# Observation of a reversible Isomorphous Phase Transtion and an interplay of " $\sigma$ -hole" and " $\pi$ -hole" in Fmoc-Leu- $\psi$ [CH<sub>2</sub>-NCS]

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Data collection and Multipole details for the experimental charge density dataset of Fmoc– Leu–CH<sub>2</sub>NCS

#### **S1. Experimental Methods**

#### Single crystal X-ray diffraction

A good quality Single crystal of size ~ 0.3 mm was chosen using a polarizing microscope and affixed to a Hampton Research Cryoloop using Paratone-N oil. X-ray diffraction data at room temperature (resolution, d=0.77 Å) was collected on an Oxford Xcalibur (Mova) diffractometer equipped with an EOS CCD detector using MoK<sub>a</sub> radiation ( $\lambda = 0.71073$  Å). The crystal to detector distance was fixed at 45 mm and the scan width ( $\Delta \omega$ ) was 1° per frame during the data collection. The crystal was cooled to 100 K with a liquid nitrogen stream using an Oxford Instruments Cryojet-HT nitrogen gas-stream cooling device. A high resolution X-ray data set at 100K of charge density quality (d = 0.45 Å), with high redundancy and completeness of 100% was collected for the low temperature Z'=2 form. Cell refinement, data integration and reduction were carried out using the program CrysAlisPro.<sup>1</sup> Face indexing was done for the accurate numerical absorption correction. Sorting, scaling, and merging of the data sets were carried out using the program SORTAV.<sup>2</sup> The crystal structure was solved by direct methods using SHELXS97 and refined according to spherical-atom approximation (based on F<sup>2</sup>) using

SHELXL97 included in the WinGX suite.<sup>3, 4</sup> The hydrogen atoms were fixed stereochemically and the position and isotropic thermal parameters were allowed to refine in the spherical atom model for the room temperature form.

The reversibility of the phase transition was established by determining the unit cell parameters at different temperatures during the heating and cooling cycles from 290-100K in steps of 10K on the same crystal.

#### Multipole Refinement.

The charge density modeling and multipolar non–spherical atom refinements for Fmoc-Leu- $\psi$ [CH<sub>2</sub>-NCS] have been performed with XD2006<sup>5</sup> using the Hansen and Coppens multipole formalism.<sup>6</sup> The function minimized in the least-square procedure was  $\Sigma w \{|F_o|^2 - K|F_c|^2\}$ , with only those reflections with  $I > 3\sigma(I)$ . The core and valence scattering factors of all atoms were derived from Su, Coppens and Macchi wave functions.<sup>7, 8</sup> The multipole expansion was truncated at the hexadecapole level for the S atoms, octupole level for the O, N and C atoms and quadrupole level for the H atoms. Initially, the scale factor was refined against the whole resolution range of diffraction data. The scatter plots (Figure S3) showing the dependence of  $F_{obs}/F_{cal}$  with  $\sin\theta/\lambda$  and the variation of  $F_{obs}$  with  $F_{cal}$  clearly depicts the quality of the collected data sets. The positional and anisotropic displacement parameters of the non-hydrogen atoms were refined against the reflections with  $\sin\theta/\lambda > 0.7$  Å<sup>-1</sup>. In the next step, the position and displacement parameters of all non-hydrogen atoms were kept fixed to the obtained values and X—H bond lengths were constrained to the values determined by neutron diffraction experiments.<sup>9</sup> The isotropic displacement parameters for H-atoms were refined using reflections

 $\sin\theta/\lambda < 0.7$  Å<sup>-1</sup>. The converged model was used to calculate anisotropic displacement parameters of H-atoms using the SHADE2 analysis.<sup>10, 11</sup> Estimated ADPs for H-atoms were kept fixed during the subsequent multipole refinements and only monopole, bond directed dipole ( $d_z$ )

and quadrupole ( $q_{3z^2-1}$ ) components were allowed to refine. For non-hydrogen atoms, the scale, positional and anisotropic displacement parameters,  $P_{val}$ ,  $P_{lm}$ , upto octupole level (l=3),  $\kappa$  and  $\kappa'$  were allowed to refine in a stepwise manner, until the convergence was reached. Two molecules in the asymmetric unit were treated chemically equivalent except the terminal isothiocyanate group during the least-square refinement. Separate  $\kappa$  and  $\kappa'$  were used to define different atom types based on chemical environment. Anharmonic motion for the sulfur atoms was modeled with third and fourth-order Gram-Charlier components.<sup>12</sup> The resultant probability density function (pdf) indicated that this modeling was physically reasonable.

#### **S2.** Computational methods:

Two approaches have been considered for theoretical charge density analysis (i) generating theoretical structure factors from CRYSTAL14<sup>13</sup> followed by multipole modelling<sup>6</sup> in XD2006<sup>5</sup> at B3LYP/TZVP level<sup>14, 15</sup> (ii) obtaining topological features directly from wave function analysis using TOPOND program<sup>16</sup> as implemented in CRYSTAL14.

(i) The coordinates from final experimental charge density model was taken as input for periodic quantum mechanical calculations using CRYSTAL14. The single point calculation was performed at the B3LYP/TZVP level of theory. The shrinking factors (IS1, IS2 and IS3) along with the reciprocal lattice vectors were set to 4 (18 k–points in irreducible Brillouin zone). The bi-electronic Coulomb and exchange series values for the truncation parameter were set as ITOL1–ITOL4 = 7 and ITOL5 = 18, respectively. The level shifter was set to 0.7 Hartree/cycle

for better convergence. Upon convergence on energy ( $\sim 10^{-7}$  Hartree), the periodic wave functions were obtained and the XFAC keyword was used to generate the theoretical structure factors at the same resolution as observed from the experiments. The atomic positions were held fixed to the values obtained from the experimental charge density during the multipolar refinement with theoretical structure factors. All theoretical structure factors were assigned unit weights during the refinements based on the methodology followed in the literature. The anisotropic displacement parameters were set to zero to consider a static model and multipolar refinements of the theoretical data were carried out up to the same levels as those used for the experimental charge density modelling.

(ii) TOPOND<sup>16</sup> is considerably different from other existing implementations of QTAIM<sup>17</sup> for crystalline systems due to its interface with CRYSTAL package and thus becomes a powerful tool for applying QTAIM to molecules, polymers, surfaces and crystals, exploiting the full symmetry of each of these systems. It calculates full topological features of  $\rho(r)$  and  $\nabla^2 \rho(r)$  scalar fields along with other QTAIM descriptors directly from wave function analysis. The level of theory used is B3LYP/TZVP in our systems.

#### S3. CSD analysis

A Cambridge Structural Database (CSD v5.35 February 2014) analysis was carried out to investigate the number of reported structures of isothiocyanates and also to find out the propensity of forming the perpendicular N=C=S…N=C=S intermolecular interaction. It has been observed that though isothiocyanates are more common in organometallics, it is relatively rare as organic molecules. (Table S1) Moreover, the perpendicular interaction mode of the NCS groups is sparse (Table S1, Figure S1).

	Total No. of hits	No. of hits for specific intermolecular interactions*
N=C=S	$5359^{a}$	$154^{a}$
C-N=C=S	$\frac{400}{66^{a}}$	$1^a$ $0^b$

Table S1. Summary of CSD analysis

\*The interaction geometry is specified in Figure S1.<sup>a</sup>organics+ organometalics, <sup>b</sup>only organics, given in italics.



**Figure S1.** The perpendicular approach of the NCS groups are specified by three parameters,  $\theta_1 = 90^{\circ} \pm 30^{\circ}$ ,  $\theta_2 = 160^{\circ} \pm 20^{\circ}$  and  $d \le \text{sum of van der Waals radii of S and N + 0.3 Å$ 

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Figure S2a. ORTEP diagram (with 50% probability ellipsoid) of (a) Fmoc-Leu-CH<sub>2</sub>NCS



**Figure S2b.** ORTEP diagram (with 50% probability ellipsoid) of Fmoc–X–CH<sub>2</sub>NCS (b) X=Ile, (c) X=Val, (d) X=Ala.



**Figure S3**. Packing diagrams (a) projection along c axis in Fmoc–Leu–CH<sub>2</sub>NCS. The S···N distance is 3.29(1) Å in MOL1 (green) and 3.56(1) Å in MOL2 (blue). The edge to face C–H··· $\pi$  distance involving fluorene moiety is 3.08(1). (b) projection along c axis in Fmoc–Ile–CH<sub>2</sub>NCS showing N–H···O hydrogen bonds and face to face  $\pi$ ··· $\pi$  interaction involving fluorene moiety.



**Figure S4.** Experimental charge density in Fmoc–Leu–CH<sub>2</sub>NCS indicating the quality of the dataset; (a) Scatter plot depicting the variation of  $F_{obs}$  with  $F_{calc}$ , (b) Variation of  $F_{obs}/F_{calc}$  with  $\sin\theta/\lambda$ 



Figure S5. Fractal dimension plot of (a) experimental (b) theoretical multipole model



**Figure S6a.** (a) Residual (b) deformation and (c) Laplacian of the electron density maps of the isothiocyanate group in MOL1 obtained from experimental charge density analysis (1<sup>st</sup> row); second row depicts (d) residual (e) deformation and (f) Laplacian maps from theoretical multipole model.



**Figure S6b.** (a) Residual (b) deformation and (c) Laplacian of the electron density maps of the isothiocyanate group in MOL2 obtained from experimental charge density analysis (1<sup>st</sup> row); second row depicts (d) residual (e) deformation and (f) Laplacian maps from theoretical multipole model.



Figure S7. DSC thermograph of Fmoc–Leu–CH<sub>2</sub>NCS for heating and cooling cycles.

