

**The details of the BG method:**

The dimensions of simulation boxes:

- Series 1,2 and 3:  $6.5 \times 6.5 \times 6.5$  nm
- Series 1 x 1.125:  $7.0 \times 7.0 \times 7.0$  nm
- Series 1 x 1.25:  $7.5 \times 7.5 \times 7.5$  nm
- Series 1x 1.50:  $8.5 \times 8.5 \times 8.5$  nm

Periodic boundary conditions applied in all three dimensions.

Density of nodes:  $200 \times 200 \times 200$

Atom radius:

$$r_C = 0.17 \text{ nm}$$

$$r_O = 0.15 \text{ nm}$$

Average effective micropore diameters from BG method were calculated using:

$$d_{mi,av} = \frac{\sum_{d \leq 2 \text{ nm}} d \cdot P(d)}{\sum_{d \leq 2 \text{ nm}} P(d)}$$

**Table ESI 1.** The average micropore diameters of all VPCs.

$d_{mi,av}$ [nm]												
<b>S1_000</b>	0.712	<b>S2_000</b>	0.712	<b>S3_000</b>	0.712	<b>S1_000x1.125</b>	0.875	<b>S1_000x1.25</b>	1.058	<b>S1_000x1.5</b>	1.461	
<b>S1_060</b>	0.707	<b>S2_060</b>	0.707	<b>S3_060</b>	0.706	<b>S1_060x1.125</b>	0.864	<b>S1_060x1.25</b>	1.047	<b>S1_060x1.5</b>	1.445	
<b>S1_120</b>	0.692	<b>S2_120</b>	0.703	<b>S3_120</b>	0.697	<b>S1_120x1.125</b>	0.848	<b>S1_120x1.25</b>	1.029	<b>S1_120x1.5</b>	1.417	
<b>S1_180</b>	0.690	<b>S2_180</b>	0.692	<b>S3_180</b>	0.691	<b>S1_180x1.125</b>	0.841	<b>S1_180x1.25</b>	1.019	<b>S1_180x1.5</b>	1.405	
<b>S1_240</b>	0.685	<b>S2_240</b>	0.681	<b>S3_240</b>	0.685	<b>S1_240x1.125</b>	0.830	<b>S1_240x1.25</b>	1.005	<b>S1_240x1.5</b>	1.390	

**Table ESI 2.** Characteristics of simulation boxes.  $N_{H2O}$  is the number of water molecules in the simulation box having starting diameters  $L_{box,x}$ ,  $L_{box,y}$ , and  $L_{box,z}$ , respectively. Method 1 – uses Gromax Genbox procedure, method 2 – simulation in water sphere.

