

C1CE06011B_ccdc_838535_838540_cif.txt

data_global

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_journal_page_first ?
_journal_year ?

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_publ_author_name
'Nather, Christian'
'Boeckmann, Jan'
'Evers, Nils'

_publ_contact_author_name 'Dr Christian Nather'
_publ_contact_author_email cnaether@ac.uni-kiel.de

_publ_section_title

;
New Nickel(II) Thiocyanato Coordination Compounds:
Synthetic Aspects, Polymorphism, Thermal Reactivity and Magnetic Properties

;

Attachment '- TA71.CIF'

data_ta71

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#TrackingRef '- TA71.CIF'

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_chemical_name_systematic

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_chemical_name_common ?
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H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
S S 0.1246 0.1234 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
Ni Ni 0.3393 1.1124 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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_symmetry_equiv_pos_as_xyz
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'-x, -y, -z'

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;
Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is

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not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

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S1 S 0.3929(3) -0.1875(2) 0.8553(3) 0.0760(6) Uani 1 1 d . . .  
C1 C 0.2863(8) -0.0414(6) 0.8517(6) 0.0485(13) Uani 1 1 d . . .  
N1 N 0.2124(7) 0.0622(6) 0.8485(6) 0.0599(13) Uani 1 1 d . . .  
S2 S 0.1828(3) 0.2907(2) 1.11887(19) 0.0675(5) Uani 1 1 d . . .  
C2 C 0.0787(8) 0.4339(7) 1.1534(6) 0.0519(14) Uani 1 1 d . . .  
N2 N 0.0097(7) 0.5348(6) 1.1780(6) 0.0576(13) Uani 1 1 d . . .  
N11 N -0.1209(7) 0.1436(7) 0.8629(7) 0.0676(15) Uani 1 1 d . . .  
H17A H -0.1018 0.0445 0.8751 0.081 Uiso 1 1 calc R . .  
H17B H -0.1420 0.1779 0.9476 0.081 Uiso 1 1 calc R . .  
C11 C -0.2696(11) 0.1426(13) 0.7610(13) 0.102(3) Uani 1 1 d . . .  
H11A H -0.3082 0.2438 0.7606 0.123 Uiso 1 1 calc R . .  
H11B H -0.3538 0.0689 0.7895 0.123 Uiso 1 1 calc R . .  
C12 C -0.2461(13) 0.1014(13) 0.6128(14) 0.110(4) Uani 1 1 d . . .  
H12A H -0.3541 0.0903 0.5504 0.132 Uiso 1 1 calc R . .  
H12B H -0.2054 0.0011 0.6162 0.132 Uiso 1 1 calc R . .  
C13 C -0.1315(12) 0.2102(10) 0.5414(9) 0.083(3) Uani 1 1 d . . .  
H13A H -0.1414 0.1766 0.4412 0.099 Uiso 1 1 calc R . .  
H13B H -0.1679 0.3122 0.5415 0.099 Uiso 1 1 calc R . .  
N12 N 0.0439(8) 0.2214(8) 0.6101(6) 0.0689(16) Uani 1 1 d . . .  
H18 H 0.0690 0.1232 0.6013 0.083 Uiso 1 1 calc R . .  
C14 C 0.1496(15) 0.3075(11) 0.5237(9) 0.096(3) Uani 1 1 d . . .  
H14A H 0.1175 0.4113 0.5144 0.116 Uiso 1 1 calc R . .  
H14B H 0.1276 0.2604 0.4273 0.116 Uiso 1 1 calc R . .  
C15 C 0.3271(13) 0.3191(12) 0.5768(10) 0.095(3) Uani 1 1 d . . .  
H15A H 0.3834 0.3482 0.4971 0.113 Uiso 1 1 calc R . .
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H15B H 0.3559 0.2178 0.6067 0.113 Uiso 1 1 calc R . .
C16 C 0.3905(13) 0.4284(10) 0.6974(13) 0.099(3) Uani 1 1 d . . .
H16A H 0.3567 0.5288 0.6699 0.119 Uiso 1 1 calc R . .
H16B H 0.5106 0.4378 0.7141 0.119 Uiso 1 1 calc R . .
N13 N 0.3342(7) 0.3859(7) 0.8354(7) 0.0667(15) Uani 1 1 d . . .
H19A H 0.3386 0.4739 0.8872 0.080 Uiso 1 1 calc R . .
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_atom_site_aniso_U_13
_atom_site_aniso_U_12
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S1 0.0750(12) 0.0512(10) 0.0995(15) -0.0100(9) -0.0008(10) 0.0246(9)
C1 0.053(3) 0.038(3) 0.053(3) 0.000(2) 0.006(3) 0.007(2)
N1 0.070(4) 0.049(3) 0.064(3) -0.002(2) 0.012(3) 0.017(3)
S2 0.0983(14) 0.0559(9) 0.0531(9) 0.0014(7) 0.0086(9) 0.0391(9)
C2 0.069(4) 0.044(3) 0.041(3) 0.004(2) 0.005(3) 0.008(3)
N2 0.072(4) 0.044(3) 0.058(3) 0.002(2) 0.006(3) 0.018(3)
N11 0.064(4) 0.058(3) 0.083(4) 0.011(3) 0.019(3) 0.010(3)
C11 0.059(5) 0.098(7) 0.135(9) 0.036(6) -0.007(5) -0.015(5)
C12 0.076(6) 0.095(7) 0.139(10) -0.029(7) -0.024(6) 0.002(5)
C13 0.107(7) 0.066(5) 0.064(4) -0.008(4) -0.017(4) 0.015(5)
N12 0.082(4) 0.083(4) 0.044(3) -0.001(3) 0.006(3) 0.029(3)
C14 0.152(10) 0.079(6) 0.060(5) 0.008(4) 0.023(5) 0.014(6)
C15 0.113(8) 0.105(7) 0.087(6) 0.019(5) 0.058(6) 0.042(6)
C16 0.099(7) 0.068(5) 0.145(9) -0.005(6) 0.068(7) -0.002(5)
N13 0.062(3) 0.055(3) 0.081(4) -0.002(3) 0.009(3) 0.000(3)

