2.5	0.13 ± 0.02	0.15 ± 0.02	0.73 ± 0.05	2.7 ± 0.1	3.7 ± 0.1
5.0	0.12 ± 0.04	0.18 ± 0.03	1.1 ± 0.1	4.4 ± 0.1	5.7 ± 0.1
7.5	0.12 ± 0.03	0.21 ± 0.06	0.80 ± 0.02	3.7 ± 0.1	4.9 ± 0.1



Figure S9: Effect of feed flow rate on GPC profiles of product mixtures from G1 lignin following ozonolysis (Other experimental conditions are identical to those shown in Figure S2 caption).

Table S6: Effect of feed flow rate on aromatic product yields (wt.%) for G1 lignin following ozonolysis (Other experimental conditions are identical to those shown in Figure S2 caption).

Flow Rate	[Vanillic Acid]	[4HBA]	[Vanillin]	[4HB]	Total	Residence Time*
(mL/min)	(wt. %)	(wt. %)	(wt. %)	(wt. %)	(wt. %)	seconds
50	0.10 ± 0.03	0.16 ± 0.02	0.83 ± 0.03	4.56 ± 0.1	5.7 ± 0.1	9.2 ± 0.2
75	0.11 ± 0.02	0.15 ± 0.04	0.83 ± 0.01	4.40 ± 0.2	5.5 ± 0.1	8.3 ± 0.3
100	0.11 ± 0.06	0.14 ± 0.03	0.80 ± 0.01	4.15 ± 0.1	5.2 ± 0.1	7.9 ± 0.2
125	0.11 ± 0.04	0.13 ± 0.04	0.77 ± 0.03	3.80 ± 0.1	4.8 ± 0.1	7.6 ± 0.4

*see Equation S1 for definition



Table S7: Macromolecular changes in molar mass from GPC spectra

(d)	$mass_{unreacted} - mass_{ozonized}$	$\frac{1}{2} * 100 - 1 mass (%)$
	$mass_{unreacted}$	$-*100 - \Delta mass (%)$



Figure S10: Scanning Electron Micrographs of 1.0 wt. % G2 grass lignin before (top) and after (bottom) ozonolysis at the nanometer (left) and micron (right) scale highlighting the globular modular components of lignin. Experimental conditions are identical to those in Figure S2 caption.

SI Methods

Gas Chromatography

The starting materials and recovered product solutions were analyzed by GC-FID by diluting 300 μ L of recovered product solution with 1 mL of methanol. Purchased vanillin, 4-hydroxybenzaldehyde, vanillic acid, and 4-hydroxybenzoic acid were used as standards for the chromatographic analysis. The GC method used an HP-INNOWAX column on an Agilent 7890A GC and uses a carrier gas (He) flow of 1 std. cm³/min, an inlet temperature of 250 °C, and an injection volume of 1 μ L. The oven temperature was initially held at 40 °C for 5 min, then ramped at 10 °C per minute to 220 °C and held at this temperature for a further 20 min. Masses were scanned from 20 to 500 Da. Products were identified by comparison of retention times with known compounds and from their mass spectrometry fragmentation patterns. Quantification was performed using GC-FID analysis with calibration curves generated from known samples (0.01 – 5.0 wt. % solutions) employing previously reported methods.⁷ After subtracting the solvent blank, the areas of the GC-FID peaks (at ~24.7 and ~31.5 minutes for aldehydes: vanillin and 4HB respectively, and ~18.1 and 19.5 minutes for vanillic and 4-hydroxybenzoic acid respectively) were integrated in Plot2, and converted to mass fractions based on calibration curves.

Size Exclusion Chromatography Gel Permeation Chromatography

For GPC analysis, the solvent is evaporated from samples and replaced with dimethylformamide (1.0 mL). GPC was performed on an Agilent 1260 Infiniti GPC system fitted with an Agilent refractive index detector. Two columns, a 300 mm Polargel-M followed by a 300 mm Polargel-L, were used in series at 40 °C. The samples were eluted with dimethylformamide at a flow rate of 1.0 mL/min. Poly(methyl methacrylate) standards were used for calibration. Gel permeation chromatograms are calibrated against a polymethylmethacrylate standard before analysis in Plot2 for peak locations.

¹H-¹³C HSQC Nuclear Magnetic Resonance Spectroscopy

NMR spectra were recorded using a Bruker AVIII 500 MHz spectrometer with a multinuclear BFFO cryoprobe. Approximately 100 mg of lignin, ozonized lignin product, or model compound was dissolved in 0.7 mL dimethylsulfoxide-d₆. For the ¹³C NMR analysis, a power-gated decoupling sequence was used to screen out the Nuclear Overhauser Effect (NOE) with the following parameters: 150 ms relaxation delay, 64 K data points, and 1024 scans. 2D ¹H-¹³C HSQC NMR spectra were obtained using the hsqcedetgpsisp2.2 HSQC program. The central solvent peak was used as an internal chemical shift reference point ($\delta C/\delta H$ 39.5/2.49). The spectral widths were 20 ppm and 234 ppm for ¹H and ¹³C dimensions, respectively, along with the following parameters: 2 second relaxation delay, 8 scans, and 256 time increments were recorded in the ¹³C dimension. NMR spectra (.fid/.ser files) were analyzed in MestreNova following automated integration of 1D and 2D spectra.

Scanning Electron Microscopy

Lignin and reaction products were dried directly placed on the head of an SEM pin. The samples were sputter coated with 5 nm of gold before being imaged with a FEI Versa 3D Dual Beam machine, at a voltage of 5 kV and a spot size of 4.5. Images were processed in ImageJ to determine average particle sizes.

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