# Trinuclear First Row Transition Metal Complexes of a Hexapyridyl, Trialkoxy 1,3,5-Triarylbenzene Ligand

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#### **Experimental Details**

**General Considerations**. Reactions performed under inert atmosphere were carried out in a glovebox under a nitrogen atmosphere. Anhydrous THF was purchased from Aldrich in 18 L Pure-Pac<sup>TM</sup> containers. Anhydrous dichloromethane, acetonitrile, diethyl ether, and THF were purified by sparging with nitrogen for 15 minutes and then passing under nitrogen pressure through a column of activated A2 alumina (Zapp's). All non-dried solvents used were reagent grade or better. All NMR solvents were purchased from Cambridge Isotope Laboratories, Inc. CDCl<sub>3</sub>, CD<sub>2</sub>Cl<sub>2</sub>, and CD<sub>3</sub>CN were dried over calcium hydride, then degassed by three freeze-pump-thaw cycles and vacuum-transferred prior to use. <sup>1</sup>H NMR and <sup>13</sup>C NMR spectra were recorded on a Varian 300 MHz instrument or a Varian 500 MHz instrument, with shifts reported relative to the residual solvent peak. Elemental analyses were performed by Midwest Microlab, LLC, Indianapolis, IN. High resolution mass spectrometry data (HRMS) were obtained at the California Institute of Technology Mass Spectrometry Facility. UV-Vis spectra were taken on a Varian Cary 50 spectrophotometer using a quartz crystal cell.

Unless indicated otherwise, all commercial chemicals were used as received. Di(2pyridyl)ketone was purchased from Aldrich or from Frontier Chemicals. 1,3,5-tris(2bromophenyl)benzene<sup>1</sup> was prepared according to literature procedures.



Synthesis of 1, 3, 5-Tris(2-di(2'-pyridyl)hydroxymethylphenyl)benzene (H<sub>3</sub>L). In the glovebox, a Schlenk flask equipped with a stir bar was charged with 1,3,5-tris(2-bromophenyl)benzene (4.0 g, 7.37 mmol) and diethyl ether (80 mL). On the Schlenk line, the suspension was cooled to -78 °C, and *t*-BuLi (1.61 M, 27.9 mL, 44.9 mmol) was added slowly via syringe. The mixture was stirred for 15 min. at -78 °C, and a solution of di(2-pyridyl)ketone (4.21 g, 22.8 mmol) in diethyl ether (30 mL) was added slowly via cannula transfer. The reaction mixture was allowed to warm to room temperature and stirred for 8 h under nitrogen. The mixture was quenched with methanol (30 mL), and the orange solution was diluted with water and extracted with dichloromethane. The organic layer was washed with brine and dried over magnesium sulfate, then filtered. The solvent was removed under reduced pressure, and the

yellow residue was recrystallized from acetone/dichloromethane to yield the product as a white solid (2.65 g, 42%). <sup>1</sup>H NMR (300 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  8.41 (d, *J* = 6 Hz, 6 H, *a*), 7.66 (bs, 6 H, *c*), 7.55 (bs, 6 H, *d*), 7.25 (t, *J* = 7.5 Hz, 3 H, *f*), 7.13 (t, *J* = 7.5 Hz, 3 H, *g*), 7.02 (bs, 6 H, *b*), 6.81 (bs, 3 H, *e*), 6.74 (*J* = 6 Hz, 3 H, *h*), 6.37 (bs, 3 H, O<u>H</u>), 6.14 (bs, 3 H, *j*). <sup>13</sup>C NMR (CDCl<sub>3</sub>):  $\delta$  164.0, 147.2, 144.0, 143.5, 139.5, 136.2, 133.2, 129.2, 126.6, 126.1, 123.7, 121.9, 81.9. IR (CH<sub>2</sub>Cl<sub>2</sub>): 3330, 1751 cm<sup>-1</sup>. HRMS (FAB+): calcd. for C<sub>57</sub>H<sub>43</sub>N<sub>6</sub>O<sub>3</sub>: 859.3397; found: 859.3436 [M+H].

Synthesis of LMn<sub>3</sub>(OAc)<sub>3</sub>. Under an N<sub>2</sub> atmosphere, H<sub>3</sub>L (335.5 mg, 0.39 mmol) and Mn(OAc)<sub>2</sub> (202.8 mg, 1.17 mmol) were combined in a scintillation vial equipped with a stirbar, to which a 1:1 CH<sub>3</sub>CN/H<sub>2</sub>O solution was added. To the stirring tan suspension was added a 1 M solution of KOH in H<sub>2</sub>O. After the solution became yellow and homogeneous, the solvent was removed *in vacuo*. The residue was partially dissolved in CHCl<sub>3</sub> then dried under vacuum twice to ensure evaporation of CH<sub>3</sub>CN and H<sub>2</sub>O. The residue was triturated in CHCl<sub>3</sub> and a white solid was filtered from the yellow solution. Yellow crystals were grown by vapor diffusion of diethyl ether into a CHCl<sub>3</sub> solution of LMn<sub>3</sub>(OAc)<sub>3</sub> (247 mg, 53%). <sup>1</sup>H NMR (300 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  41.76 ( $\Delta v_{1/2} = 2000$  Hz), 11.15 ( $\Delta v_{1/2} = 1230$  Hz), 4.49 ( $\Delta v_{1/2} = 850$  Hz), -10.56 ( $\Delta v_{1/2} = 1530$  Hz). UV-Vis (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  ( $\epsilon$ )): 256 (47,200 M<sup>-1</sup> cm<sup>-1</sup>); 350 (585 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for C<sub>63</sub>H<sub>48</sub>Mn<sub>3</sub>N<sub>6</sub>O<sub>9</sub>: C, 63.17; H, 4.04; N, 7.02. Found: C, 62.96; H, 4.20; N, 6.77.

Synthesis of LFe<sub>3</sub>(OAc)<sub>3</sub>. In a glovebox, a scintillation vial equipped with a stir bar was charged with a suspension of Fe(OAc)<sub>2</sub> (0.061 g, 0.349 mmol) in CH<sub>2</sub>Cl<sub>2</sub> (2 mL). Triethylamine (0.052 mL, 0.407 mmol) was added via syringe, and then a solution of H<sub>3</sub>L (0.100 g, 0.116 mmol) in CH<sub>2</sub>Cl<sub>2</sub> (3 mL) was added. The pale yellow mixture was stirred at room temperature and slowly darkened over 20 h to form a homogeneous orange solution. The solvent was removed under reduced pressure and the residue was recrystallized twice from CH<sub>2</sub>Cl<sub>2</sub>/diethyl ether to yield the product as orange-red crystals (0.087 g, 62%). <sup>1</sup>H NMR (300 MHz, CD<sub>2</sub>Cl<sub>2</sub>, 25 °C):  $\delta$  109.04 (3 H), 69.06 (3 H), 65.32 (6 H), 43.77 (3 H), 38.34 (9 H), 37.96 (3 H), 28.40 (3 H), 13.43 (3 H), 12.93 (3 H), 9.47 (3 H), 8.08 (3 H), 3.49 (3 H), -4.13 (3 H). UV-Vis (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  (ε)): 254 (50,500 M<sup>-1</sup> cm<sup>-1</sup>); 443 (2610 M<sup>-1</sup> cm<sup>-1</sup>); 793 (83 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for C<sub>63</sub>H<sub>48</sub>Fe<sub>3</sub>N<sub>6</sub>O<sub>9</sub>: C, 63.02; H, 4.03; N, 7.00. Found: C, 62.91; H, 3.97; N, 6.90.

Synthesis of LCo<sub>3</sub>(OAc)<sub>3</sub>. H<sub>3</sub>L (310.5 mg, 0.36 mmol) was suspended in a 1:1 solution of CH<sub>3</sub>CN and H<sub>2</sub>O (~6 mL). Co(OAc)<sub>2</sub>•4H<sub>2</sub>O (270.1 mg, 1.08 mmol) was added as a crystalline solid to the stirring suspension. To this mixture, a 1 M KOH solution in H<sub>2</sub>O (1.1 mL) was added dropwise. The reaction was stirred at room temperature until it became a homogenous solution (12 h), then the solvent was removed *in vacuo*. The red-purple solid was extracted with CH<sub>2</sub>Cl<sub>2</sub>, and the resulting red solution was dried *in vacuo* for 8 hrs. The resulting red-purple powder was dissolved in CHCl<sub>3</sub> and diethyl ether was allowed to diffuse into the solution slowly as a vapor. White precipitate collected at the bottom of the vial and the red homogeneous solution was decanted off. This precipitation procedure was repeated until no more white precipitate appeared and the red crystalline clusters of LCo<sub>3</sub>(OAc)<sub>3</sub> were collected (250 mg, 57%). <sup>1</sup>H NMR (300 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  128.16 (3 H), 89.12 (3 H), 65.30 (3 H), 57.02 (3 H), 36.52 (3 H), 27.29 (3 H). 16.67 (3 H), 14.72 (9 H), 10.17 (3 H), 8.99(3 H), 6.06 (3 H), 1.01 (3 H), -0.42 (3 H), -14.24 (3H). UV-Vis: (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  ( $\epsilon$ )): 251 (39,000 M<sup>-1</sup> cm<sup>-1</sup>); 331 (2350 M<sup>-1</sup> cm<sup>-1</sup>); 457 (76 M<sup>-1</sup> cm<sup>-1</sup>); 551 (86 M<sup>-1</sup> cm<sup>-1</sup>); 580 (70 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for

# C<sub>63</sub>H<sub>48</sub>Co<sub>3</sub>N<sub>6</sub>O<sub>9</sub>: C, 62.54; H, 4.00; N, 6.95. Found: C, 62.36; H, 4.02; N, 6.90.

**Synthesis of LNi<sub>3</sub>(OAc)**<sub>3</sub>. H<sub>3</sub>L (270.4 mg, 0.31 mmol) was suspended in a 1:1 solution of CH<sub>3</sub>CN and H<sub>2</sub>O (~5 mL). Ni(OAc)<sub>2</sub>•4H<sub>2</sub>O (235.0 mg, 0.94 mmol) was added as a crystalline solid to the stirring suspension. To this, a 1 M KOH solution in H<sub>2</sub>O (0.94 mL) was added dropwise. When all of the H<sub>3</sub>L was dissolved to give a green homogeneous solution (~12 h), the solvent was removed under reduced pressure. The green residue was taken up in CH<sub>2</sub>Cl<sub>2</sub> and a white solid was filtered from the green solution. The solution was pumped down and dried *in vacuo* for 8 hrs. The resulting green powder was dissolved in CHCl<sub>3</sub> and diethyl ether was allowed to diffuse into the solution as a vapor. White precipitate collected at the bottom of the vial and the green homogeneous solution was decanted off. This precipitation procedure was repeated until no more white precipitate appeared and green crystalline clusters of LNi<sub>3</sub>(OAc)<sub>3</sub> grew (100 mg, 27%). <sup>1</sup>H NMR (300 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  150.81 (3 H), 136.93 (3 H), 58.87 (3 H), 46.53 (3 H), 34.58 (3 H), 32.08 (3 H), 21.36 (9 H), 15.85 (3 H), 12.31 (6 H), 10.76 (3 H), 7.74 (3 H), 4.90 (3 H), 3.8 (3 H). UV-Vis: (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  (ε)): 254 (35,900 M<sup>-1</sup> cm<sup>-1</sup>); 385 (192 M<sup>-1</sup> cm<sup>-1</sup>); 450 (45 M<sup>-1</sup> cm<sup>-1</sup>); 500 (29 M<sup>-1</sup> cm<sup>-1</sup>); 676 (37 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for C<sub>63H48</sub>N<sub>6</sub>Ni<sub>3</sub>O<sub>9</sub>: C, 62.58; H, 4.00; N, 6.95. Found: C, 62.49; H, 4.20; N, 7.05.

Synthesis of LCu<sub>3</sub>(OAc)<sub>3</sub>. A scintillation vial equipped with a stir bar was charged with H<sub>3</sub>L (0.100 g, 0.116 mmol) and Cu(OAc)<sub>2</sub>•H<sub>2</sub>O (0.071 g, 0.355 mmol). Dichloromethane (5 mL) was added, and then triethylamine (0.052 mL, 0.407 mmol) was added via syringe. The mixture was stirred at room temperature for 12 h, becoming a homogeneous green mixture. The solvent was removed under reduced pressure and the green residue was washed with THF (5 mL), then recrystallized from CH<sub>2</sub>Cl<sub>2</sub>/diethyl ether to yield LCu<sub>3</sub>(OAc)<sub>3</sub> as clusters of pale green needles (0.041 g, 29%). <sup>1</sup>H NMR (500 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  126.26 (3 H), 49.44 (3 H), 36.45 (3 H), 33.15 (3 H), 22.02 (3 H), 12.93 (3 H), 10.96 (3 H), 9.80 (9 H), 8.78 (6 H), 8.12 (3 H), 6.55 (3 H), 6.08 (3 H). UV-Vis (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  ( $\epsilon$ )): 253 (49,100 M<sup>-1</sup> cm<sup>-1</sup>); 860 (270 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for C<sub>63</sub>H<sub>48</sub>Cu<sub>3</sub>N<sub>6</sub>O<sub>9</sub>: C, 61.83; H, 3.95; N, 6.87. Anal. Calcd. for C<sub>63</sub>H<sub>50</sub>Cu<sub>3</sub>N<sub>6</sub>O<sub>10</sub> (LCu<sub>3</sub>(OAc)<sub>3</sub>•H<sub>2</sub>O): C, 60.94; H, 4.06; N, 6.77. Found: C, 60.79; H, 4.04; N, 6.92.

