Electronic Supplementary Information

Section 1 Experimental

Section 2 CIFs

- (1) BAF845
- (2) BAF847
- (3) BAF1011
- (4) BAF1013
- (5) BAF1074
- (6) BAF1125
- (7) BAF1152
- (8) BAF2021

Section 3. Output from "TOTOPOL" for BAF1125

Section 4. Figure S4.1 VT PXD and Figure S4.2 combined TGA/DTA data from BAF1125

Section 5 Figure S5.11. The structure of BAF845

Section 6 Comparison of Framework Densities for different zeotype topologies based on T = (AlSi), T = (BeSi), T = (BeP) and T = (BeAs).

1. Experimental

All of the samples were prepared from commercially available materials of reagent grade that did not require further purification. An example preparation is as follows: Warning. Be(OH)₂ is very toxic and may cause cancer by inhalation, H₃AsO₄ is very toxic and is regarded as a carcinogen by all routes of exposure and may be fatal if ingested; for both these materials ensure adequate control measures are in place and the authors recommend that Be(OH)₂ is handled in a glove box. $[{H-pyridine}_2]^{2+} {Be_2[BeOH_2][AsO_4]_2[AsO_3OH]}^{2-} (BAF1011)$ was synthesised via hydrothermal methods. To a stirred mixture of Be(OH)₂ (0.11 g, 2.56 mmoles), H₃AsO₄ (75% wt, 0.61 g, 4.34 mmol) and H₂O (3 mL), pyridine (4.11 g, 0.05 moles) was added and the solution left to stir for a further 60 minutes. The reaction mixture was transferred to a 23 mL TeflonTM-lined Parr autoclave and heated at 160 °C for 7 days. The autoclave was allowed to cool slowly to room temperature over 4 h. and the solid product removed from the solution by vacuum filtration, washed with H₂O (40 mL) and EtOH (20 mL) and transfered to an oven to dry at 80 °C for 12 hours. Crystals of each product were isolated for study via single-crystal X-ray diffraction. Data were measured at 120 K on a Bruker Nonius KappaCCD diffractometer, using Mo-K α (λ =0.71073 Å) radiation. Structures were solved using the WinGX package²² by direct methods²³ using XPREP²⁴ and SHELXS-97²⁵ and refined using SHELXL-97. All of the non-hydrogen atoms were refined anisotropically using the F^2 leastsquares method.

- 22 L. J. Farrugia, J. Appl. Crystallogr., 1999, 32, 837.
- 23 G. M. Sheldrick, Acta Crystallogr., Sect. A: 1990,46, 467.
- 24 XPREP Bruker AXS Inc., Madison, Wisconsin, USA
- 25 G. M. Sheldrick, University of Goettingen, Germany, 1997, Release 97-2, 1997.

Section 2 CIFs

BAF845

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H2B H 0.9191 0.1965 0.4827 0.042 Uiso 1 1 calc R . . C4 C 0.8465(5) 0.2695(14) 0.5698(7) 0.040(3) Uiso 1 1 d . . . H4A H 0.8215 0.3327 0.5890 0.048 Uiso 1 1 calc R . . H4B H 0.8340 0.1787 0.5790 0.048 Uiso 1 1 calc R . . N1 N 0.8955(3) 0.2205(9) 0.3785(4) 0.0207(19) Uiso 1 1 d . . . H5A H 0.9176 0.1583 0.3626 0.031 Uiso 1 1 calc R . . H5B H 0.9097 0.3021 0.3738 0.031 Uiso 1 1 calc R . . H5C H 0.8653 0.2165 0.3531 0.031 Uiso 1 1 calc R . . CN1 N 0.8983(3) 0.2890(9) 0.6065(4) 0.0190(18) Uiso 1 1 d . . . HN1A H 0.8954 0.2757 0.6533 0.028 Uiso 1 1 calc R . . HN1B H 0.9095 0.3728 0.5989 0.028 Uiso 1 1 calc R . . HN1C H 0.9212 0.2302 0.5896 0.028 Uiso 1 1 calc R . . Bel Be 0.8647(5) 0.4053(12) 0.8140(6) 0.012(2) Uiso 1 1 d . . . Be2 Be 0.8649(4) -0.0868(12) 0.6713(6) 0.008(2) Uiso 1 1 d . . . Be3 Be 0.9729(5) 0.6297(13) 0.5905(7) 0.016(3) Uiso 1 1 d . . . Be4 Be 0.9748(4) 0.1351(11) 0.9097(6) 0.007(2) Uiso 1 1 d . . O1 O 0.8848(2) 0.5999(7) 0.3973(3) 0.0140(14) Uani 1 1 d . . . 02 0 0.8890(2) -0.2119(6) 0.7193(3) 0.0128(13) Uani 1 1 d . . . O3 O 0.8819(2) -0.0977(6) 0.5888(3) 0.0108(13) Uani 1 1 d . . . 04 0 0.9395(2) -0.4298(7) 0.6591(3) 0.0128(13) Uani 1 1 d . . . O5 O 0.9674(2) 0.0683(6) 0.5803(3) 0.0124(13) Uani 1 1 d . . . 06 0 0.8939(3) 0.2878(6) 0.7675(3) 0.0142(14) Uani 1 1 d . . 07 0 0.8425(2) 0.0699(7) 0.8352(3) 0.0138(14) Uani 1 1 d . 08 0 0.9475(2) 0.0729(7) 0.8324(3) 0.0127(13) Uani 1 1 d . . . 09 0 0.9397(2) 0.5798(7) 0.5204(3) 0.0148(14) Uani 1 1 d . . . 010 0 0.8333(3) -0.4216(8) 0.6465(3) 0.0202(15) Uani 1 1 d . . . 011 0 0.9344(2) -0.1009(6) 0.4702(3) 0.0128(13) Uani 1 1 d . . . 012 0 0.9830(3) -0.2059(7) 0.5957(3) 0.0138(14) Uani 1 1 d . . . 013 0 0.8807(3) 0.5479(7) 0.7798(3) 0.0162(15) Uani 1 1 d . . . 014 0 0.9861(2) 0.7042(6) 0.4015(3) 0.0128(13) Uani 1 1 d . . . 015 0 0.6992(2) 0.4166(7) 0.8334(4) 0.0190(15) Uani 1 1 d . . . 016 0 0.7491(3) 0.5562(7) 0.7269(4) 0.0191(15) Uani 1 1 d . . . 017 0 0.7317(3) 0.2911(8) 0.7096(4) 0.0308(19) Uani 1 1 d . . . 018 0 0.8025(2) 0.3727(7) 0.8176(4) 0.0216(16) Uani 1 1 d . . . 019 0 0.9686(2) 0.4325(6) 0.4022(3) 0.0133(13) Uani 1 1 d . . . 020 0 0.8916(3) 0.0479(7) 0.7047(3) 0.0138(14) Uani 1 1 d . As1 As 0.94646(3) 0.58202(9) 0.43157(5) 0.0097(2) Uani 1 1 d . . . As2 As 0.94340(3) -0.08609(9) 0.55941(5) 0.0087(2) Uani 1 1 d . . . As3 As 0.88616(4) -0.37752(9) 0.70152(5) 0.0105(2) Uani 1 1 d . . . As4 As 0.89441(3) 0.12143(9) 0.78439(5) 0.0102(2) Uani 1 1 d . . . As5 As 0.74642(4) 0.41218(10) 0.77481(5) 0.0152(2) Uani 1 1 d . . . OW1 O 0.0000 0.1150(12) 0.2500 0.030(3) Uani 1 2 d S . . OW2 O 0.0000 0.5971(12) 0.2500 0.031(3) Uani 1 2 d S . . N10A N 0.1696(4) 0.7958(11) 0.0324(5) 0.026(3) Uani 0.94(3) 1 d PD . . C11A C 0.2272(9) 0.775(2) 0.0335(12) 0.026(5) Uani 0.50 1 d P . . C12A C 0.2630(8) 0.836(3) 0.0227(12) 0.028(5) Uani 0.50 1 d P . . C10A C 0.2099(9) 0.892(2) 0.0198(11) 0.028(5) Uani 0.50 1 d P . . loop_ _atom_site_aniso_label _atom_site_aniso_U_11 _atom_site_aniso_U_22 _atom_site_aniso_U_33 atom site aniso U 23 atom site aniso U 13 _atom_site_aniso_U_12 01 0.008(3) 0.017(4) 0.017(3) -0.001(3) 0.001(2) 0.002(3)