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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Ni1 N11 2.069(6) . ?
Ni1 N1 2.070(5) . ?
Ni1 N12 2.092(5) . ?
Ni1 N13 2.099(6) . ?
Ni1 S2 2.6404(19) . ?
S1 C1 1.622(6) . ?
C1 N1 1.142(8) . ?
S2 C2 1.653(7) . ?
C2 N2 1.142(8) . ?
N2 Ni1 2.055(5) 2_567 ?
N11 C11 1.414(11) . ?
C11 C12 1.485(15) . ?
C12 C13 1.511(14) . ?
C13 N12 1.468(11) . ?
N12 C14 1.450(11) . ?
C14 C15 1.453(14) . ?
C15 C16 1.459(14) . ?
C16 N13 1.488(11) . ?

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N2 Ni1 N11 89.6(2) 2_567 . ?
N2 Ni1 N1 179.4(2) 2_567 . ?
N11 Ni1 N1 90.5(2) . . ?
N2 Ni1 N12 93.6(2) 2_567 . ?
N11 Ni1 N12 91.7(3) . . ?
N1 Ni1 N12 87.0(2) . . ?
N2 Ni1 N13 91.5(2) 2_567 . ?
N11 Ni1 N13 172.2(2) . . ?
N1 Ni1 N13 88.3(2) . . ?
N12 Ni1 N13 95.9(3) . . ?
N2 Ni1 S2 92.14(16) 2_567 . ?
N11 Ni1 S2 87.75(19) . . ?
N1 Ni1 S2 87.24(16) . . ?
N12 Ni1 S2 174.24(18) . . ?
N13 Ni1 S2 84.51(18) . . ?
N1 C1 S1 179.3(6) . . ?
C1 N1 Ni1 173.5(6) . . ?
C2 S2 Ni1 101.2(2) . . ?
N2 C2 S2 178.6(7) . . ?
C2 N2 Ni1 163.7(5) . 2_567 ?
C11 N11 Ni1 123.0(5) . . ?
N11 C11 C12 111.6(9) . . ?
C11 C12 C13 118.0(8) . . ?
N12 C13 C12 114.9(7) . . ?
C14 N12 C13 111.9(7) . . ?
C14 N12 Ni1 116.6(6) . . ?
C13 N12 Ni1 117.2(5) . . ?
N12 C14 C15 117.0(7) . . ?
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H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
S S 0.1246 0.1234 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
Ni Ni 0.3393 1.1124 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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'-x, y+1/2, -z+1/2'
'-x, -y, -z'
'x, -y-1/2, z-1/2'

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_cell_length_c                  12.2373(7)
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_cell_angle_gamma               90.00
_cell_volume                    2080.4(2)
_cell_formula_units_Z           4
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_cell_measurement_reflns_used   12789
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_diffn_standards_decay_%         ?
_diffn_reflns_number             12789
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_computing_cell_refinement      ?
_computing_data_reduction       ?
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_computing_structure_refinement 'SHELXL-97 (Sheldrick, 1997)'
_computing_molecular_graphics   ?
_computing_publication_material ?

_refine_special_details
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Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
;

