

Supplementary Information

Balanced strain-dependent carrier dynamics in flexible organic-inorganic hybrid perovskites

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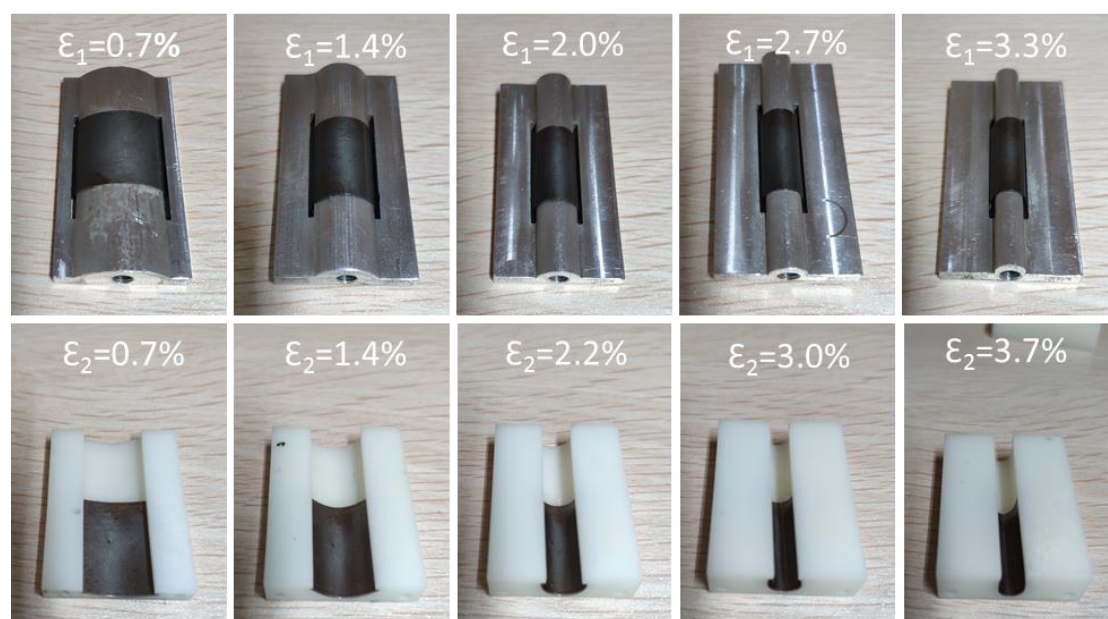
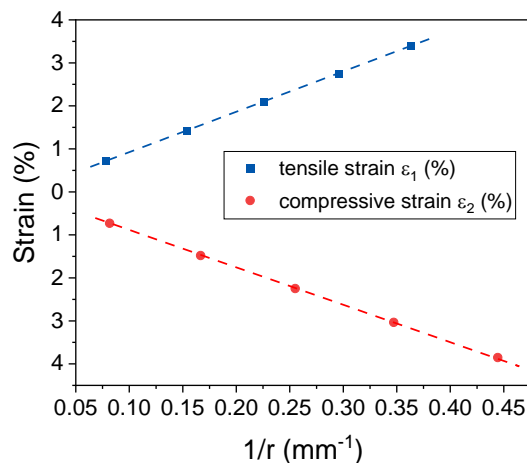


Fig. S1 Images of convex and concave bending molds (with perovskite film attached).

Table S1. The tensile (ε_1) or compressive (ε_2) strains applied and corresponding bending radius.

Convex bending	Bending radius r (mm)	12.75	6.50	4.42	3.38	2.75
	Tensile strain ε_1 (%)	0.7	1.4	2.0	2.7	3.3
Concave bending	Bending radius r (mm)	12.25	6.00	3.92	2.88	2.25
	Compressive strain ε_2 (%)	0.7	1.4	2.2	3.0	3.7

**Figure S2.** The relation between applied strain versus the reciprocal bending radius shown in table S1 (the dash lines are for eye guidance).**Table S2.** Fitting parameters of time-resolve PL kinetics of MAPbI₃ film under different strain.