**Synthesis of LZn<sub>3</sub>(OAc)<sub>3</sub>**. A scintillation vial equipped with a stir bar was charged with H<sub>3</sub>L (0.100 g, 0.116 mmol) and Zn(OAc)<sub>2</sub> (0.065 g, 0.355 mmol). Dichloromethane (5 mL) was added, then triethylamine (0.052 mL, 0.407 mmol) was added via syringe. The yellow solution was stirred at room temperature for 12 h, and the solvent was removed under reduced pressure. The pale pink residue was washed with THF, then recrystallized twice from CH<sub>2</sub>Cl<sub>2</sub>/diethyl ether to yield LZn<sub>3</sub>(OAc)<sub>3</sub> as colorless crystals (0.024 g, 17%). <sup>1</sup>H NMR (500 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  8.70 (d, *J* = 4.5 Hz, 3 H, *a*), 8.02 (t, *J* = 7.5 Hz, 3 H, *f*), 7.86 (t, *J* = 7.5 Hz, 3 H, *g*), 7.80 (d, *J* = 8 Hz, 3 H, *d*), 7.74 (d, *J* = 4.5 Hz, 3 H, *a'*), 7.37 (dd, *J* = 7.5, 4.5 Hz, 3 H, *b* or *b'*), 7.25 (dd, *J* = 7.5, 4.5 Hz, 3 H, *b* or *b'*), 7.21 (t, *J* = 8 Hz, 3 H, *c* or *c'*), 7.17 (t, *J* = 7.5 Hz, 3 H, *c* or *c'*), 7.16 (d, *J* = 8 Hz, 3 H, *d'*), 6.98 (d, *J* = 7.5 Hz, 3 H, *e*), 6.51 (d, *J* = 7.5 Hz, 3 H, *h*), 5.66 (s, 3 H, *j*), 1.42 (s, 9 H, OAc). <sup>13</sup>C NMR (125.70 MHz, CDCl<sub>3</sub>, 25 °C):  $\delta$  177.5, 165.7, 164.0, 150.6, 147.1, 144.7, 142.5, 141.5, 140.0, 138.7, 131.3, 130.5, 127.7, 127.0, 126.7, 126.2, 123.8, 123.6, 121.6, 84.4, 23.6. UV-Vis (CH<sub>2</sub>Cl<sub>2</sub>,  $\lambda_{max}$  (ε)): 253 (48,700 M<sup>-1</sup> cm<sup>-1</sup>) nm. Anal. Calcd. for C<sub>63</sub>H<sub>48</sub>N<sub>6</sub>O<sub>9</sub>Zn<sub>3</sub>: C, 61.56; H, 3.94; N, 6.84. Anal. Calcd. for C<sub>63</sub>H<sub>50</sub>N<sub>6</sub>O<sub>10</sub>Zn<sub>3</sub> (LZn<sub>3</sub>(OAc)<sub>3</sub>•H<sub>2</sub>O): C, 60.67; H, 4.04; N, 6.74. Found: C, 60.93; H, 4.09; N, 6.71.



**Figure S1**. <sup>1</sup>H NMR spectrum of  $H_3L$  in  $CD_2Cl_2$  at 25 °C.



Figure S2.  $^{13}$ C NMR spectrum of H<sub>3</sub>L in CDCl<sub>3</sub> at 25 °C.



Figure S4. <sup>1</sup>H NMR spectrum of LFe<sub>3</sub>(OAc)<sub>3</sub> in  $CD_2Cl_2$  at 25 °C.



Figure S6. <sup>1</sup>H NMR spectrum of LNi<sub>3</sub>(OAc)<sub>3</sub> in CDCl<sub>3</sub> at 25 °C.





Figure S8. <sup>1</sup>H NMR spectrum of LZn<sub>3</sub>(OAc)<sub>3</sub> in CDCl<sub>3</sub> at 25 °C.



Figure S9. <sup>13</sup>C NMR spectrum of LZn<sub>3</sub>(OAc)<sub>3</sub> in CDCl<sub>3</sub> at 25 °C.

### Magnetic Susceptibility Measurements

**General Considerations**. Magnetic susceptibility measurements were carried out in the Molecular Materials Research Center in the Beckman Institute of the California Institute of Technology on a Quantum Design MPMS instrument running MPMS Multivu software. Crystalline samples (0.030–0.100 g) were powdered and suspended in clear plastic straws in gelatin capsules. Data were recorded at 0.5 and 5 T from 4–300 K. Diamagnetic corrections were made using Pascal's constants as follows: –710, –648, –645, –645, and –642 × 10<sup>-6</sup> cm<sup>3</sup>/mol respectively for M = Mn, Fe, Co, Ni, and Cu. The data for LMn<sub>3</sub>(OAc)<sub>3</sub> were processed and simulated with the inclusion of one equivalent of chloroform, which was found to be in the sample by both elemental analysis and <sup>1</sup>H NMR spectroscopy. Anal. Calcd. for C<sub>64</sub>H<sub>39</sub>Cl<sub>3</sub>Mn<sub>3</sub>N<sub>6</sub>O<sub>9</sub> (LMn<sub>3</sub>(OAc)<sub>3</sub>•CHCl<sub>3</sub>): C, 58.35; H, 3.75; N, 6.38. Found: C, 58.74; H, 3.87; N, 6.31.

The  $\chi_M T$  data were fit to the magnetic susceptibility equation derived from the isotropic spin Hamiltonian for two coupling constants, J and  $J_{13}$  [Eq. (1)].

$$\hat{H} = -2J[(\hat{S}_1\hat{S}_2) + (\hat{S}_2\hat{S}_3)] - 2J_{13}(\hat{S}_3\hat{S}_1)]$$

The Kambe vector method<sup>2</sup> yields the magnetic susceptibility equation [Eq. (2)]. In this equation, spin levels are defined by the quantum number S' = 3S, 3S-1, 3S-2, ..., 0 or  $\frac{1}{2}$ , where  $S = \frac{5}{2}$ , 2,  $\frac{3}{2}$ , 1, and  $\frac{1}{2}$  respectively for M = Mn, Fe, Co, Ni, and Cu. Application of the Van Vleck equation gives the energy of each spin state [Eq. (3)].<sup>3</sup> The multiplicity of each spin level is defined by  $\Omega(S')$ .

$$\chi_{M} = \frac{N_{A}\beta^{2}g^{2}}{3kT} \frac{\sum S'(S'+1)(2S'+1)\Omega(S')\exp(-W(S')/kT)}{\sum (2S'+1)\Omega(S')\exp(-W(S')/kT)}$$
(2)  
$$W(S') = -J[S'(S'+1) - 3S(S+1)]$$
(3)

The data were fit using Matlab by minimizing  $R = \sum |(\chi_M T)_{obs} - (\chi_M T)_{calcd}|^2 / \sum (\chi_M T)_{obs}^2$ .

The  $\chi_M T$  data below T = 40 K for LCu<sub>3</sub>(OAc)<sub>3</sub> did not fit the model equation as well as the higher temperature data. This discrepancy may be due to other exchange interactions whose effects are stronger at low temperatures, such as intermolecular interactions or interactions due to temperature-dependent structural changes.

# Crystallographic Information:

Crystallographic data have been deposited at the CCDC, 12 Union Road, Cambridge CB2 1EZ, UK and copies can be obtained on request, free of charge, by quoting the publication citation and the deposition numbers 787163 (Mn), 803594 (Fe), 777599 (Co), 803595 (Ni), 803593 (Cu), and 803592 (Zn).

	LMn <sub>3</sub> (OAc) <sub>3</sub>	LFe <sub>3</sub> (OAc) <sub>3</sub>	LCo <sub>3</sub> (OAc) <sub>3</sub>	LNi <sub>3</sub> (OAc) <sub>3</sub>	LCu <sub>3</sub> (OAc) <sub>3</sub>	
empirical formula	$C_{63}H_{48}Mn_3N_6O_9$	C <sub>63</sub> H <sub>48</sub> Fe <sub>3</sub> N <sub>6</sub> O <sub>9</sub>	$C_{63}H_{48}Co_3N_6O_9$	C <sub>63</sub> H <sub>48</sub> Ni <sub>3</sub> N <sub>6</sub> O <sub>9</sub>	$C_{63}H_{48}Cu_3N_6O_9$	С
formula wt	1197.90	1200.62	1209.89	1209.17	1164.65	
T (K)	100(2)	100(2)	100(2)	100(2)	100(2)	
a, Å	10.5708(8)	10.6327(4)	20.8675(10)	20.7019(9)	18.9118(5)	
b, Å	19.6592(14)	18.9722(8)	20.8675(10)	20.7019(9)	19.0501(5)	
c, Å	20.2109(15)	19.6009(8)	10.5670(6)	10.6229(6)	36.0732(9)	
α, deg	71.889(4)	72.453(2)	90	90	90	

**Table S1**. Crystal and refinement data for  $LM_3(OAc)_3$  (M = Mn, Fe, Co, Ni, Cu, Zn).

β, deg	88.967(4)	89.924(2)	90	90	90	
γ, deg	75.160(4)	75.857(2)	120	120	90	
V, Å <sup>3</sup>	3850.2(5)	3644.5(3)	3985.0(4)	3942.7(3)	12996.1(6)	
Z	2	2	3	3	8	
cryst syst	triclinic	triclinic	trigonal	trigonal	orthorhombic	
space group	P-1	P-1	R 3	R 3	P bcn	
$d_{calcd}, g/cm^3$	1410	1094	1512	1528	1190	
$\theta$ range, deg	2.00-30.2	1.98-30.60	2.23-30.10	1.97-30.16	1.89-26.40	
μ, mm <sup>-1</sup>	0.531	0.638	0.993	1.132	1.023	
abs cor	none	none	Semi-empirical from equivalents	none	none	
GOF	2.775	3.896	2.172	2.887	2.988	
		0.0576,				
$R1,^{a} wR2^{b} (I > 2\sigma(I))$	0.0504, 0.0863	0.1052	0.0380, 0.0788	0.0443, 0.0690	0.0481, 0.0898	0
<sup><i>a</i></sup> R1 = $\Box   F_{o}  -  F_{c}  /\Box  F$	$F_{o} . \ ^{b} \mathbf{wR2} = \{\Box[w(F_{o})] $	$F_{\rm o}^{2} - F_{\rm c}^{2})^{2}]/\Box[w(h)]$	$F_{o}^{2})^{2}]\}^{1/2}.$			

Figure S10. Structural drawing of LMn<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids.



**Special refinement details for LMn<sub>3</sub>(OAc)<sub>3</sub>.** Crystals were mounted in a loop with oil then placed on the diffractometer under a nitrogen stream at 100K. The solvent are contains four molecules of chloroform and one of diethyl ether. Although they were discernable we were unable to obtain a satisfactory solvent model due to disorder. Due to the considerable percentage of the unit cell occupied by the solvent (37.4%) and the presence of strong scatterers (12 Cl atoms) SQUEEZE<sup>4</sup> was employed to produce a bulk solvent correction to the observed

intensities. The program accounted for 430 electrons of approximately 550 expected. The resulting model is vastly superior to the model including solvent specifically. Refinement of  $F^2$  against ALL reflections. The weighted R-factor (*w*R) and goodness of fit (S) are based on F<sup>2</sup>, conventional R-factors (R) are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2s(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F<sup>2</sup> are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Table S2. Atomic coordinates (x 104) and equivalent isotropic displacement parameters (Å	$^{2}X$
10 <sup>3</sup> ) for LMn <sub>3</sub> (OAc) <sub>3</sub> . U(eq) is defined as the trace of the orthogonalized U <sup>ij</sup> tensor.	

	Х	У	Z	$\mathrm{U}_{\mathbf{eq}}$
Mn(1)	7930(1)	1884(1)	5911(1)	13(1)
Mn(2)	8658(1)	592(1)	7529(1)	15(1)
Mn(3)	7434(1)	2417(1)	7390(1)	16(1)
O(1)	7542(1)	892(1)	6592(1)	13(1)
O(2)	7215(2)	1386(1)	7872(1)	14(1)
O(3)	6636(1)	2574(1)	6402(1)	13(1)
O(4)	9488(2)	1620(1)	5288(1)	21(1)
O(5)	11223(2)	1857(1)	4718(1)	29(1)
O(6)	10393(2)	551(1)	8042(1)	27(1)
O(7)	11088(2)	-626(1)	8693(1)	41(1)
O(8)	9270(2)	2686(1)	7153(1)	20(1)
O(9)	9268(2)	1707(1)	6821(1)	17(1)
N(1)	6842(2)	1456(1)	5264(1)	14(1)
N(2)	9582(2)	-268(1)	6967(1)	15(1)
N(3)	7759(2)	-40(1)	8467(1)	16(1)
N(4)	8287(2)	2066(1)	8542(1)	19(1)
N(5)	5975(2)	3503(1)	7133(1)	19(1)
N(6)	7972(2)	3120(1)	5368(1)	16(1)
C(1)	4609(2)	1478(1)	6322(1)	15(1)
C(2)	4933(2)	882(1)	6941(1)	15(1)
C(3)	4843(2)	1028(1)	7571(1)	16(1)
C(4)	4506(2)	1754(1)	7595(1)	16(1)
C(5)	4215(2)	2335(1)	6976(1)	16(1)
C(6)	4297(2)	2206(1)	6331(1)	16(1)
C(7)	4147(2)	2811(1)	5655(1)	17(1)
C(8)	3260(2)	2837(1)	5132(1)	21(1)
C(9)	3136(2)	3336(2)	4467(1)	24(1)
C(10)	3914(2)	3829(1)	4296(1)	23(1)
C(11)	4799(2)	3807(1)	4800(1)	20(1)
C(12)	4953(2)	3315(1)	5481(1)	16(1)
C(13)	5443(2)	101(1)	6953(1)	16(1)
C(14)	4742(3)	-406(2)	7307(1)	23(1)
C(15)	5172(3)	-1152(2)	7385(1)	24(1)

C(16)	6332(2)	-1417(1)	7115(1)	21(1)
C(17)	7033(2)	-924(1)	6758(1)	19(1)
C(18)	6636(2)	-170(1)	6674(1)	14(1)
C(19)	4543(2)	1905(1)	8268(1)	17(1)
C(20)	3389(2)	2350(1)	8427(1)	23(1)
C(21)	3325(3)	2544(1)	9035(1)	24(1)
C(22)	4412(3)	2292(1)	9500(1)	24(1)
C(23)	5572(2)	1848(1)	9346(1)	20(1)
C(24)	5663(2)	1654(1)	8731(1)	14(1)
C(25)	6025(2)	3294(1)	6002(1)	14(1)
C(26)	7511(2)	348(1)	6289(1)	13(1)
C(27)	7015(2)	1196(1)	8581(1)	15(1)
C(28)	7110(2)	3619(1)	5601(1)	14(1)
C(29)	7253(2)	4313(1)	5507(1)	18(1)
C(30)	8313(2)	4524(1)	5153(1)	22(1)
C(31)	9172(2)	4023(1)	4902(1)	23(1)
C(32)	8978(2)	3328(1)	5021(1)	21(1)
C(33)	5427(2)	3760(1)	6478(1)	16(1)
C(34)	4410(2)	4403(1)	6252(1)	21(1)
C(35)	3935(3)	4802(2)	6706(2)	28(1)
C(36)	4495(3)	4535(2)	7381(2)	33(1)
C(37)	5499(3)	3885(2)	7575(1)	28(1)
C(38)	6948(2)	722(1)	5525(1)	13(1)
C(39)	6496(2)	352(1)	5137(1)	17(1)
C(40)	5870(2)	753(1)	4479(1)	19(1)
C(41)	5709(2)	1514(1)	4235(1)	19(1)
C(42)	6226(2)	1839(1)	4637(1)	16(1)
C(43)	8945(2)	-149(1)	6356(1)	14(1)
C(44)	9513(2)	-464(1)	5867(1)	15(1)
C(45)	10769(2)	-942(1)	6015(1)	18(1)
C(46)	11411(2)	-1072(1)	6652(1)	21(1)
C(47)	10793(2)	-716(1)	7106(1)	18(1)
C(48)	7119(2)	364(1)	8865(1)	14(1)
C(49)	6583(2)	31(1)	9466(1)	19(1)
C(50)	6672(2)	-725(1)	9660(1)	22(1)
C(51)	7291(3)	-1125(2)	9240(1)	24(1)
C(52)	7833(2)	-766(1)	8654(1)	21(1)
C(53)	8109(2)	1405(1)	8928(1)	18(1)
C(54)	8833(2)	978(1)	9544(1)	20(1)
C(55)	9784(2)	1236(2)	9783(1)	25(1)
C(56)	9989(3)	1904(2)	9392(1)	27(1)
C(57)	9221(3)	2299(2)	8781(1)	25(1)
C(58)	10721(3)	1495(1)	5231(1)	20(1)
C(59)	11597(2)	864(1)	5797(1)	23(1)
C(60)	11192(3)	12(2)	8483(1)	21(1)
C(61)	12330(3)	212(2)	8743(1)	38(1)
C(62)	9843(2)	2172(2)	6915(1)	20(1)
C(63)	11241(2)	2116(2)	6725(2)	34(1)