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02 0.014(3) 0.006(3) 0.019(4) 0.000(3) -0.001(3) 0.002(3)
03 0.010(3) 0.010(3) 0.012(3) -0.004(2) 0.001(2) -0.005(3)
04 0.010(3) 0.014(3) 0.014(3) 0.003(3) 0.004(2) 0.004(3)
05 0.010(3) 0.010(3) 0.017(3) -0.001(3) 0.000(2) 0.001(3)
06 0.016(3) 0.005(3) 0.022(4) -0.004(3) 0.007(3) -0.001(3)
07 0.013(3) 0.018(4) 0.011(3) 0.000(3) 0.002(2) -0.003(3)
08 0.010(3) 0.018(4) 0.010(3) -0.004(3) 0.000(2) 0.004(3)
09 0.013(3) 0.018(4) 0.014(3) -0.002(3) 0.001(3) 0.001(3)
010 0.016(3) 0.029(4) 0.015(3) -0.005(3) -0.005(3) 0.001(3)
011 0.014(3) 0.014(3) 0.011(3) -0.002(3) 0.002(2) 0.005(3)
012 0.018(3) 0.015(4) 0.008(3) -0.002(3) -0.001(3) 0.002(3)
013 0.024(4) 0.010(3) 0.016(3) 0.001(3) 0.007(3) -0.002(3)
014 0.015(3) 0.009(3) 0.015(3) -0.004(3) 0.008(3) -0.004(3)
015 0.010(3) 0.026(4) 0.021(4) -0.003(3) 0.004(3) 0.001(3)
016 0.011(3) 0.012(4) 0.034(4) 0.005(3) 0.001(3) 0.000(3)
017 0.048(5) 0.018(4) 0.027(4) -0.005(3) 0.005(4) 0.009(4)
018 0.007(3) 0.025(4) 0.032(4) 0.010(3) -0.003(3) 0.001(3)
019 0.014(3) 0.009(3) 0.017(3) -0.005(3) -0.001(3) 0.004(3)
020 0.017(3) 0.013(3) 0.012(3) -0.004(3) 0.000(3) 0.000(3)
As1 0.0111(4) 0.0086(4) 0.0093(4) -0.0005(3) 0.0010(3) -0.0009(4)
As2 0.0099(4) 0.0072(4) 0.0091(4) -0.0001(3) 0.0006(3) -0.0005(3)
As3 0.0116(4) 0.0097(5) 0.0103(4) 0.0002(3) 0.0008(3) -0.0007(4)
As4 0.0102(4) 0.0106(5) 0.0096(4) 0.0002(3) -0.0003(3) 0.0000(4)
As5 0.0100(4) 0.0129(5) 0.0227(5) 0.0016(4) 0.0018(4) 0.0006(4)
OW1 0.025(6) 0.037(7) 0.028(6) 0.000 0.002(5) 0.000
OW2 0.035(6) 0.035(7) 0.024(6) 0.000 0.004(5) 0.000
N10A 0.017(5) 0.037(7) 0.024(6) 0.001(5) -0.003(4) 0.005(4)
C11A 0.024(12) 0.021(12) 0.033(13) -0.003(10) -0.006(9) -0.001(10)
C12A 0.019(11) 0.040(14) 0.025(12) -0.001(10) -0.007(9) -0.011(10)
C10A 0.035(12) 0.025(13) 0.023(11) 0.004(9) -0.003(9) -0.017(10)
_geom_special_details
;
 All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes)
 are estimated using the full covariance matrix. The cell s.u.'s are taken
 into account individually in the estimation of s.u.'s in distances, angles
 and torsion angles; correlations between s.u.'s in cell parameters are only
 used when they are defined by crystal symmetry. An approximate (isotropic)
 treatment of cell s.u.'s is used for estimating s.u.'s involving l.s.
planes.
;
loop
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C1 C4 1.500(17) . ?
C2 N1 1.508(14) . ?
C4 CN1 1.474(15) . ?
Bel 013 1.608(14) . ?
Bel 018 1.618(13) . ?
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Bel 01 1.622(13) 6_566 ?
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Be1 06 1.646(13) . ?
Be2 020 1.611(13) . ?
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Be2 03 1.622(12) . ? Be2 015 1.629(12) 4_646 ? Be2 O2 1.634(13) . ? Be3 09 1.610(14) . ? Be3 019 1.612(14) 5 766 ? Be3 012 1.649(15) 1 565 ? Be3 04 1.673(14) 1 565 ? Be4 011 1.595(12) 6_556 ? Be4 05 1.616(12) 2_756 ? Be4 014 1.623(13) 6_566 ? Be4 08 1.698(12) . ? O1 Be1 1.622(13) 6_565 ? O1 As1 1.681(6) . ? O2 As3 1.673(6) . ? O3 As2 1.682(6) . ? O4 Be3 1.673(14) 1_545 ? O4 As3 1.678(6) . ? O5 Be4 1.616(12) 2_756 ? O5 As2 1.684(6) . ? O6 As4 1.676(6) . ? 07 As4 1.732(6) . ? O8 As4 1.663(6) . ? 09 As1 1.679(6) . ? 010 As3 1.717(6) . ? O11 Be4 1.595(12) 6 ? O11 As2 1.682(6) . ? O12 Be3 1.649(15) 1 545 ? O12 As2 1.681(6) . ? O13 As3 1.651(6) 1_565 ? O14 Be4 1.623(13) 6_565 ? 014 As1 1.684(6) . ? O15 Be2 1.629(12) 4_656 ? 015 As5 1.656(6) . ? O16 As5 1.686(7) . ? 017 As5 1.741(8) . ? 018 As5 1.654(6) . ? O19 Be3 1.612(14) 5 766 ? 019 As1 1.683(6) . ? 020 As4 1.658(6) . ? As3 013 1.651(6) 1_545 ? N10A C10A 1.43(2) . ? N10A C11A 1.48(2) . ? C11A C12A 1.12(3) . ? C11A C10A 1.26(3) . ? C11A C12A 1.55(3) 7_565 ? C11A C11A 1.81(5) 7_565 ? C12A C10A 1.46(3) . ? C12A C11A 1.55(3) 7_565 ? C12A C12A 2.00(5) 7_565 ? loop_ _geom_angle_atom_site_label_1 _geom_angle_atom_site_label_2 geom angle atom site label 3 geom angle

_geom_angle_site_symmetry_1
_geom_angle_site_symmetry_3

_geom_angle_publ_flag C2 C1 C4 113.0(11) . . ? C1 C2 N1 116.0(10) . . ? CN1 C4 C1 111.8(10) . . ? 013 Bel 018 117.0(8) . . ? O13 Be1 O1 109.6(8) . 6 566 ? O18 Bel O1 103.1(7) . 6_566 ? 013 Bel 06 106.4(7) . . ? 018 Bel 06 110.1(8) . . ? O1 Be1 O6 110.7(8) 6_566 . ? O20 Be2 O3 107.6(7) . . ? O20 Be2 O15 114.2(8) . 4_646 ? O3 Be2 O15 104.6(7) . 4_646 ? O20 Be2 O2 105.6(7) . . ? O3 Be2 O2 111.4(7) . . ? O15 Be2 O2 113.4(7) 4_646 ? . O9 Be3 O19 113.9(8) . 5_766 ? O9 Be3 O12 115.2(8) . 1_565 ? O19 Be3 O12 103.3(8) 5_766 1_565 ? O9 Be3 O4 104.6(8) . 1_565 ? O19 Be3 O4 107.1(8) 5_766 1_565 ? O12 Be3 O4 112.6(8) 1_565 1_565 ? O11 Be4 O5 116.0(7) 6_556 2_756 ? O11 Be4 O14 113.3(7) 6_556 6_566 ? O5 Be4 O14 104.4(7) 2_756 6_566 ? O11 Be4 O8 105.9(7) 6 556 . ? O5 Be4 O8 106.9(7) 2 756 . ? O14 Be4 O8 110.0(7) 6_566 . ? Bel Ol Asl 128.2(6) 6_565 . ? Be2 O2 As3 128.3(6) . . ? Be2 O3 As2 126.2(5) . . ? Be3 O4 As3 134.2(6) 1_545 . ? Be4 05 As2 135.8(6) 2_756 . ? Bel 06 As4 126.4(6) . . ? As4 08 Be4 130.7(5) . . ? Be3 09 As1 137.2(6) . . ? Be4 011 As2 130.9(6) 6 . ? Be3 012 As2 125.6(6) 1 545 . ? Be1 013 As3 141.0(6) . 1_565 ? Be4 014 As1 124.2(5) 6_565 . ? Be2 015 As5 135.4(6) 4_656 . ? Bel 018 As5 139.3(6) . . ? Be3 019 As1 128.8(6) 5_766 . ? Be2 020 As4 135.7(6) . . ? 09 As1 01 104.5(3) . . ? 09 As1 019 111.1(3) . . ? O1 As1 O19 106.6(3) . . ? 09 As1 014 115.2(3) . . ? O1 As1 O14 111.0(3) . . ? 019 As1 014 108.1(3) . . ? 012 As2 03 111.7(3) . . ? 012 As2 011 113.4(3) . . ? O3 As2 O11 103.0(3) . . ? 012 As2 05 109.9(3) . . ? O3 As2 O5 108.6(3) . . ? 011 As2 05 110.1(3) . . ? 013 As3 02 105.5(3) 1_545 . ?

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O2 As3 O4 111.5(3) . . ?
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O6 As4 O7 113.1(3) . . ?
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N10A C10A C12A 113.9(19) . . ?
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BAF1011

data_BAF1011 SHELXL-97 audit creation method _chemical_name_systematic ; ? ; ? _chemical_name_common _chemical_melting_point ? _chemical_formula_moiety 'As3 Be3 H3 O13, C5 H6 N' _chemical_formula_sum 'C5 H9 As3 Be3 N 013' 542.92 _chemical_formula_weight loop_ _atom_type_symbol _atom_type_description _atom_type_scat_dispersion_real _atom_type_scat_dispersion_imag _atom_type_scat_source 'C' 'C' 0.0033 0.0016 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' 'H' 'H' 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' 'Be' 'Be' 0.0005 0.0002 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' 'N' 'N' 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' '0' '0' 0.0106 0.0060 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' 'As' 'As' 0.0499 2.0058 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' _symmetry_cell_setting Monoclinic _symmetry_space_group_name_H-M 'C 1 2/c 1' loop_ _symmetry_equiv_pos_as_xyz 'x, y, z' '-x, y, -z+1/2' 'x+1/2, y+1/2, z' '-x+1/2, y+1/2, -z+1/2' '-x, -y, -z' 'x, -y, z-1/2' -x+1/2, -y+1/2, -z''x+1/2, -y+1/2, z-1/2' _cell_length_a 26.2341(6) 4.91270(10) _cell_length_b 24.6048(5) _cell_length_c 90.00 _cell_angle_alpha _cell_angle_beta 118.7180(10) _cell_angle_gamma 90.00