Structure	method 1				method 2			
	$N_{H2O}$	$L_{box,x}$	$L_{box,y}$	$L_{box,z}$	$N_{H2O}$	$L_{box,x}$	$L_{box,y}$	$L_{box,z}$
		[nm]	[nm]			[nm]		
<i>carbonyl groups introduced randomly</i>								
<b>S1_000</b>	3567	5.395	5.057	5.057	6252	6.500	6.500	6.500
<b>S1_060</b>	3701	5.418	5.114	5.133	6252	6.500	6.500	6.500
<b>S1_120</b>	3672	5.418	5.114	5.133	6252	6.500	6.500	6.500
<b>S1_180</b>	3659	5.429	5.115	5.133	6252	6.500	6.500	6.500
<b>S1_240</b>	3715	5.429	5.170	5.144	6252	6.500	6.500	6.500
<i>carbonyl groups introduced randomly</i>								
<b>S2_000</b>	3567	5.395	5.057	5.057	6252	6.500	6.500	6.500
<b>S2_060</b>	3551	5.406	5.057	5.057	6252	6.500	6.500	6.500
<b>S2_120</b>	3551	5.406	5.058	5.057	6252	6.500	6.500	6.500
<b>S2_180</b>	3534	5.406	5.058	5.068	6252	6.500	6.500	6.500
<b>S2_240</b>	3548	5.406	5.071	5.127	6252	6.500	6.500	6.500
<i>carbonyl groups on the edges of structures</i>								
<b>S3_000</b>	3567	5.395	5.057	5.057	6252	6.500	6.500	6.500
<b>S3_060</b>	3593	5.42	5.071	5.057	6252	6.500	6.500	6.500
<b>S3_120</b>	3713	5.42	5.18	5.078	6252	6.500	6.500	6.500
<b>S3_180</b>	3684	5.42	5.18	5.078	6252	6.500	6.500	6.500
<b>S3_240</b>	3671	5.42	5.18	5.109	6252	6.500	6.500	6.500
<i>carbonyl groups introduced randomly – structures with shifted fragments</i>								
<b>S1_000x1.125</b>	4847	5.886	5.433	5.494	n.a.			
<b>S1_060x1.125</b>	5111	5.909	5.528	5.570				
<b>S1_120x1.125</b>	5082	5.909	5.528	5.570				
<b>S1_180x1.125</b>	5055	5.920	5.529	5.570				
<b>S1_240x1.125</b>	5100	5.920	5.546	5.582				
<i>carbonyl groups introduced randomly – structures with shifted fragments</i>								
<b>S1_000x1.25</b>	6200	6.377	5.824	5.932	n.a.			
<b>S1_060x1.25</b>	6549	6.399	5.944	6.008				
<b>S1_120x1.25</b>	6526	6.399	5.944	6.008				
<b>S1_180x1.25</b>	6515	6.410	5.945	6.008				
<b>S1_240x1.25</b>	6530	6.410	5.958	6.019				
<i>carbonyl groups introduced randomly – structures with shifted fragments</i>								
<b>S1_000x1.5</b>	9918	7.359	6.653	6.806	n.a.			
<b>S1_060x1.5</b>	10367	7.381	6.773	6.882				
<b>S1_120x1.5</b>	10349	7.381	6.773	6.882				
<b>S1_180x1.5</b>	10335	7.392	6.787	6.893				
<b>S1_240x1.5</b>	10369	7.392	6.787	6.893				

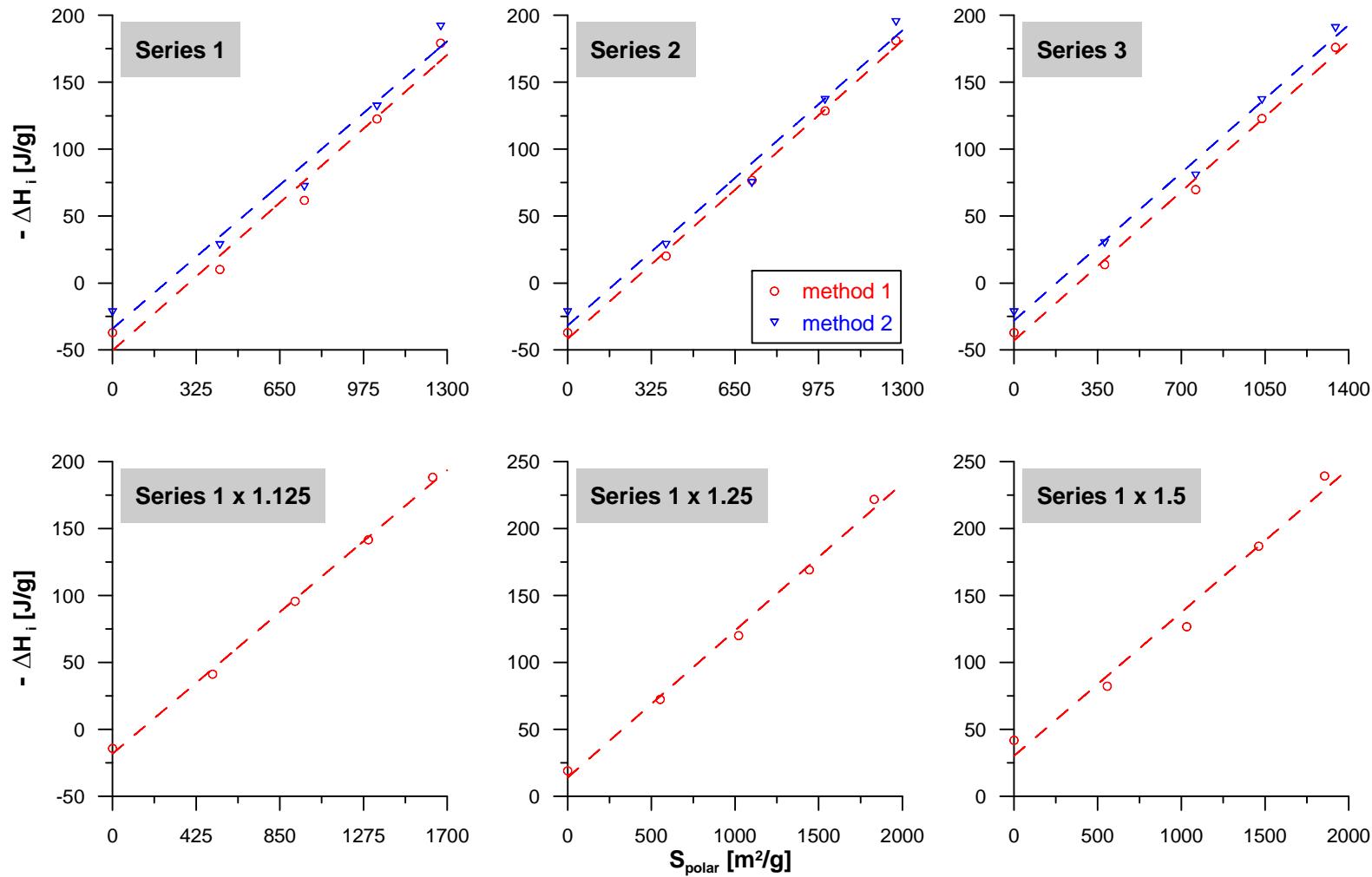
**Table ESI 3.** The dependence between enthalpy of immersion and the percentage contents of oxygen.  $-\Delta H_i = A_1 \cdot \{O\} + A_0$