CCDC number	1030735	1030363					
Empirical Formula	C22 H24 N2 O2 S1	C22 H24 N2 O2 S1					
<b>C</b> rystal habit	Block	Block					
Crystal size (mm)	0.530 x 0.231 x 0.141	0.599 x 0.310 x 0.256					
Crystallizing solvent	Ethyl acetate: hexane	Ethyl acetate: hexane					
Crystallizing solvent	(1:1)	(1:1)					
Space Group	P 4 <sub>1</sub>	$P 4_1$					
a(Å)	12.4405(5)	17.4665(1)					
c(Å)	13.4141(8)	13.1291(1)					
Volume (Å <sup>3</sup> )	2076.1(2)	4005.41(4)					
Z	4	8					
Z'	1	2					
Formula weight	380.50	380.50					
Calculated density (g/cm <sup>3</sup> )	1.217	1.262					
F(0 0 0)	808	1616					
Radiation	Mo K <sub>α</sub> ( 0.71073 Å )	Mo K <sub>α</sub> ( 0.71073 Å )					
Temperature (K)	298 (2)	100(2)					
θ range (°)	2.6-26.0	2.6-50.1					
Measured reflections	10114	530944					
Observed reflection	5371	32688(42280)					
	Spherical atom refinement						
R_obs, wR2_obs	0.0596/0.1041	0.0390,0.0969					
GoF	1.027	1.0					
Max/min $\Delta \rho$ (e/ Å <sup>3</sup> )	0.235/-0.167	0.617/-0.529					
Data to parameter ratio	5371/250=21.5:1	42280/499=84.7					
	Multipole	refinement					
Refinement based on		$F^2$					
Observed reflections		27177					
[ I>3σ(I) ]		2/1//					
Parameters		940					
$R(F^2)$ , $wR(F^2)$		0.023, 0.046					
GoF		1.067					
Max/min $\Delta \rho$ (e/Å <sup>3</sup> )	-0.141/0.123						

**Table S2a**.Crystallographic data of Fmoc-Leu- $\psi$ [CH<sub>2</sub>NCS]

**Table S2b.** Crystallographic data of Fmoc–X– $\psi$ [CH<sub>2</sub>NCS], X=Ile, Val and Ala

CCDC number	1030364	1030365	1030366
Empirical Formula	Empirical Formula C22 H24 N2 O2 S1		C19 H18 N2 O2 S1
Crystal habit	plate	plate	plate
Crystal size (mm)	0.276 x 0.204 x 0.072	0.257 x 0.239 x 0.048	0.409 x 0.239 x 0.066
Crustellizing solvent	Ethyl acetate: hexane	Ethyl acetate: hexane	Ethyl acetate: hexane
Crystallizing solvent	(1:1)	(1:1)	(1:1)
Space Group	P 2 <sub>1</sub>	P 2 <sub>1</sub>	P 2 <sub>1</sub>
a(Å)	4.9386(3)	4.9807(2)	4.9690(2)
b(Å)	15.0974(9)	15.9306(6)	11.3897(4)
c(Å)	13.3932(15)	12.0456(5)	15.0388(5)
β(°)	97.286(7)	99.174(4)	91.707(3)

Volume (Å <sup>3</sup> )	990.53(14)	943.54(7)	850.75(5)				
Z	2	2	2				
Ζ'	1	1	1				
Formula weight	380.50	366.48	338.42				
Calculated density $(g/cm^3)$	1.276	1.290	1.321				
F(0 0 0)	404	388	356				
Radiation	Mo K <sub>α</sub> ( 0.71073 Å )	Mo K <sub>α</sub> ( 0.71073 Å )	Mo K <sub>α</sub> ( 0.71073 Å )				
Temperature (K)	100 (2)	100(2)	100(2)				
θ range (°)	2.7-26.0	2.6-26.0	2.7-26.0				
Measured reflections	7233	6646	6544				
Observed reflection	3881	3702	3343				
R_obs/ wR2_obs	0.0613/0.0938	0.0444/0.0812	0.0337/0.0695				
GoF	0.983	1.034	1.054				
Max/min $\Delta \rho$ (e/ Å <sup>3</sup> )	0.234/-0.204	0.189/-0.206	0.196/-0.198				
Data to parameter ratio	3881/250=15.5:1	3702/237=15.6:1	3343/222=15.1:1				

**Table S3**. H-bond geometry in Fmoc–Leu– $\psi$ [CH<sub>2</sub>NCS]

	D—H…A	D—H (Å)	H…A (Å)	D…A (Å)	∠D—H…A (°)	Symmetry
MOL1	N1—H1N…O2A	0.85(2)	2.17(2)	2.995(1)	164(2)	x,y,z
	C2—H2···Cg9 <sup>a</sup>	1.0812	3.314	4.321	155.49	
MOL2	N1A—H1NA …O2	0.85(2)	2.18(2)	3.007(1)	165(2)	-x+1,-y,+z+1/2
	C2A—H2A…Cg3 <sup>a</sup>	1.0824	3.085	4.033	146.68	
	<sup>a</sup> Call is the contraid of	fthe 6 members	dring CGA C7A	$C_{0} \wedge C_{0} \wedge C_{0$	C10A = C11A = Ca2 is	the contraid of

<sup>a</sup>Cg9 is the centroid of the 6-membered ring C6A—C7A—C8A—C9A—C10A—C11A. Cg3 is the centroid of the 6-membered ring C6—C7—C8—C9—C10—C11.

**Table S4.** Topological parameters obtained at the bond critical point (BCP) for NCS moiety in MOL1 and MOL2 of Fmoc–Leu– $\psi$ [CH<sub>2</sub>NCS]. r<sub>1</sub> and r<sub>2</sub> are the distances from the BCP to the first atom (A) and second atom (B), respectively. The interaction length, R<sub>ij</sub>= (r<sub>1</sub> +r<sub>2</sub>).<sup>a</sup>

	Atom	Atom	R <sub>ii</sub> (Å)	r <sub>1</sub> (Å)	r <sub>2</sub> (Å)	$\rho(\mathbf{r})$	$\nabla^2 \rho(\mathbf{r})$	$\lambda_1$	$\lambda_2$	λ3	3
	А	В	(A–B)	(A–CP)	(A–CP)	(eÅ <sup>-3</sup> )	(eÅ-5)				
MOL1	S1	C18	1.5891	0.842	0.747	1.82	-10.9	-10.23	-8.91	8.25	0.15
			1.5930	0.606	0.987	1.41	14.4	-4.39	-3.49	22.28	0.26
			1.5887	0.627	0.962	1.40	14.4				
	N2	C18	1.1817	0.754	0.428	3.16	-31.8	-28.66	-26.27	23.08	0.09
			1.1833	0.711	0.472	2.95	-28.2	-21.21	-20.55	13.58	0.03
			1.1812	0.765	0.416	3.00	-14.6				
MOL2	S1A	C18A	1.5914	0.882	0.710	1.81	-8.1	-10.59	-10.03	12.47	0.06
			1.6052	0.619	0.986	1.42	7.4	-4.47	-3.90	15.73	0.15
			1.5961	0.629	0.967	1.38	13.9				
	N2A	C18A	1.1685	0.7448	0.4237	3.04	-22.8	-25.29	-23.90	26.36	0.06
			1.1700	0.712	0.458	3.04	-29.8	-22.99	-21.82	14.97	0.05
			1.1669	0.758	0.409	3.02	-7.1				

<sup>a</sup> First/second/third row displays **experimental**/ theoretical multipole/TOPOND calculated values.

Data collection and multipole details of the experimental charge density of Fmoc-Leu-CH<sub>2</sub>NCS

```
#\#CIF 1.1
#
 Archive CIF produced by XD routine XDCIF
  Created on 14-Oct-10 at 08:01:53
#
# Using CIFtbx version 2.6.2 16 Jun 1998
#
 Dictionary name : cif_core.dic
# Dictionary vers : 2.3
# Request file : c:/winxd/lib/xd/xdcif.dat
# CIF files read : geo lsm
data_redo
_audit_creation_date '14-Oct-10 T08:01:53-00:00'
_audit_creation_method 'XD routine XDCIF'
_audit_conform_dict_name cif_core.dic
_audit_conform_dict_version 2.3
_audit_conform_dict_location ftp://ftp.iucr.org/pub/cif_core.dic
loop
_atom_type_symbol
_atom_type_description
_atom_type_scat_dispersion_real
_atom_type_scat_dispersion_imag
_atom_type_scat_source
S S 0.1246 0.1234
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
  0 0.0106 0.0060
0
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
N N 0.0061 0.0033
 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
н н 0.0000 0.0000
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
C C 0.0033 0.0016
 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
#
#
                CHEMICAL INFORMATION
#
#
                           ?
_chemical_name_common
_chemical_melting_point
                          ?
_chemical_formula_moiety
                          'C22 H24 N2 O2 S'
_chemical_formula_sum
                           'C22 H24 N2 O2 S'
chemical formula weight
                          380.50
#-----
#
#
                UNIT CELL INFORMATION
#
```