**Table S3.** Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LMn<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2$ [  $h^2a^{*2}U^{11} + ... + 2 h k a^* b^* U^{12}$ ]

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
$\overline{\mathrm{Mn}(1)}$	121(2)	137(2)	144(2)	-49(2)	19(2)	-41(2)
Mn(2)	124(2)	180(2)	146(2)	-64(2)	10(2)	-32(2)
Mn(3)	148(2)	167(2)	158(2)	-43(2)	14(2)	-52(2)
O(1)	114(9)	147(9)	156(9)	-64(7)	7(7)	-43(7)
O(2)	126(9)	175(10)	126(9)	-49(8)	35(7)	-49(8)
O(3)	98(9)	117(9)	150(9)	-21(7)	3(7)	3(7)
O(4)	151(10)	275(11)	251(10)	-142(9)	76(8)	-74(9)
O(5)	250(11)	341(12)	279(11)	-46(10)	73(9)	-131(10)
O(6)	213(11)	333(12)	266(11)	-82(10)	-33(9)	-70(10)
O(7)	591(16)	298(13)	304(12)	-33(10)	-26(11)	-131(12)
O(8)	167(10)	232(11)	245(10)	-126(9)	54(8)	-60(8)
O(9)	130(9)	182(10)	206(10)	-61(8)	0(7)	-70(8)
N(1)	89(11)	164(12)	150(11)	-36(9)	19(9)	-24(9)
N(2)	111(11)	168(12)	176(11)	-56(9)	-8(9)	-19(9)
N(3)	142(12)	170(12)	162(11)	-50(9)	0(9)	-30(10)
N(4)	212(13)	220(13)	172(11)	-73(10)	23(9)	-110(10)
N(5)	178(12)	186(12)	223(12)	-101(10)	45(10)	-42(10)
N(6)	144(12)	157(12)	193(11)	-59(9)	38(9)	-59(10)
C(1)	54(13)	237(15)	182(13)	-77(12)	25(10)	-56(11)
C(2)	39(12)	192(14)	234(14)	-65(12)	17(10)	-60(11)
C(3)	70(13)	222(15)	191(13)	-36(11)	37(10)	-85(11)
C(4)	52(13)	232(15)	213(14)	-88(12)	33(10)	-58(11)
C(5)	62(13)	191(14)	249(14)	-101(12)	43(11)	-43(11)
C(6)	64(13)	220(15)	177(13)	-10(11)	-6(10)	-60(11)
C(7)	105(13)	178(14)	202(14)	-70(11)	30(11)	-6(11)
C(8)	109(14)	249(16)	263(15)	-58(13)	18(11)	-53(12)
C(9)	165(15)	283(17)	260(15)	-90(13)	-75(12)	-11(13)
C(10)	242(16)	201(15)	183(14)	-4(12)	-37(12)	-27(13)
C(11)	186(15)	126(14)	262(15)	-54(12)	-14(12)	-19(12)
C(12)	139(14)	142(14)	180(13)	-65(11)	29(11)	-5(11)
C(13)	150(14)	185(14)	152(13)	-38(11)	-19(11)	-68(12)
C(14)	227(16)	256(16)	241(15)	-81(13)	45(12)	-125(13)
C(15)	255(16)	253(16)	239(15)	-41(13)	48(12)	-164(14)
C(16)	239(16)	140(14)	248(15)	-44(12)	-16(12)	-70(12)
C(17)	163(14)	196(15)	205(14)	-66(12)	-7(11)	-53(12)
C(18)	155(14)	163(14)	128(12)	-41(11)	-7(10)	-84(11)
C(19)	150(14)	183(14)	192(14)	-68(11)	68(11)	-57(12)
C(20)	153(15)	262(16)	248(15)	-64(13)	23(12)	-34(12)
C(21)	191(15)	231(16)	290(16)	-102(13)	96(13)	-14(13)
C(22)	268(17)	254(16)	208(15)	-101(13)	96(13)	-71(13)
C(23)	181(15)	204(15)	221(14)	-61(12)	54(12)	-71(12)
C(24)	153(14)	127(13)	156(13)	-50(11)	56(11)	-42(11)
C(25)	145(14)	114(13)	159(13)	-39(11)	2/(10)	-4/(11)
C(26)	112(13)	130(13)	149(12)	-40(11)	10(10)	-40(11)
C(27)	140(14)	200(14)	$\frac{11}{(12)}$	-3/(11)	21(10) 12(10)	-12(11)
C(28)	150(13)	165(14)	139(12)	-40(11)	-12(10)	-43(11)
C(29)	150(14)	100(14) 120(14)	198(14)	-33(12)	/(11)	$-\delta(12)$
C(30)	2/3(10)	138(14)	204(15)	-55(12)	15(12)	-89(13)
C(31)	191(15)	241(10) 102(15)	233(13)	-01(13)	95(12)	-98(13)
C(32)	1/0(13) 161(14)	173(13) 126(14)	230(13)	-34(12)	00(12)	-33(12)
C(33)	101(14)	130(14)	200(14)	-44(11)	49(11)	-01(11)

C(34)	175(15)	178(15)	245(15)	-50(12)	37(12)	-39(12)
C(35)	212(16)	209(16)	384(18)	-103(14)	83(14)	7(13)
C(36)	349(19)	316(18)	349(18)	-204(15)	108(15)	-26(15)
C(37)	349(18)	274(17)	237(15)	-108(13)	29(13)	-78(14)
C(38)	81(13)	176(14)	156(13)	-64(11)	25(10)	-43(11)
C(39)	128(14)	191(14)	205(14)	-70(12)	42(11)	-66(12)
C(40)	131(14)	260(16)	213(14)	-95(12)	21(11)	-74(12)
C(41)	128(14)	217(15)	178(14)	-36(12)	-8(11)	-13(12)
C(42)	137(14)	159(14)	183(13)	-44(11)	22(11)	-26(11)
C(43)	158(14)	111(13)	172(13)	-35(11)	22(11)	-76(11)
C(44)	156(14)	138(13)	171(13)	-61(11)	4(11)	-40(11)
C(45)	185(15)	193(14)	190(14)	-74(12)	48(11)	-65(12)
C(46)	177(15)	179(15)	250(15)	-44(12)	6(12)	-13(12)
C(47)	167(14)	198(15)	158(13)	-50(11)	0(11)	-32(12)
C(48)	114(13)	185(14)	139(13)	-60(11)	-14(10)	-32(11)
C(49)	146(14)	215(15)	194(14)	-59(12)	40(11)	-54(12)
C(50)	155(15)	256(16)	222(14)	-17(12)	49(11)	-76(13)
C(51)	292(17)	176(15)	253(15)	-64(12)	-10(13)	-79(13)
C(52)	223(15)	173(15)	230(15)	-60(12)	-10(12)	-39(12)
C(53)	135(14)	255(16)	179(14)	-113(12)	49(11)	-57(12)
C(54)	174(15)	202(15)	202(14)	-60(12)	31(11)	-42(12)
C(55)	212(16)	331(17)	198(14)	-68(13)	-29(12)	-70(14)
C(56)	263(17)	339(18)	274(16)	-112(14)	-16(13)	-170(14)
C(57)	307(17)	259(16)	248(15)	-83(13)	66(13)	-164(14)
C(58)	201(16)	203(15)	247(15)	-135(12)	46(12)	-76(13)
C(59)	265(16)	196(15)	237(15)	-65(12)	-17(12)	-53(13)
C(60)	256(17)	240(16)	121(13)	-59(12)	33(12)	-39(13)
C(61)	213(17)	680(20)	254(16)	-160(17)	-32(13)	-121(17)
C(62)	167(15)	275(16)	157(13)	-53(12)	-20(11)	-54(13)
C(63)	119(15)	470(20)	560(20)	-310(18)	110(14)	-129(14)



**Figure S11**. Structural drawing of LFe<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids. One acetate is disordered over two populations, denoted A and B.

**Special refinement details for LFe<sub>3</sub>(OAc)<sub>3</sub>.** Crystals were mounted on a glass fiber using Paratone oil then placed on the diffractometer under a nitrogen stream at 100K. Approximately 35% of the unit cell volume is solvent and poorly ordered. To account for solvent the program SQUEEZE<sup>4</sup> was employed to apply bulk solvent flattening. A total of 685 electrons were accounted for. One of the bound acetate is disordered and was modeled without restraints. Refinement of  $F^2$  against ALL reflections. The weighted R-factor (*w*R) and goodness of fit (S) are based on  $F^2$ , conventional R-factors (R) are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two 1.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving 1.s. planes.

**Table S4.** Atomic coordinates (  $x \ 10^4$ ) and equivalent isotropic displacement parameters (Å<sup>2</sup>x 10<sup>3</sup>) for LFe<sub>3</sub>(OAc)<sub>3</sub>. U(eq) is defined as the trace of the orthogonalized U<sup>ij</sup> tensor.

Fe(1)	3088(1)	6800(1)	970(1)	20(1)	1
Fe(2)	3569(1)	5413(1)	2628(1)	22(1)	1
Fe(3)	2704(1)	7294(1)	2416(1)	21(1)	1
O(1)	2601(2)	5818(1)	1663(1)	20(1)	1
O(2)	2292(2)	6321(1)	2910(1)	19(1)	1
O(3)	1805(2)	7468(1)	1424(1)	17(1)	1
O(4)	4627(2)	6432(1)	459(1)	33(1)	1
O(5)	6418(2)	6680(1)	-26(1)	48(1)	1
O(8)	4226(2)	7889(1)	2094(1)	28(1)	1
O(9)	4461(2)	6793(1)	1868(1)	29(1)	1
O(6A)	5226(5)	5492(4)	3019(4)	25(2)	0.403(9)
O(7A)	6096(9)	4295(4)	3740(3)	40(3)	0.403(9)
O(6B)	5154(4)	5055(4)	3331(3)	36(2)	0.597(9)
O(7B)	7092(5)	4278(3)	3722(2)	45(2)	0.597(9)
N(1)	1959(2)	6428(1)	299(1)	21(1)	1
N(2)	4515(2)	4595(1)	2053(1)	21(1)	1
N(3)	2608(2)	4877(1)	3526(1)	22(1)	1
N(4)	3579(2)	6954(1)	3529(1)	23(1)	1
N(5)	1278(2)	8370(1)	2221(1)	25(1)	1
N(6)	3132(2)	8011(2)	385(1)	23(1) 27(1)	1
C(1)	-310(2)	6421(2)	1350(2)	27(1) 20(1)	1
C(1)	-510(2) 14(2)	5811(2)	2000(2)	$\frac{20(1)}{16(1)}$	1
C(2)	102(2)	5082(2)	2000(2) 2639(2)	10(1) 10(1)	1
C(3)	-102(2)	5732(2)	2039(2) 2650(2)	19(1) 18(1)	1
C(4)	-396(2)	$\frac{0739(2)}{7220(2)}$	2030(2) 2010(2)	10(1) 20(1)	1
C(3)	-0.02(2)	7520(2)	2010(2) 1248(2)	20(1) 18(1)	1
C(0)	-601(2)	7103(2)	1348(2)	18(1) 10(1)	1
C(7)	498(2)	5010(2)	2020(1)	19(1)	1
C(8)	-183(3)	44/4(2)	2397(2)	$\frac{2}{(1)}$	1
C(9)	240(3)	3/02(2)	24/6(2)	20(1)	1
C(10)	1341(3)	3450(2)	2158(2)	$\frac{2}{(1)}$	1
C(11)	2023(3)	3957(2)	17/5(2)	23(1)	1
C(12)	1642(2)	4/40(2)	1/13(2)	18(1)	1
C(13)	-309(2)	6933(2)	3319(1)	18(1)	1
C(14)	-1387(2)	7434(2)	3486(2)	24(1)	l
C(15)	-1370(3)	7668(2)	4082(2)	30(1)	1
C(16)	-288(3)	7419(2)	4544(2)	29(1)	1
C(17)	815(3)	6895(2)	4415(2)	24(1)	1
C(18)	840(2)	6658(2)	3807(2)	23(1)	1
C(19)	-720(2)	7777(2)	651(2)	19(1)	1
C(20)	-1621(2)	7805(2)	115(2)	23(1)	1
C(21)	-1734(3)	8329(2)	-572(2)	28(1)	1
C(22)	-949(3)	8837(2)	-728(2)	32(1)	1
C(23)	-40(3)	8802(2)	-210(2)	25(1)	1
C(24)	99(2)	8288(2)	485(2)	19(1)	1
C(25)	2532(2)	5273(2)	1323(2)	17(1)	1
C(26)	1991(2)	5680(2)	538(2)	17(1)	1
C(27)	1505(2)	5331(2)	114(2)	21(1)	1
C(28)	933(2)	5762(2)	-570(2)	24(1)	1
C(29)	824(3)	6532(2)	-809(2)	25(1)	1
C(30)	1389(2)	6849(2)	-363(2)	22(1)	1
C(31)	3925(2)	4758(2)	1399(2)	19(1)	1
C(32)	4501(3)	4447(2)	883(2)	26(1)	1
C(33)	5727(3)	3925(2)	1075(2)	30(1)	1
			· ·		

C(34)	6311(3)	3747(2)	1735(2)	32(1)	1
C(35)	5692(3)	4098(2)	2220(2)	30(1)	1
C(36)	2126(2)	6149(2)	3648(2)	21(1)	1
C(37)	2133(2)	5301(2)	3949(2)	20(1)	1
C(38)	1627(2)	4983(2)	4591(2)	24(1)	1
C(39)	1550(3)	4238(2)	4785(2)	26(1)	1
C(40)	2005(3)	3806(2)	4324(2)	28(1)	1
C(41)	2535(3)	4153(2)	3706(2)	29(1)	1
C(42)	3270(2)	6344(2)	3978(2)	23(1)	1
C(43)	3922(2)	5931(2)	4650(2)	24(1)	1
C(44)	4911(3)	6191(2)	4883(2)	31(1)	1
C(45)	5239(3)	6816(2)	4426(2)	42(1)	1
C(46)	4549(3)	7184(2)	3764(2)	36(1)	1
C(47)	1219(2)	8225(2)	1035(2)	21(1)	1
C(48)	704(2)	8676(2)	1552(2)	20(1)	1
C(49)	-302(3)	9342(2)	1365(2)	27(1)	1
C(50)	-710(3)	9705(2)	1860(2)	34(1)	1
C(51)	-117(3)	9386(2)	2555(2)	40(1)	1
C(52)	865(3)	8713(2)	2720(2)	31(1)	1
C(53)	2286(3)	8554(2)	602(2)	26(1)	1
C(54)	2410(3)	9287(2)	456(2)	29(1)	1
C(55)	3423(3)	9484(2)	54(2)	42(1)	1
C(56)	4241(3)	8951(2)	-194(2)	46(1)	1
C(57)	4083(3)	8235(2)	-19(2)	35(1)	1
C(58)	5875(3)	6333(2)	467(2)	35(1)	1
C(59)	6648(3)	5723(2)	1121(2)	41(1)	1
C(62)	4873(3)	7365(2)	1863(2)	28(1)	1
C(63)	6182(3)	7419(2)	1587(2)	39(1)	1
C(60A)	6180(30)	4962(14)	3441(16)	10(3)	0.403(9)
C(61A)	7281(11)	5245(9)	3624(7)	38(3)	0.403(9)
C(60B)	6350(30)	4905(13)	3514(13)	41(6)	0.597(9)
C(61B)	6888(9)	5603(6)	3380(5)	51(2)	0.597(9)

**Table S5.** Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LFe<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2$ [ h<sup>2</sup>a<sup>\*2</sup>U<sup>11</sup> + ... + 2 h k a<sup>\*</sup> b<sup>\*</sup> U<sup>12</sup> ].

