# Description of Pentacoordinated Phosphorus under an External Electric Field: which basis sets and semi-empirical methods are needed?

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### (Electronic Supplementary Information)





**Figure S1.** Variation of the energy of optimised structures with respect to the intensity of the electric field (F). Blue and red curves correspond to the intermediate and the transition state, respectively. The green straight line refers to the dependence of the energy barrier on the field.  $\Delta E$  (in kcal·mol<sup>-1</sup>) stands for the energy at a given field with respect to the energy at zero-field. These results have been obtained by means of the *m*PW1PW91 functional and the 6-31+G(d) basis set.



**Fig. S2** Representation of the dependence of both apical bond distances (in Å) on the electric field (F) for models **1** and **2**, where  $d_1$  corresponds to the weakest apical bond and  $d_2$  the strongest one, for different semi-empirical methods (AM1: solid line with dots, PM3: dashed line with crosses, RM1: dashed line with triangles, AM1/Arantes: dashed line with squares, MNDO/d: dashed line with empty circles, AM1\*: solid line with crosses, AM1/d-PhoT: solid line with triangles, PM6: solid line with squares). DFT results (dashed line with filled circles) are obtained by means of the *m*PW1PW91 functional and the 6-31+G(d) basis set.

**Table S1.** Calculation of the apical electric field (F) generated by the NAGK enzyme at the crystallographic position of the Aluminum atom using different QM/MM partitions. The different QM regions have included all the protein residues within a sphere of radius  $\mathbf{r}$  and both the substrates and magnesium ion. The QM wave function has been computed by means of the AM1 semiempirical method and the corresponding Mulliken charges have been used to evaluate the contribution from this region to the total electric field.

r/Å	F/a.u.
0.0	0.0019
3.0	0.0021
4.0	0.0017
5.0	0.0018
6.0	0.0017
7.0	0.0017
8.0	0.0018

**Table S2.** Optimized apical bond distances (in angstroms) of the transition states of model reaction **1** for different electric fields (in a.u.).<sup>a</sup>

F	<b>d</b> <sub>1</sub>	<b>d</b> <sub>2</sub>
0.000	2.162	1.671
0.002	2.204	1.673
0.004	2.254	1.677
0.006	2.283	1.683
0.008	2.303	1.689
0.010	2.317	1.696