# loop\_ \_space\_group\_symop\_id \_space\_group\_symop\_operation\_xyz 1 + X, + Y, + Z2 - X, -Y, 1/2 + Z3 - Y, +X, 1/4 + Z4 + Y, -X, 3/4 + Z\_symmetry\_cell\_setting Tetragonal 'P 4w' \_symmetry\_space\_group\_name\_Hall \_symmetry\_space\_group\_name\_H-M 'P 41' \_symmetry\_Int\_Tables\_number 76 \_cell\_length\_a 17.46650(10)\_cell\_length\_b 17.46650(10)\_cell\_length\_c 13.12910(10)90 \_cell\_angle\_alpha 90 \_cell\_angle\_beta \_cell\_angle\_gamma 90 \_cell\_volume 4005.41(4)\_cell\_formula\_units\_Z 8 \_cell\_measurement\_temperature 100(2) \_cell\_measurement\_reflns\_used 106248 \_cell\_measurement\_theta\_min 3.0040 \_cell\_measurement\_theta\_max 43.8880 #-\_\_\_\_\_ # # CRYSTAL INFORMATION # # \_exptl\_crystal\_description block \_exptl\_crystal\_colour colourless exptl crystal size max 0.5992 0.3100 \_exptl\_crystal\_size\_mid \_exptl\_crystal\_size\_min 0.2556 ? \_exptl\_crystal\_size\_rad \_exptl\_crystal\_density\_meas ? 1.262 \_exptl\_crystal\_density\_diffrn \_exptl\_crystal\_density\_method 'Not Measured' \_exptl\_crystal\_F\_000 1616 \_exptl\_crystal\_density\_meas\_temp ? # # ABSORPTION CORRECTION # # \_\_\_\_\_ # loop exptl crystal face index h \_exptl\_crystal\_face\_index\_k \_exptl\_crystal\_face\_index\_l \_exptl\_crystal\_face\_perp\_dist

```
_exptl_oxdiff_crystal_face_indexfrac_h
_exptl_oxdiff_crystal_face_indexfrac_k
_exptl_oxdiff_crystal_face_indexfrac_l
_exptl_oxdiff_crystal_face_x
_exptl_oxdiff_crystal_face_y
exptl oxdiff crystal face z
-18 -17
           -1 0.1676 -17.8258 -16.9032 -1.1698 0.7845 -0.6022 0.1477
-20 -10
           7 0.1522 -19.9993 -10.4895 7.3699 0.7323 -0.5616 -0.3851
         13 0.1999 4.2840 16.6937 13.2219 -0.4089 0.3148 -0.8566
  4
      17
         14 0.1598 9.2059 -13.0523 14.0926 -0.4896 -0.7983 -0.3507
  9
     -13
 23
      1
          -7 0.1637 22.8914 0.8631 -6.7821 -0.8134 0.1948 0.5482
 -24
      -4
           3 0.1338 -24.0164 -4.2392 2.5160 0.9269 -0.2223 -0.3025
 23
      7
           2 0.1640 23.4429 7.1527 1.7033 -0.9712 0.2332 0.0488
 22
      -9
          -4 0.1550 22.4442 -8.8926 -3.6350 -0.7961 -0.2362 0.5572
 -23
      8
           1 0.1166 -23.2098 8.0058 1.3756 0.8591 0.2548 -0.4439
           15 0.1961 14.0517 3.0710 15.0244 -0.7587 -0.2242 -0.6116
      3
 14
 24
      -7
          1 0.1560 23.5989 -6.8018 1.2814 -0.9138 -0.2709 0.3025
  2
      -4 -18 0.3395 2.0044 -3.6699 -18.2484 0.1734 0.2816 0.9437
 -14
      20 -3 0.1125 -13.6575 20.0534 -3.1609 0.4933 0.8053 -0.3290
 -14
      -9 -13 0.2852 -13.9987 -8.9986 -13.0007 0.7551 -0.0401 0.6152
 14 -20
           1 0.1327 13.8024 -20.3537 0.9410 -0.4689 -0.7657 0.4403
          -2 0.1334 10.0752 22.3701 -1.5326 -0.4682 0.8622 -0.1931
 10
      22
           -1 0.1324 9.8451 22.5184 -1.0849 -0.4656 0.8574 -0.2192
 10
      23
         13 0.1833 13.0504 12.4330 12.6078 -0.7270 0.1752 -0.6639
 13
      12
 -10 -23
           1 0.1932 -9.7533 -22.5720 0.9099 0.4645 -0.8554 0.2293
 -9
     -1 17 0.2492 -8.8727 -1.0893 17.2546 0.1287 -0.4367 -0.8904
 19
     16 0 0.1348 18.5329 16.1979 -0.1934 -0.7916 0.6076 -0.0641
 -8 -19
         10 0.2071 -8.2007 -19.3441 9.6534 0.2768 -0.9352 -0.2207
 13
      16 -10 0.1619 13.0018 15.9985 -9.9995 -0.4467 0.8217 0.3435
_exptl_absorpt_coefficient_mu
                                                0.181
_exptl_absorpt_correction_T_min
                                                0.859
                                                1.843
_exptl_absorpt_correction_T_max
_exptl_absorpt_correction_type
                                      'gaussian'
_exptl_absorpt_process_details
;
CrysAlisPro, Agilent Technologies,
Version 1.171.36.28 (release 01-02-2013 CrysAlis171 .NET)
(compiled Feb 1 2013,16:14:44)
Numerical absorption correction based on gaussian integration over
                a multifaceted crystal model
;
               _____
#-----
#
#
                  DATA COLLECTION
#
#-
     _____
#
_exptl_special_details
A nitrogen gas-flow low temperature device was used to cool the crystal.
A face indexed analytical absorption correction was performed.
diffrn ambient temperature
                              100(2)
diffrn radiation wavelength
                             0.71073
_diffrn_radiation_probe
                             x-ray
_diffrn_radiation_type
                             MoK∖a
```

```
_diffrn_radiation_source
                                 'Mova (Mo) X-ray Source'
_diffrn_radiation_monochromator mirror
_diffrn_measurement_device_type 'Xcalibur, Eos, Nova'
_diffrn_detector_area_resol_mean 8.0419
_diffrn_reflns_number 530944
diffrn reflns av R equivalents 0.0683
diffrn reflns av sigmaI/netI 0.0851
_diffrn_reflns_limit_h_min -37
_diffrn_reflns_limit_h_max 37
_diffrn_reflns_limit_k_min -37
_diffrn_reflns_limit_k_max 37
_diffrn_reflns_limit_l_min -28
_diffrn_reflns_limit_l_max 28
_diffrn_reflns_theta_min 2.6076
_diffrn_reflns_theta_max 50.5794
_diffrn_measured_fraction_theta_max 0.9998
_diffrn_reflns_theta_full 26.3154
_diffrn_measured_fraction_theta_full 0.9986
_diffrn_orient_matrix_UB_11
                            -0.0392178000
_diffrn_orient_matrix_UB_12
                                -0.0041571000
_diffrn_orient_matrix_UB_13
                                -0.0129721000
_diffrn_orient_matrix_UB_21
                                 0.0003703000
                                 0.0368155000
_diffrn_orient_matrix_UB_22
_diffrn_orient_matrix_UB_23
                                -0.0227934000
_diffrn_orient_matrix_UB_31
                                 0.0105873000
_diffrn_orient_matrix_UB_32
                                -0.0166369000
_diffrn_orient_matrix_UB_33
                                 -0.0472079000
_diffrn_measurement_details
#____type__start___ end_____width____ exp.time_
  1 omega -17.00 67.00 1.0000 5.0000
omega____ theta____ kappa___ phi___
                                      _ frames
            0.0000 57.0000 60.0000 84
#___ type__ start___ end____ width____ exp.time_
2 omega -44.00 42.00 1.0000 5.0000
omega_____ theta_____ kappa____ phi_____ frame
                                       frames
            22.0000 -65.0000 -35.3935 86
#____type___start___ end_____ width____ exp.time_
  3 omega -6.00 47.00 1.0000 5.0000
omega____ theta____ kappa____ phi___
                                      ____frames
            22.0000 79.0000 -119.0273 53
  -
#____ type__ start___ end_____ width____ exp.time_
  4 omega -41.00 50.00 1.0000 5.0000
omega____ theta____ kappa____ phi___
                                     ____ frames
           26.0000 -72.0000 -112.7324 91
#____type__start___ end_____width____ exp.time_
  5 omega -40.00 46.00 1.0000 5.0000
omega____ theta____
                  _ kappa____ phi___
                                      _ frames
            26.0000 -65.0000 93.4368 86
#___ type__ start___ end____ width____ exp.time_
  6 omega 6.00 47.00 1.0000 10.0000
omega____ theta____ kappa____ phi_____ frames
```

- 34.0000 79.0000 83.1354 41

#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_ exp.time\_ 7 omega 10.00 46.00 1.0000 15.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_ \_\_\_\_ frames 38.0000 80.0000 100.7223 36 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 
 8 omega
 14.00
 47.00
 1.0000
 15.0000

 omega
 theta
 kappa
 phi
 frames
 42.0000 79.0000 -79.9077 33 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 9 omega 14.00 46.00 1.0000 15.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 42.0000 80.0000 -21.9823 32 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 10 omega 18.00 46.00 1.0000 20.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames -46.0000 80.0000 67.9150 28 #\_\_\_\_type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 11 omega 18.00 47.00 1.0000 20.0000 omega\_\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 46.0000 79.0000 21.5631 29 \_ #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 12 omega 19.00 49.00 1.0000 20.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 46.0000 78.0000 -154.6487 30 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 13 omega 19.00 49.00 1.0000 20.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 46.0000 78.0000 136.6745 30 -#\_\_\_\_type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 14 omega 18.00 47.00 1.0000 20.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 46.0000 79.0000 -125.5837 29 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 15 omega 23.00 49.00 1.0000 20.0000 omega theta kappa phi frame \_\_\_\_ frames 50.0000 78.0000 154.8597 26 #\_\_\_\_type\_\_start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 16 omega 29.00 121.00 1.0000 30.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 54.0000 74.0000 -89.2875 92 \_ #\_\_\_\_type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 17 omega 27.00 122.00 1.0000 30.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames -54.0000 77.0000 39.6605 95