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
Fe(1)	135(2)	290(3)	248(3)	-135(2)	59(2)	-103(2)
Fe(2)	114(2)	327(3)	242(3)	-146(2)	-10(2)	-9(2)
Fe(3)	126(2)	255(3)	256(3)	-100(2)	2(2)	-53(2)
O(1)	114(9)	280(12)	249(12)	-135(9)	22(8)	-69(8)
O(2)	115(9)	271(11)	203(11)	-108(9)	28(8)	-54(8)
O(3)	126(9)	190(11)	201(11)	-50(9)	5(8)	-49(8)
O(4)	213(11)	474(15)	420(14)	-285(12)	164(10)	-143(10)
O(5)	364(13)	637(18)	682(18)	-373(15)	322(13)	-345(13)
O(8)	224(11)	354(13)	320(13)	-178(11)	52(9)	-114(10)
O(9)	114(9)	437(14)	435(14)	-271(12)	14(9)	-91(9)
O(6A)	200(30)	260(40)	300(40)	-80(30)	-60(30)	-90(30)
O(7A)	570(60)	270(40)	310(40)	20(30)	-60(30)	-140(40)
O(6B)	200(20)	610(50)	310(30)	-250(30)	-27(19)	-40(20)
O(7B)	360(30)	390(30)	420(30)	-50(20)	-70(20)	130(20)

N(1)	115(11)	331(15)	221(14)	-128(12)	31(10)	-90(10)
N(2)	150(11)	301(15)	214(14)	-128(11)	30(10)	-58(10)
N(3)	164(11)	267(14)	208(14)	-107(11)	-83(10)	24(10)
N(4)	184(12)	229(14)	287(15)	-80(12)	-58(11)	-57(11)
N(5)	199(12)	301(15)	308(16)	-148(13)	56(11)	-120(11)
N(6)	214(13)	382(17)	266(15)	-93(13)	55(11)	-159(12)
C(1)	84(12)	294(18)	253(17)	-118(14)	-2(11)	-72(12)
C(1)	65(11)	221(16)	209(16)	-70(13)	24(11)	-79(11)
C(2)	65(12)	221(10) 282(17)	200(10) 213(16)	-35(13)	8(11)	-66(11)
C(3)	80(12)	202(17) 275(17)	190(16)	-33(13) -72(13)	42(11)	-61(11)
$C(\tau)$	78(12)	273(17) 232(16)	280(18)	-72(13) 80(14)	$\frac{42(11)}{24(11)}$	-61(11)
C(3)	73(12)	252(10) 265(17)	209(10) 243(17)	-60(14)	24(11)	-30(11)
C(0)	$\frac{4}{(11)}$	203(17) 266(17)	243(17) 157(15)	-09(13)	-7(11) 12(11)	-76(11)
C(7)	130(13) 102(15)	200(17)	137(13) 242(18)	-01(13)	-12(11) 16(12)	-90(12)
C(8)	193(13)	400(20)	243(18) 271(18)	-91(13)	10(13) 12(12)	-123(14)
C(9)	282(10)	214(17)	$\frac{2}{1(18)}$	-21(14)	-12(13)	-100(13)
C(10)	245(16) 170(14)	201(18) 222(17)	293(18)	-64(14)	1(13)	-83(14)
C(11)	170(14)	222(17)	2/5(18)	-73(14)	-43(12)	-36(12)
C(12)	134(13)	237(16)	193(16)	-/2(13)	-22(11)	-62(12)
C(13)	151(13)	216(16)	183(16)	-65(13)	19(11)	-82(12)
C(14)	138(13)	254(17)	296(18)	-78(14)	5(12)	-23(12)
C(15)	236(16)	280(18)	350(20)	-127(15)	136(14)	9(13)
C(16)	300(17)	332(19)	244(18)	-130(15)	64(14)	-61(14)
C(17)	219(15)	314(18)	248(18)	-156(15)	12(13)	-69(13)
C(18)	151(13)	242(17)	288(18)	-79(14)	69(12)	-40(12)
C(19)	117(12)	257(17)	184(16)	-63(13)	33(11)	-46(12)
C(20)	160(14)	286(17)	246(17)	-74(14)	28(12)	-78(12)
C(21)	218(15)	360(20)	258(18)	-84(15)	-51(13)	-88(14)
C(22)	296(17)	380(20)	214(18)	8(15)	33(14)	-103(15)
C(23)	215(15)	294(18)	276(18)	-96(15)	27(13)	-131(13)
C(24)	134(13)	223(16)	223(17)	-90(13)	-6(11)	-21(12)
C(25)	161(13)	203(16)	202(16)	-116(13)	20(11)	-67(11)
C(26)	108(12)	193(16)	234(16)	-93(13)	36(11)	-60(11)
C(27)	156(13)	280(17)	215(17)	-94(14)	22(12)	-71(12)
C(28)	185(14)	380(20)	216(17)	-162(15)	32(12)	-109(13)
C(29)	181(14)	360(20)	208(17)	-97(14)	10(12)	-78(13)
C(30)	181(14)	233(17)	232(17)	-55(14)	40(12)	-50(12)
C(31)	123(13)	242(16)	277(17)	-171(14)	37(12)	-61(12)
C(32)	198(15)	316(18)	268(18)	-121(15)	5(13)	-57(13)
C(33)	166(14)	380(20)	360(20)	-158(16)	61(14)	-21(13)
C(34)	209(15)	380(20)	340(20)	-168(16)	24(14)	52(14)
C(35)	212(15)	390(20)	253(18)	-124(15)	-22(13)	12(14)
C(36)	162(13)	290(17)	206(17)	-135(14)	-22(12)	-44(12)
C(37)	112(13)	239(16)	216(16)	-67(13)	-49(11)	-17(12)
C(38)	138(13)	281(18)	310(18)	-160(15)	14(12)	-14(12)
C(39)	166(14)	290(18)	301(19)	-64(15)	-24(13)	-44(13)
C(40)	249(16)	252(18)	350(20)	-108(15)	-72(14)	-51(13)
C(41)	287(16)	276(19)	302(19)	-144(15)	-95(14)	6(14)
C(42)	157(14)	287(18)	318(19)	-184(15)	25(13)	-74(13)
C(43)	176(14)	200(16)	337(19)	-104(14)	-34(13)	-12(12)
C(44)	285(17)	257(18)	360(20)	-90(16)	-137(15)	-3(14)
C(45)	310(18)	340(20)	590(30)	-84(19)	-219(17)	-119(16)
C(46)	361(19)	228(18)	460(20)	-46(16)	-97(16)	-123(15)
C(47)	167(14)	228(17)	245(17)	-81(13)	-2(12)	-87(12)
C(48)	158(13)	223(16)	253(17)	-74(13)	42(12)	-94(12)
$\mathcal{L}(\mathcal{D})$	120(12)	223(10)		, (15)		> ((12)

C(49)	244(15)	242(17)	292(19)	-43(14)	9(13)	-75(13)
C(50)	342(18)	218(18)	410(20)	-95(16)	35(16)	-2(14)
C(51)	450(20)	390(20)	420(20)	-261(18)	83(17)	-62(17)
C(52)	270(16)	370(20)	340(20)	-201(16)	-5(14)	-74(15)
C(53)	164(14)	320(19)	276(18)	-38(15)	5(13)	-117(13)
C(54)	233(15)	250(18)	370(20)	-32(15)	24(14)	-126(14)
C(55)	357(19)	310(20)	520(20)	42(18)	-18(17)	-200(17)
C(56)	327(19)	530(30)	490(20)	-20(20)	192(17)	-207(18)
C(57)	243(16)	480(20)	330(20)	-82(17)	126(14)	-174(16)
C(58)	245(16)	490(20)	540(20)	-410(20)	160(16)	-193(16)
C(59)	233(16)	480(20)	610(30)	-310(20)	47(17)	-98(16)
C(62)	153(14)	460(20)	265(18)	-146(16)	22(13)	-77(14)
C(63)	191(16)	580(20)	510(20)	-300(20)	60(15)	-160(16)
C(60A)	200(80)	100(60)	20(60)	0(40)	-40(50)	-100(60)
C(61A)	170(50)	800(110)	240(60)	-260(70)	40(40)	-100(50)
C(60B)	330(80)	640(100)	220(90)	-180(70)	50(70)	-20(60)
C(61B)	390(60)	740(80)	540(60)	-240(50)	50(40)	-350(50)

Figure S12. Structural drawing of LCo<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids.



Special refinement details for  $LCo_3(OAc)_3$ . Crystals were mounted on a glass fiber using Paratone oil then placed on the diffractometer under a nitrogen stream at 100K. The molecule sits around a 3-fold axis. The bound acetate displays two bonding modes, both mono- and bidentate. The populations of both modes were refined to a ratio of 73:27 respectively. The bi-

dentate mode places one oxygen and the methyl group nearly on the 3-fold axis and so can not be present more than  $1/3^{rd}$  of the time. A refined population of 27% suggest a mixture in the crystal with a species where all three acetate ligands are mono-dentate. Refinement of F<sup>2</sup> against ALL reflections. The weighted R-factor (*w*R) and goodness of fit (S) are based on F<sup>2</sup>, conventional Rfactors (R) are based on F, with F set to zero for negative F<sup>2</sup>. The threshold expression of F<sup>2</sup> > 2s( F<sup>2</sup>) is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F<sup>2</sup> are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Table S6. Atomic coc	ordinates (x 104) and equivalent isotropic displacement parameters (Å <sup>2</sup> x	
$10^3$ ) for LCo <sub>3</sub> (OAc) <sub>3</sub> .	U(eq) is defined as the trace of the orthogonalized U <sup>ij</sup> tensor.	

	Х	у	Z	U <sub>eq</sub>	Occ
				-1	
Co(1)	2781(1)	5636(1)	9358(1)	26(1)	1
O(1)	3780(1)	6185(1)	8442(2)	23(1)	1
N(1)	1628(1)	5181(1)	10019(2)	33(1)	1
N(2)	2808(1)	4780(1)	8375(2)	26(1)	1
C(1)	2760(1)	6819(1)	5878(2)	26(1)	1
C(2)	2604(1)	6090(1)	5902(2)	25(1)	1
C(3)	1830(1)	5458(1)	6017(2)	26(1)	1
C(4)	1556(1)	4942(1)	5044(3)	32(1)	1
C(5)	852(1)	4314(1)	5101(3)	33(1)	1
C(6)	417(1)	4204(1)	6173(3)	33(1)	1
C(7)	676(1)	4709(1)	7141(3)	31(1)	1
C(8)	1381(1)	5350(1)	7105(2)	26(1)	1
C(9)	1648(1)	5896(1)	8221(2)	24(1)	1
C(10)	1262(2)	5475(1)	9450(2)	30(1)	1
C(11)	612(1)	5402(2)	9945(3)	37(1)	1
C(12)	342(2)	5025(2)	11066(3)	48(1)	1
C(13)	714(2)	4731(2)	11669(3)	53(1)	1
C(14)	1346(2)	4808(2)	11119(3)	46(1)	1
C(15)	3480(1)	4942(1)	7967(2)	27(1)	1
C(16)	3610(2)	4423(1)	7378(3)	38(1)	1
C(17)	3005(2)	3710(2)	7201(3)	45(1)	1
C(18)	2317(2)	3545(2)	7603(3)	41(1)	1
C(19)	2237(2)	4097(1)	8193(3)	34(1)	1
O(2A)	3058(4)	5351(4)	11064(6)	30(1)	0.727(2)
O(3A)	2407(2)	4109(2)	11217(3)	66(1)	0.727(2)
C(20A)	2883(2)	4730(2)	11604(4)	41(1)	0.727(2)
C(21A)	3207(3)	4751(3)	12899(5)	60(1)	0.727(2)
O(2B)	2357(13)	6902(16)	11200(20)	62(8)	0.273(2)
O(3B)	3221(4)	6685(6)	10502(3)	5(1)	0.273(2)
C(20B)	2860(4)	6733(4)	11391(7)	18(2)	0.273(2)
C(21B)	2981(5)	6542(6)	12685(8)	30(2)	0.273(2)

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
$\overline{\text{Co}(1)}$	246(2)	219(2)	329(2)	26(2)	-8(2)	121(2)
O(1)	247(8)	212(8)	248(9)	0(7)	-18(7)	119(7)
N(1)	300(11)	291(11)	301(12)	64(9)	-17(10)	84(9)
N(2)	286(10)	248(10)	230(11)	4(8)	4(8)	114(8)
C(1)	274(12)	333(13)	187(12)	-7(10)	-1(9)	162(10)
C(2)	273(12)	289(12)	154(11)	26(9)	9(9)	123(10)
C(3)	281(12)	282(12)	238(13)	-2(10)	-44(9)	154(10)
C(4)	378(14)	345(14)	269(14)	-25(11)	-37(11)	199(12)
C(5)	355(14)	296(13)	343(15)	-57(11)	-92(11)	162(11)
C(6)	288(13)	252(12)	449(16)	-15(11)	-103(12)	131(11)
C(7)	288(13)	315(13)	345(14)	47(11)	5(11)	163(11)
C(8)	260(12)	275(12)	286(13)	35(10)	-17(10)	155(10)
C(9)	241(12)	258(11)	247(13)	21(9)	13(9)	132(10)
C(10)	281(13)	271(12)	277(14)	7(11)	13(10)	85(11)
C(11)	294(13)	397(15)	336(16)	-2(12)	48(11)	109(11)
C(12)	288(14)	572(19)	383(17)	39(15)	65(13)	71(14)
C(13)	337(15)	600(20)	317(16)	175(15)	22(13)	-27(14)
C(14)	370(16)	430(16)	377(17)	135(13)	-56(13)	57(13)
C(15)	309(13)	244(11)	255(13)	25(10)	-11(10)	141(10)
C(16)	344(14)	272(13)	465(18)	-30(12)	61(12)	122(11)
C(17)	523(18)	297(14)	530(19)	-105(13)	42(15)	198(14)
C(18)	381(15)	249(13)	503(19)	-59(12)	5(13)	79(12)
C(19)	311(13)	281(13)	353(15)	-6(11)	6(11)	99(11)
O(2A)	330(20)	308(18)	219(18)	94(15)	-19(13)	133(16)
O(3A)	1020(30)	344(17)	510(20)	45(14)	30(19)	272(18)
C(20Å)	510(20)	490(20)	350(20)	111(19)	111(18)	350(20)
C(21A)	650(30)	830(40)	580(30)	10(30)	-220(30)	560(30)

**Table S7.** Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LCo<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2$ [ h<sup>2</sup>a<sup>\*2</sup>U<sup>11</sup> + ... + 2 h k a\* b\* U<sup>12</sup> ]

Figure S13. Structural drawing of LNi<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids.