<sup>a</sup> The transition states have been computed at the *m*PW1PW91/6-31+G(d) level.

Table S3. Optimized cartesian coordinates for the intermediate and transition state of model reaction 1 at zero-field<sup>a</sup>.

	INTE	RMEDIAT	Έ		TRANS	SITION STA	ТЕ
	mPW1P	PW91/6-31+0	G(d)		mPW1P	W91/6-31+0	G(d)
0	-0.054651	1.449460	-0.668968	Р	0.000000	0.000000	0.000000
Р	0.113236	-0.009269	0.087789	0	0.000000	0.000000	1.670835
0	-1.796905	-0.006123	0.058374	0	0.533584	0.000000	-2.095186
0	1.781398	0.023601	-0.210514	0	-1.468885	-0.000193	-0.337903
0	0.146363	-0.166005	1.601431	0	0.896908	1.354253	-0.117268
0	-0.054576	-1.283192	-0.950435	0	0.897463	-1.353812	-0.117265
Н	-1.017216	1.580228	-0.659694	Н	1.043415	-1.369180	-1.091643
Н	-1.016798	-1.415841	-0.965713	Н	1.042838	1.369836	-1.091554
Н	2.160450	-0.073874	0.670961	Н	-0.335327	-0.000172	-2.513719
Н	-1.998015	-0.093404	0.998510	Н	-0.935792	0.000585	1.905414
		AM1				AM1	
Р	0.000000	0.000000	0.000000	Р	0.000000	0.000000	0.000000
0	0.000000	0.000000	1.670835	0	1.633900	0.000000	0.000000
0	0.533584	0.000000	-2.095186	0	-2.064000	0.404900	0.000000
0	-1.468885	-0.000193	-0.337903	0	-0.308800	-1.437100	0.138800
0	0.896908	1.354253	-0.117268	0	-0.362700	0.838800	-1.242600
0	0.897463	-1.353812	-0.117265	0	-0.121500	0.861600	1.368100
Н	1.043415	-1.369180	-1.091643	Н	-1.004100	1.134300	1.593400
Н	1.042838	1.369836	-1.091554	Н	-1.597000	0.894900	-0.994100
Н	-0.335327	-0.000172	-2.513719	Н	-2.501100	-0.404200	-0.222700
Н	-0.935792	0.000585	1.905414	Н	1.978200	-0.813300	0.349500
		RM1				RM1	
Р	0.000000	0.000000	0.000000	Р	0.000000	0.000000	0.000000
0	0.000000	0.000000	1.670835	0	1.618000	0.000000	0.000000
0	0.533584	0.000000	-2.095186	0	-2.050300	1.158600	0.000000
0	-1.468885	-0.000193	-0.337903	0	-0.377800	-1.442800	-0.000800
0	0.896908	1.354253	-0.117268	0	-0.262900	0.817000	-1.314900
0	0.897463	-1.353812	-0.117265	0	-0.265000	0.817700	1.312700
Н	1.043415	-1.369180	-1.091643	Н	-1.173200	1.261300	1.238100
Н	1.042838	1.369836	-1.091554	Н	-1.166600	1.261500	-1.247200
Н	-0.335327	-0.000172	-2.513719	Н	-2.817400	0.621100	0.008100
Н	-0.935792	0.000585	1.905414	Н	2.026700	-0.851700	-0.002600
		PM3				PM3	
Р	0.000000	0.000000	0.000000	Р	0.000000	0.000000	0.000000
0	1.746900	0.000000	0.000000	0	1.720300	0.000000	0.000000
0	-1.616100	0.825000	0.000000	0	-2.143100	1.702200	0.000000
0	-0.357600	-1.466100	0.013700	0	-0.430900	-1.422200	0.003100