#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 
 18 omega
 29.00
 121.00
 1.0000
 30.0000

 omega
 theta
 kappa
 phi
 frame
 frames 54.0000 74.0000 -38.3141 92 \_ #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 19 omega 31.00 126.00 1.0000 40.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 58.0000 77.0000 4.2501 95 \_ #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 20 omega 31.00 126.00 1.0000 40.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_ frames 58.0000 77.0000 162.6741 95 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 
 21 omega
 32.00
 125.00
 1.0000
 40.0000
 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ \_\_ phi\_\_\_ \_\_\_\_ frames -58.0000 76.0000 95.3589 93 #\_\_\_\_type\_\_start\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 22 omega 32.00 57.00 1.0000 40.0000 omega\_\_\_\_\_ theta\_\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 58.0000 76.0000 -140.2878 25 #\_\_\_\_type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 23 omega 79.00 139.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 60.0000 60 #\_\_\_\_type\_\_start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 24 omega 80.00 132.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 120.0000 52 \_ #\_\_\_\_type\_\_start\_\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 25 omega 15.00 100.00 1.0000 50.0000 omega\_\_\_\_\_ theta\_\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 -80.0000 118.3841 85 -#\_\_\_ type\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 26 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 77.0000 120.0000 25 \_ #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 27 omega 78.00 123.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -30.0000 45 \_ #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 28 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_\_ theta\_\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 77.0000 60.0000 25 -#\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 29 omega 45.00 70.00 1.0000 50.0000

omega\_\_\_\_ theta\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames - 71.8591 77.0000 -30.0000 25 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 30 omega 3.00 69.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames \_ 71.8591 -30.0000 120.0000 66 #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 31 omega 4.00 95.00 1.0000 50.0000 omega\_\_\_\_\_ theta\_\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frame \_\_\_\_ frames 71.8591 -80.0000 -129.0744 91 \_ #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 32 omega 82.00 139.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 150.0000 57 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 33 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 150.0000 25 -#\_\_\_\_type\_\_start\_\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 34 omega 63.00 89.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 -80.0000 45.0689 26 \_ #\_\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 
 35 omega
 64.00
 90.00
 1.0000
 50.0000

 omega\_\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_frame
 \_\_\_ frames \_ 71.8591 -80.0000 -87.4654 26 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_ exp.time\_ 36 omega 4.00 53.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 -80.0000 45.0689 49 \_ #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 37 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -60.0000 25 #\_\_\_ type\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 38 omega 8.00 58.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_ \_\_\_\_ frames 71.8591 -80.0000 -87.4654 50 -#\_\_\_\_type\_\_start\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 39 omega 79.00 137.00 1.0000 50.0000 omega theta kappa phi frames 71.8591 77.0000 30.0000 58 # type start end width exp.time 40 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 77.0000 30.0000 25

#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 41 omega 78.00 139.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_ frames 71.8591 77.0000 90.0000 61 \_ #\_\_\_ type\_ start\_\_ end\_\_\_\_ width\_\_\_ exp.time\_ 42 omega 45.00 70.00 1.0000 50.0000 omega theta kappa phi frames \_ 71.8591 77.0000 90.0000 25 #\_\_\_\_type\_\_start\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 43 omega 81.00 128.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_ frames \_ 71.8591 77.0000 0.0000 47 #\_\_\_ type\_ start\_\_\_ end\_\_\_\_ width\_\_\_ exp.time\_ 44 omega 80.00 131.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 77.0000 -60.0000 51 \_ #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 
 45 omega
 45.00
 70.00
 1.0000
 50.0000

 omega
 theta
 kappa
 phi
 frames
 71.8591 77.0000 -120.0000 25 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 46 omega 81.00 137.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -120.0000 56 \_ #\_\_\_\_type\_\_start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 47 omega 45.00 78.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 0.0000 33 \_ #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 48 omega 80.00 139.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 77.0000 -90.0000 59 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 49 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_\_ theta\_\_\_\_\_ kappa\_\_\_\_\_ phi\_\_\_\_\_ frames -71.8591 77.0000 -180.0000 25 #\_\_\_\_type\_\_start\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 50 omega 77.00 127.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -180.0000 50 -#\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_ 51 omega 75.00 100.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_\_ phi\_\_\_\_\_ frames 71.8591 -80.0000 92.5700 25 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_ width\_\_\_\_ exp.time\_

52 omega 45.00 70.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -90.0000 25 #\_\_\_ type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 53 omega 78.00 133.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 77.0000 -150.0000 55 \_ #\_\_\_\_type\_\_ start\_\_\_ end\_\_\_\_\_ width\_\_\_\_ exp.time\_ 54 omega 4.00 49.00 1.0000 50.0000 omega\_\_\_\_ theta\_\_\_\_ kappa\_\_\_ phi\_\_\_\_ frames 71.8591 -80.0000 92.5700 45 \_ #\_\_\_\_type\_\_start\_\_\_end\_\_\_\_\_width\_\_\_\_exp.time\_ 
 55 omega
 45.00
 71.00
 1.0000
 50.0000

 omega\_\_\_\_\_\_theta\_\_\_\_\_kappa\_\_\_\_\_phi\_\_\_\_\_frames
 71.8591 77.0000 -150.0000 26 \_ #\_\_\_ type\_ start\_\_\_ end\_\_\_\_ width\_\_\_ exp.time\_ 
 56 omega
 8.00
 99.00
 1.0000
 50.0000

 omega
 theta
 kappa
 phi
 frames
 71.8591 -80.0000 -24.4676 91 -; \_diffrn\_measurement\_method '\w scans' \_diffrn\_reflns\_reduction\_process ; ; # number of unique reflections \_reflns\_number\_total 42280 \_reflns\_number\_gt 32688 \_reflns\_threshold\_expression I>3\s(I) #-----\_\_\_\_\_ # # COMPUTER PROGRAMS USED # \_\_\_\_\_ #----# \_computing\_data\_collection ; CrysAlisPro, Agilent Technologies, Version 1.171.36.28 (release 01-02-2013 CrysAlis171 .NET) (compiled Feb 1 2013,16:14:44) ; \_computing\_cell\_refinement CrysAlisPro, Agilent Technologies, Version 1.171.36.28 (release 01-02-2013 CrysAlis171 .NET) (compiled Feb 1 2013,16:14:44) ; \_computing\_data\_reduction ;

```
CrysAlisPro, Agilent Technologies,
Version 1.171.36.28 (release 01-02-2013 CrysAlis171 .NET)
(compiled Feb 1 2013,16:14:44)
;
_computing_structure_refinement
                                'Volkov et al, (2006)'
computing molecular graphics
                                'Volkov et al, (2006)'
_computing_publication_material
                                'Volkov et al, (2006)'
#
#
                REFINEMENT INFORMATION
#
#
_refine_special_details
;
Reflections were merged with Sortav (Blessing, 1995).
;
_refine_ls_structure_factor_coef
                                Fsqd
_refine_ls_matrix_type
                                full
_refine_ls_weighting_scheme
                                calc
_refine_ls_weighting_details
;
      calc w2 = 1/[s^2(Fo^2)]
;
                              none
_refine_ls_extinction_method
_refine_ls_number_reflns
                               27177
                               940
_refine_ls_number_parameters
_refine_ls_number_restraints
                                0
_refine_ls_R_factor_all
                                0.038
                                0.023
_refine_ls_R_factor_gt
_refine_ls_wR_factor_ref
                               0.046
_refine_ls_goodness_of_fit_ref
                               1.067
_refine_ls_shift/su_max
                                0
  _____
#-
#
#
                ATOMIC TYPES, COORDINATES AND THERMAL PARAMETERS
#
#
loop_
   _atom_site_label
   _atom_site_fract_x
   _atom_site_fract_y
   _atom_site_fract_z
   _atom_site_U_iso_or_equiv
   _atom_site_occupancy
   _atom_site_symmetry_multiplicity
S(1) 0.12844(3) -0.05971(2) 0.705283 0.031 1 4
S(1A) 0.57650(4) -0.38958(5) 0.96607(8) 0.039 1 4
O(1) 0.398795(18) -0.03949(2) 0.64976(5) 0.017 1 4
O(1A) 0.56877(2) -0.095527(18) 0.89331(5) 0.017 1 4
O(2) 0.36753(2) -0.04646(2) 0.81766(5) 0.018 1 4
O(2A) 0.57374(2) -0.14594(2) 1.05290(5) 0.017 1 4
```

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H(4A) 0.826286 -0.202308 0.587704 0.037 1 4 H(7) 0.404835 -0.389163 0.451931 0.038 1 4 H(7A) 0.923782 -0.128098 0.706837 0.038 1 4 H(8) 0.474542 -0.458207 0.587775 0.038 1 4 H(8A) 0.995494 -0.063082 0.853001 0.04 1 4 H(9) 0.496723 -0.397893 0.755449 0.036 1 4 H(9A) 0.931762 -0.034815 1.010127 0.039 1 4 H(10) 0.44354 -0.26511 0.790821 0.033 1 4 H(10A) 0.797753 -0.073854 1.040503 0.036 1 4 H(12) 0.319453 -0.167664 0.703882 0.03 1 4 H(12A) 0.688094 -0.187339 0.94782 0.032 1 4 H(14A) 0.458747 -0.125816 0.725207 0.032 1 4 H(14B) 0.466805 -0.122374 0.591702 0.033 1 4 H(14D) 0.657776 -0.035981 0.84037 0.033 1 4 H(14C) 0.660251 -0.049816 0.974914 0.034 1 4 H(16) 0.341638 0.079129 0.879481 0.03 1 4 H(16A) 0.447926 -0.167752 1.114001 0.032 1 4 H(17A) 0.228906 0.159897 0.881472 0.036 1 4 H(17B) 0.226964 0.16632 0.746117 0.036 1 4 H(17D) 0.353602 -0.254604 0.954981 0.035 1 4 H(17C) 0.354802 -0.270597 1.092617 0.036 1 4 H(19A) 0.35383 0.218027 0.737501 0.035 1 4 H(19B) 0.354128 0.220068 0.87054 0.035 1 4 H(19D) 0.308713 -0.137956 1.119096 0.036 1 4  $\texttt{H(19C)} \quad \texttt{0.307402} \quad \texttt{-0.121167} \quad \texttt{0.987957} \quad \texttt{0.034} \quad \texttt{1} \quad \texttt{4}$ H(20) 0.474336 0.140295 0.739092 0.03 1 4 H(20A) 0.395506 -0.013672 1.008177 0.03 1 4 H(21A) 0.55114 0.135158 0.900026 0.039 1 4 H(21B) 0.472512 0.172666 0.966875 0.04 1 4 H(21C) 0.468248 0.082143 0.910559 0.038 1 4 H(21E) 0.38462 -0.048306 1.233604 0.042 1 4 H(21D) 0.416911 0.036636 1.193765 0.041 1 4 H(21F) 0.470606 -0.042744 1.158662 0.04 1 4 H(22A) 0.475568 0.282242 0.719963 0.041 1 4 H(22B) 0.486635 0.291292 0.850673 0.041 1 4 H(22C) 0.559835 0.248579 0.78418 0.04 1 4 H(22E) 0.257133 -0.002969 1.149321 0.042 1 4 H(22F) 0.302817 0.074151 1.093864 0.041 1 4 H(22D) 0.252386 0.009834 1.018158 0.04 1 4 loop \_atom\_site\_aniso\_label \_atom\_site\_aniso\_U\_11 \_atom\_site\_aniso\_U\_22 \_atom\_site\_aniso\_U\_33 \_atom\_site\_aniso\_U\_23 \_atom\_site\_aniso\_U\_13 \_atom\_site\_aniso\_U\_12 S(1) 0.0373(2) 0.02448(18) 0.0299(2) -0.00390(17) -0.00136(19) -0.00597(17) S(1A) 0.0268(3) 0.0482(4) 0.0410(4) -0.0090(4) -0.0013(3) 0.0178(3)O(1) 0.02126(14) 0.01499(12) 0.01404(14) -0.00241(11) 0.00361(10) -0.00125(10)O(1A) 0.01404(13) 0.02136(14) 0.01447(13) 0.00243(11) 0.00096(11) 0.00098(9)O(2) 0.02422(15) 0.01727(13) 0.01374(13) 0.00133(11) 0.00232(12) 0.00416(11)O(2A) 0.01487(12) 0.02401(15) 0.01324(13) 0.00105(12) -0.00125(11) -0.00091(11)N(1) 0.01860(13) 0.01412(11) 0.01358(13) -0.00031(10) 0.00108(9) 0.00132(9)