Strain	τ_1 (ns)	A_1	τ_2 (ns)	A_2	τ_3 (ns)	A_3	τ_{average} (ns)
$\varepsilon_1=0\%$	1.71 ± 0.01	0.80	13.7 ± 0.2	0.17	199 ± 3	0.03	9.32
$\varepsilon_1=0.7\%$	1.64 ± 0.01	0.79	13.2 ± 0.2	0.18	177 ± 3	0.03	9.10
$\varepsilon_1=1.4\%$	1.78 ± 0.01	0.74	15.6 ± 0.2	0.21	195 ± 2	0.05	13.54
$\varepsilon_1=2.0\%$	1.92 ± 0.02	0.74	16.8 ± 0.2	0.22	172 ± 3	0.04	12.59
$\varepsilon_1=2.7\%$	2.12 ± 0.02	0.71	17.2 ± 0.2	0.24	180 ± 2	0.05	14.84
$\varepsilon_1=3.3\%$	2.47 ± 0.02	0.62	20.9 ± 0.2	0.30	164 ± 2	0.07	19.83

$\varepsilon_2=0.7\%$	1.03±0.01	0.80	11.7±0.4	0.14	141±2	0.07	12.14
$\varepsilon_2=1.4\%$	1.20±0.02	0.81	11.3±0.4	0.14	141±3	0.06	10.67
$\varepsilon_2=2.2\%$	1.14±0.01	0.84	10.5±0.3	0.13	140±4	0.04	7.27
$\varepsilon_2=3.0\%$	1.13±0.01	0.84	10.1±0.3	0.13	145±4	0.03	6.85
$\varepsilon_2=3.7\%$	1.24±0.01	0.84	10.3±0.3	0.14	137±6	0.02	5.63

The time-resolved PL kinetics were fitted using three-exponential decay equation (S1):

$$I(t) = B + A_1 \times e^{\frac{-t}{\tau_1}} + A_2 \times e^{\frac{-t}{\tau_2}} + A_3 \times e^{\frac{-t}{\tau_3}} \quad (S1)$$

where A_1, A_2, A_3 are the amplitudes of each decay component, and τ_1, τ_2, τ_3 are the decay time of each decay component. B is the background constant. The average lifetime $\tau_{average}$ is determined by the following equation:

$$\tau_{average} = \frac{A_1\tau_1 + A_2\tau_2 + A_3\tau_3}{A_1 + A_2 + A_3} \quad (S2)$$

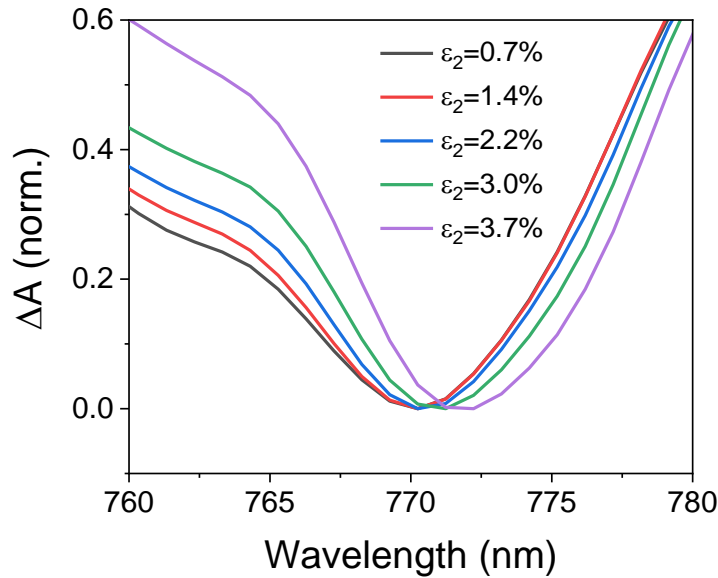


Fig. S3 Partial enlargement of transient absorption spectra of MAPbI₃ film at 9 ps after excitation ($\lambda_{pump}=650$ nm) under different compressive strains via concave bending.

