

## Supporting information

### Solvent influence structural variation from 3D 4-fold interpenetrated framework to 2D layer-type porous coordination polymer: Structure analysis and highly selective gas adsorption properties

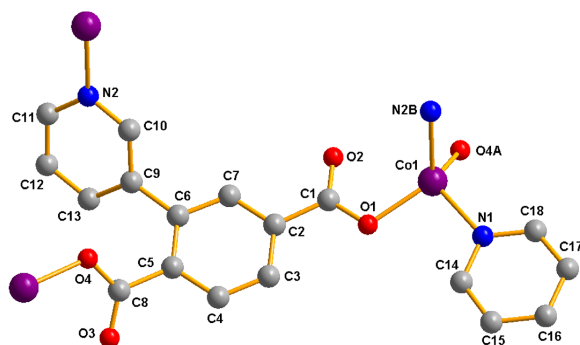
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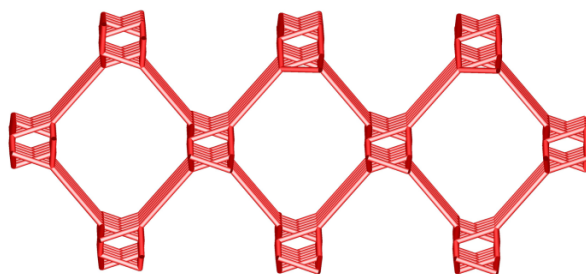
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3. **Fig. S3** The ball-and-stick drawing of the asymmetric unit in **2**, the hydrogen atoms and solvent molecules are omitted. Symmetry codes: A:  $-1/2+x, 1/2-y, -1/2+z$ ; B:  $-x, y, 1/2-z$ .
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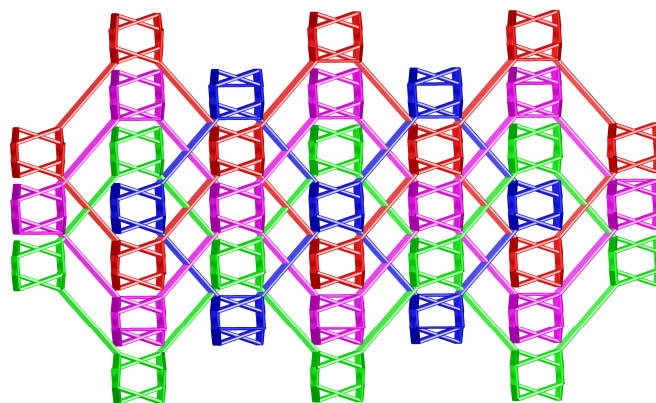


**Fig. S1** The ball-and-stick drawing of the asymmetric unit in **1**, the hydrogen atoms and solvent molecules are omitted. Symmetry codes: A:  $x, -y, -1/2+z$ ; B:  $-x, -y, 1-z$ .

a)