N(1A) 0.01247(11) 0.02004(13) 0.01366(13) 0.00036(9) -0.00017(10) 0.00082(9) N(2) 0.01903(19) 0.0241(2) 0.0323(3) -0.0055(2) 0.00370(18) -0.00392(17) N(2A) 0.0234(2) 0.0188(2) 0.0364(3) -0.0027(2) 0.0007(2) 0.00544(18) C(1) 0.01917(14) 0.01727(14) 0.02535(18) 0.00152(13) -0.00101(13) -0.00063(12)C(1A) 0.01685(14) 0.02167(15) 0.02142(17) -0.00299(13) -0.00208(13) -0.00005(11)C(2) 0.02274(16) 0.02442(18) 0.0265(2) 0.00471(16) -0.00467(15) -0.00283(13)C(2A) 0.02409(18) 0.02240(16) 0.02147(18) -0.00408(13) -0.00507(15)0.00272(13)C(3) 0.02293(16) 0.0292(2) 0.02149(18) 0.00171(16) -0.00371(14) -0.00534(15)C(3A) 0.02822(19) 0.02089(15) 0.01768(16) -0.00177(12) -0.00185(15) 0.00520(13)C(4) 0.02032(14) 0.02453(17) 0.01973(17) -0.00327(14) -0.00019(13) -0.00474(13)C(4A) 0.02334(17) 0.01984(14) 0.01725(16) 0.00073(12) 0.00271(13) 0.00419(12) C(5) 0.01594(12) 0.01720(13) 0.01862(15) -0.00213(12) 0.00113(11) -0.00261(10)C(5A) 0.01692(13) 0.01612(12) 0.01639(14) 0.00145(11) 0.00148(11) 0.00167(10)C(6) 0.01689(12) 0.01510(13) 0.02064(16) -0.00284(12) 0.00202(11) -0.00099(10)C(6A) 0.01423(13) 0.01730(13) 0.01955(15) 0.00256(11) 0.00154(11) 0.00020(10) C(7) 0.02265(16) 0.01659(14) 0.0292(2) -0.00499(14) 0.00189(15) 0.00089(13)C(7A) 0.01591(14) 0.02484(16) 0.0287(2) 0.00273(15) 0.00423(14) -0.00168(12)  $C(8) \quad 0.02636(18) \quad 0.01715(15) \quad 0.0366(3) \quad -0.00159(17) \quad 0.00089(17) \quad 0.00363(14)$ C(8A) 0.01576(15) 0.0293(2) 0.0365(3) 0.00141(18) 0.00003(16) -0.00459(14)C(9) 0.02552(18) 0.02002(16) 0.0314(2) 0.00305(16) -0.00102(16) 0.00370(13)C(9A) 0.01808(16) 0.02812(19) 0.0324(2) -0.00131(16) -0.00490(16) -0.00452(13)C(10) 0.02226(15) 0.02023(15) 0.02184(18) 0.00141(14) -0.00016(13)0.00097(13)C(10A) 0.01780(15) 0.02320(16) 0.02192(17) -0.00110(13) -0.00326(13) -0.00164(12) $C(11) \quad 0.01757(13) \quad 0.01543(12) \quad 0.01814(15) \quad -0.00084(12) \quad 0.00200(11) \quad -0.0008(12) \quad -$ 0.00048(10)C(11A) 0.01383(12) 0.01803(13) 0.01737(15) 0.00141(11) -0.00060(11) -0.00047(10)C(12) 0.01605(13) 0.01542(13) 0.01759(15) -0.00146(11) 0.00315(11) -0.00074(10)C(12A) 0.01393(12) 0.01687(13) 0.01567(14) 0.00143(11) 0.00025(11) -0.00009(10)C(13) 0.01543(12) 0.01547(12) 0.01924(15) -0.00070(11) 0.00105(11) -0.00154(10)C(13A) 0.01478(13) 0.01651(12) 0.01659(14) 0.00004(10) -0.00023(11)0.00056(10) $\texttt{C(14)} \quad \texttt{0.01619(13)} \quad \texttt{0.01657(13)} \quad \texttt{0.01814(15)} \quad \texttt{-0.00400(10)} \quad \texttt{0.00295(10)} \quad \texttt{-}$ 0.00075(11)C(14A) 0.01522(13) 0.01702(13) 0.01752(15) 0.00099(10) 0.00162(10) -0.00010(10)C(15) 0.01570(12) 0.01463(12) 0.01223(12) -0.00078(10) 0.00104(9) 0.00076(9)C(15A) 0.01312(12) 0.01700(12) 0.01234(12) -0.00062(10) 0.00003(10)0.00036(9)C(16) 0.01584(13) 0.01516(13) 0.01567(14) -0.00106(11) 0.00118(11)0.00111(10)C(16A) 0.01349(12) 0.01570(13) 0.01554(14) -0.00082(11) 0.00017(11) -0.00006(10)C(17) 0.01570(14) 0.01882(15) 0.0320(2) -0.00344(13) 0.00252(12) 0.00135(12)

C(17A) 0.01720(14) 0.01522(14) 0.0286(2) -0.00187(12) -0.00061(12) 0.00004(11)C(18) 0.01954(17) 0.02006(18) 0.0221(2) -0.00096(16) 0.00265(15) -0.00091(15)C(18A) 0.02003(18) 0.02078(17) 0.0218(2) -0.00101(15) -0.00135(15) 0.00371(15)C(19) 0.01666(13) 0.01507(13) 0.01902(15) -0.00139(10) -0.00011(10)0.00060(10)C(19A) 0.01425(12) 0.01627(13) 0.02034(16) -0.00191(10) 0.00210(10) 0.00042(10)C(20) 0.01613(13) 0.01868(14) 0.01669(15) -0.00058(12) -0.00192(11) -0.00099(11)C(20A) 0.01963(15) 0.01624(14) 0.02051(16) -0.00253(12) 0.00360(12)0.00077(11)C(21) 0.02449(19) 0.0350(2) 0.0236(2) 0.00751(18) -0.00743(16) -0.00084(17) $\texttt{C(21A)} \quad \texttt{0.0292(2)} \quad \texttt{0.02391(19)} \quad \texttt{0.0244(2)} \quad \texttt{-0.00763(16)} \quad \texttt{-0.00124(17)} \quad \texttt{-0.00179(16)}$ C(22) 0.02270(18) 0.02269(18) 0.0323(2) 0.00158(17) -0.00285(17) -0.00584(15)C(22A) 0.0262(2) 0.02278(19) 0.0417(3) - 0.00534(19) 0.0034(2) 0.00787(16)H(1) 0.038907 0.029121 0.032782 -0.007064 -0.003701 0.002795 H(1A) 0.026981 0.039797 0.032582 -0.002692 0.006365 -0.001936 H(1N) 0.037388 0.029806 0.028707 0.003538 0.004763 0.001932 H(2) 0.039442 0.034732 0.035696 0.000527 -0.008877 0.003921 H(1NA) 0.029216 0.034833 0.030192 0.007061 -0.003017 -0.000129 H(2A) 0.029609 0.039248 0.034862 -0.007574 -0.000532 -0.004027 H(3) 0.044927 0.042698 0.028645 -0.006231 -0.009353 -0.002333 H(3A) 0.036709 0.043325 0.030166 -0.009924 0.005162 -0.000055 H(4) 0.045872 0.033025 0.035163 -0.011611 -0.00259 0.000278 H(4A) 0.027438 0.046874 0.037288 -0.004676 0.008614 -0.000236 H(7) 0.046644 0.034778 0.031999 -0.010814 -0.001506 0.000676 H(7A) 0.031097 0.050063 0.03327 -0.00428 0.006231 0.000444 H(8) 0.045783 0.025944 0.043273 -0.00738 0.001121 0.00644 H(8A) 0.023537 0.053202 0.0428 -0.001526 0.000391 -0.004003 H(9) 0.041046 0.03104 0.036064 0.001049 -0.003721 0.006918 H(9A) 0.031372 0.050776 0.034651 -0.004658 -0.006021 -0.004683 H(10) 0.040185 0.031157 0.028208 -0.006032 -0.002126 0.002782 H(10A) 0.033112 0.047684 0.027944 -0.002715 0.002365 -0.001401 H(12) 0.02837 0.032227 0.029133 -0.002545 0.005245 0.00003 H(12A) 0.033284 0.032595 0.029561 0.005853 0.001299 0.000694 H(14A) 0.036244 0.032573 0.028603 0.000415 -0.007448 -0.000238 H(14B) 0.034402 0.033771 0.030947 -0.003467 0.008993 -0.001125 H(14D) 0.032865 0.035482 0.031443 0.008029 0.002168 0.000641 H(14C) 0.033634 0.041294 0.027442 -0.007268 -0.003078 0.001028 H(16) 0.032366 0.029848 0.027686 0.002268 -0.001266 0.001531 H(16A) 0.032664 0.036146 0.0261 0.000723 -0.003147 0.00012 H(17A) 0.034936 0.037166 0.035548 -0.009947 0.004017 0.000337 H(17B) 0.034355 0.034893 0.038001 0.007024 -0.004414 0.000825 H(17D) 0.037922 0.034743 0.031404 -0.001556 -0.005593 0.001885 H(17C) 0.040294 0.035483 0.033073 0.005025 0.010459 -0.000567 H(19A) 0.035591 0.034381 0.034879 0.006407 -0.005607 -0.000579 H(19B) 0.036073 0.034062 0.035545 -0.010107 0.004408 -0.000186 H(19D) 0.038001 0.036058 0.032741 0.00312 0.011158 -0.001072 H(19C) 0.035512 0.035554 0.031093 -0.003138 -0.005836 0.001819 H(20) 0.032684 0.028728 0.027438 -0.005541 0.000922 0.000648 H(20A) 0.0308 0.033002 0.026237 0.000779 0.005443 -0.001424 H(21A) 0.024756 0.05185 0.039644 0.005176 0.000362 0.001222 H(21B) 0.050492 0.03865 0.029798 -0.008998 0.001835 0.009666 H(21C) 0.04661 0.027666 0.040454 0.00255 -0.006768 -0.009392 H(21E) 0.042206 0.054382 0.029291 0.005992 0.005521 -0.01026