2781.01(10) _cell_volume _cell_formula_units_Z 8 _cell_measurement_temperature 120(2) _cell_measurement_reflns_used 16959 _cell_measurement_theta_min 2.91 _cell_measurement_theta_max 27.48 _exptl_crystal_description Block _exptl_crystal_colour Colourless _exptl_crystal_size_max 0.01 _exptl_crystal_size_mid 0.01 _exptl_crystal_size_min 0.01 _exptl_crystal_density_meas ? _exptl_crystal_density_diffrn 2.593 _exptl_crystal_density_method 'not measured' _exptl_crystal_F_000 2088 _exptl_absorpt_coefficient_mu 7.242 _exptl_absorpt_correction_type none _exptl_absorpt_correction_T_min ? _exptl_absorpt_correction_T_max ? _exptl_absorpt_process_details ? _exptl_special_details ; ? ; _diffrn_ambient_temperature 120(2)_diffrn_radiation_wavelength 0.71073 _diffrn_radiation_type MoK∖a 'fine-focus sealed tube' _diffrn_radiation_source _diffrn_radiation_monochromator '10cm confocal mirrors' _diffrn_measurement_device_type 'Bruker-Nonius APEX II CCD camera' _diffrn_measurement_method '\f & \w scans' _diffrn_detector_area_resol_mean '4096x4096pixels / 62x62mm' diffrn standards number 3567 _diffrn_standards_interval_count 10981 _diffrn_standards_interval_time ? _diffrn_standards_decay_% ? _diffrn_reflns_number 16316 _diffrn_reflns_av_R_equivalents 0.0513 _diffrn_reflns_av_sigmaI/netI 0.0435 _diffrn_reflns_limit_h_min -34 _diffrn_reflns_limit_h_max 34 _diffrn_reflns_limit_k_min -5 _diffrn_reflns_limit_k_max 6 _diffrn_reflns_limit_l_min -31 _diffrn_reflns_limit_l_max 31 3.11 _diffrn_reflns_theta_min _diffrn_reflns_theta_max 27.51 _reflns_number_total 3197 _reflns_number_gt 2751 _reflns_threshold_expression $>2 \ (I)$ computing data collection 'COLLECT (Hooft, R.W.W., 1998)' _computing_cell_refinement 'DENZO (Otwinowski & Minor, 1997)' 'DENZO (Otwinowski & Minor, 1997)' _computing_data_reduction

```
_computing_structure_solution
                                  ?
_computing_structure_refinement
                                  'SHELXL-97 (Sheldrick, 2008)'
_computing_molecular_graphics
                                  ?
_computing_publication_material
                                  ?
_refine_special_details
;
 Refinement of F^2^ against ALL reflections. The weighted R-factor wR and
 goodness of fit S are based on F^2^, conventional R-factors R are based
 on F, with F set to zero for negative F^{2}. The threshold expression of
 F^2 > 2 \setminus s(F^2) is used only for calculating R-factors(gt) etc. and is
 not relevant to the choice of reflections for refinement. R-factors based
 on F^{2^{-}} are statistically about twice as large as those based on F, and R-
 factors based on ALL data will be even larger.
;
_refine_ls_structure_factor_coef Fsqd
_refine_ls_matrix_type
                                  full
_refine_ls_weighting_scheme
                                  calc
_refine_ls_weighting_details
 'calc w=1/[\s^2^(Fo^2^)+(0.0000P)^2^+42.3673P] where P=(Fo^2^+2Fc^2^)/3'
_atom_sites_solution_primary
                                  direct
_atom_sites_solution_secondary
                                  difmap
_atom_sites_solution_hydrogens
                                  qeom
_refine_ls_hydrogen_treatment
                                  mixed
_refine_ls_extinction_method
                                  none
refine ls extinction coef
                                  ?
_refine_ls_number_reflns
                                  3197
_refine_ls_number_parameters
                                  238
_refine_ls_number_restraints
                                  3
                                  0.0492
_refine_ls_R_factor_all
                                  0.0381
_refine_ls_R_factor_gt
                                  0.0794
_refine_ls_wR_factor_ref
_refine_ls_wR_factor_gt
                                  0.0741
_refine_ls_goodness_of_fit_ref
                                  1.139
_refine_ls_restrained_S_all
                                  1.138
refine ls shift/su max
                                  0.001
                                  0.000
_refine_ls_shift/su_mean
loop_
 _atom_site_label
 _atom_site_type_symbol
 _atom_site_fract_x
 _atom_site_fract_y
 _atom_site_fract_z
 _atom_site_U_iso_or_equiv
 _atom_site_adp_type
 _atom_site_occupancy
 _atom_site_symmetry_multiplicity
 _atom_site_calc_flag
 _atom_site_refinement_flags
_atom_site_disorder_assembly
 atom site disorder group
As1 As 0.178692(19) 0.80184(9) 0.24364(2) 0.00591(11) Uani 1 1 d . . .
As2 As 0.050636(19) 0.85473(9) 0.34221(2) 0.00650(11) Uani 1 1 d . . .
As3 As 0.261890(19) 0.97593(9) 0.56991(2) 0.00630(11) Uani 1 1 d . . .
Bel Be 0.0691(3) 1.0009(13) 0.2379(3) 0.0112(12) Uani 1 1 d . . .
```

```
Be2 Be 0.1749(2) 1.0171(12) 0.4338(3) 0.0085(11) Uani 1 1 d . . .
Be3 Be 0.2582(3) 1.1908(12) 0.6843(3) 0.0094(12) Uani 1 1 d . .
01 0 0.18458(13) 0.4753(6) 0.26578(14) 0.0080(6) Uani 1 1 d . .
02 0 0.20313(13) 0.8586(7) 0.19409(14) 0.0107(7) Uani 1 1 d . . .
O3 O 0.21855(13) 0.9874(6) 0.31022(14) 0.0083(6) Uani 1 1 d . . .
04 0 0.10901(13) 0.8898(7) 0.21000(14) 0.0086(7) Uani 1 1 d . . .
06 0 0.06560(13) 0.7693(6) 0.28537(14) 0.0084(6) Uani 1 1 d . . .
07 0 0.02791(15) 0.5761(7) 0.36595(16) 0.0116(7) Uani 1 1 d D . .
H7 H 0.017(2) 0.439(8) 0.343(2) 0.023(17) Uiso 1 1 d D . .
08 0 -0.00367(13) 1.0825(7) 0.31602(14) 0.0086(7) Uani 1 1 d . . .
09 0 0.10604(13) 0.9770(7) 0.40544(14) 0.0094(7) Uani 1 1 d . . .
010 0 0.20408(13) 0.8304(6) 0.39756(14) 0.0082(6) Uani 1 1 d . . .
011 0 0.18967(13) 1.3354(7) 0.43734(15) 0.0088(6) Uani 1 1 d . . .
012 0 0.20297(13) 0.8878(7) 0.50376(14) 0.0089(7) Uani 1 1 d . . .
013 0 0.23599(13) 1.1050(6) 0.61384(14) 0.0086(7) Uani 1 1 d . .
N1 N 0.36866(18) 0.8905(9) 0.46413(19) 0.0151(9) Uani 1 1 d . . .
H6 H 0.3465 0.8063 0.4753 0.018 Uiso 1 1 calc R . .
C1 C 0.3712(2) 0.8032(10) 0.4138(2) 0.0160(11) Uani 1 1 d . . .
H1 H 0.3482 0.6577 0.3909 0.019 Uiso 1 1 calc R . .
C2 C 0.4076(2) 0.9285(11) 0.3961(2) 0.0167(11) Uani 1 1 d . . .
H2 H 0.4105 0.8653 0.3621 0.020 Uiso 1 1 calc R . .
C3 C 0.4399(2) 1.1492(11) 0.4295(2) 0.0171(11) Uani 1 1 d . .
H3 H 0.4643 1.2384 0.4177 0.021 Uiso 1 1 calc R . .
C4 C 0.4356(2) 1.2382(11) 0.4812(2) 0.0170(11) Uani 1 1 d . . .
H4 H 0.4571 1.3870 0.5041 0.020 Uiso 1 1 calc R . .
C5 C 0.3994(2) 1.1033(11) 0.4975(2) 0.0160(11) Uani 1 1 d . . .
H5 H 0.3962 1.1598 0.5318 0.019 Uiso 1 1 calc R . .
O5 O 0.09870(14) 1.2758(7) 0.27762(16) 0.0104(7) Uani 1 1 d D . .
H5A H 0.127(2) 1.322(18) 0.273(4) 0.07(3) Uiso 1 1 d D . .
H5B H 0.082(2) 1.419(8) 0.280(3) 0.030(18) Uiso 1 1 d D . .
loop_
 _atom_site_aniso_label
 _atom_site_aniso_U_11
 _atom_site_aniso_U_22
 _atom_site_aniso_U_33
 atom site aniso U 23
 _atom_site_aniso_U_13
 _atom_site_aniso_U_12
As1 0.0061(2) 0.0063(2) 0.0057(2) 0.00015(18) 0.00312(17) 0.00028(17)
As2 0.0063(2) 0.0071(2) 0.0063(2) -0.00044(18) 0.00314(18) -0.00002(17)
As3 0.0070(2) 0.0064(2) 0.0057(2) -0.00039(18) 0.00317(17) -0.00021(17)
Be1 0.009(3) 0.011(3) 0.015(3) 0.001(3) 0.007(2) 0.000(2)
Be2 0.008(3) 0.009(3) 0.009(3) 0.001(2) 0.005(2) -0.002(2)
Be3 0.011(3) 0.006(3) 0.011(3) -0.002(2) 0.005(2) -0.003(2)
01 0.0070(14) 0.0075(15) 0.0081(15) 0.0033(13) 0.0025(12) -0.0002(12)
02 0.0095(16) 0.0134(17) 0.0099(16) 0.0042(14) 0.0051(13) 0.0021(13)
03 0.0108(15) 0.0067(15) 0.0077(15) -0.0014(13) 0.0047(13) -0.0030(13)
04 0.0054(15) 0.0115(17) 0.0065(15) 0.0010(13) 0.0009(12) 0.0007(13)
06 0.0109(16) 0.0066(15) 0.0084(15) 0.0007(13) 0.0054(13) 0.0004(13)
07 0.0185(17) 0.0062(16) 0.0146(17) -0.0022(14) 0.0116(15) -0.0049(14)
08 0.0047(14) 0.0098(16) 0.0098(16) -0.0002(13) 0.0022(12) 0.0013(12)
09 0.0060(15) 0.0131(17) 0.0074(15) -0.0025(13) 0.0019(12) -0.0011(13)
010 0.0105(15) 0.0083(15) 0.0079(15) -0.0002(13) 0.0061(13) 0.0024(13)
0.0093(15) 0.0080(15) 0.0116(16) -0.0002(13) 0.0069(13) -0.0019(13)
012 0.0054(14) 0.0140(17) 0.0052(15) -0.0015(13) 0.0008(12) -0.0027(13)
013 0.0100(15) 0.0075(15) 0.0108(16) -0.0014(13) 0.0070(13) -0.0012(13)
```

```
N1 0.013(2) 0.021(2) 0.014(2) 0.0041(18) 0.0077(17) -0.0005(18)
C1 0.016(2) 0.011(2) 0.016(3) 0.003(2) 0.004(2) 0.002(2)
C2 \ 0.020(3) \ 0.019(3) \ 0.011(2) \ 0.004(2) \ 0.007(2) \ 0.006(2)
C3 0.015(2) 0.017(3) 0.022(3) 0.003(2) 0.011(2) -0.003(2)
C4 0.016(2) 0.014(2) 0.018(3) -0.002(2) 0.006(2) -0.003(2)
C5 0.016(2) 0.020(3) 0.011(2) -0.001(2) 0.006(2) 0.005(2)
05 0.0107(17) 0.0073(16) 0.0151(17) -0.0034(14) 0.0077(14) -0.0004(14)
_geom_special_details
;
 All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes)
 are estimated using the full covariance matrix. The cell s.u.'s are taken
 into account individually in the estimation of s.u.'s in distances, angles
 and torsion angles; correlations between s.u.'s in cell parameters are only
 used when they are defined by crystal symmetry. An approximate (isotropic)
 treatment of cell s.u.'s is used for estimating s.u.'s involving l.s.
planes.
;
loop_
 _geom_bond_atom_site_label_1
 _geom_bond_atom_site_label_2
 _geom_bond_distance
 _geom_bond_site_symmetry_2
 _geom_bond_publ_flag
As1 02 1.651(3) . ?
As1 04 1.661(3) . ?
As1 01 1.677(3) . ?
As1 03 1.721(3) . ?
As2 09 1.649(3) . ?
As2 06 1.677(3) . ?
As2 08 1.678(3) . ?
As2 07 1.705(3) . ?
As3 011 1.650(3) 7_576 ?
As3 013 1.655(3) . ?
As3 012 1.676(3) . ?
As3 010 1.737(3) 7 566 ?
Bel 04 1.599(7) . ?
Be1 05 1.629(7) . ?
Be1 08 1.636(7) 2 ?
Bel 06 1.664(7) . ?
Be2 011 1.604(7) . ?
Be2 09 1.605(6) . ?
Be2 012 1.640(7) . ?
Be2 010 1.696(7) . ?
Be3 O2 1.594(7) 6_576 ?
Be3 013 1.597(7) . ?
Be3 01 1.629(7) 7_566 ?
Be3 O3 1.676(7) 7_576 ?
O1 Be3 1.629(7) 7_566 ?
O2 Be3 1.594(7) 6_575 ?
O3 Be3 1.676(7) 7_576 ?
O8 Bel 1.636(7) 2 ?
```

O10 As3 1.737(3) 7_566 ? O11 As3 1.650(3) 7 576 ?