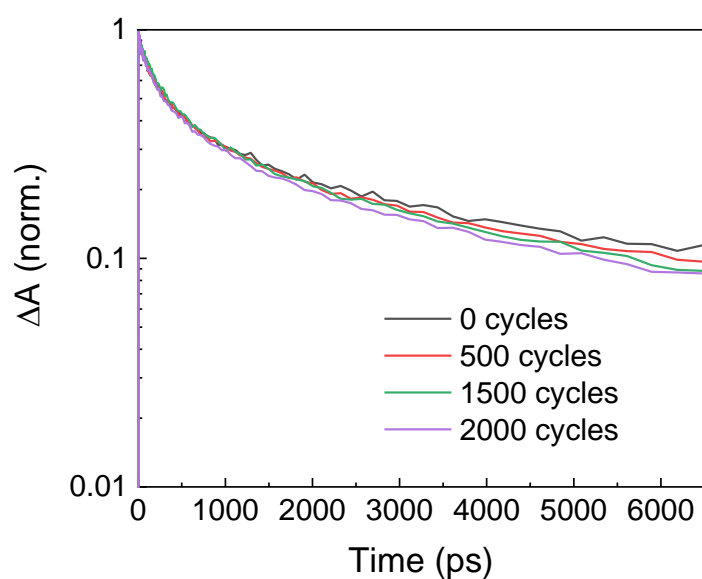


Fig. S4 Carrier dynamics in a flexible MAPbI₃ film versus bending cycles under convex bending radius of 1.1 mm.

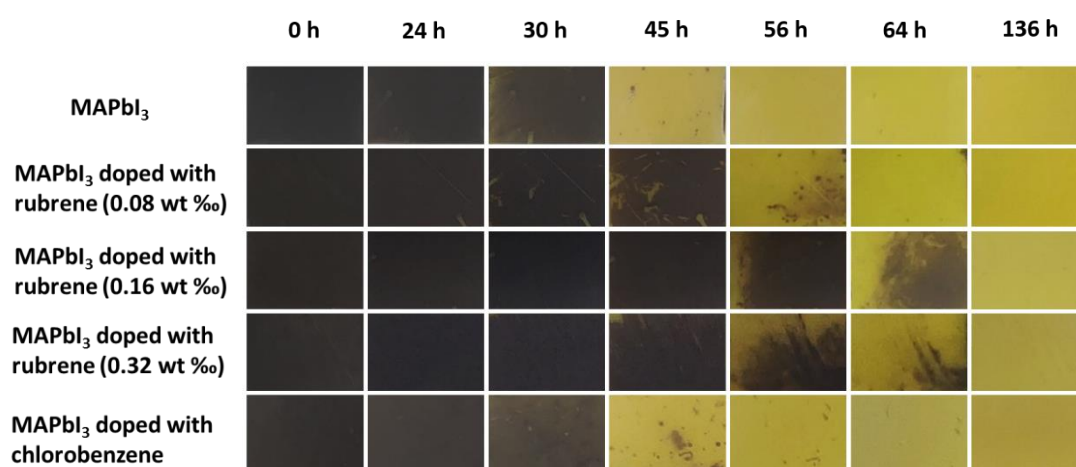


Fig. S5 Stabilities of MAPbI₃ film doped with rubrene at various concentrations.

The stabilities of rubrene doped MAPbI₃ films with various doping concentrations are shown in Figure S5. To investigate the influence of chlorobenzene solvent, the stability of MAPbI₃ film with adding chlorobenzene into the precursor solution was also recorded which shows no noticeable impact on the perovskite film stability.