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_refine_ls_matrix_type          full
_refine_ls_weighting_scheme     calc
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_atom_sites_solution_secondary difmap
_atom_sites_solution_hydrogens  geom
_refine_ls_hydrogen_treatment   constr
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S1 S 1.13954(9) 0.28241(5) 0.44891(7) 0.0344(2) Uani 1 1 d . . .
C1 C 1.2083(4) 0.36538(17) 0.4473(2) 0.0281(6) Uani 1 1 d . . .
N1 N 1.2569(4) 0.42426(16) 0.4447(2) 0.0470(8) Uani 1 1 d . . .
S2 S 0.80309(11) 0.15317(5) 0.34935(7) 0.0419(2) Uani 1 1 d . . .
C2 C 0.7178(4) 0.0773(2) 0.3566(3) 0.0350(7) Uani 1 1 d . . .
N2 N 0.6698(5) 0.02053(15) 0.3590(3) 0.0680(14) Uani 1 1 d . . .
N11 N 0.6119(2) 0.52349(11) 0.31584(17) 0.0180(4) Uani 1 1 d . . .
H11A H 0.5164 0.5144 0.2967 0.022 Uiso 1 1 calc R . .
H11B H 0.6241 0.5282 0.3911 0.022 Uiso 1 1 calc R . .
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C25 C 0.4146(3) 0.33067(16) 0.1631(2) 0.0264(6) Uani 1 1 d . . .
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H25B H 0.3521 0.2916 0.1278 0.032 Uiso 1 1 calc R . .
C26 C 0.5240(3) 0.35161(16) 0.0860(2) 0.0249(6) Uani 1 1 d . . .
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are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
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used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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H16A H 0.0632 0.9450 0.0923 0.049 Uiso 1 1 calc R . .
H16B H 0.0822 0.9029 0.0190 0.049 Uiso 1 1 calc R . .
N21 N 0.4185(8) 0.8603(3) 0.3017(6) 0.0330(19) Uani 1 1 d . . . .
H1A H 0.5041 0.8438 0.3122 0.040 Uiso 1 1 calc R . .
H1B H 0.4448 0.8890 0.2858 0.040 Uiso 1 1 calc R . .
N22 N 0.1481(8) 0.7952(2) 0.2579(6) 0.0303(18) Uani 1 1 d . . . .
H2 H 0.1922 0.7671 0.2652 0.036 Uiso 1 1 calc R . .
N23 N 0.1705(8) 0.8074(3) 0.0286(7) 0.036(2) Uani 1 1 d . . . .
H3A H 0.1859 0.8267 -0.0244 0.044 Uiso 1 1 calc R . .
H3B H 0.2140 0.7807 0.0151 0.044 Uiso 1 1 calc R . .
C21 C 0.3588(11) 0.8625(4) 0.4033(8) 0.040(2) Uani 1 1 d . . . .
H1C H 0.2837 0.8865 0.4009 0.048 Uiso 1 1 calc R . .
H1D H 0.4392 0.8699 0.4590 0.048 Uiso 1 1 calc R . .
C22 C 0.2908(12) 0.8185(4) 0.4272(8) 0.044(3) Uani 1 1 d . . . .
H2A H 0.2815 0.8175 0.5022 0.053 Uiso 1 1 calc R . .
H2B H 0.3579 0.7940 0.4122 0.053 Uiso 1 1 calc R . .
C23 C 0.1392(12) 0.8101(4) 0.3660(8) 0.043(3) Uani 1 1 d . . . .
H3C H 0.0873 0.7869 0.4021 0.052 Uiso 1 1 calc R . .
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H3D H 0.0805 0.8380 0.3644 0.052 Uiso 1 1 calc R . . .
C24 C -0.0068(10) 0.7857(3) 0.2115(9) 0.036(3) Uani 1 1 d . . .
H4A H -0.0637 0.8140 0.2083 0.043 Uiso 1 1 calc R . . .
H4B H -0.0521 0.7648 0.2576 0.043 Uiso 1 1 calc R . . .
C25 C -0.0185(12) 0.7657(4) 0.1043(10) 0.046(3) Uani 1 1 d . . .
H5A H -0.1188 0.7533 0.0862 0.056 Uiso 1 1 calc R . . .
H5B H 0.0522 0.7406 0.1049 0.056 Uiso 1 1 calc R . . .
C26 C 0.0121(11) 0.7993(4) 0.0199(9) 0.041(3) Uani 1 1 d . . .
H6A H -0.0236 0.7871 -0.0495 0.050 Uiso 1 1 calc R . . .
H6B H -0.0405 0.8278 0.0289 0.050 Uiso 1 1 calc R . . .
N31 N 0.8642(10) 0.9505(3) 0.4567(8) 0.048(2) Uani 1 1 d . . .
H21C H 0.8391 0.9265 0.4137 0.058 Uiso 1 1 calc R . . .
H21D H 0.8237 0.9754 0.4224 0.058 Uiso 1 1 calc R . . .
N32 N 0.9433(8) 0.9272(3) 0.6890(6) 0.0292(19) Uani 1 1 d . . .
H22 H 0.9506 0.8961 0.6884 0.035 Uiso 1 1 calc R . . .
N33 N 0.6116(9) 0.9324(3) 0.6972(7) 0.040(2) Uani 1 1 d . . .
H23A H 0.5284 0.9493 0.6785 0.048 Uiso 1 1 calc R . . .
H23B H 0.5828 0.9028 0.6945 0.048 Uiso 1 1 calc R . . .
C31 C 1.0209(13) 0.9554(5) 0.4611(11) 0.063(4) Uani 1 1 d . . .
H21A H 1.0468 0.9876 0.4688 0.075 Uiso 1 1 calc R . . .
H21B H 1.0520 0.9448 0.3950 0.075 Uiso 1 1 calc R . . .
C32 C 1.1035(12) 0.9296(4) 0.5499(9) 0.048(3) Uani 1 1 d . . .
H22A H 1.0752 0.8976 0.5414 0.058 Uiso 1 1 calc R . . .
H22B H 1.2099 0.9316 0.5435 0.058 Uiso 1 1 calc R . . .
C33 C 1.0826(10) 0.9431(4) 0.6549(9) 0.041(2) Uani 1 1 d . . .
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H24B H 1.0311 0.9267 0.8377 0.051 Uiso 1 1 calc R . . .
C35 C 0.8050(12) 0.9205(4) 0.8448(9) 0.050(3) Uani 1 1 d . . .
H25A H 0.7947 0.8881 0.8297 0.059 Uiso 1 1 calc R . . .
H25B H 0.8235 0.9240 0.9211 0.059 Uiso 1 1 calc R . . .
C36 C 0.6652(13) 0.9430(5) 0.8067(9) 0.055(3) Uani 1 1 d . . .
H26A H 0.6788 0.9758 0.8139 0.066 Uiso 1 1 calc R . . .
H26B H 0.5894 0.9339 0.8506 0.066 Uiso 1 1 calc R . . .
O1w O 0.2407(12) 0.6940(3) 0.2439(10) 0.094(4) Uani 1 1 d . . .
H10 H 0.1637 0.6789 0.2282 0.142 Uiso 1 1 d R . . .
H20 H 0.3073 0.6766 0.2701 0.142 Uiso 1 1 d R . . .