N1 C5 1.334(7) . ? N1 C1 1.343(7) . ? C1 C2 1.370(7) . ? C2 C3 1.378(7) . ? C3 C4 1.399(7) . ? C4 C5 1.367(7) . ? loop _geom_angle_atom_site_label_1 _geom_angle_atom_site_label_2 _geom_angle_atom_site_label_3 _geom_angle _geom_angle_site_symmetry_1 _geom_angle_site_symmetry_3 _geom_angle_publ_flag O2 As1 O4 108.23(15) . . ? O2 As1 O1 113.18(16) . . ? O4 As1 O1 108.56(15) . . ? O2 As1 O3 109.84(16) . . ? O4 As1 O3 110.88(15) . . ? O1 As1 O3 106.16(15) . . ? 09 As2 06 115.11(15) . . ? 09 As2 08 108.67(16) . . ? O6 As2 O8 110.02(15) . . ? 09 As2 07 105.32(16) . . ? O6 As2 O7 110.19(16) . . ? 08 As2 07 107.17(16) . . ? O11 As3 O13 115.77(16) 7 576 . ? O11 As3 O12 116.04(16) 7 576 . ? 013 As3 012 104.89(16) . . ? O11 As3 O10 106.53(15) 7_576 7_566 ? 013 As3 010 108.20(15) . 7_566 ? 012 As3 010 104.69(16) . 7_566 ? O4 Be1 O5 108.6(4) . . ? O4 Bel O8 112.6(4) . 2 ? O5 Be1 O8 107.2(4) . 2 ? O4 Bel O6 109.6(4) . . ? O5 Be1 O6 108.5(4) . . ? O8 Bel O6 110.3(4) 2 . ? O11 Be2 O9 109.6(4) . . ? O11 Be2 O12 110.2(4) . . ? O9 Be2 O12 104.6(4) . . ? Oll Be2 Ol0 113.4(4) . . ? 09 Be2 010 113.8(4) . . ? 012 Be2 010 104.7(4) . . ? O2 Be3 O13 103.8(4) 6 576 . ? O2 Be3 O1 112.5(4) 6_576 7_566 ? O13 Be3 O1 114.2(4) . 7_566 ? O2 Be3 O3 116.9(4) 6_576 7_576 ? O13 Be3 O3 105.4(4) . 7_576 ? O1 Be3 O3 104.1(4) 7_566 7_576 ? Be3 O1 As1 129.2(3) 7_566 . ? Be3 O2 As1 142.0(3) 6_575 . ? Be3 O3 As1 127.4(3) 7_576 . ? Bel 04 Asl 131.7(3) . . ? Be1 06 As2 121.8(3) . . ? Bel 08 As2 120.9(3) 2 . ? Be2 09 As2 138.8(3) . . ? Be2 O10 As3 119.2(3) . 7_566 ?

Be2 O11 As3 136.1(3) . 7_576 ? Be2 012 As3 131.2(3) . . ? Be3 013 As3 139.4(3) . . ? C5 N1 C1 122.3(5) . . ? N1 C1 C2 120.0(5) . . ? C1 C2 C3 119.1(5) . . ? C2 C3 C4 119.5(5) . . ? C5 C4 C3 119.0(5) . . ? N1 C5 C4 119.9(5) . . ? loop_ _geom_hbond_atom_site_label_D _geom_hbond_atom_site_label_H _geom_hbond_atom_site_label_A _geom_hbond_distance_DH _geom_hbond_distance_HA _geom_hbond_distance_DA _geom_hbond_angle_DHA _geom_hbond_site_symmetry_A O7 H7 O8 0.84(2) 1.86(3) 2.664(5) 161(6) 1_545 N1 H6 O12 0.86 1.87 2.730(5) 177.3 7_566 O5 H5A O1 0.85(2) 1.76(3) 2.598(5) 170(9) 1_565 O5 H5B O6 0.85(2) 1.79(3) 2.613(5) 162(6) 1_565 _diffrn_measured_fraction_theta_max 0.996 _diffrn_reflns_theta_full 27.51 _diffrn_measured_fraction_theta_full 0.996 _refine_diff_density_max 0.894 _refine_diff_density_min -0.783 _refine_diff_density_rms 0.188