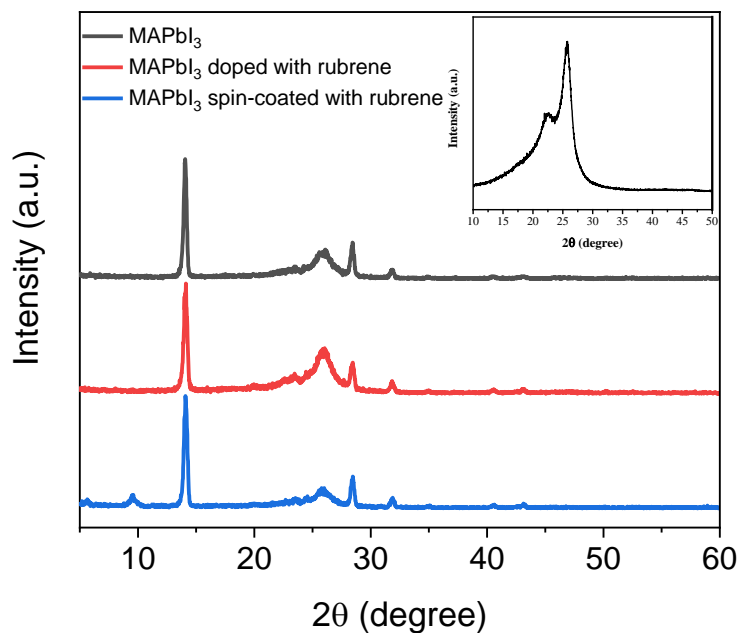


Fig. S6 GIXRD diffraction patterns of pristine MAPbI₃, MAPbI₃ doped with rubrene, and MAPbI₃ spin-coated with rubrene on PET films. The inset shows the GIXRD diffraction pattern of PET substrate.

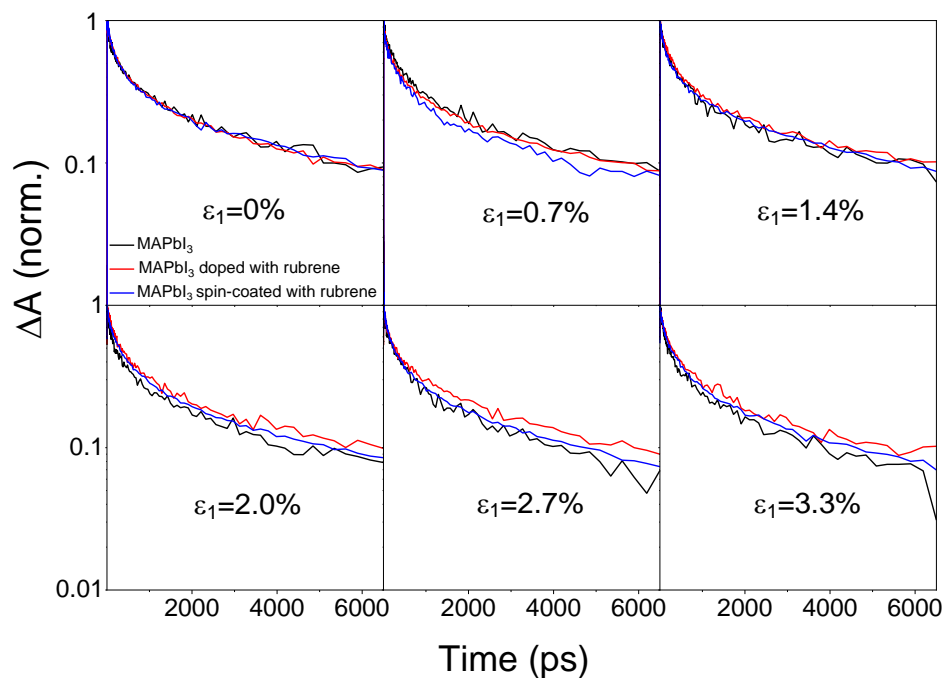


Fig. S7 TA kinetics at 760 nm of pristine MAPbI₃ (black), MAPbI₃ doped with rubrene (red), and MAPbI₃ spin-coated with rubrene (blue) films under various tensile strains.