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Ni2 0.0333(6) 0.0307(7) 0.0316(8) -0.0027(6) -0.0007(5) -0.0035(6)
N1 0.166(14) 0.064(8) 0.045(8) -0.013(6) 0.026(9) -0.009(10)
C1 0.052(6) 0.026(5) 0.041(7) -0.008(5) -0.001(5) -0.006(5)
S1 0.093(3) 0.073(2) 0.056(2) 0.005(2) -0.002(2) 0.004(2)
N2 0.045(5) 0.052(6) 0.044(7) 0.005(5) -0.010(5) 0.001(5)
C2 0.029(5) 0.039(6) 0.055(8) -0.002(5) 0.004(5) -0.004(5)
S2 0.0467(16) 0.0478(17) 0.0424(19) -0.0013(14) -0.0091(13) 0.0002(13)
N3 0.053(6) 0.037(5) 0.055(7) -0.009(5) 0.001(5) -0.011(4)
C3 0.036(5) 0.040(6) 0.041(7) 0.003(5) 0.002(5) -0.001(5)
S3 0.0441(15) 0.0353(14) 0.0385(17) -0.0025(13) 0.0027(13) 0.0062(12)
N4 0.040(5) 0.034(5) 0.047(6) 0.002(4) 0.003(4) -0.003(4)
C4 0.028(5) 0.038(6) 0.037(6) 0.011(5) 0.007(4) 0.008(5)
S4 0.0427(14) 0.0341(14) 0.058(2) -0.0025(13) 0.0018(13) 0.0034(12)
N11 0.039(5) 0.028(5) 0.055(7) 0.007(4) 0.010(4) 0.001(4)
N12 0.038(4) 0.037(5) 0.026(5) -0.005(4) 0.010(4) -0.009(4)
N13 0.032(4) 0.036(5) 0.025(5) 0.006(4) -0.004(3) 0.002(3)
C11 0.038(6) 0.050(7) 0.044(7) -0.011(6) 0.021(5) 0.011(5)
C12 0.038(6) 0.035(6) 0.064(9) -0.007(6) 0.023(6) -0.010(5)
C13 0.052(6) 0.061(7) 0.034(6) 0.005(6) 0.023(5) 0.021(6)

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C14 0.060(7) 0.046(7) 0.045(8) 0.018(6) 0.014(6) 0.006(6)
C15 0.056(7) 0.041(6) 0.041(7) 0.008(6) 0.008(5) 0.006(5)
C16 0.054(6) 0.037(6) 0.031(6) 0.017(5) 0.008(5) 0.013(5)
N21 0.035(4) 0.034(4) 0.031(5) -0.006(4) 0.006(4) -0.005(4)
N22 0.034(4) 0.029(4) 0.030(5) 0.008(4) 0.011(4) -0.002(3)
N23 0.032(4) 0.041(5) 0.036(5) 0.000(4) -0.001(4) 0.004(4)
C21 0.043(6) 0.046(6) 0.031(6) 0.001(5) 0.003(5) -0.007(5)
C22 0.049(6) 0.063(7) 0.018(6) 0.008(5) -0.004(5) 0.002(6)
C23 0.056(7) 0.053(7) 0.023(6) 0.005(5) 0.016(5) -0.007(5)
C24 0.029(5) 0.032(5) 0.051(7) 0.000(5) 0.019(5) -0.006(4)
C25 0.041(6) 0.049(7) 0.049(8) 0.000(6) 0.005(5) -0.008(5)
C26 0.041(6) 0.046(6) 0.036(7) -0.006(5) 0.001(5) -0.015(5)
N31 0.057(6) 0.051(6) 0.033(6) 0.001(5) -0.004(4) -0.001(5)
N32 0.033(4) 0.027(4) 0.028(5) -0.005(4) 0.003(4) -0.003(3)
N33 0.035(5) 0.040(5) 0.049(6) 0.012(4) 0.017(4) -0.003(4)
C31 0.061(8) 0.083(10) 0.051(8) -0.001(7) 0.035(7) -0.012(7)
C32 0.044(6) 0.056(7) 0.047(8) 0.005(6) 0.016(6) -0.003(5)
C33 0.025(5) 0.051(6) 0.049(7) -0.003(6) 0.007(4) -0.007(5)
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C35 0.063(7) 0.061(7) 0.028(6) 0.003(6) 0.017(5) 0.001(6)
C36 0.056(7) 0.073(8) 0.041(7) -0.008(7) 0.022(6) -0.014(7)
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All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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Ni1 N21 2.152(8) . ?
Ni1 N22 2.189(7) . ?
Ni1 N12 2.207(8) . ?
Ni2 N33 2.070(8) . ?
Ni2 N4 2.089(9) . ?
Ni2 N31 2.092(10) . ?
Ni2 N2 2.103(10) . ?
Ni2 N32 2.130(8) . ?
Ni2 N3 2.140(9) . ?
N1 C1 1.052(16) . ?
C1 S1 1.636(14) . ?
N2 C2 1.137(13) . ?
C2 S2 1.649(12) . ?
N3 C3 1.182(13) . ?
C3 S3 1.626(11) . ?
N4 C4 1.156(13) . ?
C4 S4 1.640(11) . ?
N11 C11 1.504(13) . ?
N12 C13 1.461(13) . ?
N12 C14 1.486(13) . ?
N13 C16 1.466(12) . ?
C11 C12 1.525(14) . ?
C12 C13 1.482(16) . ?
C14 C15 1.503(15) . ?
C15 C16 1.520(15) . ?
N21 C21 1.493(13) . ?

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N22 C23 1.485(13) . ?
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N23 C26 1.460(12) . ?
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N13 Ni1 N21 86.9(3) . . ?
N11 Ni1 N21 88.4(3) . . ?
N23 Ni1 N22 89.7(3) . . ?
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N13 Ni1 N12 92.0(3) . . ?
N11 Ni1 N12 91.1(3) . . ?
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N22 Ni1 N12 177.1(3) . . ?
N33 Ni2 N4 91.3(4) . . ?
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N4 Ni2 N31 90.9(4) . . ?
N33 Ni2 N2 88.1(4) . . ?
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N1 C1 S1 177.0(14) . . ?
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C13 N12 C14 107.6(8) . . ?
C13 N12 Ni1 116.4(7) . . ?
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C16 N13 Ni1 118.1(6) . . ?
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C13 C12 C11 116.0(9) . . ?