BAF1013

data BAF1013

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5787 _cell_measurement_reflns_used _cell_measurement_theta_min 2.91 _cell_measurement_theta_max 27.48 _exptl_crystal_description Plate exptl crystal colour Colourless _exptl_crystal_size_max 0.01 _exptl_crystal_size_mid 0.01 _exptl_crystal_size_min 0.01 _exptl_crystal_density_meas ? _exptl_crystal_density_diffrn 4.041 _exptl_crystal_density_method 'not measured' _exptl_crystal_F_000 466 _exptl_absorpt_coefficient_mu 20.714 _exptl_absorpt_correction_type none _exptl_absorpt_correction_T_min ? _exptl_absorpt_correction_T_max ? ? _exptl_absorpt_process_details _exptl_special_details ; ? ; _diffrn_ambient_temperature 120(2)_diffrn_radiation_wavelength 0.71073 diffrn radiation type MoK∖a _diffrn_radiation_source 'Bruker-Nonius FR591 rotating anode' _diffrn_radiation_monochromator '10cm confocal mirrors' _diffrn_measurement_device_type 'Bruker-Nonius APEX II CCD camera on \kgoniostat' _diffrn_measurement_method '\f & \w scans' _diffrn_detector_area_resol_mean '4096x4096pixels / 62x62mm' _diffrn_standards_number 1033 _diffrn_standards_interval_count 3808 _diffrn_standards_interval_time ? _diffrn_standards_decay_% ? _diffrn_reflns_number 5767 _diffrn_reflns_av_R_equivalents 0.0321 _diffrn_reflns_av_sigmaI/netI 0.0259 _diffrn_reflns_limit_h_min -6 _diffrn_reflns_limit_h_max 6 _diffrn_reflns_limit_k_min -10 _diffrn_reflns_limit_k_max 8 _diffrn_reflns_limit_l_min -13 _diffrn_reflns_limit_l_max 12 _diffrn_reflns_theta_min 3.23 _diffrn_reflns_theta_max 27.57 961 _reflns_number_total _reflns_number_gt 892 _reflns_threshold_expression >2\s(I) _computing_data_collection 'COLLECT (Hooft, R.W.W., 1998)' computing cell refinement 'DENZO (Otwinowski & Minor, 1997) & COLLECT (Hooft, R.W.W., 1998)' _computing_data_reduction 'DENZO (Otwinowski & Minor, 1997) & COLLECT (Hooft, R.W.W., 1998)'

```
_computing_structure_solution
                                  ?
_computing_structure_refinement
                                  'SHELXL-97 (Sheldrick, 2008)'
_computing_molecular_graphics
                                  ?
_computing_publication_material
                                  ?
_refine_special_details
;
 Refinement of F^2^ against ALL reflections. The weighted R-factor wR and
 goodness of fit S are based on F^2^, conventional R-factors R are based
 on F, with F set to zero for negative F^{2}. The threshold expression of
 F^2 > 2 \setminus s(F^2) is used only for calculating R-factors(gt) etc. and is
 not relevant to the choice of reflections for refinement. R-factors based
 on F^{2^{-}} are statistically about twice as large as those based on F, and R-
 factors based on ALL data will be even larger.
;
_refine_ls_structure_factor_coef Fsqd
_refine_ls_matrix_type
                                  full
_refine_ls_weighting_scheme
                                  calc
_refine_ls_weighting_details
 'calc w=1/[\s^2^(Fo^2^)+(0.0000P)^2^+2.5941P] where P=(Fo^2^+2Fc^2^)/3'
_atom_sites_solution_primary
                                  direct
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O4 Be2 O3 107.0(2) . 1_565 ?
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Bel Ol Asl 127.52(17) . . ?
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BAF1025

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_cell_angle_beta
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As2 As 0.20042(4) -0.13923(5) 0.25115(4) 0.00620(13) Uani 1 1 d . . .
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09 0 0.3688(3) 0.1619(4) 0.0335(3) 0.0093(7) Uani 1 1 d . . .
06 0 0.2037(3) 0.3694(4) 0.1094(3) 0.0092(6) Uani 1 1 d . . .
05 0 0.2996(3) -0.0908(4) 0.1487(3) 0.0103(7) Uani 1 1 d . . .
01 0 0.2409(3) 0.3953(4) -0.1076(3) 0.0098(7) Uani 1 1 d . . .
07 0 0.0694(3) -0.0128(4) 0.2391(3) 0.0099(7) Uani 1 1 d . .
02 0 0.5591(3) 0.0123(4) 0.1887(3) 0.0105(7) Uani 1 1 d . . .
O3 O 0.8209(3) 0.0979(4) 0.1694(3) 0.0091(7) Uani 1 1 d . . .
010 0 0.3598(3) 0.1775(4) 0.2750(3) 0.0080(6) Uani 1 1 d . . .
04 0 0.6462(3) 0.3221(4) 0.2182(3) 0.0089(6) Uani 1 1 d . . .
Bel Be 0.2289(6) 0.2626(7) -0.0055(5) 0.0105(12) Uani 1 1 d . . .
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_atom_site_aniso_U_22
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N2 \ 0.0097(19) \ 0.012(2) \ 0.0082(19) \ 0.0004(17) \ 0.0007(16) \ 0.0009(17)
N1 0.0092(19) 0.012(2) 0.015(2) -0.0001(18) 0.0025(17) -0.0005(17)
Be2 0.013(3) 0.002(3) 0.009(3) 0.000(2) -0.004(2) 0.001(2)
Be3 0.009(3) 0.010(3) 0.011(3) 0.000(2) 0.003(2) -0.001(2)
As1 0.0064(2) 0.0058(2) 0.0058(2) -0.00026(17) 0.00103(16) 0.00046(17)
As2 0.0058(2) 0.0065(2) 0.0063(2) -0.00049(18) 0.00118(16) -0.00064(17)
08 0.0110(15) 0.0070(17) 0.0062(15) 0.0002(14) 0.0010(12) -0.0023(12)
09 0.0109(16) 0.0110(18) 0.0066(16) -0.0023(15) 0.0029(13) 0.0006(13)
06 0.0100(15) 0.0112(17) 0.0055(14) -0.0013(13) -0.0011(12) 0.0014(13)
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04 0.0082(14) 0.0068(16) 0.0108(15) 0.0008(13) -0.0006(12) 0.0003(12)
Be1 0.014(3) 0.008(3) 0.009(3) 0.000(2) 0.000(2) 0.003(2)
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All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes)
 are estimated using the full covariance matrix. The cell s.u.'s are taken
 into account individually in the estimation of s.u.'s in distances, angles
 and torsion angles; correlations between s.u.'s in cell parameters are only
 used when they are defined by crystal symmetry. An approximate (isotropic)
 treatment of cell s.u.'s is used for estimating s.u.'s involving l.s.
planes.
;
loop
 geom bond atom site label 1
 geom bond atom site label 2
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Bel Ol Asl 123.2(3) . 4_565 ?
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Be2 010 As2 121.6(3) . 2 ?
Be3 04 As1 125.5(3) 4_666 . ?
O8 Be1 O6 112.5(4) . . ?
O8 Be1 O1 111.0(4) . . ?
O6 Bel O1 101.4(4) . . ?
O8 Be1 O9 109.3(4) . . ?
O6 Be1 O9 109.2(4) . . ?
O1 Be1 O9 113.3(4) . . ?
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BAF1152

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_computing_molecular_graphics
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_computing_publication_material
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Refinement attempted in Cmca but has proven to be unconclusive
High degree of disorder of templating organic materal
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 _atom_site_fract_y
 _atom_site_fract_z
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Bel Be -0.0696(6) 0.3297(6) 0.1554(5) 0.0133(16) Uiso 1 1 d . . .
C1 C 0.2565(11) 0.1320(10) 0.2164(8) 0.053(5) Uiso 0.81(4) 1 d P . .
N3 N 0.5000 0.8937(7) 0.7500 0.029(2) Uani 1 2 d S . .
N4 N 0.7500 0.7500 0.5000 0.025(2) Uani 1 2 d S . .
N2 N 0.0000 0.1024(7) 0.2500 0.035(3) Uani 1 2 d S . .
N1 N 0.7564(5) 0.5069(4) 0.1025(3) 0.0189(13) Uani 1 1 d . . .
C4 C 0.2488(9) 0.2522(9) 0.0394(6) 0.032(4) Uiso 0.72(3) 1 d P . .
C2 C 0.3062(14) 0.1878(13) 0.1090(10) 0.037(6) Uiso 0.50(4) 1 d P . .
C6 C 0.203(3) 0.187(3) 0.110(2) 0.043(15) Uiso 0.23(4) 1 d P . .
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 All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes)
 are estimated using the full covariance matrix. The cell s.u.'s are taken
 into account individually in the estimation of s.u.'s in distances, angles
 and torsion angles; correlations between s.u.'s in cell parameters are only
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Bel 03 1.617(9) . ?
Bel 010 1.622(9) . ?
Bel 013 1.689(9) . ?
C4 C4 1.47(2) 7 ?
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O4 Be2 1.630(9) . ?
O5 Be4 1.640(9) 6 566 ?
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O7 Be4 1.610(9) 5 665 ?
O12 Bel 1.593(9) 2 ?
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014 As1 1.663(5) 3 ? O15 Be2 1.654(9) . ? O15 As1 1.686(4) 5_565 ? O16 Be2 1.640(9) . ? 019 As4 1.677(4) 2_655 ? Be4 07 1.610(9) 5 665 ? Be4 05 1.640(9) 6_565 ? loop_ _geom_angle_atom_site_label_1 _geom_angle_atom_site_label_2 _geom_angle_atom_site_label_3 _geom_angle _geom_angle_site_symmetry_1 _geom_angle_site_symmetry_3 _geom_angle_publ_flag 011 Be3 08 114.7(5) . . ? O11 Be3 O1 112.3(5) . . ? O8 Be3 O1 104.1(5) . . ? O11 Be3 O19 105.2(5) . . ? O8 Be3 O19 110.8(5) . . ? O1 Be3 O19 109.9(5) . . ? O12 Bel O3 109.9(5) 2 . ? 012 Bel 010 115.3(6) 2 . ? O3 Be1 O10 112.4(5) . . ? 012 Bel 013 108.9(5) 2 . ? O3 Be1 O13 105.7(5) . . ? O10 Be1 O13 103.9(5) . . ? C4 C4 C6 139.3(19) 7 . ? C4 C4 C2 135.4(14) 7 . ? C6 C4 C2 45.4(16) . . ? C6 C2 C4 66(2) . . ? C2 C6 C7 134(4) . . ? C2 C6 C4 68(2) . . ? C7 C6 C4 155(3) . . ? 014 As1 06 106.8(2) 3_445 . ? 014 As1 03 111.4(2) 3 445 . ? O6 As1 O3 113.9(2) . . ? O14 As1 O15 107.3(2) 3_445 5_565 ? O6 As1 O15 109.4(2) . 5_565 ? O3 As1 O15 107.8(2) . 5_565 ? 012 As2 011 111.7(2) . . ? 012 As2 016 104.9(2) . . ? O11 As2 O16 111.8(2) . . ? 012 As2 010 111.8(2) . . ? O11 As2 O10 104.9(2) . . ? 016 As2 010 111.9(2) . . ? O7 As3 O4 109.1(2) . . ? 07 As3 08 113.7(2) . . ? O4 As3 O8 112.3(2) . . ? O7 As3 O2 113.4(2) . . ? O4 As3 O2 104.3(2) . . ? O8 As3 O2 103.5(2) . . ? O1 As4 O5 108.2(2) . . ? O1 As4 O19 115.4(2) . 2 655 ? O5 As4 O19 114.1(2) . 2_655 ? O1 As4 O9 106.3(2) . . ?

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O16 Be2 O15 102.8(5) . . ?
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O7 Be4 O5 113.3(6) 5_665 6_565 ?
O14 Be4 O5 112.1(5) . 6_565 ?
O7 Be4 O2 110.8(5) 5 665 . ?
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'SHELXL-97 (Sheldrick, 2008)' _computing_structure_refinement _computing_molecular_graphics ? _computing_publication_material ? _refine_special_details ; Refinement of F^2^ against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2^, conventional R-factors R are based on F, with F set to zero for negative $F^{2^{-}}$. The threshold expression of $F^2^ > 2 \setminus (F^2^)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on $F^{2^{-}}$ are statistically about twice as large as those based on F, and Rfactors based on ALL data will be even larger. ; _refine_ls_structure_factor_coef Fsqd full _refine_ls_matrix_type _refine_ls_weighting_scheme calc _refine_ls_weighting_details 'calc w=1/[\s^2^(Fo^2^)+(0.0231P)^2^+2.1223P] where P=(Fo^2^+2Fc^2^)/3' _atom_sites_solution_primary direct _atom_sites_solution_secondary difmap _atom_sites_solution_hydrogens geom _refine_ls_hydrogen_treatment mixed _refine_ls_extinction_method none _refine_ls_extinction_coef ? refine ls number reflns 1339 _refine_ls_number_parameters 111 _refine_ls_number_restraints 0 _refine_ls_R_factor_all 0.0224 _refine_ls_R_factor_gt 0.0200 0.0507 _refine_ls_wR_factor_ref 0.0486 _refine_ls_wR_factor_gt _refine_ls_goodness_of_fit_ref 0.835 _refine_ls_restrained_S_all 0.835 _refine_ls_shift/su_max 0.031 refine ls shift/su mean 0.005 loop_ _atom_site_label _atom_site_type_symbol _atom_site_fract_x _atom_site_fract_y _atom_site_fract_z _atom_site_U_iso_or_equiv _atom_site_adp_type _atom_site_occupancy _atom_site_symmetry_multiplicity _atom_site_calc_flag _atom_site_refinement_flags _atom_site_disorder_assembly _atom_site_disorder_group 07 0 0.5780(3) 0.90359(17) 0.6656(2) 0.0108(3) Uani 1 1 d . . . 06 0 0.7668(3) 0.60025(16) 0.5330(2) 0.0108(3) Uani 1 1 d . . . 05 0 0.9501(3) 0.80366(15) 0.6726(2) 0.0090(3) Uani 1 1 d . . . Bel Be 0.9723(5) 0.6962(3) 0.5524(3) 0.0084(5) Uani 1 1 d . . . Be2 Be 0.8085(4) 0.9236(3) 0.6250(4) 0.0085(5) Uani 1 1 d . . .

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H3 H 1.025(6) 0.812(3) 0.749(5) 0.027(10) Uiso 1 1 d . . .
H4 H 0.720(6) 0.591(3) 0.605(5) 0.026(9) Uiso 1 1 d . . .
H5 H 0.781(6) 0.530(4) 0.493(5) 0.041(11) Uiso 1 1 d . . .
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Be2 0.0062(13) 0.0098(13) 0.0094(13) 0.0013(10) 0.0018(10) 0.0007(10)
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04 0.0084(7) 0.0109(8) 0.0076(7) 0.0006(6) 0.0026(6) 0.0025(6)
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All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes)
 are estimated using the full covariance matrix. The cell s.u.'s are taken
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 and torsion angles; correlations between s.u.'s in cell parameters are only
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O6 Bel 1.678(3) . ?
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O5 Be2 1.604(3) . ?
Be1 03 1.620(3) . ?
Bel 02 1.640(3) . ?
Be2 01 1.622(3) . ?
Be2 04 1.625(3) . ?
As1 01 1.6754(15) . ?
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0.999

27.48

0.999

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0.095

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O5 Be1 O2 111.89(19) . . ?
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O3 Be1 O6 107.80(18) . . ?
O2 Be1 O6 103.08(17) . . ?
O5 Be2 O1 113.30(19) . . ?
O5 Be2 O4 111.00(19) . . ?
O1 Be2 O4 109.52(19) . . ?
O5 Be2 O7 109.13(19) . . ?
O1 Be2 O7 106.19(18) . . ?
O4 Be2 O7 107.44(18) . . ?
O1 As1 O2 110.48(8) . 3_776 ?
O1 As1 O3 105.36(8) . 2_756 ?
O2 As1 O3 110.75(8) 3_776 2_756 ?
O1 As1 O4 112.29(8) . 3_776 ?
O2 As1 O4 109.09(8) 3_776 3_776 ?
O3 As1 O4 108.83(8) 2_756 3_776 ?
Be1 03 As1 127.30(14) . 2_746 ?
Be1 02 As1 124.85(14) . 3_776 ?
Be2 O1 As1 125.41(14) . . ?
Be2 04 As1 125.97(14) . 3 776 ?
_diffrn_measured_fraction_theta_max
_diffrn_reflns_theta_full
_diffrn_measured_fraction_theta_full
_refine_diff_density_max 0.362
```

_refine_diff_density_min

_refine_diff_density_rms

Section 3. BAF1125 Output from "TOTOPOL", version 1.68, 20 May 2010). Written by Mike Treacy, with input from Srinivasen Srivilliputhur, Martin Foster, Keith Randall.