Series	<i>method 1</i>		<i>method 2</i>	
	$A_1$ [J/g/%]	$A_0$ [J/g]	$A_1$ [J/g/%]	$A_0$ [J/g]
<b>1</b>	14.70	- 45.71	14.30	- 29.59
<b>2</b>	14.74	- 39.44	14.61	- 29.69
<b>3</b>	14.46	- 42.13	14.35	- 27.26
<b>1 x 1.125</b>	13.67	-14.78	-	-
<b>1 x 1.25</b>	13.57	19.09	-	-
<b>1 x 1.50</b>	13.45	31.89	-	-

**Table ESI 4.** The dependence between enthalpy of immersion and the polar surface area values.

$$-\Delta H_i = B_1 \cdot S_{polar} + B_0$$

Series	<i>method 1</i>		<i>method 2</i>	
	$B_1$ [J/m <sup>2</sup> ]	$B_0$ [J/g]	$B_1$ [J/m <sup>2</sup> ]	$B_0$ [J/g]
<b>1</b>	0.1699	- 50.38	0.1652	- 34.10
<b>2</b>	0.1714	- 41.76	0.1696	- 31.78
<b>3</b>	0.1592	- 43.05	0.1578	- 28.09
<b>1 x 1.125</b>	0.1245	- 18.20	-	-
<b>1 x 1.25</b>	0.1098	13.96	-	-
<b>1 x 1.5</b>	0.1072	30.13	-	-



**Figure ESI 1.** The relation between enthalpy of immersion and polar surface area calculated from Vega ZZ.

**Table ESI 5.** The dependence between enthalpy of immersion and the ratio polar/nonpolar surface area.

$$-\Delta H_i = C_1 \cdot \frac{S_{polar}}{S_{nonpolar}} + C_0$$

<i>Series</i>	<i>method 1</i>		<i>method 2</i>	
	$C_1$ [J/g]	$C_0$ [J/g]	$C_1$ [J/g]	$C_0$ [J/g]
<b>1</b>	318.9	-32.89	310.9	-17.36
<b>2</b>	311.8	-22.22	312.9	-13.71
<b>3</b>	288.9	-24.27	287.3	-9.74
<b>1 x 1.125</b>	303.0	-1.13	-	-
<b>1 x 1.25</b>	305.7	28.98	-	-
<b>1 x 1.5</b>	309.4	43.62	-	-