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N12 C13 C12 115.0(10) . . ?
N12 C14 C15 116.8(10) . . ?
C14 C15 C16 114.3(10) . . ?
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C21 N21 Ni1 121.1(6) . . ?
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N23 C26 C25 108.8(9) . . ?
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C33 C32 C31 117.5(10) . . ?
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H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
S S 0.1246 0.1234 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
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'-x, y+1/2, -z+1/2'
'-x, -y, -z'
'x, -y-1/2, z-1/2'

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_refine_special_details
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Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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C1 C 0.97436(13) 0.74568(19) 0.56931(10) 0.0183(3) Uani 1 1 d . . .
S1 S 1.08902(4) 0.74797(7) 0.53805(4) 0.03661(14) Uani 1 1 d . . .
N2 N 0.60089(12) 0.65218(18) 0.65594(10) 0.0229(3) Uani 1 1 d . . .
C2 C 0.51465(13) 0.62296(18) 0.65918(10) 0.0176(3) Uani 1 1 d . . .
S2 S 0.39285(3) 0.58240(6) 0.66316(3) 0.02590(11) Uani 1 1 d . . .
N11 N 0.74403(12) 0.50005(17) 0.54898(9) 0.0212(3) Uani 1 1 d . . .
H11D H 0.6995 0.5135 0.4967 0.025 Uiso 1 1 calc R . .
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N12 N 0.81645(11) 0.57610(16) 0.73973(9) 0.0193(3) Uani 1 1 d . . .
H12C H 0.7624 0.5477 0.7699 0.023 Uiso 1 1 calc R . .
N13 N 0.74674(12) 0.89741(17) 0.69815(9) 0.0210(3) Uani 1 1 d . . .
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H13D H 0.7418 0.9755 0.6584 0.025 Uiso 1 1 calc R . .
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C12 C 0.79160(17) 0.3171(2) 0.67321(14) 0.0321(4) Uani 1 1 d . . .
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C13 C 0.86646(15) 0.4365(2) 0.71459(12) 0.0267(4) Uani 1 1 d . . .
H13A H 0.9085 0.3947 0.7685 0.032 Uiso 1 1 calc R . .
H13B H 0.9143 0.4617 0.6718 0.032 Uiso 1 1 calc R . .
C14 C 0.89165(16) 0.6598(2) 0.80451(12) 0.0280(4) Uani 1 1 d . . .
H14A H 0.9536 0.6830 0.7763 0.034 Uiso 1 1 calc R . .
H14B H 0.9142 0.5950 0.8566 0.034 Uiso 1 1 calc R . .
C15 C 0.84880(17) 0.8047(2) 0.83714(12) 0.0309(4) Uani 1 1 d . . .
H15A H 0.7811 0.7834 0.8567 0.037 Uiso 1 1 calc R . .
H15B H 0.8964 0.8398 0.8899 0.037 Uiso 1 1 calc R . .
C16 C 0.83413(15) 0.9295(2) 0.76906(11) 0.0247(4) Uani 1 1 d . . .
H16A H 0.8207 1.0240 0.7991 0.030 Uiso 1 1 calc R . .
H16B H 0.8984 0.9419 0.7423 0.030 Uiso 1 1 calc R . .
N21 N 0.67586(11) 0.82235(15) 0.50925(9) 0.0183(3) Uani 1 1 d . . .
C21 C 0.58133(14) 0.7884(2) 0.46604(11) 0.0238(4) Uani 1 1 d . . .
H21 H 0.5476 0.7021 0.4840 0.029 Uiso 1 1 calc R . .
C22 C 0.53064(15) 0.8729(2) 0.39662(12) 0.0290(4) Uani 1 1 d . . .
H22 H 0.4643 0.8439 0.3673 0.035 Uiso 1 1 calc R . .
C23 C 0.57808(15) 1.0005(2) 0.37058(11) 0.0254(4) Uani 1 1 d . . .
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C25 C 0.72220(14) 0.94459(19) 0.48203(11) 0.0201(3) Uani 1 1 d . . .
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S1 0.0172(3) 0.0483(3) 0.0479(3) -0.0090(2) 0.0168(2) -0.0052(2)
N2 0.0151(8) 0.0289(8) 0.0258(7) 0.0037(6) 0.0062(5) -0.0014(6)
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C11 0.0276(11) 0.0187(9) 0.0397(10) -0.0043(7) 0.0071(8) -0.0044(7)
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C14 0.0274(11) 0.0304(10) 0.0231(8) 0.0028(7) -0.0069(7) 0.0012(8)
C15 0.0387(12) 0.0336(11) 0.0182(8) -0.0027(7) -0.0028(7) 0.0000(9)
C16 0.0239(10) 0.0248(9) 0.0246(8) -0.0044(7) 0.0007(7) -0.0020(7)
N21 0.0179(7) 0.0196(7) 0.0171(6) 0.0016(5) 0.0014(5) -0.0006(5)
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All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles

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and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.
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C21 N21 Ni1 122.49(11) . . ?
C25 N21 Ni1 120.22(12) . . ?
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H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
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Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based

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on F^2 are statistically about twice as large as those based on F , and R -factors based on ALL data will be even larger.