O 0.022500 0.873200 -1.474500	O -0.273000 0.873600 -1.380600
O 0.039600 0.914600 1.448400	O -0.273000 0.874000 1.381000
Н -0.755100 1.437700 1.482600	Н -1.057200 1.442900 1.262400
Н -0.777900 1.387000 -1.516500	Н -1.056900 1.442900 -1.260300
Н -2.375200 0.270100 0.015200	Н -2.891600 1.136400 -0.000100
Н 2.069100 -0.886200 -0.024100	Н 2.064400 -0.877000 0.046100
PM6	PM6
<b>D</b> 0.000000 0.000000 0.000000	<b>B</b> 0.000000 0.000000 0.000000
P 0.000000 0.000000 0.000000	P 0.000000 0.000000 0.000000
0 1.719500 0.000000 0.000000	0 1.69/500 0.000000 0.000000
0 -1.77400 0.540000 0.0000000	0 -2.039000 0.873800 0.0000000
0 -0.284600 -1.475200 0.010400	0 -0.383900 -1.440600 0.049100
0 0.035300 0.913200 -1.418800	0 -0.223300 -0.891900 -1.340300
0 0.040400 0.934000 1.405100	0 -0.150000 0.894000 1.388800
H -0.851100 1.336100 1.600900	H -1.101000 1.304300 1.439500
H $-0.860500$ $1.300500$ $-1.624700$	H -1.301700 1.268200 -1.240400
H -2.376700 -0.195900 0.006200	H -2.682/00 0.225300 -0.092800
H 2.081100 -0.904400 -0.004300	H 2.074600 -0.887800 0.156700
MNDO/d	MNDO/d
B 0.000000 0.000000 0.000000	B 0.000000 0.000000 0.000000
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
$\bigcirc 1.703200 0.000000 0.000000 0.000000 0.0000000 0.000000$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
O = 1.752800 = 0.305300 = 0.0000000	0 -2.003500 2.210800 0.000000
0 -0.233100 -1.494200 -0.003000	0 -0.323300 -1.401200 -0.007000
0 0.140400 0.801300 -1.403000 0 0.140600 0.862400 1.461000	0 -0.221900 -0.834400 -1.380400
0 0.149000 0.805400 1.401900	0 -0.245500 -0.815500 -1.595900
$\Pi -0.423900  1.553200  1.740300$	H = -0.804300 = 1.383300 = 1.304100
H = -0.423800 = 1.538300 = 1.741700	H = -0.723600 = 1.044200 = -1.470200
H = -2.444300 = -0.047600 = -0.012400	H -2.997000 2.200300 -0.026300
H 2.236100 -0.811900 -0.052300	H 2.18/800 -0./61900 0.240400
AM1*	AM1*
P 0.000000 0.000000 0.000000	P 0.000000 0.000000 0.000000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O = 1.679100 = 0.000000 = 0.000000
$O_{-1}657800 0.602400 0.000000$	O = 1.978500 = 0.792800 = 0.000000
O = 0.305700 = 1.479800 = 0.017200	O = 0.457800 = 1.429800 = 0.027700
O = 0.166800 = 0.860300 = 1.433500	O = 0.176400 + 1.018200 + 1.213500
O = 0.175700 = 0.898400 = 1.408800	O = 0.040700 = 0.724500 = 1.500800
H -0.631100 1.325600 1.726100	H -0.928600 0.989100 1.791300
H $-0.639100$ 1 288900 $-1.751300$	H $-1.335000$ $1.308700$ $-1.044800$
H = -2.312300 = 0.095800 = 0.000600	H -2 666400 0 192800 -0 255500
Н 2.052700 -0.899800 -0.022400	H 2.034400 -0.722500 0.535500
AM1/Arantes	AM1/Arantes
P 0.000000 0.000000 0.000000	P 0.000000 0.000000 0.000000
O 1.694800 0.000000 0.000000	O 1.666900 0.000000 0.000000
O -1.747600 0.280400 0.000000	O -2.072800 0.472700 0.000000
O -0.165700 -1.532600 -0.060100	O -0.296000 -1.444200 0.380000
O -0.001300 0.891500 -1.412900	O -0.203100 0.388400 -1.583800
O -0.011800 0.780700 1.475600	O -0.304000 1.183100 1.055100
Н -0.915200 1.025700 1.755600	Н -1.386700 1.228700 0.887600
Н -0.899400 1.183700 -1.663900	Н -1.134100 0.635300 -1.775100
Н -2.231900 -0.562500 -0.044300	Н -2.552000 -0.261900 0.411100
Н 2.022500 -0.915800 -0.070300	Н 2.011000 -0.905200 0.120100
AM1/d-PhoT	AM1/d-PhoT
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
$O_{-1}$ 815400 0.471000 0.000000	$O_{-2} 013700 0.000000 0.0000000 0.00000000000000$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
0 -0.273400 -1.403200 0.011200	
0 -0.011000 -0.846000 -1.412100	$( ) _0 _0 _0 /0 0 0 885400 1.257000$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0 & -0.120700 & 0.885400 & -1.357200 \\ 0 & -0.128400 & 0.848200 & 1.370700 \end{array}$
O -0.011900 0.846900 -1.413100 O -0.005400 0.880700 1.392300	O -0.120700 0.885400 -1.357200 O -0.128400 0.848300 1.379700 H 1.082800 1.120700 1.520200
O -0.011900 0.846900 -1.413100 O -0.005400 0.880700 1.392300 H -0.909700 1.236800 1.597600 H -0.919700 1.188000 1.622100	O -0.120700 0.885400 -1.357200 O -0.128400 0.848300 1.379700 H -1.082800 1.139700 1.520300 H -1.073600 1.182600 1.495200