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S(1A) -0.000004(11) 0.00062(2) -0.00027(5) 0.000026(8) 0.000170(10) -
0.00030(9)
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0.000004(2) - 0.0000029(13) - 0.0000005(12) - 0.0000026(17)
S(1A) 0.000002(4) 0.000013(7) 0.00015(2) 0.000009(2) 0.000004(3) -0.000004(3)
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# MULTIPOLE PARAMETERS
#
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loop\_

atom rho multipole atom label atom rho multipole coeff Pv atom rho multipole coeff P00 \_atom\_rho\_multipole\_coeff\_P11 \_atom\_rho\_multipole\_coeff\_P1-1 \_atom\_rho\_multipole\_coeff\_P10 \_atom\_rho\_multipole\_coeff\_P20 \_atom\_rho\_multipole\_coeff\_P21 \_atom\_rho\_multipole\_coeff\_P2-1 \_atom\_rho\_multipole\_coeff\_P22 \_atom\_rho\_multipole\_coeff\_P2-2 \_atom\_rho\_multipole\_coeff\_P30 \_atom\_rho\_multipole\_coeff\_P31 \_atom\_rho\_multipole\_coeff\_P3-1 \_atom\_rho\_multipole\_coeff\_P32 \_atom\_rho\_multipole\_coeff\_P3-2 \_atom\_rho\_multipole\_coeff\_P33 \_atom\_rho\_multipole\_coeff\_P3-3 \_atom\_rho\_multipole\_coeff\_P40 \_atom\_rho\_multipole\_coeff\_P41 \_atom\_rho\_multipole\_coeff\_P4-1 \_atom\_rho\_multipole\_coeff\_P42 atom rho multipole coeff P4-2 \_atom\_rho\_multipole\_coeff\_P43 \_atom\_rho\_multipole\_coeff\_P4-3 \_atom\_rho\_multipole\_coeff\_P44 \_atom\_rho\_multipole\_coeff\_P4-4 \_atom\_rho\_multipole\_kappa \_atom\_rho\_multipole\_kappa\_prime0 \_atom\_rho\_multipole\_kappa\_prime1 \_atom\_rho\_multipole\_kappa\_prime2 \_atom\_rho\_multipole\_kappa\_prime3 \_atom\_rho\_multipole\_kappa\_prime4 \_atom\_rho\_multipole\_radial\_slater\_n0 \_atom\_rho\_multipole\_radial\_slater\_zeta0 \_atom\_rho\_multipole\_radial\_slater\_n1 \_atom\_rho\_multipole\_radial\_slater\_zeta1 \_atom\_rho\_multipole\_radial\_slater\_n2 \_atom\_rho\_multipole\_radial\_slater\_zeta2 \_atom\_rho\_multipole\_radial\_slater\_n3 \_atom\_rho\_multipole\_radial\_slater\_zeta3 \_atom\_rho\_multipole\_radial\_slater\_n4 \_atom\_rho\_multipole\_radial\_slater\_zeta4  $S(1) \quad 6.75(6) \quad 0 \quad -0.01(2) \quad -0.01(2) \quad 0.03(2) \quad 0.05(2) \quad -0.03(2) \quad -0.03(2) \quad -0.02(2)$  $0.05(2) \ 0.147(19) \ 0.029(16) \ -0.036(17) \ 0.021(17) \ -0.038(17) \ 0.063(17) \ -0.036(17) \ -0.038(17) \ 0.063(17) \ -0.063(17)$ 0.001(17)0.06(2) - 0.016(18) 0.011(19) 0.035(19) 0.020(18) - 0.027(19) - 0.039(19)-0.002(19) -0.054(19) 0.946976 1.094612 1.094612 1.094612 1.094612 1.094612 4 3.85126666666667 4 3.8512666666667 4 3.85126666666667 4 3.85126666666667 4 3.8512666666667 S(1A) 6.64(6) 0 0.02(3) -0.10(3) -0.012(19) 0.12(2) -0.05(2) 0.02(2) 0.01(3)0.09(3) 0.135(19) -0.036(18) 0.050(18) -0.01(2) 0.00(2) -0.03(2) -0.08(2)

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0.08(2) - 0.04(2) - 0.03(2) - 0.03(2) - 0.02(2) 0.02(3) - 0.03(3) - 0.02(30.03(3) $0.94767 \ 1.359433 \ 1.359433 \ 1.359433 \ 1.359433 \ 1.359433 \ 4 \ 3.8512666666667 \ 4$ 3.8512666666667 4 3.8512666666667 4 3.85126666666667 4 3.85126666666667 O(1) 6.000(16) 0 -0.031(9) -0.043(8) 0 0.051(9) 0 0 -0.018(9) 0.034(9) 0 -0.007(6) -0.011(6) 0 0 0.078(6) -0.010(6) 0 0 0 0 0 0 0 0 0.988798 1.055753 1.055753 1.055753 1.055753 1.055753 2 4.466 2 4.466 2 4.466 3 4.466 4 4.466 O(1A) 6.0004 0 -0.0309 -0.0427 0 0.0506 0 0 -0.0177 0.0336 0 -0.0074 -0.0114 0 0 0.0777 -0.0102 0 0 0 0 0 0 0 0 0 0.988798 1.055753 1.055753 1.055753 1.055753 1.055753 2 4.466 2 4.466 2 4.466 3 4.466 4 4.466 O(2) 5.976(17) 0 -0.100(11) 0.011(9) -0.018(9) -0.052(10) -0.013(9) 0.019(8) -0.082(10) 0.009(9) 0.014(7) -0.004(7) -0.003(7) -0.007(7) 0.006(7) 0.031(7)-0.010(7) 0 0 0 0 0 0 0 0 0 0.985393 0.924662 0.924662 0.924662 0.924662 0.924662 2 4.466 2 4.466 2 4.466 3 4.466 4 4.466 O(2A) 5.9761 0 -0.1001 0.0107 -0.0175 -0.0516 -0.0127 0.0185 -0.0824 0.0092 0.985393 0.924662 0.924662 0.924662 0.924662 0.924662 2 4.466 2 4.466 2 4.466 3 4.466 4 4.466 N(1) 4.91(2) 0 0.008(10) 0.032(11) 0 0.007(9) 0 0 0.000(9) -0.018(9) 0 -0.046(8)-0.006(7) 0 0 0.166(8) 0.016(8) 0 0 0 0 0 0 0 0 0 0 0.982488 0.957744 0.957744 0.957744 0.957744 0.957744 2 3.83936 2 3.83936 2 3.83936 3 3.83936 4 3.83936 N(1A) 4.9097 0 0.0078 0.0318 0 0.0069 0 0 0.0003 -0.0181 0 -0.0455 -0.0064 0 Ο 0.1658 0.0161 0 0 0 0 0 0 0 0 0 0.982488 0.957744 0.957744 0.957744 0.957744 0.957744 2 3.83936 2 3.83936 2 3.83936 3 3.83936 4 3.83936 N(2) 5.05(4) 0 0.043(16) 0.049(14) 0.05(2) 0.10(2) -0.029(17) -0.002(15) 0.009(14) 0.031(14) 0.011(16) 0.081(15) 0.062(14) -0.013(13) -0.028(13)0.002(12) 0.030(12) 0 0 0 0 0 0 0 0 0 0 0.981436 0.963224 0.963224 0.963224 0.963224 0.963224 2 3.83936 2 3.83936 2 3.83936 3 3.83936 4 3.83936 N(2A) 5.01(4) 0 0.000(17) 0.049(15) 0.03(2) 0.14(2) 0.027(16) 0.049(15) -0.021(15) 0.004(15) -0.072(15) 0.019(14) 0.031(13) -0.011(12) 0.003(12)-0.030(12) -0.003(12) 0 0 0 0 0 0 0 0 0 0 0.986582 1.00161 1.00161 1.00161 1.00161 1.00161 2 3.83936 2 3.83936 2 3.83936 3 3.83936 4 3.83936 C(1) 4.15(4) 0 0.003(14) -0.023(11) 0 -0.189(11) 0 0 -0.013(12) 0.001(11) 0 -0.010(11) 0.027(9) 0 0.238(11) 0.014(11) 0 0 0 0 0 0 0 0.9621751.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3,1762 C(1A) 4.1498 0 0.0028 -0.0227 0 -0.1894 0 0 -0.0128 0.0011 0 -0.0096 0.0269 0 Ω 0.2376 0.0139 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762  $\texttt{C(2)} \ 4.16(3) \ 0 \ 0.025(14) \ 0.007(13) \ 0 \ -0.183(12) \ 0 \ 0 \ 0.039(13) \ -0.017(12) \ 0$ 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(2A) 4.1623 0 0.0248 0.0074 0 -0.1828 0 0 0.0387 -0.0174 0 0.0314 0.0157 0 0 0.2447 -0.0185 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(3) 4.15(3) 0 -0.010(14) 0.013(13) 0 -0.198(12) 0 0 0.013(13) -0.022(13) 0