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Ni2 Ni 0.78131(7) 0.70916(4) 0.41196(3) 0.03697(15) Uani 1 1 d . . .
S1 S 0.66965(11) 0.55673(7) 0.13565(6) 0.0305(2) Uani 1 1 d . . .
C1 C 0.5346(4) 0.4713(2) 0.1094(2) 0.0223(6) Uani 1 1 d . . .
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S3 S 0.42440(15) 0.77484(13) 0.67638(9) 0.0646(4) Uani 1 1 d . A .
C3 C 0.5502(6) 0.7610(3) 0.5860(3) 0.0390(9) Uani 1 1 d . . .
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S4 S 1.14787(11) 0.59295(7) 0.16663(7) 0.0349(2) Uani 1 1 d . A .
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N4 N 0.9289(4) 0.6627(3) 0.3015(2) 0.0376(8) Uani 1 1 d . A .
N11 N 0.9116(3) 0.6273(2) -0.0491(2) 0.0287(6) Uani 1 1 d . . .
H11A H 0.9608 0.6081 0.0070 0.034 Uiso 1 1 calc R . .
H11B H 0.8894 0.5689 -0.0747 0.034 Uiso 1 1 calc R . .
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H13B H 0.4323 0.7203 0.0881 0.037 Uiso 1 1 calc R . .
C11 C 1.0378(4) 0.6856(3) -0.1114(3) 0.0403(9) Uani 1 1 d . . .
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H11D H 1.0853 0.7395 -0.0786 0.048 Uiso 1 1 calc R . .
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H13D H 0.8344 0.8613 -0.2517 0.045 Uiso 1 1 calc R . .
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C15 C 0.4185(5) 0.8879(3) -0.0942(3) 0.0364(9) Uani 1 1 d . . .
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C16 C 0.3975(5) 0.8484(3) 0.0081(3) 0.0370(9) Uani 1 1 d . . .
H16A H 0.4698 0.8880 0.0447 0.044 Uiso 1 1 calc R . .
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H21A H 1.0022 0.6887 0.5369 0.076 Uiso 1 1 calc R . .
H21B H 1.0950 0.7018 0.4452 0.076 Uiso 1 1 calc R . .
N22 N 0.7759(4) 0.8583(2) 0.3455(2) 0.0301(6) Uani 1 1 d . A .
H22 H 0.8305 0.8557 0.2875 0.036 Uiso 1 1 calc R . .
N23 N 0.5700(5) 0.6664(3) 0.3466(3) 0.0531(10) Uani 1 1 d . A .
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H23B H 0.5226 0.6116 0.3836 0.064 Uiso 1 1 calc R . .
C21 C 1.0625(7) 0.8294(4) 0.4965(4) 0.0669(16) Uani 1 1 d . . .
H21C H 1.1806 0.8267 0.5162 0.080 Uiso 1 1 calc R A .
H21D H 0.9911 0.8519 0.5480 0.080 Uiso 1 1 calc R . .
C22 C 1.0491(6) 0.9045(4) 0.4104(4) 0.0586(13) Uani 1 1 d . A .
H22A H 1.1013 0.8750 0.3563 0.070 Uiso 1 1 calc R . .
H22B H 1.1139 0.9661 0.4186 0.070 Uiso 1 1 calc R . .
C23 C 0.8696(6) 0.9349(3) 0.3885(3) 0.0447(10) Uani 1 1 d . . .
H23C H 0.8087 0.9478 0.4472 0.054 Uiso 1 1 calc R A .
H23D H 0.8718 0.9991 0.3456 0.054 Uiso 1 1 calc R . .
C24 C 0.6071(5) 0.9011(3) 0.3238(3) 0.0408(9) Uani 1 1 d . . .
H24A H 0.6218 0.9689 0.2873 0.049 Uiso 1 1 calc R A .
H24B H 0.5452 0.9103 0.3832 0.049 Uiso 1 1 calc R . .
C25 C 0.5020(6) 0.8366(4) 0.2694(3) 0.0527(12) Uani 1 1 d . A .
H25A H 0.4066 0.8777 0.2438 0.063 Uiso 1 1 calc R . .
H25B H 0.5717 0.8174 0.2158 0.063 Uiso 1 1 calc R . .
C26 C 0.4332(5) 0.7420(4) 0.3249(4) 0.0559(13) Uani 1 1 d . . .
H26A H 0.3785 0.7589 0.3840 0.067 Uiso 1 1 calc R A .
H26B H 0.3467 0.7121 0.2889 0.067 Uiso 1 1 calc R . .
O1w O 0.8181(8) 0.5598(5) 0.4811(5) 0.0529(15) Uani 0.70 1 d P A 1
H101 H 0.7548 0.5358 0.5265 0.079 Uiso 1 1 d R . .
H201 H 0.7843 0.5105 0.4557 0.079 Uiso 1 1 d R . .
O1w' O 0.722(2) 0.5503(11) 0.4751(11) 0.061(4) Uani 0.30 1 d P A 2
O2w O 0.8197(7) 0.4190(3) 0.3537(3) 0.0914(15) Uani 1 1 d . . .
H102 H 0.7152 0.4236 0.3475 0.137 Uiso 1 1 d R . .
H202 H 0.8907 0.4319 0.3090 0.137 Uiso 1 1 d R . .
O3w O 0.6633(6) 0.5288(3) 0.6564(3) 0.0851(14) Uani 1 1 d . . .
H103 H 0.5879 0.5655 0.6772 0.128 Uiso 1 1 d R . .
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S1 0.0326(4) 0.0285(4) 0.0315(5) -0.0044(4) -0.0099(4) -0.0115(3)
C1 0.0250(15) 0.0211(14) 0.0212(16) -0.0023(12) -0.0039(13) -0.0010(12)
N1 0.0283(14) 0.0219(13) 0.0292(15) -0.0030(12) -0.0033(12) -0.0048(11)
S2 0.0384(5) 0.0381(5) 0.0400(5) -0.0180(4) 0.0027(4) -0.0174(4)
C2 0.0245(15) 0.0223(15) 0.0260(17) -0.0074(13) 0.0000(13) -0.0021(12)
N2 0.0313(15) 0.0275(15) 0.0372(17) -0.0101(13) -0.0052(13) -0.0029(12)
S3 0.0368(6) 0.1249(12) 0.0393(6) -0.0393(7) -0.0003(5) 0.0075(7)