H 2.005600 -0.929800 -0.010400 H 1.993100 -0.930000 -0.011100	H -2.385300 -0.315300 0.016600 H 2.005600 -0.929800 -0.010400	H -2.600200 -0.198300 -0.013800 H 1.993100 -0.930000 -0.011100
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<sup>a</sup> The geometry of both stationary points has been computed at different levels of theory.

Table S3. Optimized cartesian coordinates for intermediates and of model reaction 2 at zero-field<sup>a</sup>.

INTERMEDIATE	TRANSITION STATE
<i>m</i> PW1PW91/6-31+G(d)	<i>m</i> PW1PW91/6-31+G(d)
C -2.431920 -0.216802 -0.321296	C -2.619439 -0.243911 -0.270171
O -1.486277 0.086044 0.515474	O -1.679094 0.198177 0.478700
P 0.385769 0.067772 -0.022258	P 0.557212 0.130821 -0.086160
O 2.056021 0.455460 -0.186355	O 2.207528 0.429538 -0.091842
C 2.979191 -0.598576 -0.134501	C 3.070156 -0.685244 -0.054621
Н 3.028570 -1.037709 0.872078	Н 3.020773 -1.187903 0.919457
O -3.624715 -0.261143 -0.043580	O -3.799024 -0.426636 0.046487
O 0.056021 1.608862 -0.486044	O 0.214384 1.685490 -0.415053
O 0.243342 -1.103021 -0.947700	O 0.299428 -0.929714 -1.094875
O 0.590297 -0.131680 1.593771	O 0.469450 -0.190446 1.491468
Н 2.717728 -1.387067 -0.850319	Н 2.814674 -1.403090 -0.841500
Н -2.074791 -0.447596 -1.338818	Н -2.298970 -0.471671 -1.308599
Н -0.298103 -0.273901 1.957297	H -0.502138 -0.244281 1.654267
H 0.913500 1.975183 -0.751156	Н 1.068596 2.117979 -0.564907
Н 3.965414 -0.189399 -0.384968	Н 4.087534 -0.313867 -0.211514
PM6	PM6
P 0.0000 0.0000 0.0000	P 0.0000 0.0000 0.0000
O 1.7296 0.0000 0.0000	O 1.7052 0.0000 0.0000
O -1.7367 0.7521 0.0000	O -1.9095 0.6450 0.0000
O -0.4172 -1.4282 -0.0605	O -0.4073 -1.4340 0.0009
O 0.0329 0.8463 1.4501	O 0.0277 0.8505 -1.4411
O 0.1376 0.9085 -1.4123	O -0.0692 0.9994 1.3200
C 2.3301 -0.9090 0.9205	C 2.2791 -0.7403 1.0810
C -2.6992 0.2258 -0.7330	C -2.9247 -0.1155 -0.3025
O -3.8388 0.6784 -0.6667	O -4.0846 0.2660 -0.1341
Н -2.4352 -0.6159 -1.3828	Н -2.6995 -1.1072 -0.7175
Н 1.0760 1.0970 -1.6677	Н -0.9864 1.4326 1.4350
Н -0.8357 1.2958 1.6677	H 0.0832 0.2856 -2.2387
H 1.9260 -1.9231 0.7887	H 2.1214 -0.2087 2.0288
H $2.1/36 - 0.5565 1.9483$	H 3.3482 -0.7735 0.8420
H 3.3960 -0.8879 0.0097	Н 1.8/11 -1./002 1.1281
MNDO/d	MNDO/d
P 0.0000 0.0000 0.0000	P 0.0000 0.0000 0.0000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 1.7094 0.0000 0.0000
0 -1.8851 0.5946 0.0000	0 -2.3/16 0.8/32 0.0000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C = 2.6758 = 0.6735 = 0.7245
C = 2.7524 - 0.0192 = 0.7504 C = -3.0180 = 0.3419 = 0.5937	C = -3.6296 = 0.8556 = 0.2027
0 -40330 10039 -0.3937	$\begin{array}{c} -3.0270 & 0.0330 & -0.2027 \\ 0 & -4.4095 & 1.7227 & 0.2556 \end{array}$
H -3 0513 -0 4825 -1 3475	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Н 0.4483 1.6800 -1.5665	Н -0.9234 1.2406 1.7576
Н -0.6714 1.3046 1.8501	Н -0.3828 1.7623 -1.4758
Н 2.6308 -1.7323 0.7974	Н 3.6789 -0.4240 0.2928
Н 2.8321 -0.2349 1.7825	Н 2.5593 -1.7865 0.6814
Н 3.7483 -0.4309 0.2449	Н 2.6926 -0.3757 1.8043
AM1/Arantes	AM1/Arantes