Special refinement details for LNi<sub>3</sub>(OAc)<sub>3</sub>. Crystals were mounted on a glass fiber using Paratone oil then placed on the diffractometer under a nitrogen stream at 100K. The molecule sits around a 3-fold axis. The bound acetate displays two bonding modes, both mono- and bidentate. The populations of both modes were refined to a ratio of 74:26 respectively. The bidentate mode places one oxygen and the methyl group nearly on the 3-fold axis and so can not be present more than 1/3<sup>rd</sup> of the time. A refined population of 26% suggest a mixture in the crystal with a species where all three acetate ligands are mono-dentate. Refinement of  $F^2$  against ALL reflections. The weighted R-factor (wR) and goodness of fit (S) are based on  $F^2$ , conventional Rfactors (R) are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2s($  $F^2$ ) is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

	Х	у	Z	U <sub>eq</sub>	Occ
$\overline{\text{Ni}(1)}$	7212(1)	4357(1)	643(1)	27(1)	1
O(1)	6222(1)	3797(1)	1598(2)	22(1)	1
N(1)	8318(2)	4786(2)	-42(3)	33(1)	1
N(2)	7215(1)	5198(1)	1645(2)	29(1)	1
C(1)	7243(2)	3184(2)	4128(2)	26(1)	1
C(2)	7403(2)	3913(2)	4115(3)	25(1)	1
C(3)	8184(2)	4557(2)	3974(3)	25(1)	1
C(4)	8466(2)	5074(2)	4933(3)	31(1)	1
C(5)	9175(2)	5703(2)	4860(3)	34(1)	1
C(6)	9611(2)	5818(2)	3780(3)	30(1)	1
C(7)	9331(2)	5300(2)	2833(3)	29(1)	1
C(8)	8620(2)	4660(2)	2877(3)	26(1)	1
C(9)	8331(2)	4106(2)	1774(3)	26(1)	1
C(10)	8709(2)	4524(2)	551(3)	34(1)	1
C(11)	9383(2)	4628(2)	50(3)	40(1)	1
C(12)	9643(2)	5000(2)	-1072(3)	53(1)	1
C(13)	9245(2)	5272(2)	-1688(3)	57(1)	1
C(14)	8592(2)	5169(2)	-1163(3)	50(1)	1
C(15)	6526(2)	5048(2)	2024(3)	29(1)	1
C(16)	6405(2)	5586(2)	2571(3)	38(1)	1
C(17)	7028(2)	6295(2)	2764(4)	48(1)	1
C(18)	7726(2)	6454(2)	2396(3)	42(1)	1
C(19)	7790(2)	5875(2)	1824(3)	34(1)	1
O(2A)	6859(3)	4648(3)	-966(4)	27(1)	0.741(2)
O(3A)	7563(2)	5889(2)	-1154(4)	72(1)	0.741(2)
C(20A)	7072(3)	5260(3)	-1553(6)	53(2)	0.741(2)
C(21A)	6790(3)	5265(3)	-2908(5)	65(2)	0.741(2)
O(2B)	7666(10)	3181(10)	-1321(15)	54(6)	0.259(2)
O(3B)	6790(6)	3330(10)	-520(4)	2(2)	0.259(2)
C(20B)	7163(6)	3318(6)	-1391(10)	17(2)	0.259(2)
C(21B)	7019(6)	3471(8)	-2598(10)	30(3)	0.259(2)

**Table S8**. Atomic coordinates (  $x \ 10^4$ ) and equivalent isotropic displacement parameters (Å<sup>2</sup>x 10<sup>3</sup>) for LNi<sub>3</sub>(OAc)<sub>3</sub>. U(eq) is defined as the trace of the orthogonalized U<sup>ij</sup> tensor.

**Table S9**. Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LNi<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2$ [ h<sup>2</sup>a<sup>\*2</sup>U<sup>11</sup> + ... + 2 h k a\* b\* U<sup>12</sup> ]

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
 Ni(1)	281(2)	244(2)	292(2)	26(2)	-19(2)	134(2)
O(1)	229(12)	213(12)	230(13)	7(10)	7(10)	116(10)
N(1)	367(17)	293(16)	260(16)	27(13)	-46(14)	103(14)
N(2)	299(15)	263(15)	269(16)	-25(12)	-9(13)	109(13)
C(1)	275(18)	344(18)	201(17)	-8(14)	-13(13)	186(16)
C(2)	322(18)	256(17)	122(15)	28(13)	21(13)	106(15)
C(3)	287(18)	244(17)	255(18)	-4(14)	-64(14)	157(14)
C(4)	380(20)	333(19)	232(18)	-38(15)	-64(15)	198(17)
C(5)	322(19)	275(18)	400(20)	-49(16)	-132(16)	135(16)
C(6)	300(18)	257(18)	350(20)	-9(16)	-115(16)	150(16)

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C(7)	282(19)	317(19)	281(18)	117(15)	3(15)	150(16)
C(8)	258(18)	252(17)	315(19)	42(15)	-19(15)	153(15)
C(9)	316(19)	274(17)	221(18)	42(13)	50(14)	173(15)
C(10)	310(20)	298(19)	330(20)	-48(16)	-2(15)	88(17)
C(11)	280(19)	430(20)	370(20)	-29(18)	79(17)	89(17)
C(12)	270(20)	660(30)	380(20)	-10(20)	68(18)	20(20)
C(13)	340(20)	750(30)	240(20)	180(20)	31(17)	-10(20)
C(14)	510(30)	430(20)	310(20)	104(18)	-24(19)	70(20)
C(15)	331(19)	273(18)	271(19)	12(14)	-21(15)	162(16)
C(16)	330(20)	266(19)	490(20)	-3(17)	106(18)	111(17)
C(17)	600(30)	310(20)	540(30)	-103(18)	40(20)	240(20)
C(18)	360(20)	290(20)	590(30)	-38(18)	60(18)	134(17)
C(19)	292(19)	330(20)	320(20)	4(16)	-9(16)	92(16)
O(2A)	350(20)	310(20)	190(20)	100(20)	18(18)	192(19)
O(3A)	1060(40)	420(20)	580(30)	-10(20)	20(20)	280(20)
C(20A)	560(40)	500(40)	690(40)	190(30)	270(30)	380(30)
C(21A)	770(40)	820(40)	640(40)	-190(30)	-460(30)	610(40)

Figure S14. Structural drawing of LCu<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids.



Special refinement details for  $LCu_3(OAc)_3$ . Crystals were mounted on a glass fiber using Paratone oil then placed on the diffractometer under a nitrogen stream at 100K. Presumably the solvent region of the crystal contains an acetate which would balance the charge on the Cu complex. Approximately 32% of the unit cell volume contains potential solvent. Electron

density in this space is poorly defined suggesting disorder and a suitable solvent model was not obtained. SQUEEZE<sup>4</sup> was employed to produce a bulk solvent correction which accounted for 964 electrons which is a good fit to two chloroform and one acetate per unit cell. Refinement of  $F^2$  against ALL reflections. The weighted R-factor (*w*R) and goodness of fit (S) are based on  $F^2$ , conventional R-factors (R) are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Table S10.	Atomic coordinates (x 104) and equivalent isotropic displacement parameters (Å2	K
10 <sup>3</sup> ) for LCu	$U_3(OAc)_3$ . U(eq) is defined as the trace of the orthogonalized U <sup>ij</sup> tensor.	

	Х	У	Z	U <sub>eq</sub>
$\overline{\mathrm{Cu}(1)}$	3111(1)	5800(1)	1289(1)	25(1)
Cu(2)	4625(1)	6570(1)	1052(1)	25(1)
Cu(3)	3921(1)	6865(1)	1838(1)	24(1)
O(1)	3605(1)	6386(1)	929(1)	20(1)
O(2)	4266(1)	7299(1)	1384(1)	21(1)
O(3)	2984(1)	6595(1)	1615(1)	21(1)
O(4)	3704(2)	5209(1)	1675(1)	29(1)
O(5)	4571(2)	5997(1)	1797(1)	30(1)
O(6)	4951(2)	5606(1)	982(1)	33(1)
O(7)	5721(2)	5748(2)	515(1)	52(1)
N(1)	3335(2)	5069(2)	905(1)	28(1)
N(2)	4520(2)	6828(2)	457(1)	26(1)
N(3)	5554(2)	6946(2)	1262(1)	27(1)
N(4)	4143(2)	7822(2)	2038(1)	24(1)
N(5)	3480(2)	6394(2)	2285(1)	24(1)
N(6)	2095(2)	5631(2)	1445(1)	24(1)
C(1)	2196(2)	7444(2)	1158(1)	22(1)
C(2)	2514(2)	7367(2)	816(1)	20(1)
C(3)	3097(2)	7763(2)	734(1)	21(1)
C(4)	3399(2)	8207(2)	997(1)	21(1)
C(5)	3079(2)	8283(2)	1342(1)	21(1)
C(6)	2480(2)	7883(2)	1428(1)	20(1)
C(7)	2263(2)	6801(2)	567(1)	23(1)
C(8)	1556(2)	6801(2)	464(1)	39(1)
C(9)	1242(3)	6292(3)	239(1)	45(1)
C(10)	1666(3)	5768(3)	118(1)	41(1)
C(11)	2367(2)	5735(2)	222(1)	31(1)
C(12)	2682(2)	6243(2)	451(1)	23(1)
C(13)	4093(2)	8538(2)	916(1)	22(1)
C(14)	4142(2)	8998(2)	613(1)	27(1)
C(15)	4762(2)	9328(2)	514(1)	33(1)
C(16)	5367(2)	9199(2)	712(1)	33(1)

C(17)	5350(2)	8735(2)	1011(1)	27(1)
C(18)	4717(2)	8390(2)	1113(1)	23(1)
C(19)	2219(2)	7868(2)	1815(1)	23(1)
C(20)	2021(2)	8504(2)	1979(1)	31(1)
C(21)	1791(2)	8531(2)	2338(1)	41(1)
C(22)	1726(3)	7921(2)	2544(1)	40(1)
C(23)	1918(2)	7291(2)	2387(1)	32(1)
C(24)	2173(2)	7244(2)	2025(1)	23(1)
C(25)	3466(2)	6138(2)	567(1)	22(1)
C(26)	4744(2)	7857(2)	1446(1)	21(1)
C(27)	2463(2)	6510(2)	1888(1)	24(1)
C(28)	3598(2)	5343(2)	586(1)	25(1)
C(29)	3898(2)	4926(2)	314(1)	37(1)
C(30)	3919(3)	4213(2)	368(1)	50(2)
C(31)	3650(3)	3930(2)	694(1)	53(2)
C(32)	3377(2)	4369(2)	958(1)	42(1)
C(33)	3956(2)	6525(2)	301(1)	23(1)
C(34)	3813(2)	6588(2)	-72(1)	28(1)
C(35)	4249(3)	6985(2)	-290(1)	36(1)
C(36)	4829(2)	7309(2)	-127(1)	36(1)
C(37)	4949(2)	7213(2)	244(1)	30(1)
C(38)	5477(2)	7529(2)	1473(1)	23(1)
C(39)	6035(2)	7788(2)	1680(1)	31(1)
C(40)	6686(2)	7455(3)	1674(1)	36(1)
C(41)	6748(2)	6859(3)	1456(1)	41(1)
C(42)	6171(3)	6619(2)	1253(1)	40(1)
C(43)	4523(2)	8220(2)	1807(1)	23(1)
C(44)	4662(2)	8908(2)	1891(1)	26(1)
C(45)	4362(2)	9200(2)	2205(1)	28(1)
C(46)	3941(2)	8801(2)	2427(1)	28(1)
C(47)	3859(2)	8106(2)	2339(1)	28(1)
C(48)	2824(2)	6152(2)	2224(1)	22(1)
C(49)	2515(2)	5653(2)	2451(1)	30(1)
C(50)	2884(3)	5420(2)	2755(1)	38(1)
C(51)	3548(3)	5691(2)	2820(1)	36(1)
C(52)	3834(2)	6168(2)	2581(1)	28(1)
C(53)	1873(2)	6052(2)	1724(1)	22(1)
C(54)	1173(2)	6079(2)	1830(1)	30(1)
C(55)	681(2)	5670(2)	1644(1)	34(1)
C(56)	907(2)	5252(2)	1348(1)	33(1)
C(57)	1611(2)	5245(2)	1264(1)	29(1)
C(58)	4303(3)	5370(2)	1774(1)	33(1)
C(59)	4803(2)	4790(2)	1879(1)	57(2)
C(60)	5411(3)	5393(3)	743(2)	44(1)
C(61)	5557(3)	4634(3)	773(2)	103(3)