Report for the framework in file "temp.cif"

There are 20 T-atoms per unit cell There are 37 O-atoms per unit cell

```
Framework density = 21.44 T-atoms per nm<sup>3</sup>
Material density = 2.313 grams per cm<sup>3</sup> (excluding extra-framework material)
```

Cell volume = 932.9 Angstrom³ Available Volume = 527.8 +/- 1.5 Angstrom³ Occupiable Volume = 31.8 +/- 0.5 Angstrom³ Available Area = 719.3 +/- 1.5 Angstrom² Occupiable Area = 162.3 +/- 2.4 Angstrom²

```
----- T-O Analysis -----
```

```
[As] Ideal TO distance = 1.671 Angstroms
T1 -- O2 = 1.6878 Angstrom
T1 -- O11 = 1.6751 Angstrom
T1 -- O13 = 1.6779 Angstrom
T1 -- O16 = 1.6866 Angstrom
mean = 1.6818 Angstrom
t1 = 0.011486
t2 = 0.006330
[As] Ideal TO distance = 1.671 Angstroms
T2 -- O6 = 1.6878 Angstrom
```

```
12 - 06 = 1.68/8 Angstrom
```

```
T2 -- O9 = 1.6779 Angstrom
T2 -- O12 = 1.6866 Angstrom
```

T2 -- O15 = 1.6751 Angstrom mean = 1.6818 Angstrom t1 = 0.011486

```
t2 = 0.006680
```

[As] Ideal TO distance = 1.671 Angstroms T3 -- O3 = 1.6751 Angstrom T3 -- O5 = 1.6779 Angstrom T3 -- O8 = 1.6866 Angstrom T3 -- O10 = 1.6878 Angstrom mean = 1.6818 Angstrom t1 = 0.011486 t2 = 0.006098

```
[As] Ideal TO distance = 1.671 Angstroms
T4 -- O1 = 1.6779 Angstrom
T4 - O4 = 1.6866 Angstrom
T4 -- O7 = 1.6751 Angstrom
T4 -- O14 = 1.6878 Angstrom
   mean = 1.6818 Angstrom
    t1 = 0.011486
    t2 = 0.011211
[As] Ideal TO distance = 1.671 Angstroms
T5 -- O17 = 1.6769 Angstrom
T5 -- O18 = 1.6780 Angstrom
T5 -- O20 = 1.6870 Angstrom
T5 -- O23 = 1.6843 Angstrom
   mean = 1.6816 Angstrom
    t1 = 0.008147
    t2 = 0.003455
[As] Ideal TO distance = 1.671 Angstroms
T6 -- O19 = 1.6843 Angstrom
T6 -- O21 = 1.6769 Angstrom
T6 -- O22 = 1.6780 Angstrom
T6 -- O24 = 1.6870 Angstrom
   mean = 1.6816 Angstrom
    t1 = 0.008147
    t2 = 0.004537
[As] Ideal TO distance = 1.671 Angstroms
T7 -- O25 = 1.6769 Angstrom
T7 -- O26 = 1.6780 Angstrom
T7 -- O28 = 1.6870 Angstrom
T7 -- O31 = 1.6843 Angstrom
   mean = 1.6816 Angstrom
    t1 = 0.008147
    t2 = 0.003455
[As] Ideal TO distance = 1.671 Angstroms
T8 -- O27 = 1.6843 Angstrom
T8 -- O29 = 1.6769 Angstrom
T8 -- O30 = 1.6780 Angstrom
T8 -- O32 = 1.6870 Angstrom
   mean = 1.6816 Angstrom
    t1 = 0.008146
    t2 = 0.004537
```

```
[Be] Ideal TO distance = 1.634 Angstroms
T9 -- O2 = 1.6270 Angstrom
T9 -- O34 = 1.6154 Angstrom
T9 -- O17 = 1.6295 Angstrom
   mean = 1.6240 Angstrom
[Be] Ideal TO distance = 1.634 Angstroms
T10 - O6 = 1.6270 Angstrom
T10 -- O21 = 1.6295 Angstrom
T10 -- O35 = 1.6154 Angstrom
   mean = 1.6240 Angstrom
[Be] Ideal TO distance = 1.634 Angstroms
T11 - O10 = 1.6270 Angstrom
T11 -- O36 = 1.6154 Angstrom
T11 -- O25 = 1.6295 Angstrom
   mean = 1.6240 Angstrom
[Be] Ideal TO distance = 1.634 Angstroms
T12 - O14 = 1.6270 Angstrom
T12 -- O29 = 1.6295 Angstrom
T12 -- O33 = 1.6256 Angstrom
T12 - O37 = 1.6154 Angstrom
   mean = 1.6244 Angstrom
    t1 = 0.024766
    t2 = 0.022086
[Be] Ideal TO distance = 1.634 Angstroms
T13 - O1 = 1.6209 Angstrom
T13 - O3 = 1.6475 Angstrom
T13 - O18 = 1.6408 Angstrom
T13 -- O37 = 1.6304 Angstrom
   mean = 1.6349 Angstrom
    t1 = 0.010226
    t2 = 0.006590
[Be] Ideal TO distance = 1.634 Angstroms
T14 - O5 = 1.6209 Angstrom
T14 -- O36 = 1.6304 Angstrom
T14 - O7 = 1.6475 Angstrom
T14 - O22 = 1.6408 Angstrom
   mean = 1.6349 Angstrom
    t1 = 0.010225
    t2 = 0.006468
```

```
[Be] Ideal TO distance = 1.634 Angstroms
```

T15 - O9 = 1.6209 Angstrom T15 -- O11 = 1.6475 Angstrom T15 - O26 = 1.6408 Angstrom T15 -- O35 = 1.6304 Angstrom mean = 1.6349 Angstrom t1 = 0.010226t2 = 0.006590[Be] Ideal TO distance = 1.634 Angstroms T16 -- O13 = 1.6209 Angstrom T16 -- O34 = 1.6304 Angstrom T16 -- O30 = 1.6408 Angstrom T16 - O15 = 1.6475 Angstrom mean = 1.6349 Angstrom t1 = 0.010225t2 = 0.006590[Be] Ideal TO distance = 1.634 Angstroms T17 - O4 = 1.6338 Angstrom T17 -- O20 = 1.6515 Angstrom T17 - O19 = 1.6662 Angstrom mean = 1.6505 Angstrom [Be] Ideal TO distance = 1.634 Angstroms T18 - O23 = 1.6662 Angstrom T18 -- O24 = 1.6515 Angstrom T18 - 08 = 1.6338 Angstrom mean = 1.6505 Angstrom [Be] Ideal TO distance = 1.634 Angstroms T19 -- O12 = 1.6338 Angstrom T19 -- O28 = 1.6515 Angstrom T19 - O27 = 1.6662 Angstrom mean = 1.6505 Angstrom [Be] Ideal TO distance = 1.634 Angstroms T20 - O31 = 1.6662 Angstrom T20 - O32 = 1.6515 Angstrom T20 -- O33 = 1.6499 Angstrom T20 - O16 = 1.6338 Angstrom mean = 1.6503 Angstrom t1 = 0.014317t2 = 0.009278**T-O SUMMARY** Range = 1.6154 A <--> 1.6878 A

Mean = 1.6560 AStdDev = 0.0253 A

----- O-T-O Analysis -----------O2 - T1 - O11 = 109.250 degrees ; O2 - O11 = 2.7420 Angstrom O2 - T1 - O13 = 108.846 degrees ; O2 - O13 = 2.7374 Angstrom O2 - T1 - O16 = 109.690 degrees ; O2 - O16 = 2.7589 Angstrom O11 - T1 - O13 = 107.557 degrees ; O11 - O13 = 2.7050 Angstrom O11 - T1 - O16 = 109.272 degrees ; O11 - O16 = 2.7415 Angstrom O13 -- T1 -- O16 = 112.167 degrees ; O13 -- O16 = 2.7921 Angstrom O6 - T2 - O9 = 108.846 degrees ; O6 - O9 = 2.7374 Angstrom O6 - T2 - O12 = 109.690 degrees ; O6 - O12 = 2.7589 Angstrom O6 - T2 - O15 = 109.250 degrees ; O6 - O15 = 2.7420 Angstrom O9 - T2 - O12 = 112.167 degrees ; O9 - O12 = 2.7921 Angstrom O9 - T2 - O15 = 107.557 degrees ; O9 - O15 = 2.7050 Angstrom O12 - T2 - O15 = 109.272 degrees ; O12 - O15 = 2.7415 Angstrom $O_3 - T_3 - O_5 = 107.557$ degrees; $O_3 - O_5 = 2.7050$ Angstrom O3 - T3 - O8 = 109.272 degrees; O3 - O8 = 2.7415 Angstrom O3 - T3 - O10 = 109.250 degrees; O3 - O10 = 2.7420 Angstrom O5 - T3 - O8 = 112.167 degrees; O5 - O8 = 2.7921 Angstrom O5 - T3 - O10 = 108.846 degrees ; O5 - O10 = 2.7374 Angstrom O8 - T3 - O10 = 109.690 degrees ; O8 - O10 = 2.7589 Angstrom O1 - T4 - O4 = 112.167 degrees; O1 - O4 = 2.7921 Angstrom O1 - T4 - O7 = 107.557 degrees; O1 - O7 = 2.7050 Angstrom O1 - T4 - O14 = 108.846 degrees ; O1 - O14 = 2.7374 Angstrom O4 - T4 - O7 = 109.272 degrees; O4 - O7 = 2.7415 Angstrom O4 -- T4 -- O14 = 109.690 degrees ; O4 -- O14 = 2.7589 Angstrom O7 - T4 - O14 = 109.250 degrees ; O7 - O14 = 2.7420 Angstrom O17 - T5 - O18 = 110.669 degrees ; O17 - O18 = 2.7593 Angstrom O17 - T5 - O20 = 109.133 degrees ; O17 - O20 = 2.7409 Angstrom O17 - T5 - O23 = 108.332 degrees ; O17 - O23 = 2.7250 Angstrom O18 - T5 - O20 = 109.939 degrees ; O18 - O20 = 2.7555 Angstrom O18 - T5 - O23 = 108.698 degrees ; O18 - O23 = 2.7322 Angstrom O20 - T5 - O23 = 110.050 degrees ; O20 - O23 = 2.7625 Angstrom O19 - T6 - O21 = 108.332 degrees ; O19 - O21 = 2.7250 Angstrom O19 - T6 - O22 = 108.698 degrees ; O19 - O22 = 2.7322 Angstrom O19 - T6 - O24 = 110.050 degrees ; O19 - O24 = 2.7625 Angstrom O21 - T6 - O22 = 110.669 degrees ; O21 - O22 = 2.7593 Angstrom O21 - T6 - O24 = 109.133 degrees ; O21 - O24 = 2.7409 Angstrom O22 -- T6 -- O24 = 109.939 degrees ; O22 -- O24 = 2.7555 Angstrom