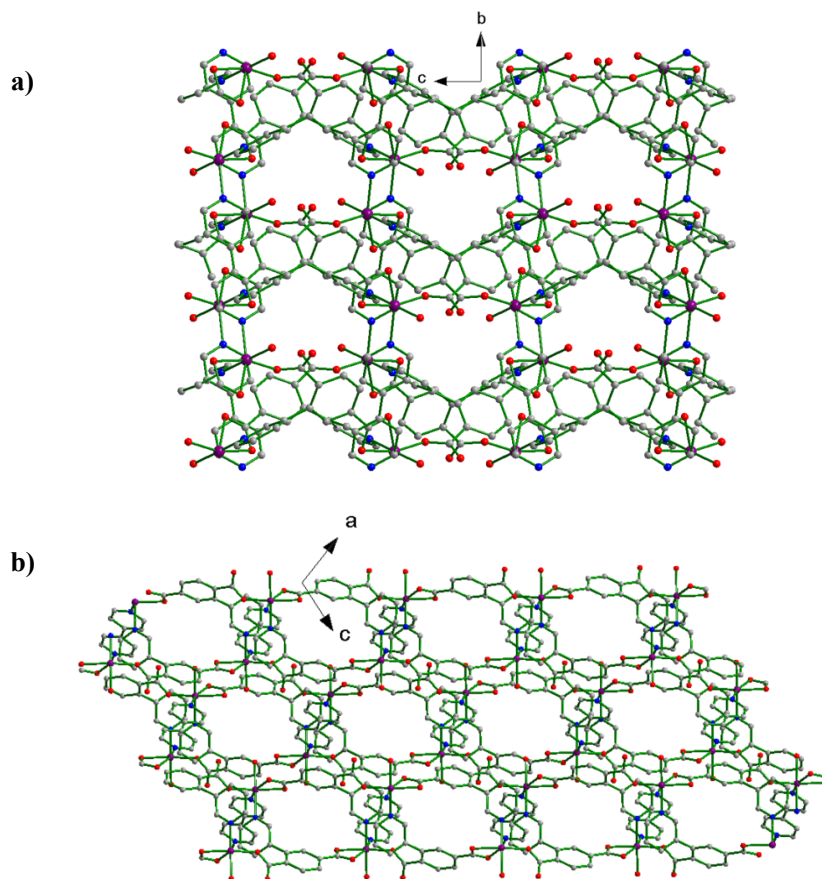


b)

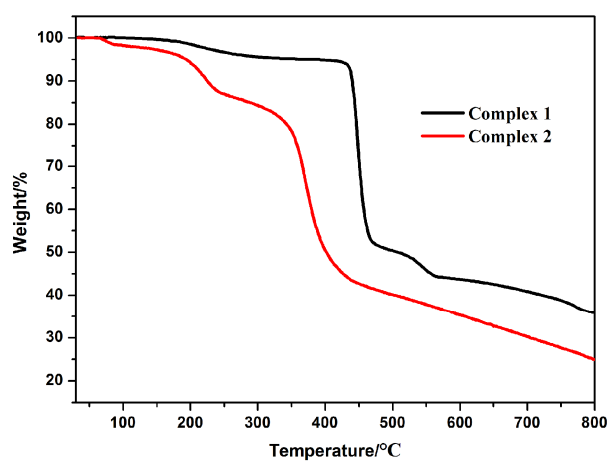


**Fig. S2** Schematic representation of the single 3D net a), and the 4-fold interpenetrated net b) of **1** (each  $\text{Co}^{2+}$  acts as a four-connecting node and each  $\text{dcp}^{2-}$  as a three-connecting node).