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
$\frac{1}{C_{\rm P}(1)}$	220(2)	100(2)	249(2)	42(2)	72(2)	20(2)
Cu(1) Cu(2)	320(3)	100(3) 185(3)	240(3) 276(3)	-42(3)	73(3)	-39(3)
Cu(2) Cu(3)	207(3) 316(3)	105(3)	270(3)	-30(2)	42(3)	-7(3)
O(1)	270(18)	155(5) 157(17)	180(16)	21(12)	21(3) 35(13)	-23(3)
O(1)	270(18) 252(17)	137(17) 186(17)	180(10) 182(16)	-21(12) 18(12)	33(13) 30(13)	-2(13) -2(14)
O(2)	232(17) 230(17)	180(17) 181(16)	211(15)	24(13)	50(13) 63(13)	-34(14) 21(14)
O(3)	230(17) 300(20)	227(19)	358(19)	-24(13) 14(14)	-38(16)	-27(14)
O(4)	330(20)	100(18)	376(18)	20(14)	-50(10)	-37(10) 33(15)
O(5)	370(20)	199(18) 190(18)	430(20)	20(14) 76(15)	95(16)	18(15)
O(0)	570(20) 540(30)	600(30)	430(20)	-17(19)	201(19)	90(20)
N(1)	370(30)	180(20)	280(20)	-51(17)	66(19)	-44(18)
N(1) N(2)	370(30) 340(20)	160(20)	280(20)	-19(17)	109(19)	-44(18)
N(2) N(3)	260(20)	220(20)	340(20)	-19(17) 7(18)	34(18)	-0(19) 18(18)
N(3) N(4)	200(20) 350(20)	220(20) 210(20)	160(20)	26(16)	34(10) 3(17)	53(18)
N(4) N(5)	330(20)	210(20) 200(20)	100(20) 190(20)	-20(10)	-3(17) 52(18)	-33(10)
N(5) N(6)	300(20)	100(20)	150(20)	1/(10) 10(17)	32(10) 25(18)	21(18)
C(1)	200(20)	190(20) 180(30)	230(20) 280(30)	-10(17) 10(20)	23(10) 40(20)	-21(18)
C(1)	200(30) 220(30)	170(30)	230(30)	10(20) 30(10)	-40(20)	60(20)
C(2)	220(30) 310(30)	170(30) 130(20)	180(20)	-39(19) 18(10)	-30(20)	60(20)
C(3)	270(30)	130(20) 130(20)	230(20)	87(19)	10(20)	40(20)
C(4)	270(30) 280(30)	130(20) 110(20)	250(20)	22(19)	-10(20)	40(20) 30(20)
C(5)	250(30)	110(20) 140(20)	230(20) 220(30)	-22(19)	10(20)	100(20)
C(0)	230(30) 210(30)	240(30)	220(30) 240(20)	-0(1)	20(20)	0(20)
C(7)	210(30) 430(30)	240(30) 330(30)	240(20)	110(20)	-20(20)	140(30)
C(0)	360(30)	460(40)	520(30)	-230(30)	-160(30)	70(30)
C(10)	530(40)	390(30)	310(30)	-130(20)	-120(30)	-120(30)
C(10)	380(30)	300(30)	270(30)	-60(20)	60(20)	20(30)
C(12)	300(30)	220(30)	170(20)	-60(20)	20(20)	-70(20)
C(12) C(13)	310(30)	160(20)	200(20)	-47(19)	10(20)	0(20)
C(13)	350(30)	210(30)	250(20)	10(20)	-30(20)	40(20)
C(14)	450(30)	290(30)	260(30)	70(20)	40(20)	0(20)
C(15)	350(30)	320(30)	330(30)	70(20)	120(20)	-80(30)
C(17)	330(30)	220(30)	260(30)	0(20)	10(20)	20(20)
C(18)	360(30)	130(20)	190(20)	-32(19)	60(20)	-10(20)
C(19)	240(30)	200(30)	250(30)	-20(20)	-30(20)	10(20)
C(20)	450(30)	260(30)	210(30)	-20(20)	60(20)	30(20)
C(21)	560(40)	260(30)	410(30)	-120(20)	110(30)	70(30)
C(22)	650(40)	310(30)	230(30)	-30(20)	160(30)	20(30)
C(23)	440(30)	260(30)	270(30)	10(20)	140(20)	20(20)
C(24)	270(30)	240(30)	190(20)	-70(20)	10(20)	20(20)
C(25)	320(30)	150(20)	190(20)	-60(20)	80(20)	-30(20)
C(26)	280(30)	140(20)	200(20)	-24(19)	10(20)	-50(20)
C(27)	250(30)	220(30)	240(30)	-20(20)	60(20)	-60(20)
C(28)	290(30)	230(30)	240(30)	-60(20)	20(20)	-60(20)
C(29)	570(40)	180(30)	350(30)	-40(20)	180(30)	0(30)
C(30)	840(40)	220(30)	440(30)	-130(20)	240(30)	0(30)
C(31)	940(50)	130(30)	510(30)	-60(30)	350(30)	-50(30)
C(32)	650(40)	230(30)	390(30)	0(20)	200(30)	-120(30)

**Table S11.** Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LCu<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2 [h^2a^{*2}U^{11} + ... + 2h k a^* b^* U^{12}]$ .

C(33)	290(30)	140(20)	260(30)	-50(20)	80(20)	0(20)
C(34)	400(30)	200(30)	230(30)	-30(20)	40(20)	-80(20)
C(35)	520(40)	290(30)	250(30)	-20(20)	50(30)	30(30)
C(36)	390(30)	250(30)	420(30)	0(20)	190(30)	0(20)
C(37)	310(30)	240(30)	350(30)	-50(20)	80(20)	-30(20)
C(38)	260(30)	200(30)	230(30)	60(20)	30(20)	-50(20)
C(39)	370(30)	310(30)	250(30)	0(20)	0(20)	0(30)
C(40)	310(30)	480(40)	290(30)	50(20)	-30(20)	-40(30)
C(41)	260(30)	400(30)	580(30)	50(30)	30(30)	90(30)
C(42)	320(30)	320(30)	570(30)	-30(30)	60(30)	30(30)
C(43)	300(30)	210(30)	170(20)	0(20)	-20(20)	-10(20)
C(44)	350(30)	200(30)	230(30)	20(20)	0(20)	-40(20)
C(45)	430(30)	210(30)	210(30)	-10(20)	-80(20)	-20(20)
C(46)	350(30)	300(30)	190(20)	-20(20)	10(20)	-10(20)
C(47)	370(30)	230(30)	230(20)	-40(20)	30(20)	-70(20)
C(48)	330(30)	160(30)	180(20)	-10(20)	50(20)	70(20)
C(49)	320(30)	280(30)	290(30)	30(20)	30(20)	-10(20)
C(50)	540(40)	280(30)	330(30)	150(20)	140(30)	120(30)
C(51)	390(30)	400(30)	280(30)	100(20)	-30(20)	160(30)
C(52)	320(30)	290(30)	240(30)	10(20)	10(20)	70(20)
C(53)	290(30)	140(20)	230(30)	39(19)	50(20)	-30(20)
C(54)	370(30)	210(30)	320(30)	-40(20)	40(20)	-10(20)
C(55)	250(30)	290(30)	490(30)	20(20)	100(20)	-70(20)
C(56)	380(30)	210(30)	400(30)	-40(20)	50(20)	-100(20)
C(57)	340(30)	190(30)	330(30)	-30(20)	50(20)	-40(20)
C(58)	470(40)	180(30)	330(30)	60(20)	80(30)	80(30)
C(59)	450(40)	240(30)	1030(50)	50(30)	-210(30)	30(30)
C(60)	440(40)	260(30)	600(40)	-250(30)	10(30)	100(30)
C(61)	1010(60)	350(40)	1740(70)	-210(40)	640(50)	180(40)



Figure S15. Structural drawing of LZn<sub>3</sub>(OAc)<sub>3</sub> with 50% thermal probability ellipsoids.

Special refinement details for LZn<sub>3</sub>(OAc)<sub>3</sub>. Crystals were mounted in a loop using oil then placed on the diffractometer under a nitrogen stream at 100K. Presumably the solvent region of the crystal contains an acetate which would balance the charge on the Zn complex. Approximately 31% of the unit cell volume contains potential solvent. Electron density in this space is poorly defined suggesting disorder and a suitable solvent model was not obtained. SQUEEZE<sup>4</sup> was employed to produce a bulk solvent correction which accounted for 1066 electrons which is a good fit to two chloroform and one acetate per unit cell. Refinement of  $F^2$ against ALL reflections. The weighted R-factor (wR) and goodness of fit (S) are based on  $F^2$ , conventional R-factors (R) are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

·····	X	у	Z	U <sub>eq</sub>
$\overline{Zn(1)}$	3194(1)	5747(1)	1307(1)	22(1)
Zn(2)	4668(1)	6594(1)	999(1)	22(1)
Zn(3)	3957(1)	6853(1)	1845(1)	22(1)
O(1)	3596(2)	6343(2)	915(1)	18(1)
O(2)	4338(2)	7297(2)	1370(1)	19(1)
O(3)	3044(2)	6602(2)	1660(1)	18(1)
O(4)	3802(2)	5196(2)	1658(1)	24(1)
O(5)	4586(2)	6002(2)	1865(1)	25(1)
O(6)	4991(2)	5607(2)	1064(1)	$\frac{28(1)}{28(1)}$
O(7)	5696(2)	5706(2)	569(1)	45(1)
N(1)	3387(2)	4969(2)	854(1)	27(1)
N(2)	4520(2)	6808(2)	445(1)	21(1)
N(2)	5652(2)	7076(2)	1202(1)	21(1) 28(1)
N(4)	4181(2)	7848(2)	2038(1)	20(1)
N(5)	3457(2)	6394(2)	2357(1)	25(1)
N(6)	2147(2)	5653(2)	1444(1)	23(1)
C(1)	2147(2) 2209(3)	7412(2)	1160(2)	23(1) 21(2)
C(1)	2200(3) 2523(3)	7338(3)	816(2)	19(1)
C(2)	2020(3)	7330(3) 7740(2)	724(2)	$\frac{1}{22(2)}$
C(3)	3390(3)	8190(2)	$\frac{724(2)}{080(2)}$	22(2) 21(1)
C(4)	3085(3)	8190(2) 8264(2)	1330(2)	21(1) 21(1)
C(5)	3083(3)	$\frac{3204(2)}{7863(2)}$	1339(2) 1431(2)	21(1) 21(2)
C(0)	2404(3)	7803(2)	560(2)	21(2) 22(1)
C(7)	1548(3)	674(3)	309(2)	23(1) 36(2)
$C(\delta)$	1346(3) 1246(3)	6740(3)	407(2) 241(2)	30(2)
C(3)	1240(3) 1670(3)	5702(3)	241(2) 110(2)	38(2)
C(10)	10/0(3)	5702(3)	119(2) 207(1)	38(2)
C(11)	2502(5)	5074(5)	207(1) 441(2)	20(2)
C(12)	2090(3)	0193(3)	441(2)	23(2)
C(13)	40/2(3)	0.000(2)	899(2) 599(2)	21(1) 26(2)
C(14)	4003(3)	9000(2)	388(2) 478(2)	20(2)
C(15)	4097(3)	9340(3)	478(2)	29(2)
C(10)	5293(3) 5200(3)	9230(3)	073(2) 073(2)	29(2)
C(17)	3309(3) 4708(3)	8432(2)	973(2)	23(1) 10(1)
C(10)	4/06(3)	0432(2)	1094(1) 1921(2)	19(1)
C(19)	2227(3)	/809(3)	1821(2) 1072(2)	19(1)
C(20)	2014(3) 1772(2)	8318(3)	1973(2)	$\frac{2}{2}$
C(21)	1/2(3) 1724(2)	$\frac{8370(3)}{7072(2)}$	2521(2)	34(2)
C(22)	1/34(3) 1054(2)	7972(3)	2342(2)	38(2) 20(2)
C(23)	1934(3)	7319(3) 7259(2)	2390(2)	30(2)
C(24)	2203(3) 2484(2)	(238(3))	2040(2)	21(2) 10(1)
C(25)	3464(3)	$\frac{010}{(3)}$	334(2)	19(1)
C(20)	4/04(3)	/890(3)	1428(2)	22(2)
C(27)	2502(3)	5388(3)	1914(2)	23(2)
$C(2\delta)$	3044(3) 2072(2)	5288(3)	540(2)	23(2)
C(29)	<i>39/2(3)</i>	4935(3)	20/(2)	55(2) 52(2)
C(30)	4029(4)	4219(3)	294(2)	55(2) (5(2)
C(31)	5/62(4)	3870(3) 4250(2)	603(2) 979(2)	65(3) 44(2)
C(32)	5458(3)	4259(3)	8/8(2)	44(2)

**Table S12.** Atomic coordinates (  $x \ 10^4$ ) and equivalent isotropic displacement parameters (Å<sup>2</sup>x 10<sup>3</sup>) for LZn<sub>3</sub>(OAc)<sub>3</sub>. U(eq) is defined as the trace of the orthogonalized U<sup>ij</sup> tensor.

C(33)	3952(3)	6514(2)	290(2)	19(1)
C(34)	3807(3)	6606(2)	-73(2)	26(2)
C(35)	4234(3)	7025(3)	-280(2)	32(2)
C(36)	4816(3)	7338(3)	-120(2)	33(2)
C(37)	4946(3)	7213(3)	242(2)	25(2)
C(38)	5526(3)	7615(3)	1450(2)	24(2)
C(39)	6053(3)	7860(3)	1688(2)	28(2)
C(40)	6709(3)	7563(3)	1677(2)	37(2)
C(41)	6823(3)	7017(3)	1425(2)	46(2)
C(42)	6289(3)	6790(3)	1189(2)	44(2)
C(43)	4540(3)	8248(3)	1805(2)	22(1)
C(44)	4663(3)	8960(2)	1881(2)	24(1)
C(45)	4387(3)	9253(3)	2196(2)	28(2)
C(46)	3991(3)	8837(3)	2419(2)	25(2)
C(47)	3905(3)	8144(3)	2333(1)	22(1)
C(48)	2815(3)	6138(3)	2258(2)	25(2)
C(49)	2480(3)	5590(3)	2452(2)	32(2)
C(50)	2809(4)	5327(3)	2760(2)	41(2)
C(51)	3454(3)	5612(3)	2866(2)	37(2)
C(52)	3764(3)	6130(3)	2655(2)	30(2)
C(53)	1916(3)	6069(3)	1724(2)	20(1)
C(54)	1224(3)	6097(3)	1822(2)	28(2)
C(55)	752(3)	5712(3)	1622(2)	34(2)
C(56)	960(3)	5302(3)	1326(2)	32(2)
C(57)	1674(3)	5278(2)	1246(2)	28(2)
C(58)	4369(3)	5377(3)	1810(2)	26(2)
C(59)	4826(3)	4784(2)	1939(2)	37(2)
C(60)	5426(4)	5373(3)	817(2)	39(2)
C(61)	5586(4)	4581(3)	862(2)	86(3)

**Table S13.** Anisotropic displacement parameters (Å<sup>2</sup>x 10<sup>4</sup>) for LZn<sub>3</sub>(OAc)<sub>3</sub>. The anisotropic displacement factor exponent takes the form:  $-2\pi^2$ [  $h^2a^{*2}U^{11} + ... + 2 h k a^* b^* U^{12}$ ].

