Passive droplet generation in aqueous two-phase systems with a variable-width microchannel

Daeho Choi[†][†]^{*}, Eunjeong Lee[†]^{*}, Sung-Jin Kim[¶], and Minsub Han^{†*}

- † Mechanical Engineering, Incheon National University, Incheon, 22012, Korea
- ¶ Mechanical Engineering, Konkuk University, 05029, Seoul, Korea
- ‡ Department of Research and Development, Hanil Knuckle Press Co. Ltd., Incheon, Korea

***** equal contributions



[Fig.SI-1] The concentration case of DEX/PEG= 6.4/5 (% w/v). The triangle symbol stands for DEX-inlet width of 2.89 ± 0.08 , the circular symbol for 4.74 ± 0.03 , and the rectangular symbol for $10.36 \pm 0.09 \ \mu m$. The open symbol stands for the droplet-generation regime, the half-filled symbol for the transition regime, the filled symbol for the stable jet regime. The solid line stands for the width of 2.89 ± 0.08 , the dashed line for 4.74 ± 0.03 , and the dotted line for $10.36 \pm 0.09 \ \mu m$.



[Fig.SI-2] The concentration case of DEX/PEG= 16/10 (% w/v). The triangle symbol stands for DEXinlet width of 2.89 ± 0.08 , the circular symbol for 4.74 ± 0.03 , and the rectangular symbol for $10.36 \pm 0.09 \ \mu m$. The open symbol stands for the droplet-generation regime, the half-filled symbol for the transition regime, the filled symbol for the stable jet regime. The solid line stands for the width of 2.89 ± 0.08 , the dashed line for 4.74 ± 0.03 , and the dotted line for $10.36 \pm 0.09 \ \mu m$.



[Fig.SI-3] The breakup time error(%) of theoretical prediction (Eq.(3)) from the measured data. X is the ratio of the thread diameter and channel height.

(SI-2)

[Derivation of Eq. (1)]

An incompressible, laminar flow in a cylindrical pipe is considered that is fully-developed, unidirectional, and with no applied body force. The Navier-Stokes equation then gives

$$0 = -\frac{dP}{dx} + \mu \frac{1}{r dr} \left(r \frac{dv}{dr} \right)$$
(SI-1)

We first consider the inlet channel of the DEX-rich phase the radius of which is R_D . The velocity profile is then obtained as

$$v_{D}^{i} = -\frac{1}{4\mu dx} (R_{D}^{2} - r^{2})$$

$$Q_{D} = \int_{0}^{R_{D}} 2\pi r dr v_{D}^{i}$$
and
. So,
$$Q_{D} = -\frac{1}{8\mu dx} R_{D}^{4}$$
(S)

Here we put the pressure gradient as

 $\frac{dP}{dx} = \frac{P_j - P_D}{l_D}$ And get

$$Q_{D} = -\frac{\pi P_{j} - P_{D}}{8\mu l_{D}} R_{D}^{4}$$
(SI-3)

Where the subscript j stands for the location where the DEX and PEG flows joins. We then consider the flow in the main channel where the DEX-rich phase occupies the inner region in the pipe, $0 \le r < r_D$, and the PEG-rich phase occupies the outer region, $r_D < r \le R$. After integrating Eq. (SI-1), the boundary condition determine that, at $r = r_D$,

$$\frac{1}{4\mu_D dx}r_D^2 + B_D = \frac{1}{4\mu_p dx}r_D^2 + B_P$$

and, at r = R,

$$0 = \frac{1}{4\mu_p dx} R^2 + B_p$$

So that we get the velocity profiles as

$$v_{P} = \frac{1}{4\mu_{p}dx}r^{2} - \frac{1}{4\mu_{p}dx}R^{2}$$

and
$$v_{D} = \frac{1}{4\mu_{D}dx}r^{2} + \frac{1}{4}\left(\frac{1}{\mu_{p}} - \frac{1}{\mu_{D}}\right)\frac{dP}{dx}r_{D}^{2} - \frac{1}{4\mu_{p}dx}R^{2}$$

By integration, we get the volume flow rates, $R_{\rm p}$

$$Q_{P} = \int_{r_{D}}^{r} 2\pi r dr v_{P}$$

$$Q_{P} = -\frac{\pi}{8\mu_{p} dx} (r_{D}^{2} - R^{2})^{2}$$

$$Q_{D} = \int_{0}^{r_{D}} 2\pi r dr v_{D}$$

$$\therefore Q_{D} = -\frac{\pi}{8\mu_{D} dx} r_{D}^{4} - \frac{\pi}{4\mu_{D} dx} r_{D}^{2} (R^{2} - r_{D}^{2}) \quad ..(3)$$

Applying $\frac{dP}{dx} = \frac{P_{out} - P_j}{l_D}$ to Eq. (SI-4), we get

$$Q_P = -\frac{\pi}{8\mu_p} \frac{P_{out} - P_j}{l_D} (r_D^2 - R^2)^2$$

And, therefore,

$$P_{j} = Q_{p} \frac{8\mu_{p}}{\pi} \frac{l_{D}}{(r_{D}^{2} - R^{2})^{2}} + P_{out}$$
(SI-5)

Putting Eq.(SI-5) into Eq.(SI-3), we get Eq.(1):

$$Q_{D} = \frac{\pi R_{D}^{4}}{8\mu_{D} l_{D}} (P_{D} - P_{out}) - Q_{P} \frac{\mu_{P}}{\mu_{D}} \left(\frac{l}{l_{D}}\right) \frac{R_{D}^{4}}{(r_{D}^{2} - R^{2})^{2}}$$
(SI-6)

We can also start out with a geometry with rectangular channel with a high aspect ratio such as width, 2w, height, 2h, and $w \gg h$. Following similar steps in the previous derivation, we can obtain:

$$Q_{D} = \frac{4}{3} (P_{D} - P_{out}) / \mu_{D} \left(\frac{l}{wh^{3}} + \frac{l_{D}}{w_{D}h_{D}^{3}} \right) - Q_{P} \frac{\mu_{P}}{\mu_{D}} \frac{1}{1 + \frac{l_{D} wh^{3}}{l_{w_{D}}h_{D}^{3}}}$$
(SI-7)

(SI-4)