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C3 0.054(2) 0.038(2) 0.0252(19) -0.0049(16) -0.0015(18) 0.0116(18)
N3 0.092(3) 0.049(2) 0.037(2) -0.0074(18) 0.026(2) 0.009(2)
S4 0.0258(4) 0.0426(5) 0.0393(5) -0.0181(4) 0.0031(4) 0.0008(4)
C4 0.0297(17) 0.0249(16) 0.0318(18) -0.0088(14) -0.0064(15) 0.0013(13)
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N11 0.0225(13) 0.0258(14) 0.0394(17) -0.0090(13) -0.0043(13) 0.0033(11)
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N13 0.0236(14) 0.0357(16) 0.0345(16) -0.0067(13) 0.0035(12) 0.0015(12)
C11 0.0176(16) 0.042(2) 0.061(3) -0.011(2) 0.0077(17) 0.0018(15)
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C13 0.0318(19) 0.0293(18) 0.049(2) 0.0038(17) 0.0116(18) -0.0058(15)
C14 0.039(2) 0.0210(16) 0.040(2) 0.0030(15) -0.0030(17) 0.0063(14)
C15 0.0319(18) 0.0369(19) 0.040(2) -0.0039(17) -0.0032(16) 0.0158(16)
C16 0.0347(19) 0.041(2) 0.037(2) -0.0127(17) 0.0008(17) 0.0142(16)
N21 0.074(3) 0.070(3) 0.053(2) -0.024(2) -0.030(2) 0.034(2)
N22 0.0302(15) 0.0334(15) 0.0278(15) -0.0085(13) -0.0025(13) 0.0044(12)
N23 0.047(2) 0.050(2) 0.066(3) -0.027(2) 0.0136(19) -0.0071(17)
C21 0.066(3) 0.078(4) 0.067(3) -0.037(3) -0.037(3) 0.023(3)
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C23 0.050(2) 0.039(2) 0.049(2) -0.0162(19) -0.012(2) 0.0043(18)
C24 0.033(2) 0.041(2) 0.047(2) 0.0006(19) -0.0032(18) 0.0061(16)
C25 0.033(2) 0.081(3) 0.045(3) -0.010(2) -0.0101(19) 0.002(2)
C26 0.032(2) 0.070(3) 0.071(3) -0.032(3) -0.001(2) -0.004(2)
O1W 0.066(4) 0.040(3) 0.052(3) -0.001(2) 0.000(3) -0.002(3)
O1W' 0.097(12) 0.042(7) 0.041(7) 0.003(6) 0.011(9) 0.030(9)
O2W 0.148(4) 0.057(2) 0.069(3) -0.013(2) 0.016(3) -0.009(3)
O3W 0.097(3) 0.081(3) 0.067(3) 0.028(2) 0.012(2) 0.033(2)