	U <sup>11</sup>	U <sup>22</sup>	U <sup>33</sup>	U <sup>23</sup>	U <sup>13</sup>	U <sup>12</sup>
$\overline{Zn(1)}$	250(4)	185(3)	210(4)	-11(3)	32(4)	-18(3)
Zn(2)	245(4)	197(3)	226(4)	-22(3)	26(4)	-7(3)
Zn(3)	249(4)	203(3)	212(4)	-4(3)	14(4)	-22(3)
O(1)	220(20)	164(19)	140(20)	-15(16)	-7(19)	6(16)
O(2)	200(20)	180(19)	190(30)	-23(17)	7(19)	-46(17)
O(3)	200(20)	178(19)	160(20)	-1(17)	46(19)	-23(18)
O(4)	290(30)	180(20)	250(30)	12(17)	20(20)	13(19)
O(5)	290(20)	180(20)	290(30)	30(18)	40(20)	10(19)
O(6)	320(30)	160(20)	360(30)	-20(18)	60(20)	43(18)
O(7)	510(30)	480(30)	350(30)	20(20)	200(30)	120(20)
N(1)	350(30)	160(30)	300(40)	-60(20)	10(30)	20(20)
N(2)	260(30)	170(20)	200(30)	30(20)	80(20)	30(20)
N(3)	210(30)	250(30)	380(40)	0(20)	20(30)	0(20)
N(4)	260(30)	210(30)	130(30)	20(20)	0(20)	-70(20)
N(5)	300(30)	200(30)	240(30)	-20(20)	30(30)	20(20)
N(6)	280(30)	180(30)	240(30)	10(20)	10(30)	-40(20)
C(1)	140(30)	130(30)	350(40)	-10(30)	-120(30)	10(30)

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(2)	180(40)	180(30)	210(40)	-40(30)	-60(30)	30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(3)	270(40)	180(30)	200(40)	0(30)	-40(30)	0(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(4)	240(40)	120(30)	280(40)	90(30)	30(30)	30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(5)	220(40)	110(30)	310(40)	-10(30)	30(30)	20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(6)	170(30)	110(30)	360(40)	20(30)	-20(30)	70(30)
$\begin{array}{c} C(8) & 250(40) & 330(40) & 510(50) & -270(30) & -160(40) & 500(30) \\ C(9) & 290(40) & 350(40) & 510(50) & -270(30) & -160(40) & 500(30) \\ C(10) & 470(50) & 350(40) & 300(40) & -120(30) & -180(40) & -110(40) \\ C(11) & 440(40) & 230(30) & 150(40) & -60(30) & 100(30) & -30(30) \\ C(12) & 290(40) & 180(30) & 180(40) & -100(30) & 40(30) & 20(30) \\ C(13) & 270(40) & 180(30) & 180(40) & -100(30) & 40(30) & 70(30) \\ C(15) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 100(30) \\ C(15) & 250(40) & 280(30) & 340(40) & 140(30) & 150(30) & -20(30) \\ C(16) & 250(40) & 280(30) & 310(40) & -30(30) & 0(30) & 10(30) \\ C(18) & 290(40) & 130(30) & 140(40) & -10(20) & 10(30) & 20(30) \\ C(19) & 170(30) & 220(30) & 180(40) & -40(30) & 20(30) & -20(30) \\ C(21) & 450(40) & 230(30) & 210(40) & -10(30) & 40(30) & -10(30) \\ C(21) & 450(40) & 230(30) & 230(40) & -90(30) & 30(40) & 20(30) \\ C(21) & 450(40) & 250(30) & 280(40) & 40(30) & 100(30) & -20(30) \\ C(24) & 210(40) & 250(30) & 280(40) & 40(30) & 100(30) & -20(30) \\ C(25) & 220(40) & 160(30) & 180(40) & -30(30) & 80(30) & -50(30) \\ C(25) & 220(40) & 160(30) & 180(40) & -20(30) & 10(30) & -50(30) \\ C(26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -50(30) \\ C(27) & 260(40) & 220(30) & 220(40) & -30(30) & 80(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & -10(30) & 150(40) & 90(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 160(40) & 20(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 20(40) & -30(30) & 30(30) & -60(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(31) & 1160(70) & 140(30) & 210(40) & -10(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 120(40) & -20(30) & 10(30) & -50(30) \\ C(33) & 20(40) & 30(40) & 120(40) & -20(30) & 10(30) & -30(30) \\ C(31) & 1160(7) & 140(30) & 20(40) & -00(30) & 10(30) & -30(30) \\ C(31) & 150(40) & 200(30) & 20(40) & -70(30) & 10(30) & -70(30) \\ C(44) & 280(40) & 20(30) & 20(40) & -70$	C(7)	280(40)	230(30)	170(40)	10(30)	-40(30)	-20(30)
$\begin{array}{c} C(9) & 290(40) & 350(40) & 510(50) & -270(30) & -160(40) & 50(30) \\ C(10) & 470(50) & 360(40) & 300(40) & -120(30) & -180(40) & -1010(40) \\ C(11) & 440(40) & 230(30) & 150(40) & -60(30) & -30(30) & -20(30) \\ C(12) & 290(40) & 220(30) & 170(40) & 60(30) & 10(30) & -30(30) \\ C(13) & 270(40) & 180(30) & 180(40) & -100(30) & 40(30) & 70(30) \\ C(14) & 370(40) & 210(30) & 180(40) & -100(30) & 40(30) & 70(30) \\ C(15) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 10(30) \\ C(16) & 260(40) & 280(30) & 340(40) & 140(30) & 150(30) & -20(30) \\ C(17) & 170(30) & 280(30) & 310(40) & -30(30) & 0(30) & 10(30) \\ C(18) & 290(40) & 130(30) & 140(40) & -10(20) & 10(30) & 20(30) \\ C(20) & 350(40) & 230(30) & 210(40) & -40(30) & 20(30) & -20(30) \\ C(21) & 450(40) & 230(30) & 230(40) & -90(30) & 30(40) & 20(30) \\ C(22) & 470(50) & 430(40) & 230(40) & -90(30) & 150(40) & -10(40) \\ C(23) & 370(40) & 250(30) & 280(40) & 40(30) & 150(40) & -10(40) \\ C(23) & 370(40) & 250(30) & 280(40) & -90(30) & 10(30) & -30(30) \\ C(24) & 210(40) & 200(30) & 220(40) & -03(30) & 80(30) & -60(30) \\ C(25) & 220(40) & 160(30) & 180(40) & -0(30) & 10(30) & -30(30) \\ C(26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -30(30) \\ C(27) & 260(40) & 220(30) & 220(40) & -30(30) & 80(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -30(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 80(30) & -60(30) \\ C(30) & 960(50) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 210(40) & -10(30) & 180(40) & -10(30) \\ C(32) & 730(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(32) & 730(50) & 140(30) & 20(40) & -10(30) & 10(30) & -30(30) \\ C(33) & 240(40) & 160(30) & 160(40) & -10(30) & 10(30) & -30(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & 10(30) & -30(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -00(30) & 10(30) & -30(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -60(30) & 30(30) & -00(30) \\ C(44) & 380(40) & 220(30) & 250(40) & 30(30) & -50(30) & 10(30) \\ C(44) & 380(40) & 220(30) & 2$	C(8)	250(40)	330(40)	510(50)	-50(30)	10(40)	140(30)
$\begin{array}{c} C(1) & 470(50) & 560(40) & 510(50) & -100(50) & -180(10) & -180(10) \\ C(11) & 440(40) & 230(30) & 150(40) & -60(30) & -30(30) & -20(30) \\ C(12) & 290(40) & 220(30) & 170(40) & 60(30) & 40(30) & 20(30) \\ C(13) & 270(40) & 180(30) & 180(40) & 30(30) & -40(30) & 70(30) \\ C(14) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 70(30) \\ C(15) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 70(30) \\ C(16) & 260(40) & 280(30) & 310(40) & -30(30) & 0(30) & 10(30) \\ C(17) & 170(30) & 280(30) & 310(40) & -30(30) & 0(30) & 10(30) \\ C(18) & 290(40) & 130(30) & 140(40) & -10(20) & 10(30) & 20(30) \\ C(19) & 170(30) & 220(30) & 180(40) & -40(30) & 20(30) & -20(30) \\ C(20) & 350(40) & 230(30) & 230(40) & -90(30) & 150(40) & -10(40) \\ C(21) & 450(40) & 230(30) & 230(40) & -90(30) & 150(40) & -10(40) \\ C(23) & 370(40) & 250(30) & 220(40) & -90(30) & 150(40) & -10(40) \\ C(24) & 210(40) & 200(30) & 220(40) & -90(30) & 150(40) & -20(30) \\ C(24) & 210(40) & 200(30) & 220(40) & -90(30) & 10(30) & -50(30) \\ C(25) & 220(40) & 160(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(26) & 170(40) & 190(30) & 310(40) & -20(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(31) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 30(50) & 90(30) \\ C(34) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -30(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & 10(30) & -30(30) \\ C(35) & 490(50) & 340(40) & 120(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 260(40) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 20(40) & -100(30) & 50(30) & 0(30) \\ C(35) & 490(50) & 330(40) & 330(50) & 180(30) & -70(30) \\ C(35) & 490(50) & 330(40) & 330(50) & 180(30) & -70(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & 50(30) & 0(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & 50(30) \\ C$	C(9)	290(40)	350(40)	510(50)	-270(30)	-160(40)	50(30)
$\begin{array}{c} C(1) & 100(10) & 200(10) & 100(10) & -60(30) & -30(30) & -20(30) \\ C(12) & 290(40) & 220(30) & 170(40) & 60(30) & 10(30) & -30(30) \\ C(13) & 270(40) & 180(30) & 180(40) & -100(30) & 40(30) & 70(30) \\ C(14) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 10(30) \\ C(15) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 10(30) \\ C(16) & 260(40) & 280(30) & 340(40) & 140(30) & 150(30) & -20(30) \\ C(17) & 170(30) & 220(30) & 180(40) & -30(30) & 0(30) & 10(30) \\ C(18) & 290(40) & 130(30) & 140(40) & -10(20) & 10(30) & 20(30) \\ C(20) & 350(40) & 230(30) & 210(40) & -10(30) & 40(30) & -10(30) \\ C(21) & 450(40) & 230(30) & 220(40) & -90(30) & 30(40) & 20(30) \\ C(22) & 470(50) & 430(40) & 230(40) & -90(30) & 150(40) & -10(30) \\ C(24) & 210(40) & 200(30) & 220(40) & -90(30) & 10(30) & -20(30) \\ C(25) & 220(40) & 160(30) & 180(40) & 0(30) & 10(30) & -50(30) \\ C(26) & 170(40) & 190(30) & 320(40) & -30(30) & 80(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ C(28) & 310(40) & 210(30) & 10(30) & 30(40) & 30(40) \\ C(31) & 160(70) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(31) & 160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(31) & 1160(70) & 140(30) & 20(30) & 10(30) & 20(30) & 0(30) \\ C(35) & 490(50) & 30(40) & 370(50) & 50(30) & 20(30) & -00(30) \\ C(35) & 490(50) & 30(40) & 370(50) & 50(30) & -90(40) & -10(30) \\ C(34) & 360(40) & 200(30) & 260(40) & 90(30) & 30(30) & 0(30) \\ C(35) & 490(50) & 30(40) & 20(60) & 100(40) & -80(30) \\ C(35) & 490(50) & 30(40) & 20(60) & 100(30) & 50(30) & 10(30) \\ C(34) & 300(40) & 260(30) & 120(40) & -60(30) & 30(30) & -20(30) \\ C(44) & 280(40) & 260(30) & 120(40) & -60(30) & 30(30) & -20(30) \\ C(45) & 360(40) & 200(30) & 200(40) & 30(30) & -60(40) & 80(30) \\ C(44) & 280$	C(10)	470(50)	360(40)	300(40)	-120(30)	-180(40)	-110(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(10)	440(40)	230(30)	150(40)	-60(30)	-30(30)	-20(30)
$\begin{array}{cccccc} (13) & 270(40) & 180(30) & 180(40) & -100(30) & 40(30) & 20(30) \\ (14) & 370(40) & 210(30) & 180(40) & 30(30) & -40(30) & 70(30) \\ (15) & 370(40) & 240(30) & 260(40) & 60(30) & 40(40) & 10(30) \\ (16) & 260(40) & 280(30) & 340(40) & 140(30) & 150(30) & -20(30) \\ (17) & 170(30) & 280(30) & 310(40) & -30(30) & 0(30) & 10(30) \\ (219) & 170(30) & 220(30) & 180(40) & -40(30) & 20(30) & -20(30) \\ (20) & 350(40) & 230(30) & 210(40) & -10(30) & 40(30) & -10(30) \\ (21) & 450(40) & 230(30) & 330(50) & -90(30) & 30(40) & 20(30) \\ (22) & 470(50) & 430(40) & 230(40) & -90(30) & 150(40) & -10(40) \\ (23) & 370(40) & 250(30) & 280(40) & 40(30) & 100(30) & -20(30) \\ (24) & 210(40) & 200(30) & 220(40) & -90(30) & 20(30) & -20(30) \\ (25) & 220(40) & 160(30) & 180(40) & -0(30) & 10(30) & -50(30) \\ (26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -50(30) \\ (26) & 170(40) & 210(30) & 180(40) & 40(30) & 10(30) & -50(30) \\ (26) & 170(40) & 210(30) & 180(40) & 40(30) & 10(30) & -60(30) \\ (23) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -60(30) \\ (23) & 310(40) & 210(30) & 180(40) & -10(30) & 150(40) & 90(30) \\ (23) & 30(40) & 210(30) & 180(40) & -10(30) & 150(40) & 90(30) \\ (23) & 30(40) & 210(30) & 180(40) & -10(30) & 150(40) & 90(30) \\ (23) & 30(40) & 200(30) & 20(40) & -10(30) & 150(40) & 90(30) \\ (23) & 230(40) & 300(40) & 120(40) & -10(30) & 180(40) & -00(30) \\ (33) & 240(40) & 160(30) & 160(40) & 20(30) & -10(30) & 80(30) \\ (34) & 360(40) & 200(30) & 260(40) & 90(30) & 30(30) & -00(30) \\ (35) & 490(50) & 340(40) & 120(40) & -20(30) & 10(30) & -30(30) \\ (35) & 490(50) & 340(40) & 120(40) & -20(30) & 10(30) & -30(30) \\ (34) & 260(40) & 240(30) & 370(50) & 50(30) & -90(40) & -20(40) \\ (33) & 240(40) & 350(40) & 250(40) & 20(30) & -50(30) & -60(30) \\ (34) & 260(40) & 350(40) & 250(40) & 20(30) & -50(30) & -60(30) \\ (35) & 490(50) & 330(40) & 30(50) & 180(30) & -50(30) & -60(30) \\ (34) & 360(40) & 230(40) & 30(50) & 180(30) & -50(30) & -60(30) \\ (35) & 260(40) & 330(40) & 30(50) & 180(30) & 10(30) & -60(30) \\ ($	C(12)	290(40)	220(30)	170(40)	60(30)	10(30)	-30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(12) C(13)	270(40) 270(40)	180(30)	170(40) 180(40)	-100(30)	40(30)	20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(13)	270(40) 370(40)	210(30)	180(40) 180(40)	30(30)	-40(30)	70(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(14)	370(40) 370(40)	210(30) 240(30)	260(40)	50(30) 60(30)	-40(30)	10(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(15)	260(40)	240(30) 280(30)	200(40) 340(40)	140(30)	150(30)	20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(10) C(17)	170(30)	280(30)	340(40) 310(40)	30(30)	0(30)	-20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(17)	170(30)	120(30)	140(40)	-30(30)	10(30)	20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(10)	170(30)	130(30) 220(30)	140(40) 180(40)	-10(20)	10(30)	20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(19)	170(30) 350(40)	220(30)	130(40) 210(40)	-40(30)	20(30)	-20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(20)	330(40)	230(30)	210(40) 220(50)	-10(30)	40(30) 20(40)	-10(30)