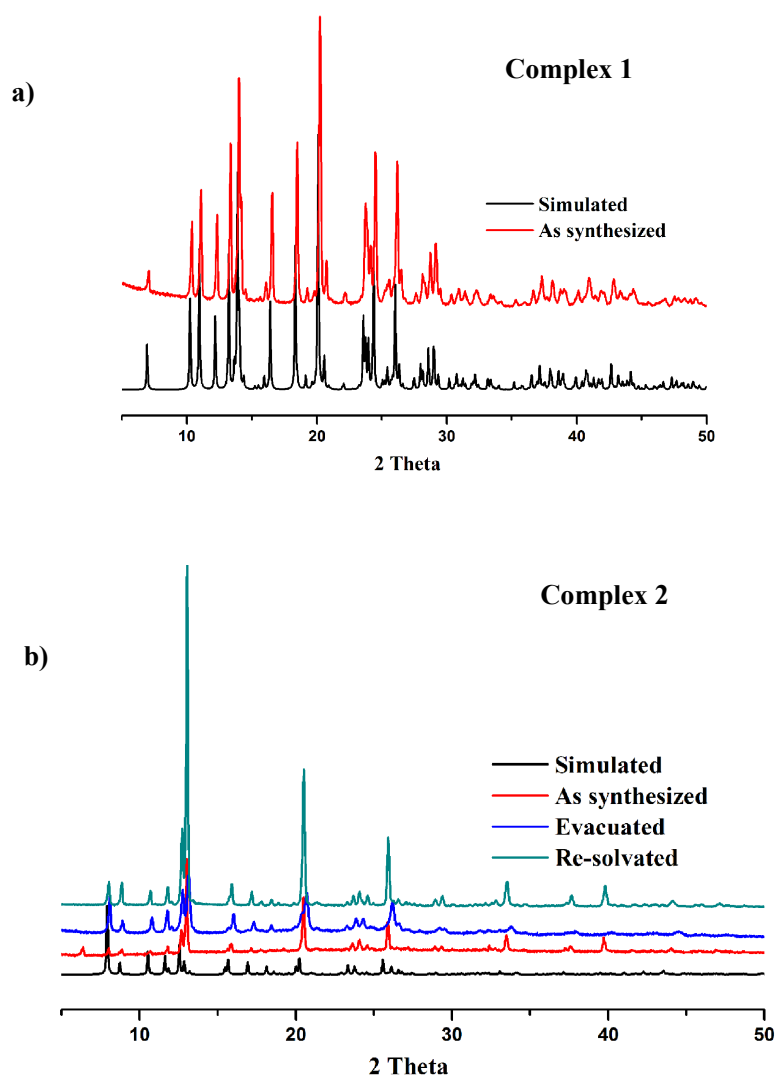




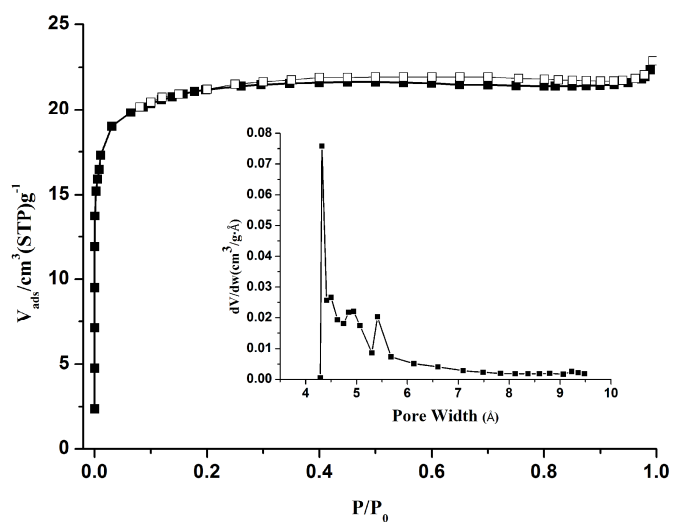
**Fig. S5** View of the 2D stacked layers of **2**: a) along the crystallographic (100)-axis; b) along the crystallographic (010)-axis.



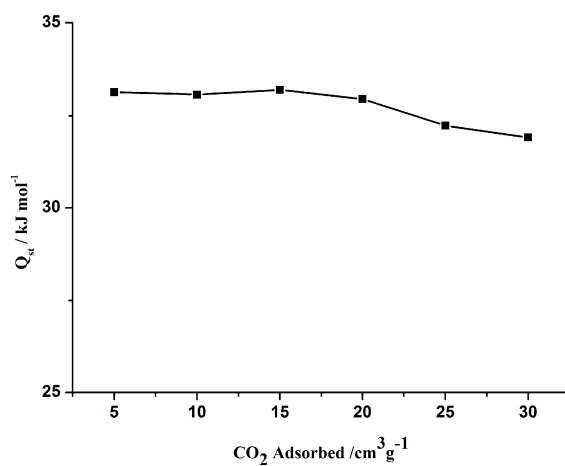
**Fig. S6.** TGA curves for **1** and **2** measured under nitrogen.



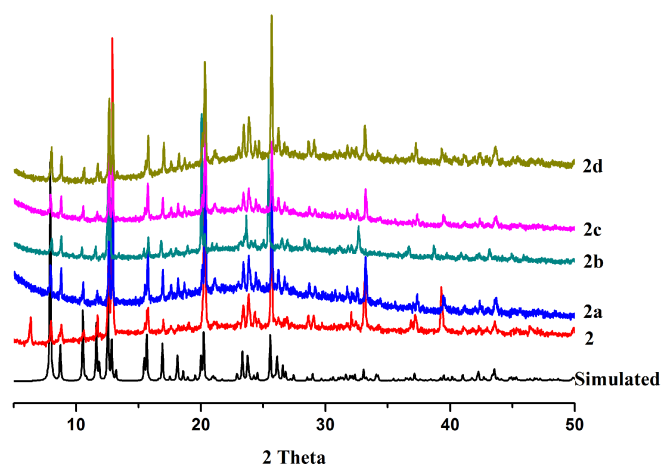
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**Fig. S8** Differential pore volume as a function of pore width calculated from the adsorption isotherm of Ar at 87 K using the Horvath-Kawazoe model, median pore width of 4.95  $\text{\AA}$ .