O25 - T7 - O26 = 110.669 degrees ; O25 - O26 = 2.7593 Angstrom O25 - T7 - O28 = 109.133 degrees ; O25 - O28 = 2.7409 Angstrom O25 - T7 - O31 = 108.332 degrees ; O25 - O31 = 2.7250 Angstrom O26 - T7 - O28 = 109.939 degrees ; O26 - O28 = 2.7555 Angstrom O26 - T7 - O31 = 108.698 degrees ; O26 - O31 = 2.7322 Angstrom O28 - T7 - O31 = 110.050 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 110.050 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 110.050 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 110.050 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 110.050 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 108.698 degrees ; O28 - O31 = 2.7625 Angstrom O28 - T7 - O31 = 0.050 degrees ; O28 - O30 degrees ; O30 - O30 degrees ; O30 -

O27 -- T8 -- O29 = 108.332 degrees ; O27 -- O29 = 2.7250 Angstrom O27 -- T8 -- O30 = 108.698 degrees ; O27 -- O30 = 2.7322 Angstrom O27 -- T8 -- O32 = 110.050 degrees ; O27 -- O32 = 2.7625 Angstrom O29 -- T8 -- O30 = 110.669 degrees ; O29 -- O30 = 2.7593 Angstrom O29 -- T8 -- O32 = 109.133 degrees ; O29 -- O32 = 2.7409 Angstrom O30 -- T8 -- O32 = 109.939 degrees ; O30 -- O32 = 2.7555 Angstrom

O2 -- T9 -- O34 = 111.000 degrees ; O2 -- O34 = 2.6722 Angstrom O2 -- T9 -- O17 = 101.401 degrees ; O2 -- O17 = 2.5200 Angstrom O34 -- T9 -- O17 = 112.486 degrees ; O34 -- O17 = 2.6978 Angstrom

O6 -- T10 -- O21 = 101.401 degrees ; O6 -- O21 = 2.5200 Angstrom O6 -- T10 -- O35 = 111.000 degrees ; O6 -- O35 = 2.6722 Angstrom O21 -- T10 -- O35 = 112.486 degrees ; O21 -- O35 = 2.6978 Angstrom

O10 -- T11 -- O36 = 111.000 degrees ; O10 -- O36 = 2.6722 Angstrom O10 -- T11 -- O25 = 101.401 degrees ; O10 -- O25 = 2.5200 Angstrom O36 -- T11 -- O25 = 112.486 degrees ; O36 -- O25 = 2.6978 Angstrom

O14 -- T12 -- O29 = 101.401 degrees ; O14 -- O29 = 2.5200 Angstrom O14 -- T12 -- O33 = 113.353 degrees ; O14 -- O33 = 2.7179 Angstrom O14 -- T12 -- O37 = 111.000 degrees ; O14 -- O37 = 2.6722 Angstrom O29 -- T12 -- O33 = 109.182 degrees ; O29 -- O33 = 2.6530 Angstrom O29 -- T12 -- O37 = 112.486 degrees ; O29 -- O37 = 2.6978 Angstrom O33 -- T12 -- O37 = 109.275 degrees ; O33 -- O37 = 2.6431 Angstrom

O1 -- T13 -- O3 = 109.427 degrees ; O1 -- O3 = 2.6679 Angstrom O1 -- T13 -- O18 = 110.138 degrees ; O1 -- O18 = 2.6740 Angstrom O1 -- T13 -- O37 = 111.759 degrees ; O1 -- O37 = 2.6916 Angstrom O3 -- T13 -- O18 = 106.074 degrees ; O3 -- O18 = 2.6274 Angstrom O3 -- T13 -- O37 = 107.473 degrees ; O3 -- O37 = 2.6430 Angstrom O18 -- T13 -- O37 = 111.752 degrees ; O18 -- O37 = 2.7080 Angstrom

O5 -- T14 -- O36 = 111.759 degrees ; O5 -- O36 = 2.6916 Angstrom O5 -- T14 -- O7 = 109.427 degrees ; O5 -- O7 = 2.6679 Angstrom O5 -- T14 -- O22 = 110.138 degrees ; O5 -- O22 = 2.6740 Angstrom O36 -- T14 -- O7 = 107.473 degrees ; O36 -- O7 = 2.6430 Angstrom O36 -- T14 -- O22 = 111.752 degrees ; O36 -- O22 = 2.7080 Angstrom O7 -- T14 -- O22 = 106.074 degrees ; O7 -- O22 = 2.6274 Angstrom

O9 -- T15 -- O11 = 109.427 degrees ; O9 -- O11 = 2.6679 Angstrom O9 -- T15 -- O26 = 110.138 degrees ; O9 -- O26 = 2.6740 Angstrom O9 -- T15 -- O35 = 111.759 degrees ; O9 -- O35 = 2.6916 Angstrom O11 -- T15 -- O26 = 106.074 degrees ; O11 -- O26 = 2.6274 Angstrom O11 -- T15 -- O35 = 107.473 degrees ; O11 -- O35 = 2.6430 Angstrom O26 -- T15 -- O35 = 111.752 degrees ; O26 -- O35 = 2.7080 Angstrom

O13 -- T16 -- O34 = 111.759 degrees ; O13 -- O34 = 2.6916 Angstrom O13 -- T16 -- O30 = 110.138 degrees ; O13 -- O30 = 2.6740 Angstrom O13 -- T16 -- O15 = 109.427 degrees ; O13 -- O15 = 2.6679 Angstrom O34 -- T16 -- O30 = 111.752 degrees ; O34 -- O30 = 2.7080 Angstrom O34 -- T16 -- O15 = 107.473 degrees ; O34 -- O15 = 2.6430 Angstrom O30 -- T16 -- O15 = 106.074 degrees ; O30 -- O15 = 2.6274 Angstrom

O4 -- T17 -- O20 = 112.909 degrees ; O4 -- O20 = 2.7381 Angstrom O4 -- T17 -- O19 = 108.753 degrees ; O4 -- O19 = 2.6825 Angstrom O20 -- T17 -- O19 = 109.308 degrees ; O20 -- O19 = 2.7061 Angstrom

O23 - T18 - O24 = 109.308 degrees ; O23 - O24 = 2.7061 Angstrom O23 - T18 - O8 = 108.753 degrees ; O23 - O8 = 2.6825 Angstrom O24 - T18 - O8 = 112.909 degrees ; O24 - O8 = 2.7381 Angstrom

O12 -- T19 -- O28 = 112.909 degrees ; O12 -- O28 = 2.7381 Angstrom O12 -- T19 -- O27 = 108.753 degrees ; O12 -- O27 = 2.6825 Angstrom O28 -- T19 -- O27 = 109.308 degrees ; O28 -- O27 = 2.7061 Angstrom

O31 -- T20 -- O32 = 109.308 degrees ; O31 -- O32 = 2.7061 Angstrom O31 -- T20 -- O33 = 107.044 degrees ; O31 -- O33 = 2.6664 Angstrom O31 -- T20 -- O16 = 108.753 degrees ; O31 -- O16 = 2.6825 Angstrom O32 -- T20 -- O33 = 110.607 degrees ; O32 -- O33 = 2.7143 Angstrom O32 -- T20 -- O16 = 112.909 degrees ; O32 -- O16 = 2.7381 Angstrom O33 -- T20 -- O16 = 108.033 degrees ; O33 -- O16 = 2.6571 Angstrom

O-T-O SUMMARY Range = 101.4008 deg <--> 113.3528 deg Mean = 109.4296 deg StdDev = 2.3281 deg

O--O SUMMARY Range = 2.5200 A <--> 2.7921 A Mean = 2.7056 A StdDev = 0.0554 A

T-T-T Analysis
T-O-T Analysis
T4 O1 T13 = 125.520 degrees ; T4 T13 = 2.9330 Angstrom
T1 O2 T9 = 123.192 degrees ; T1 T9 = 2.9159 Angstrom
T3 O3 T13 = 123.706 degrees ; T3 T13 = 2.9297 Angstrom
T4 O4 T17 = 122.956 degrees ; T4 T17 = 2.9175 Angstrom
T3 O5 T14 = 125.520 degrees ; T3 T14 = 2.9330 Angstrom
T2 O6 T10 = 123.192 degrees ; T2 T10 = 2.9159 Angstrom
T4 O7 T14 = 123.706 degrees ; T4 T14 = 2.9297 Angstrom
T3 O8 T18 = 122.956 degrees ; T3 T18 = 2.9175 Angstrom
T2 O9 T15 = 125.520 degrees ; T2 T15 = 2.9330 Angstrom
T3 O10 T11 = 123.192 degrees ; T3 T11 = 2.9159 Angstrom
T1 O11 T15 = 123.706 degrees ; T1 T15 = 2.9297 Angstrom
T2 O12 T19 = 122.956 degrees ; T2 T19 = 2.9175 Angstrom
T1 O13 T16 = 125.520 degrees ; T1 T16 = 2.9330 Angstrom
T4 O14 T12 = 123.192 degrees ; T4 T12 = 2.9159 Angstrom
T2 O15 T16 = 123.706 degrees ; T2 T16 = 2.9297 Angstrom
T1 O16 T20 = 122.956 degrees ; T1 T20 = 2.9175 Angstrom
T5 O17 T9 = 124.382 degrees ; T5 T9 = 2.9246 Angstrom
T5 O18 T13 = 122.204 degrees ; T5 T13 = 2.9056 Angstrom
T6 O19 T17 = 122.280 degrees ; T6 T17 = 2.9344 Angstrom
T5 O20 T17 = 121.576 degrees ; T5 T17 = 2.9140 Angstrom