$\begin{array}{cccccc} (22) & 470(50) & 430(40) & 250(40) & -50(50) & 150(40) & -10(40) \\ (223) & 370(40) & 250(30) & 280(40) & 40(30) & 100(30) & -20(30) \\ (24) & 210(40) & 200(30) & 220(40) & -90(30) & 20(30) & -20(30) \\ (25) & 220(40) & 160(30) & 180(40) & 0(30) & 10(30) & -50(30) \\ (26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -60(30) \\ (28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -40(30) \\ (29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ (23) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ (31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ (232) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ (233) & 240(40) & 160(30) & 160(40) & 20(30) & 110(30) & -30(30) \\ (234) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ (235) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ (236) & 400(50) & 240(30) & 370(50) & 40(30) & 180(40) & -10(30) \\ (237) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ (238) & 270(40) & 200(30) & 250(40) & 20(30) & -90(40) & -20(40) \\ (241) & 150(40) & 460(40) & 790(60) & 100(40) & -40(40) & 90(30) \\ (242) & 300(40) & 330(40) & 690(60) & -70(40) & 130(40) & 80(30) \\ (243) & 220(40) & 240(30) & 210(40) & -100(30) & -80(30) \\ (244) & 280(40) & 470(40) & 370(50) & 50(30) & -90(40) & -20(40) \\ (241) & 150(40) & 460(40) & 790(60) & 100(40) & -40(40) & 90(30) \\ (242) & 300(40) & 330(40) & 690(60) & -70(40) & 130(40) & 80(30) \\ (243) & 220(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ (244) & 280(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ (244) & 280(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ (244) & 280(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ (244) & 380(40) & 220(30) & 150(40) & 100(40) & -70(30) & 10(40) \\ (244) & 380(40) & 220(30) & 150(40) & 100(30) & 50(30) & -70(30) \\ (244) & 380(40) & 220(30) & 150(40) & -100(30) & 50(30) & -70(30) \\ (244) & 380(40) & 220(30) & 150(40) & 30(30) & -60(40) & 180(40) \\ (55) & 300(40) & 300(40) & 150(40) & 30$	C(21)	430(40)	230(30)	330(30)	-90(30)	30(40) 150(40)	20(30) 10(40)
$\begin{array}{cccccc} C(23) & 370(40) & 250(30) & 280(40) & 40(30) & 100(30) & -20(30) \\ C(24) & 210(40) & 200(30) & 220(40) & -90(30) & 20(30) & -20(30) \\ C(25) & 220(40) & 160(30) & 180(40) & 0(30) & 10(30) & -50(30) \\ C(27) & 260(40) & 220(30) & 220(40) & -30(30) & 80(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -40(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(30) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(32) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ C(36) & 400(50) & 240(30) & 370(50) & 40(30) & 180(40) & -10(30) \\ C(37) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ C(38) & 270(40) & 200(30) & 250(40) & 20(30) & -90(40) & -20(40) \\ C(41) & 150(40) & 470(40) & 370(50) & 50(30) & -90(40) & -20(30) \\ C(42) & 300(40) & 330(40) & 690(60) & -70(40) & 130(40) & 80(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & -30(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -40(30) & 40(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -40(30) & 40(30) \\ C(44) & 380(40) & 220(30) & 150(40) & 10(30) & 50(30) & 70(30) \\ C(44) & 280(40) & 200(30) & 290(40) & -100(30) & 50(30) & 70(30) \\ C(45) & 360(40) & 300(40) & 150(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(4$	C(22)	470(30)	430(40)	230(40)	-90(30)	130(40)	-10(40)
$\begin{array}{ccccccc} C(24) & 210(40) & 200(30) & 220(40) & -90(30) & 20(30) & -20(30) \\ C(25) & 220(40) & 160(30) & 180(40) & 0(30) & 10(30) & -30(30) \\ C(26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -40(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(30) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(32) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(36) & 400(50) & 240(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ C(36) & 400(50) & 240(30) & 370(50) & 400(30) & 180(40) & -10(30) \\ C(37) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ C(39) & 230(40) & 350(40) & 250(40) & 20(30) & -90(40) & -20(40) \\ C(41) & 150(40) & 460(40) & 790(60) & 100(40) & -40(40) & 90(30) \\ C(42) & 300(40) & 330(40) & 690(60) & -70(40) & 130(40) & 80(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -40(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -40(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(44) & 280(40) & 240(30) & 210(40) & -100(30) & -50(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -40(30) & 40(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -50(30) & -30(30) \\ C(44) & 280(40) & 220(30) & 150(40) & -100(30) & 50(30) & 70(30) \\ C(44) & 280(40) & 220(30) & 150(40) & -100(30) & 50(30) & 70(30) \\ C(44) & 380(40) & 220(30) & 150(40) & -100(30) & 50(30) & 70(30) \\ C(44) & 380(40) & 220(30) & 150(40) & -100(30) & 50(30) & 70(30) \\ C(45) & 560(50) & 330(40) & 330(50) & 180(30) & 170(40) & 80(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(4$	C(23)	370(40)	250(30)	280(40)	40(30)	100(30)	-20(30)
$\begin{array}{ccccccc} C(25) & 220(40) & 160(30) & 180(40) & 0(30) & 10(30) & -50(30) \\ C(26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -40(30) \\ C(27) & 260(40) & 220(30) & 220(40) & -30(30) & 80(30) & -40(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -40(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(30) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(32) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ C(36) & 400(50) & 240(30) & 370(50) & 40(30) & 180(40) & -10(30) \\ C(37) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ C(38) & 270(40) & 200(30) & 260(40) & 90(30) & 30(30) & 0(30) \\ C(39) & 230(40) & 350(40) & 250(40) & 20(30) & -90(40) & -20(30) \\ C(40) & 280(40) & 470(40) & 370(50) & 50(30) & -90(40) & -20(30) \\ C(41) & 150(40) & 460(40) & 790(60) & 100(40) & -40(40) & 90(30) \\ C(43) & 220(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ C(43) & 220(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & 30(30) & -30(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(45) & 340(40) & 220(30) & 150(40) & 10(30) & 50(30) & 70(30) \\ C(46) & 270(40) & 340(40) & 150(40) & -60(30) & 30(30) & -30(30) \\ C(45) & 360(40) & 300(30) & 290(40) & 70(30) & 10(40) & -70(30) \\ C(46) & 270(40) & 300(40) & 150(40) & 0(30) & 10(30) & 50(30) \\ C(47) & 300(40) & 240(30) & 20(40) & 70(30) & 10(40) & -70(30) \\ C(46) & 270(40) & 300(30) & 290(40) & $	C(24)	210(40)	200(30)	220(40)	-90(30)	20(30)	-20(30)
$\begin{array}{ccccccc} C(26) & 170(40) & 190(30) & 300(40) & -20(30) & 10(30) & -50(30) \\ C(27) & 260(40) & 220(30) & 220(40) & -30(30) & 80(30) & -60(30) \\ C(28) & 310(40) & 210(30) & 180(40) & 40(30) & 10(30) & -40(30) \\ C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(30) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(32) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ C(35) & 490(50) & 240(30) & 370(50) & 40(30) & 180(40) & -10(30) \\ C(37) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ C(38) & 270(40) & 200(30) & 260(40) & 90(30) & 30(30) & 0(30) \\ C(40) & 280(40) & 470(40) & 370(50) & 50(30) & -90(40) & -20(40) \\ C(41) & 150(40) & 460(40) & 790(60) & -70(40) & 130(40) & 80(30) \\ C(43) & 220(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -50(30) & -80(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(45) & 340(40) & 250(30) & 230(40) & -160(30) & -40(30) & 40(30) \\ C(46) & 270(40) & 340(40) & 140(40) & 0(30) & -50(30) & -30(30) \\ C(47) & 300(40) & 240(30) & 220(40) & 60(30) & -50(30) & -30(30) \\ C(48) & 380(40) & 220(30) & 150(40) & 10(30) & 50(30) & -70(30) \\ C(49) & 360(40) & 300(30) & 290(40) & 70(30) & 10(40) & -70(30) \\ C(49) & 360(40) & 300(30) & 290(40) & 70(30) & 10(40) & -70(30) \\ C(49) & 360(40) & 300(30) & 290(40) & 70(30) & 10(40) & -70(30) \\ C(50) & 560(50) & 330(40) & 330(50) & 180(30) & 170(40) & 80(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(52) & 390(40) & 310(40) & 170(40) & 70(30) & 10(30) & 50(30) \\ C(54) & 260(40) & 270(30) & 300(4$	C(25)	220(40)	100(30)	180(40)	0(30)	10(30)	-30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(26)	1/0(40)	190(30)	300(40)	-20(30)	10(30)	-50(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(27)	260(40)	220(30)	220(40)	-30(30)	80(30)	-60(30)
$\begin{array}{ccccccc} C(29) & 630(50) & 140(30) & 210(40) & -10(30) & 150(40) & 90(30) \\ C(30) & 960(60) & 330(40) & 300(50) & -30(30) & 320(40) & 30(40) \\ C(31) & 1160(70) & 140(30) & 640(60) & -170(40) & 360(50) & 90(40) \\ C(32) & 730(50) & 190(30) & 400(50) & 90(30) & 210(40) & -40(40) \\ C(33) & 240(40) & 160(30) & 160(40) & 20(30) & 10(30) & -30(30) \\ C(34) & 360(40) & 200(30) & 240(40) & 10(30) & 20(30) & -90(30) \\ C(35) & 490(50) & 340(40) & 120(40) & -20(30) & -10(30) & 80(30) \\ C(36) & 400(50) & 240(30) & 370(50) & 40(30) & 180(40) & -10(30) \\ C(37) & 310(40) & 260(30) & 170(40) & 0(30) & 50(30) & 10(30) \\ C(38) & 270(40) & 200(30) & 260(40) & 90(30) & 30(30) & 0(30) \\ C(39) & 230(40) & 350(40) & 250(40) & 20(30) & 0(30) & -20(30) \\ C(40) & 280(40) & 470(40) & 370(50) & 50(30) & -90(40) & -20(40) \\ C(41) & 150(40) & 460(40) & 790(60) & 100(40) & -40(40) & 90(30) \\ C(43) & 220(40) & 240(30) & 210(40) & -100(30) & -80(30) & 10(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(44) & 280(40) & 240(30) & 220(40) & 60(30) & -50(30) & -80(30) \\ C(44) & 280(40) & 240(30) & 220(40) & -160(30) & -40(30) & 40(30) \\ C(44) & 280(40) & 240(30) & 120(40) & -60(30) & 30(30) & -30(30) \\ C(44) & 280(40) & 240(30) & 120(40) & -60(30) & 30(30) & -30(30) \\ C(44) & 380(40) & 220(30) & 150(40) & 10(30) & 50(30) & 70(30) \\ C(45) & 340(40) & 220(30) & 150(40) & 10(30) & 50(30) & 70(30) \\ C(44) & 380(40) & 220(30) & 150(40) & 10(30) & 50(30) & 70(30) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 430(50) & 460(40) & 230(40) & 30(30) & -60(40) & 180(40) \\ C(51) & 300(40) & 140(30) & 150(40)$	C(28)	310(40)	210(30)	180(40)	40(30)	10(30)	-40(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(29)	630(50)	140(30)	210(40)	-10(30)	150(40)	90(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(30)	960(60)	330(40)	300(50)	-30(30)	320(40)	30(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(31)	1160(70)	140(30)	640(60)	-170(40)	360(50)	90(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(32)	730(50)	190(30)	400(50)	90(30)	210(40)	-40(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(33)	240(40)	160(30)	160(40)	20(30)	10(30)	-30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(34)	360(40)	200(30)	240(40)	10(30)	20(30)	-90(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(35)	490(50)	340(40)	120(40)	-20(30)	-10(30)	80(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(36)	400(50)	240(30)	370(50)	40(30)	180(40)	-10(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(37)	310(40)	260(30)	170(40)	0(30)	50(30)	10(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(38)	270(40)	200(30)	260(40)	90(30)	30(30)	0(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(39)	230(40)	350(40)	250(40)	20(30)	0(30)	-20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(40)	280(40)	470(40)	370(50)	50(30)	-90(40)	-20(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(41)	150(40)	460(40)	790(60)	100(40)	-40(40)	90(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(42)	300(40)	330(40)	690(60)	-70(40)	130(40)	80(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(43)	220(40)	240(30)	210(40)	-100(30)	-80(30)	10(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(44)	280(40)	240(30)	220(40)	60(30)	-50(30)	-80(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(45)	340(40)	250(30)	230(40)	-160(30)	-40(30)	40(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(46)	270(40)	340(40)	140(40)	0(30)	70(30)	-20(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(47)	300(40)	240(30)	120(40)	-60(30)	30(30)	-30(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(48)	380(40)	220(30)	150(40)	10(30)	50(30)	70(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(49)	360(40)	300(30)	290(40)	70(30)	10(40)	-70(30)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(50)	560(50)	330(40)	330(50)	180(30)	170(40)	80(40)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C(51)	430(50)	460(40)	230(40)	30(30)	-60(40)	180(40)
$\begin{array}{cccccc} C(53) & 300(40) & 140(30) & 150(40) & 0(30) & 10(30) & -10(30) \\ C(54) & 260(40) & 270(30) & 300(40) & -60(30) & 70(30) & -30(30) \\ C(55) & 260(40) & 310(40) & 440(50) & -70(30) & 120(40) & -20(30) \end{array}$	C(52)	390(40)	330(40)	170(40)	70(30)	10(30)	50(30)
$\begin{array}{ccccc} C(54) & 260(40) & 270(30) & 300(40) & -60(30) & 70(30) & -30(30) \\ C(55) & 260(40) & 310(40) & 440(50) & -70(30) & 120(40) & -20(30) \end{array}$	C(53)	300(40)	140(30)	150(40)	0(30)	10(30)	-10(30)
C(55) 260(40) 310(40) 440(50) -70(30) 120(40) -20(30)	C(54)	260(40)	270(30)	300(40)	-60(30)	70(30)	-30(30)
	C(55)	260(40)	310(40)	440(50)	-70(30)	120(40)	-20(30)

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C(56)	220(40)	240(30)	500(50)	-40(30)	20(40)	-80(30)
C(57)	400(40)	140(30)	310(40)	-30(30)	10(40)	-50(30)
C(58)	300(40)	270(40)	210(40)	80(30)	20(30)	70(30)
C(59)	380(40)	260(30)	470(50)	0(30)	-100(40)	20(30)
C(60)	380(50)	300(40)	490(60)	-180(40)	-30(40)	130(40)
C(61)	950(70)	350(40)	1270(80)	20(40)	440(60)	330(40)

#### References

- (1) X. L. Feng, J. S. Wu, V. Enkelmann, K. Mullen, Org. Lett. 2006, 8, 1145.
- (2) K. Kambe, J. Phys. Soc. Jpn. 1950, 5, 48.
- (3) F. E. Mabbs and D. J. Machin, *Magnetism and Transition Metal Complexes*, Dover Publications, Inc., Mineola, 2008.
- (4) SQUEEZE Sluis, P. v.d.; Spek, A. L. Acta Crystallogr., Sect A 1990, 46, 194-201.