Р	0.0000 0.0000 0.0000	Р	0.0000 $0.0000$ $0.0000$
0	1.7244 0.0000 0.0000	0	1.7060 0.0000 0.0000
0	-1.7648 0.4995 0.0000	0	-1.8760 0.4044 0.0000
0	-0.2786 -1.4980 -0.0224	0	-0.2653 -1.4991 0.1118
0	0.0130 0.7907 1.4591	0	-0.0065 0.6013 -1.5406
0	0.0972 0.7787 -1.4660	0	-0.0461 1.0231 1.2895
С	2.4962 -0.8650 0.8090	С	2.4595 -0.6666 0.9937
С	-2.7158 -0.0509 -0.7531	С	-2.9060 -0.4278 -0.0223
0	-3.8917 0.3428 -0.6480	0	-4.0605 -0.0027 0.1919
Н	-2.4074 -0.8283 -1.4262	Н	-2.6980 -1.4609 -0.2302
Н	1.0161 0.9241 -1.7649	Н	-0.9249 1.4339 1.4379
Н	-0.8642 1.1175 1.7449	Н	-0.1278 -0.0945 -2.2095
Н	2.1718 -1.8894 0.6676	Н	2.3577 -0.1433 1.9376
Н	2.3934 -0.5719 1.8473	Н	3.4857 -0.6290 0.6465
Н	3.5202 -0.7382 0.4764	Н	2.1257 -1.6935 1.0873
	A B #1.4		4 3 4 1 4
	AM1*		AM1^
	AM1*		AM1^
Р	AM1* 0.0000 0.0000 0.0000	Р	AMI ^ 0.0000 0.0000 0.0000
Р О	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000	P O	AM1^ 0.0000 0.0000 0.0000 1.6818 0.0000 0.0000
P O O	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000	P O O	AM1^ 0.0000 0.0000 0.0000 1.6818 0.0000 0.0000 -2.2557 1.0264 0.0000
Р О О О	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698	Р О О О	AM1^ 0.0000 0.0000 0.0000 1.6818 0.0000 0.0000 -2.2557 1.0264 0.0000 -0.5713 -1.3662 0.1489
P O O O O	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615	P O O O O	AM1* 0.0000 0.0000 0.0000 1.6818 0.0000 0.0000 -2.2557 1.0264 0.0000 -0.5713 -1.3662 0.1489 -0.1137 1.0302 1.2701
P O O O O O	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031	P O O O O	AM1*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085
P O O O O C	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303	P O O O O C	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956
P 0 0 0 0 0 0 0 0 0 0 0 0	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468	P 0 0 0 0 0 0 0 0 0 0 0	AM1* 0.0000 0.0000 0.0000 1.6818 0.0000 0.0000 -2.2557 1.0264 0.0000 -0.5713 -1.3662 0.1489 -0.1137 1.0302 1.2701 -0.0623 0.7952 -1.4085 2.4856 -1.0127 0.5956 -3.1281 1.5492 -0.7818
P 0 0 0 0 0 0 0 0 0 0 0 0 0	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411	P 0 0 0 0 0 0 0 0 0 0 0	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662
P 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395	P 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865
P O O O O C C O H H	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395 1.0637 1.0528 -1.7072	P O O O O C C O H H	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865   -1.0182 1.3138 1.5168
Р О О О О С С О Н Н Н	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395 1.0637 1.0528 -1.7072 -0.7099 1.1259 1.8385	Р О О О О С С О Н Н Н	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865   -1.0182 1.3138 1.5168   -0.9437 1.1620 -1.6923
Р О О О О С С О Н Н Н Н Н	AM1* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395 1.0637 1.0528 -1.7072 -0.7099 1.1259 1.8385 2.3198 -1.7213 1.0593	Р О О О О С С О Н Н Н Н	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865   -1.0182 1.3138 1.5168   -0.9437 1.1620 -1.6923   2.7971 -0.6694 1.6158
Р О О О О С С О Н Н Н Н Н Н	AMI* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395 1.0637 1.0528 -1.7072 -0.7099 1.1259 1.8385 2.3198 -1.7213 1.0593 2.5516 -0.1199 1.9230	Р О О О О С С О Н Н Н Н Н Н	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865   -1.0182 1.3138 1.5168   -0.9437 1.1620 -1.6923   2.7971 -0.6694 1.6158   1.9720 -2.0054 0.6603
Р О О О О С С О Н Н Н Н Н Н Н	AMI* 0.0000 0.0000 0.0000 1.7426 0.0000 0.0000 -1.6461 0.7546 0.0000 -0.3843 -1.4459 -0.0698 0.1199 0.7922 1.4615 0.1574 0.8972 -1.4031 2.5820 -0.6395 0.9303 -2.5865 0.7999 -0.9468 -3.6462 1.3664 -0.6411 -2.3807 0.3495 -1.9395 1.0637 1.0528 -1.7072 -0.7099 1.1259 1.8385 2.3198 -1.7213 1.0593 2.5516 -0.1199 1.9230 3.6192 -0.5608 0.5058	Р О О О О С С О Н Н Н Н Н Н Н	AMI*   0.0000 0.0000 0.0000   1.6818 0.0000 0.0000   -2.2557 1.0264 0.0000   -0.5713 -1.3662 0.1489   -0.1137 1.0302 1.2701   -0.0623 0.7952 -1.4085   2.4856 -1.0127 0.5956   -3.1281 1.5492 -0.7818   -2.8173 1.8519 -1.9662   -4.1551 1.7326 -0.3865   -1.0182 1.3138 1.5168   -0.9437 1.1620 -1.6923   2.7971 -0.6694 1.6158   1.9720 -2.0054 0.6603   3.3894 -1.0945 -0.0636

<sup>a</sup> The geometry of both stationary points has been computed at different levels of theory.