0.016(10) 0.005(10) 0 0 0.269(13) -0.010(12) 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(3A) 4.1521 0 -0.01 0.0125 0 -0.1975 0 0 0.0133 -0.0216 0 0.0164 0.0047 0 0 0.2685 -0.0104 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(4) 4.15(3) 0 -0.008(13) -0.006(12) 0 -0.175(11) 0 0 -0.004(12) -0.016(12) 0 -0.013(10) 0.036(10) 0 0.250(12) 0.004(11) 0 0 0 0 0 0 0 0 0.9621751.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(4A) 4.1477 0 -0.0078 -0.0061 0 -0.175 0 0 -0.0039 -0.0161 0 -0.0129 0.0363 0 0 0.2503 0.0038 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(5) 4.22(3) 0 -0.009(14) 0.044(11) 0 -0.190(10) 0 0 0.041(11) -0.012(11) 0 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(5A) 4.2157 0 -0.0092 0.0437 0 -0.1904 0 0 0.0411 -0.0117 0 -0.0123 0.0004 0 0 0.2717 -0.0401 0 0 0 0 0 0 0 0 0 0.963239 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(6) 4.11(3) 0 0.012(12) 0.033(13) 0 -0.184(10) 0 0 0.032(11) -0.014(11) 0 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762  $\texttt{C(6A)} \ \texttt{4.1113} \ \texttt{0} \ \texttt{0.0119} \ \texttt{0.0334} \ \texttt{0} \ -\texttt{0.1837} \ \texttt{0} \ \texttt{0} \ \texttt{0.0322} \ -\texttt{0.0143} \ \texttt{0} \ \texttt{0.0076} \ \texttt{0.006} \ \texttt{0} \ \texttt{0}$ 0.2373 -0.0496 0 0 0 0 0 0 0 0 0 0.963239 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(7) 4.20(3) 0 0.003(12) 0.021(14) 0 -0.172(11) 0 0 0.016(12) -0.014(12) 0  $0.007(10) \ 0.038(11) \ 0 \ 0.233(12) \ -0.039(12) \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0.962175$ 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(7A) 4.2034 0 0.0026 0.0214 0 -0.1715 0 0 0.0155 -0.0144 0 0.007 0.0381 0 0 0.2329 -0.0386 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(8) 4.07(3) 0 -0.020(16) -0.018(13) 0 -0.190(13) 0 0 -0.001(13) -0.012(13) 0 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3,1762 C(8A) 4.0704 0 -0.0202 -0.0175 0 -0.1902 0 0 -0.0009 -0.0124 0 0.0581 -0.0093 0 0 0.2434 0.0227 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(9) 4.22(3) 0 -0.020(13) 0.062(15) 0 -0.202(12) 0 0 0.029(13) -0.015(13) 0 0.028(11) -0.011(12) 0 0 0.253(12) 0.007(12) 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3,1762

C(9A) 4.2199 0 -0.0202 0.0624 0 -0.202 0 0 0.0286 -0.0149 0 0.0281 -0.0113 0 0 0.2527 0.0069 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(10) 4.12(3) 0 0.043(12) 0.009(13) 0 -0.167(11) 0 0 -0.004(12) 0.002(11) 0 0.016(10) 0.006(10) 0 0.248(11) 0.005(11) 0 0 0 0 0 0 0 0 0.9621751.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(10A) 4.1197 0 0.0432 0.009 0 -0.1667 0 0 -0.0043 0.0022 0 0.0162 0.0062 0 0 0.2479 0.0052 0 0 0 0 0 0 0 0 0 0.962175 1.016775 1.016775 1.016775 1.016775 1.016775 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(11) 4.21(3) 0 0.016(13) 0.014(12) 0 -0.182(11) 0 0 0.022(12) -0.041(11) 0 0.014(10) - 0.009(10) 0 0 0.263(11) - 0.053(12) 0 0 0 0 0 0 0 0 0 0.9632390.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(11A) 4.2051 0 0.0162 0.0142 0 -0.1823 0 0 0.0222 -0.0405 0 0.0143 -0.0092 0 Ω 0.2625 -0.0525 0 0 0 0 0 0 0 0 0 0.963239 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(12) 4.13(3) 0 0.010(11) -0.017(13) -0.004(11) -0.001(10) 0.005(9) 0.006(10) -0.015(10) 0.005(10) 0.022(10) -0.169(10) -0.176(10) 0.002(10) 0.016(10)0.154(10) -0.070(11) 0 0 0 0 0 0 0 0 0 0.962889 0.969848 0.969848 0.969848  $0.969848 \ 0.969848 \ 2 \ 3.1762 \ 2 \ 3.1762 \ 2 \ 3.1762 \ 3 \ 3.1762 \ 4 \ 3.1762$ C(12A) 4.1257 0 0.0103 -0.0168 -0.0035 -0.0007 0.0054 0.0055 -0.0153 0.0045 0.962889 0.969848 0.969848 0.969848 0.969848 0.969848 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(13) 4.18(3) 0 0.004(12) -0.008(12) 0 -0.172(10) 0 0 0.013(11) -0.011(11) 0 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(13A) 4.1826 0 0.0044 -0.0082 0 -0.1717 0 0 0.013 -0.0109 0 0.0138 0.0374 0 0 0.2642 -0.0376 0 0 0 0 0 0 0 0 0 0.963239 0.990081 0.990081 0.990081 0.990081 0.990081 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(14) 4.05(3) 0 -0.002(10) -0.074(10) 0 0.069(10) 0 0 0.032(9) 0.067(9) 0 -0.137(9) -0.187(9) 0 0 0.186(8) -0.058(8) 0 0 0 0 0 0 0 0 0 0.962807 1.037883 1.037883 1.037883 1.037883 1.037883 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(14A) 4.0536 0 -0.0022 -0.0735 0 0.0687 0 0 0.0319 0.0671 0 -0.1367 -0.1873 0 0 0.1855 -0.0581 0 0 0 0 0 0 0 0 0 0.962807 1.037883 1.037883 1.037883 1.037883  $1.037883\ 2\ 3.1762\ 2\ 3.1762\ 2\ 3.1762\ 3\ 3.1762\ 4\ 3.1762$ C(15) 4.25(3) 0 0.122(13) -0.017(11) 0 -0.301(11) 0 0 0.104(11) -0.012(11) 0 -0.015(11) 0.024(9) 0 0.381(12) 0.035(12) 0 0 0 0 0 0 0 0 0.9546760.975277 0.975277 0.975277 0.975277 0.975277 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(15A) 4.2484 0 0.1224 -0.0165 0 -0.3008 0 0 0.1039 -0.0121 0 -0.0149 0.0239 0 0 0.3812 0.0352 0 0 0 0 0 0 0 0 0 0.954676 0.975277 0.975277 0.975277 0.975277

 $0.975277\ 2\ 3.1762\ 2\ 3.1762\ 2\ 3.1762\ 3\ 3.1762\ 4\ 3.1762$ C(16) 4.04(3) 0 -0.034(10) -0.064(10) 0.039(10) 0.078(9) -0.031(9) -0.021(9) 0.024(9) 0.028(9) -0.012(9) -0.128(9) -0.185(9) 0.020(9) 0.021(9) 0.158(9)2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(16A) 4.0428 0 -0.0339 -0.0641 0.0391 0.0779 -0.0311 -0.0205 0.024 0.0284 0.962432 1.02847 1.02847 1.02847 1.02847 1.02847 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3 1762 C(17) 4.06(4) 0 -0.055(11) -0.006(11) 0 0.013(11) 0 0 -0.084(9) -0.004(9) 0 -0.095(10) -0.139(11) 0 0 0.207(10) -0.038(9) 0 0 0 0 0 0 0 0 0 0.9616140.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(17A) 4.0633 0 -0.055 -0.0059 0 0.0126 0 0 -0.0838 -0.0043 0 -0.0954 -0.1392 Ω 0 0.2065 -0.038 0 0 0 0 0 0 0 0 0 0 0.961614 0.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(18) 4.15(5) 0 0.004(16) 0.010(15) 0.11(3) 0.32(2) 0.009(16) 0.006(16) 0.019(14) 0.014(14) 0.06(2) -0.008(18) -0.010(18) -0.017(14) 0.029(15)0.012(13)-0.009(13) 0 0 0 0 0 0 0 0 0 0.970455 0.997343 0.997343 0.997343 0.997343 0.997343 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(18A) 4.19(5) 0 0.010(16) 0.040(16) 0.11(2) 0.30(2) 0.033(16) 0.009(16) 0.015(14) - 0.007(14) 0.03(2) 0.049(18) - 0.077(18) - 0.008(15) - 0.025(15)0.032(14) -0.028(14) 0 0 0 0 0 0 0 0 0 0 0.971513 0.97515 0.97515 0.97515 0.97515 0.97515 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762  $\texttt{C(19)} \ 4.07(4) \ 0 \ -0.029(10) \ -0.008(10) \ 0 \ -0.008(10) \ 0 \ 0 \ 0.002(9) \ -0.005(9) \ 0$ -0.112(10) -0.180(10) 0 0 0.190(9) -0.019(9) 0 0 0 0 0 0 0 0 0 0.9616140.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(19A) 4.0667 0 -0.0285 -0.0082 0 -0.0084 0 0 0.002 -0.0048 0 -0.1121 -0.1798 0 0 0.1895 -0.019 0 0 0 0 0 0 0 0 0 0.961614 0.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(20) 4.01(3) 0 0.006(10) 0.029(10) -0.016(9) 0.018(10) -0.012(9) 0.003(9) -0.007(9) 0.009(9) -0.013(11) -0.141(10) -0.169(10) -0.001(10) -0.025(9)0.160(9) -0.063(9) 0 0 0 0 0 0 0 0 0 0.961614 0.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(20A) 4.0149 0 0.0062 0.0291 -0.0161 0.0179 -0.0117 0.0028 -0.0066 0.0086 0.961614 0.998202 0.998202 0.998202 0.998202 0.998202 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(21) 4.06(4) 0 0.002(12) -0.013(10) -0.019(11) -0.008(11) 0.046(10) 0.018(10)0.010(10) 0.014(10) -0.048(11) -0.109(10) 0.132(11) -0.048(11) -0.020(10)0.154(10) 0.052(10) 0 0 0 0 0 0 0 0 0 0.965626 1.038539 1.038539 1.038539 1.038539 1.038539 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(21A) 4.0623 0 0.0023 -0.0128 -0.0194 -0.0083 0.0464 0.018 0.0096 0.014 -0.0479