T6 O21 T10 = 124.382 degrees ; T6 T10 = 2.9246 Angstrom
T6 O22 T14 = 122.204 degrees ; T6 T14 = 2.9056 Angstrom
T5 O23 T18 = 122.280 degrees ; T5 T18 = 2.9344 Angstrom
T6 O24 T18 = 121.576 degrees ; T6 T18 = 2.9140 Angstrom
T7 O25 T11 = 124.382 degrees ; T7 T11 = 2.9246 Angstrom
T7 O26 T15 = 122.204 degrees ; T7 T15 = 2.9056 Angstrom
T8 O27 T19 = 122.280 degrees ; T8 T19 = 2.9344 Angstrom
T7 O28 T19 = 121.576 degrees ; T7 T19 = 2.9140 Angstrom
T8 O29 T12 = 124.382 degrees ; T8 T12 = 2.9246 Angstrom
T8 O30 T16 = 122.204 degrees ; T8 T16 = 2.9056 Angstrom
T7 O31 T20 = 122.280 degrees ; T7 T20 = 2.9344 Angstrom
T8 O32 T20 = 121.576 degrees ; T8 T20 = 2.9140 Angstrom
T12 O33 T20 = 120.762 degrees ; T12 T20 = 2.8476 Angstrom
T9 O34 T16 = 119.475 degrees ; T9 T16 = 2.8036 Angstrom
T10 O35 T15 = 119.475 degrees ; T10 T15 = 2.8036 Angstrom
T11 O36 T14 = 119.475 degrees ; T11 T14 = 2.8036 Angstrom
T12 O37 T13 = 119.475 degrees ; T12 T13 = 2.8036 Angstrom

T-O-T SUMMARY Range = 119.4748 deg <--> 125.5201 deg Mean = 122.7547 deg StdDev = 1.6700 deg T--T SUMMARY Range = 2.8036 A <--> 2.9344 A

Range = 2.8036 A <--> 2.9344 A Mean = 2.9070 A StdDev = 0.0395 A

----- Topological Analysis ------_____ T1: multiplicity = 1Coordination Sequence = 1 4 8 17 30 50 66 96 116 152 198 222 277 324 364 424 508 TD10 = 738Circuit symbol = 3.8.4.8.5.8Weight = 20Vertex symbol = 3.8.4.8.8Weight = 23T2: multiplicity = 1Coordination Sequence = 1 4 7 16 29 47 62 95 118 146 189 228 264 318 378 418 481 TD10 = 714Circuit symbol = 3.8.4.8.5.8Weight = 20Vertex symbol = 3.8.4.8.8.8Weight = 23T3: multiplicity = 1Coordination Sequence = 1 4 7 17 30 50 66 95 114 157 195 223 272 333 355 436 499 TD10 = 736Circuit symbol = 3.8.4.8.5.8Weight = 20Vertex symbol = 3.8.4.8.8Weight = 23T4: multiplicity = 1Coordination Sequence = 1 4 8 17 29 51 64 98 122 155 187 240 264 327 377 437 473 TD10 = 736Circuit symbol = 3.8.4.8.5.8Weight = 20Vertex symbol = 3.8.4.8.8Weight = 23T5: multiplicity = 1Coordination Sequence = 1 4 8 18 31 47 64 94 118 151 188 230 268 321 367 434 478 TD10 = 724Circuit symbol = $4.8.8.8.8.10_{4}$ Weight = 34Vertex symbol = $4.8.8.8.8.10_{3}$ Weight = 34

```
T6: multiplicity = 1
Coordination Sequence =
  1 4 8 17 32 48 65 94 120 155 190 226 269 335 357 433 490
TD10 = 734
Circuit symbol = 4.8.8.8.9_{2}
Weight = 31
Vertex symbol = 4.8.8.8.9_{2}
Weight = 31
T7: multiplicity = 1
Coordination Sequence =
  1 4 9 18 33 52 67 96 127 152 195 235 278 317 386 426 495
TD10 = 754
Circuit symbol = 4.8.8.8.8.10_{4}
Weight = 34
Vertex symbol = 4.8.8.8.8.10_{3}
Weight = 34
T8: multiplicity = 1
Coordination Sequence =
  1 4 8 17 31 46 65 96 117 154 194 223 277 329 365 427 502
TD10 = 733
Circuit symbol = 3.8.4.8.5.8
Weight = 20
Vertex symbol = 3.8.4.8.8
Weight = 23
T9: multiplicity = 1
Coordination Sequence =
  1 3 7 15 28 48 63 90 116 151 182 236 264 318 364 428 483
TD10 = 704
Circuit symbol = 3.8_{2}.9_{3}
Weight = 15
Vertex symbol = 3.8_{2}.10_{5}
Weight = 28
T10: multiplicity = 1
Coordination Sequence =
  1 3 7 15 29 45 61 90 119 142 179 230 257 309 375 413 466
TD10 = 691
Circuit symbol = 3.8_{2}.9_{6}
Weight = 25
Vertex symbol = 3.8_{2}.9_{3}
Weight = 25
```

```
T11: multiplicity = 1
Coordination Sequence =
  1 3 7 16 30 51 67 96 118 158 187 246 258 334 367 439 476
TD10 = 734
Circuit symbol = 3.8_{2}.9_{3}
Weight = 15
Vertex symbol = 3.8_{2}.10_{5}
Weight = 28
T12: multiplicity = 1
Coordination Sequence =
  1 4 8 17 32 48 68 97 128 147 195 236 271 321 395 417 487
TD10 = 745
Circuit symbol = 3.3.8_{2}.9_{3}.9_{3}.9_{3}
Weight = 28
Vertex symbol = 3.3.8_{2}.9_{3}.*.*
Weight = 28
T13: multiplicity = 1
Coordination Sequence =
  1 4 9 16 33 46 68 97 121 150 198 224 274 330 375 423 503
TD10 = 743
Circuit symbol = 3.8_{2}.4.9_{3}.5.8
Weight = 26
Vertex symbol = 3.8_{2}.4.9_{2}.8.9
Weight = 29
T14: multiplicity = 1
Coordination Sequence =
  1 4 8 16 34 47 69 94 124 152 199 225 280 321 376 425 507
TD10 = 748
Circuit symbol = 3.8 \{2\}.4.9.5.8
Weight = 21
Vertex symbol = 3.8_{2}. 4.10_{4}.
Weight = 31
T15: multiplicity = 1
Coordination Sequence =
  1 4 8 17 33 45 69 96 118 152 195 226 270 331 362 435 488
TD10 = 738
Circuit symbol = 3.8_{2}.4.9_{3}.5.8
Weight = 27
Vertex symbol = 3.8_{2}.4.9_{2}.8.9
Weight = 30
T16: multiplicity = 1
```

```
Coordination Sequence =
  1 4 8 15 31 47 64 91 120 148 190 229 266 322 367 423 489
TD10 = 719
Circuit symbol = 3.8_{2}.4.9.5.8
Weight = 21
Vertex symbol = 3.8_{2}.4.10_{4}.8.10
Weight = 31
T17: multiplicity = 1
Coordination Sequence =
  1 3 8 16 30 46 66 93 121 149 195 220 273 323 370 418 505
TD10 = 728
Circuit symbol = 4.8.8_{2}
Weight = 20
Vertex symbol = 4.8.8_{2}
Weight = 20
T18: multiplicity = 1
Coordination Sequence =
  1 3 8 15 31 46 64 90 119 143 192 225 262 315 380 405 491
TD10 = 712
Circuit symbol = 4.8.8_{2}
Weight = 20
Vertex symbol = 4.8.8_{2}
Weight = 20
T19: multiplicity = 1
Coordination Sequence =
  1 3 8 16 30 45 66 92 120 151 195 222 269 338 357 424 504
TD10 = 727
Circuit symbol = 4.8.8_{2}
Weight = 20
Vertex symbol = 4.8.8_{2}
Weight = 20
T20: multiplicity = 1
Coordination Sequence =
  1 4 9 17 34 49 70 96 124 155 193 234 275 332 369 439 483
TD10 = 752
Circuit symbol = 3.8_{2}.4.9_{2}.5.8
Weight = 26
Vertex symbol = 3.8_{2}. 4.9.8.9_{2}
Weight = 31
<TD10> = 730.500
Average ring size = 6.4219
```

Section 4. VT PXD and combined TGA/DTA data from BAF1125

Figure S4.1 Variable temperature (25- 450°C) powder X-ray diffraction data (Bruker D8 $Cu_{K\alpha 1}$) from BAF1125; material shows main crystal reflections until >350°C.

VT PXD of BAF1125



Figure S4.2. Combined TGA/DTA trace for BAF1125 (Stanton-Redcroft 1500 thermobalance) showing evolution of ammonia starting at 300° C.



Thermogravimetric analysis of BAF1125

Section 5. The structure of BAF845.

Figure S5.1. The structure of BAF845 $[{H-pyridine}_{0.5}]^{0.5+} [As_2(As_{0.25}Be_{0.75})_2O_7(OH)_2]^{0.5-} (H_2O)_{0.65}$ showing the linked Be(O,OH)₄ and As(O,OH)₄ tetrahedra in green and purple respectively; pyridine molecules are shown, carbon-black, nitrogen-pale blue, and hydrogen as small grey spheres. Upper diagram is viewed down c and lower diagram perpendicular to c







Framework densities (FD) of aluminosilicate zeolites as known as beryllium containing zeotype analogues; IZA code is plotted as a function of increasing FD for FAU to ANA. BEN represents the **BAF1125**, $[NH_4^+]_2[As_2Be_3O_8(OH)_2]^{2-}$ topology showing a value similar to other small pore zeotypes MER, SOD, ABW and ANA. The values of AFI-SiAl and the structurally related BAF1011and also shown for comparison.