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All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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N11 N1 2.098(3) 2_665 ?
N11 N12 2.102(3) . ?
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S1 C1 1.653(3) . ?
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N1 N11 2.098(3) 2_665 ?
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N12 C13 1.488(5) . ?
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N21 C21 C22 111.4(4) . . ?
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H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
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_refine_special_details
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Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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N1 N 0.7569(2) 0.67144(14) 0.33858(7) 0.0550(5) Uani 1 1 d . . .
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C2 C 0.2352(3) 0.65319(15) 0.43588(8) 0.0454(5) Uani 1 1 d . . .
S2 S 0.07959(8) 0.67080(6) 0.46669(3) 0.0708(2) Uani 1 1 d . . .
N11 N 0.4228(2) 0.64216(14) 0.31539(7) 0.0540(5) Uani 1 1 d . . .
H11A H 0.3337 0.6733 0.3195 0.065 Uiso 1 1 calc R . .
H11B H 0.4772 0.6718 0.2935 0.065 Uiso 1 1 calc R . .
N12 N 0.6044(2) 0.51314(13) 0.38195(7) 0.0511(5) Uani 1 1 d . . .
H12 H 0.7060 0.5096 0.3732 0.061 Uiso 1 1 calc R . .
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H13A H 0.7816 0.6796 0.4293 0.060 Uiso 1 1 calc R . .
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H13B H 0.6555 0.7340 0.4476 0.060 Uiso 1 1 calc R . . .
C11 C 0.3793(4) 0.5541(2) 0.29549(10) 0.0696(8) Uani 1 1 d . . .
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C12 C 0.5061(4) 0.4844(2) 0.30159(10) 0.0741(8) Uani 1 1 d . . .
H12A H 0.6045 0.5106 0.2919 0.089 Uiso 1 1 calc R . . .
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C13 C 0.5226(4) 0.45029(19) 0.35057(10) 0.0713(8) Uani 1 1 d . . .
H13C H 0.4195 0.4385 0.3629 0.086 Uiso 1 1 calc R . . .
H13D H 0.5786 0.3933 0.3500 0.086 Uiso 1 1 calc R . . .
C14 C 0.6020(4) 0.47393(18) 0.42891(9) 0.0642(7) Uani 1 1 d . . .
H14A H 0.6309 0.4106 0.4269 0.077 Uiso 1 1 calc R . . .
H14B H 0.4963 0.4768 0.4407 0.077 Uiso 1 1 calc R . . .
C16 C 0.6634(3) 0.61478(18) 0.47625(8) 0.0574(6) Uani 1 1 d . . .
H16A H 0.5561 0.6151 0.4868 0.069 Uiso 1 1 calc R . . .
H16B H 0.7286 0.6347 0.5017 0.069 Uiso 1 1 calc R . . .
N21 N 0.5080(2) 0.79993(13) 0.37198(6) 0.0468(4) Uani 1 1 d . . .
C21 C 0.5511(3) 0.84918(17) 0.33554(8) 0.0556(6) Uani 1 1 d . . .
H21 H 0.5979 0.8199 0.3107 0.067 Uiso 1 1 calc R . . .
C22 C 0.5293(3) 0.94154(18) 0.33306(9) 0.0610(7) Uani 1 1 d . . .
H22 H 0.5600 0.9733 0.3068 0.073 Uiso 1 1 calc R . . .
C23 C 0.4625(3) 0.98612(17) 0.36930(9) 0.0596(6) Uani 1 1 d . . .
H23 H 0.4480 1.0485 0.3684 0.071 Uiso 1 1 calc R . . .
C24 C 0.4172(3) 0.93660(17) 0.40706(10) 0.0592(6) Uani 1 1 d . . .
H24 H 0.3712 0.9649 0.4323 0.071 Uiso 1 1 calc R . . .
C25 C 0.4406(3) 0.84440(16) 0.40705(9) 0.0519(5) Uani 1 1 d . . .
H25 H 0.4082 0.8113 0.4327 0.062 Uiso 1 1 calc R . . .
C15 C 0.7085(3) 0.51999(19) 0.46276(9) 0.0660(7) Uani 1 1 d . . .
H15A H 0.8124 0.5217 0.4496 0.079 Uiso 1 1 calc R . . .
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N1 0.0515(11) 0.0604(12) 0.0529(11) 0.0018(10) 0.0114(10) 0.0016(10)
C1 0.0515(13) 0.0436(11) 0.0434(12) -0.0010(9) 0.0007(10) 0.0054(10)
S1 0.0533(4) 0.0805(5) 0.0635(4) 0.0022(3) 0.0121(3) -0.0088(3)
N2 0.0474(10) 0.0549(12) 0.0540(11) 0.0013(9) 0.0071(9) -0.0021(9)
C2 0.0452(11) 0.0426(11) 0.0483(12) -0.0026(10) -0.0017(10) -0.0042(10)
S2 0.0502(3) 0.0863(5) 0.0758(5) -0.0235(4) 0.0144(3) -0.0014(3)
N11 0.0534(11) 0.0616(12) 0.0469(11) -0.0039(9) -0.0017(9) 0.0016(10)
N12 0.0560(11) 0.0474(10) 0.0501(11) -0.0011(9) 0.0068(9) 0.0030(9)
N13 0.0505(11) 0.0544(11) 0.0462(11) 0.0014(9) -0.0014(9) 0.0003(9)
C11 0.0776(19) 0.0740(19) 0.0574(16) -0.0077(14) -0.0078(14) -0.0138(16)
C12 0.104(2) 0.0616(17) 0.0563(16) -0.0154(13) 0.0042(16) -0.0059(16)
C13 0.102(2) 0.0490(15) 0.0632(17) -0.0063(12) -0.0013(16) -0.0065(15)
C14 0.0840(19) 0.0483(14) 0.0602(16) 0.0108(12) 0.0028(14) 0.0038(13)
C16 0.0611(15) 0.0677(16) 0.0434(13) 0.0040(11) -0.0038(11) 0.0038(13)
N21 0.0515(10) 0.0460(10) 0.0430(10) 0.0006(8) 0.0023(8) 0.0007(8)
C21 0.0678(15) 0.0543(14) 0.0446(12) 0.0028(11) 0.0041(11) 0.0012(13)
C22 0.0753(17) 0.0561(15) 0.0516(14) 0.0126(12) -0.0027(13) -0.0041(13)
C23 0.0672(16) 0.0451(13) 0.0664(16) 0.0045(12) -0.0040(13) 0.0015(12)
C24 0.0656(15) 0.0494(13) 0.0625(15) -0.0047(12) 0.0088(13) 0.0028(12)
C25 0.0586(14) 0.0481(12) 0.0489(12) -0.0002(10) 0.0083(11) -0.0010(11)
C15 0.0758(18) 0.0646(16) 0.0577(15) 0.0095(13) -0.0066(14) 0.0123(14)

_geom_special_details

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only

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used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.
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Ni1 N12 2.1386(19) . ?  
Ni1 N21 2.1879(19) . ?  
N1 C1 1.154(3) . ?  
C1 S1 1.629(2) . ?  
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C2 S2 1.627(2) . ?  
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C12 C13 1.511(4) . ?  
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N21 C25 1.340(3) . ?  
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N13 Ni1 N1 88.05(8) . . ?  
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C1 N1 Ni1 172.2(2) . . ?  
N1 C1 S1 179.6(2) . . ?  
C2 N2 Ni1 163.81(19) . . ?  
N2 C2 S2 178.7(2) . . ?  
C11 N11 Ni1 122.64(17) . . ?  
C13 N12 C14 108.2(2) . . ?  
C13 N12 Ni1 117.69(17) . . ?  
C14 N12 Ni1 116.23(15) . . ?  
C16 N13 Ni1 118.28(16) . . ?  
N11 C11 C12 112.0(2) . . ?
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C1CE06011B_ccdc_838535_838540_cif.txt
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N12 C14 C15 114.4(2) . . ?
N13 C16 C15 111.7(2) . . ?
C21 N21 C25 116.8(2) . . ?
C21 N21 Ni1 122.87(16) . . ?
C25 N21 Ni1 120.27(15) . . ?
N21 C21 C22 122.9(2) . . ?
C23 C22 C21 119.6(2) . . ?
C22 C23 C24 118.3(2) . . ?
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