-0.1085 0.132 -0.0477 -0.0198 0.1543 0.0519 0 0 0 0 0 0 0 0 0 0 0.965626 1.038539 1.038539 1.038539 1.038539 1.038539 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(22) 4.20(4) 0 -0.053(11) 0.010(11) 0.081(11) 0.008(11) -0.024(10) 0.016(11) 0.005(10) 0.001(10) 0.056(11) -0.136(10) 0.190(12) -0.010(11) -0.012(10)0.163(10) 0.023(10) 0 0 0 0 0 0 0 0 0 0.965626 1.038539 1.038539 1.038539 1.038539 1.038539 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 C(22A) 4.2023 0 -0.0533 0.0099 0.0809 0.0075 -0.0241 0.0161 0.0053 0.0009 0 0562 -0.136 0.1897 -0.0095 -0.0117 0.1628 0.023 0 0 0 0 0 0 0 0 0 0.965626 1.038539 1.038539 1.038539 1.038539 1.038539 2 3.1762 2 3.1762 2 3.1762 3 3.1762 4 3.1762 1.2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 0  $0 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $\texttt{H}(\texttt{2A}) \ \texttt{0.8129} \ \texttt{0} \ \texttt{0} \ \texttt{0} \ \texttt{0.1182} \ \texttt{0.0093} \ \texttt{0} \ \texttt{0}$ 1.2  $1.2\ 1.2\ 1.2\ 1.2\ 0\ 2\ 1\ 2\ 2\ 2\ 3\ 2\ 4\ 2$ 1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$  $H(7) \hspace{0.1in} 0.8129 \hspace{0.1in} 0 \hspace{0.1in} 0$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2

1.2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 0 1.2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ Ο 1.2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2\ 1.2\ 1.2\ 1.2\ 1.2\ 0\ 2\ 1\ 2\ 2\ 2\ 3\ 2\ 4\ 2$  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2\ 1.2\ 1.2\ 1.2\ 1.2\ 0\ 2\ 1\ 2\ 2\ 2\ 3\ 2\ 4\ 2$  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$  $1.2\ 1.2\ 1.2\ 1.2\ 1.2\ 0\ 2\ 1\ 2\ 2\ 2\ 3\ 2\ 4\ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$ 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2  $1.2 \ 1.2 \ 1.2 \ 1.2 \ 1.2 \ 0 \ 2 \ 1 \ 2 \ 2 \ 3 \ 2 \ 4 \ 2$  $\texttt{H(21A)} \quad \texttt{0.828(8)} \quad \texttt{0} \quad \texttt{0} \quad \texttt{0.115(6)} \quad \texttt{0.015(7)} \quad \texttt{0} \quad \texttt{$ 0 1.2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2 1.2 1.2 1.2 1.2 1.2 0 2 1 2 2 2 3 2 4 2

H(21D) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(21F) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22A) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22B) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22C) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22E) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22F) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		
H(22D) 0.8282 0	0 0	0.1151 0.0151	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.2
1.2 1.2 1.2 1.2	1.2	0 2 1 2 2 2 3	2	4	2																		

loop\_

\_atom\_local\_axes\_atom\_label \_atom\_local\_axes\_atom0 \_atom\_local\_axes\_ax1 \_atom\_local\_axes\_atom1 \_atom\_local\_axes\_atom2 \_atom\_local\_axes\_ax2 S(1) C(18) Z S(1) C(15) Y S(1A) C(18A) Z S(1A) C(15A) Y O(1) C(15) X O(1) C(14) Y O(1A) C(15A) X O(1A) C(14A) Y O(2) C(15) X O(2) O(1) Y O(2A) C(15A) X O(2A) O(1A) Y N(1) C(16) X N(1) C(15) Y N(1A) C(16A) X N(1A) C(15A) Y N(2) C(18) Z N(2) N(1) Y N(2A) C(18A) Z N(2A) N(1A) Y C(1) C(2) X C(1) C(13) Y C(1A) C(2A) X C(1A) C(13A) Y C(2) C(1) X C(2) C(3) Y C(2A) C(1A) X C(2A) C(3A) Y C(3) C(4) X C(3) C(2) Y C(3A) C(4A) X C(3A) C(2A) Y C(4) C(3) X C(4) C(5) Y C(4A) C(3A) X C(4A) C(5A) Y C(5) C(4) X C(5) C(13) Y C(5A) C(4A) X C(5A) C(13A) Y C(6) C(7) X C(6) C(11) Y C(6A) C(7A) X C(6A) C(11A) Y C(7) C(6) X C(7) C(8) Y C(7A) C(6A) X C(7A) C(8A) Y C(8) C(9) X C(8) C(7) Y C(8A) C(9A) X C(8A) C(7A) Y C(9) C(10) X C(9) C(8) Y C(9A) C(10A) X C(9A) C(8A) Y C(10) C(9) X C(10) C(11) Y C(10A) C(9A) X C(10A) C(11A) Y C(11) C(10) X C(11) C(6) Y C(11A) C(10A) X C(11A) C(6A) Y C(12) C(11) X C(12) C(13) Y

C(12A) C(11A) X C(12A) C(13A) Y C(13) C(1) X C(13) C(5) Y C(13A) C(1A) X C(13A) C(5A) Y C(14) C(12) X C(14) O(1) Y C(14A) C(12A) X C(14A) O(1A) Y C(15) O(2) X C(15) N(1) Y C(15A) O(2A) X C(15A) N(1A) Y C(16) C(17) X C(16) N(1) Y C(16A) C(17A) X C(16A) N(1A) Y C(17) N(2) X C(17) C(16) Y C(17A) N(2A) X C(17A) C(16A) Y C(18) N(2) Z C(18) N(1) Y C(18A) N(2A) Z C(18A) N(1A) Y C(19) C(16) X C(19) C(20) Y C(19A) C(16A) X C(19A) C(20A) Y C(20) C(19) X C(20) C(21) Y C(20A) C(19A) X C(20A) C(22A) Y C(21) C(20) X C(21) C(22) Y C(21A) C(20A) X C(21A) C(22A) Y C(22) C(20) X C(22) C(21) Y C(22A) C(20A) X C(22A) C(21A) Y H(1) C(1) Z H(1) C(13) Y H(1A) C(1A) Z H(1A) C(13A) Y H(1N) N(1) Z H(1N) C(15) Y H(2) C(2) Z H(2) C(1) Y H(1NA) N(1A) Z H(1NA) C(15A) Y H(2A) C(2A) Z H(2A) C(1A) Y H(3) C(3) Z H(3) C(4) Y H(3A) C(3A) Z H(3A) C(4A) Y H(4) C(4) Z H(4) C(3) Y H(4A) C(4A) Z H(4A) C(3A) Y H(7) C(7) Z H(7) C(6) Y H(7A) C(7A) Z H(7A) C(6A) Y H(8) C(8) Z H(8) C(7) Y H(8A) C(8A) Z H(8A) C(9A) Y H(9) C(9) Z H(9) C(8) Y H(9A) C(9A) Z H(9A) C(8A) Y H(10) C(10) Z H(10) C(9) Y H(10A) C(10A) Z H(10A) C(9A) Y H(12) C(12) Z H(12) C(14) Y H(12A) C(12A) Z H(12A) C(14A) Y H(14A) C(14) Z H(14A) O(1) Y H(14B) C(14) Z H(14B) O(1) Y H(14D) C(14A) Z H(14D) O(1A) Y H(14C) C(14A) Z H(14C) O(1A) Y H(16) C(16) Z H(16) N(1) Y H(16A) C(16A) Z H(16A) N(1A) Y H(17A) C(17) Z H(17A) N(2) Y H(17B) C(17) Z H(17B) N(2) Y H(17D) C(17A) Z H(17D) N(2A) Y H(17C) C(17A) Z H(17C) N(2A) Y H(19A) C(19) Z H(19A) C(16) Y H(19B) C(19) Z H(19B) C(16) Y H(19D) C(19A) Z H(19D) C(16A) Y H(19C) C(19A) Z H(19C) C(16A) Y H(20) C(20) Z H(20) C(19) Y H(20A) C(20A) Z H(20A) C(19A) Y

H(21A)	C(21) Z H(21A) C(20) Y	
H(21B)	C(21) Z H(21B) C(20) Y	
H(21C)	C(21) Z H(21C) C(20) Y	
H(21E)	C(21A) Z H(21E) C(20A) Y	
H(21D)	C(21A) Z H(21D) C(20A) Y	
H(21F)	C(21A) Z H(21F) C(20A) Y	
H(22A)	C(22) Z H(22A) C(20) Y	
H(22B)	C(22) Z H(22B) C(20) Y	
H(22C)	C(22) Z H(22C) C(20) Y	
H(22E)	C(22A) Z H(22E) C(20A) Y	
H(22F)	C(22A) Z H(22F) C(20A) Y	
H(22D)	C(22A) Z H(22D) C(20A) Y	