**Fig. S9** Isothermic heat of adsorption for  $\text{CO}_2$  at different  $\text{CO}_2$  loadings in **2**.



**Fig. S10** PXRD patterns for complexes **2**, **2a**, **2b**, **2c** and **2d**.

**Table S1.** Crystal data and structure refinements for **1**, **2**, **2a**, **2b**, **2c** and **2d**.

Complex No.	<b>1</b>	<b>2</b>	<b>2a</b>	<b>2b</b>
Empirical formula	C <sub>18</sub> H <sub>13</sub> N <sub>2</sub> CoO <sub>5</sub>	C <sub>18</sub> H <sub>17</sub> N <sub>2</sub> CoO <sub>7</sub>	C <sub>18</sub> H <sub>17</sub> N <sub>2</sub> CoO <sub>7</sub>	C <sub>18</sub> H <sub>17</sub> N <sub>2</sub> CoO <sub>7</sub>
Formula mass	396.22	432.23	432.23	432.23
Temperature [K]	296(2)	296(2)	296(2)	296(2)
Crystal system	monoclinic	monoclinic	monoclinic	monoclinic
Space group	<i>P2/c</i>	<i>C2/c</i>	<i>C2/c</i>	<i>C2/c</i>
<i>a</i> [Å]	13.1622(15)	17.795(2)	17.777(3)	17.877(4)
<i>b</i> [Å]	7.2427(8)	14.8776(19)	14.926(3)	14.730(3)
<i>c</i> [Å]	17.7408(19)	16.052(2)	16.131(3)	16.583(3)
$\beta$ [°]	103.584(2)	109.140(2)	109.324(3)	109.764(4)
<i>V</i> [Å <sup>3</sup> ]	1643.9(3)	4014.8(8)	4039.1(13)	4109.5(14)
<i>Z</i>	4	8	8	8
<i>D</i> <sub>calcd.</sub> [g·cm <sup>-3</sup> ]	1.593	1.417	1.408	1.384
$\mu$ [mm <sup>-1</sup> ]	1.077	0.895	0.890	0.874
GOF on <i>F</i> <sup>2</sup>	1.044	1.088	1.053	1.054
reflns collected/ unique	8007/2928	10042/3578	11741/4603	10135/3660
<i>R</i> <sub>int</sub>	0.0297	0.0499	0.0907	0.0756
Final <i>R</i> <sup>[a]</sup>	<i>R</i> <sub>1</sub> = 0.0353	<i>R</i> <sub>1</sub> = 0.0611	<i>R</i> <sub>1</sub> = 0.0775	<i>R</i> <sub>1</sub> = 0.0793
indices [ <i>I</i> > 2 $\sigma$ ( <i>I</i> )]	<i>wR</i> <sub>2</sub> = 0.0901	<i>wR</i> <sub>2</sub> = 0.1845	<i>wR</i> <sub>2</sub> = 0.1996	<i>wR</i> <sub>2</sub> = 0.2039

Complex No.	<b>2c</b>	<b>2d</b>
Empirical formula	C <sub>36</sub> H <sub>32</sub> CO <sub>2</sub> N <sub>4</sub> O <sub>13</sub>	C <sub>36</sub> H <sub>32</sub> CO <sub>2</sub> N <sub>4</sub> O <sub>13</sub>
Formula mass	846.47	846.47
Temperature [K]	296(2)	296(2)
Crystal system	monoclinic	monoclinic
Space group	<i>C2/c</i>	<i>C2/c</i>
<i>a</i> [Å]	17.7715(12)	17.547(10)
<i>b</i> [Å]	14.9149(10)	14.908(9)
<i>c</i> [Å]	16.1199(11)	16.176(10)
$\beta$ [°]	109.3020	108.365(9)
<i>V</i> [Å <sup>3</sup> ]	4032.6(5)	4016(4)
<i>Z</i>	4	4
<i>D</i> <sub>calcd.</sub> [g·cm <sup>-3</sup> ]	1.384	1.390
$\mu$ [mm <sup>-1</sup> ]	0.888	0.892
GOF on <i>F</i> <sup>2</sup>	1.001	1.006
reflns collected/ unique	11146/3526	8601/3560
<i>R</i> <sub>int</sub>	0.0296	0.0751
Final <i>R</i> <sup>[a]</sup>	<i>R</i> <sub>1</sub> = 0.0656	<i>R</i> <sub>1</sub> = 0.0826
indices [ <i>I</i> >2 $\sigma$ ( <i>I</i> )]	<i>wR</i> <sub>2</sub> = 0.1906	<i>wR</i> <sub>2</sub> = 0.2110

<sup>a</sup>  $R_1 = \sum ||F_o| - |F_c|| / \sum |F_o|$ ,  $wR_2 = [\sum w(F_o^2 - F_c^2)^2 / \sum w(F_o^2)^2]^{1/2}$