

## Supporting Information

**Title:** Reliable Contact Fabrication on Nanostructured Bi<sub>2</sub>Te<sub>3</sub>-Based Alloys for High Performance Flat-Panel Solar Thermoelectric Generators

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Based on the ratio of total STEG resistance at operating temperature to initial STEG resistance at room temperature, we assume that the ratio ( $\chi$ ) increases because of the increase of contact resistance, which can be calculated from,

$$\chi = \frac{R_{TE-x} + 2R_{cx}}{R_{TE-i} + 2R_{ci}} \quad (S1)$$

where  $R_{TE-i}$  and  $R_{ci}$  are the initial resistance of thermoelectric leg and the initial contact resistance respectively,  $R_{TE-x}$  and  $R_{cx}$  are the resistance of thermoelectric leg and contact resistance under operating temperature. We make the following assumptions in the modeling:

- (1) Based on the Table 1, the initial contact resistance is around 1% of the resistance of thermoelectric material.  $R_{ci} / R_{TE-i} = 1\%$ .
- (2) The resistance of Bi<sub>2</sub>Te<sub>3</sub>-based thermoelectric alloys at operating temperature ( $\Delta T=200$  °C) would increase 1.5 times compared with the initial resistance at room temperature.  $R_{TE-x} / R_{TE-i} = 1.5$ .
- (3) The average resistivity of nanostructured Bi<sub>2</sub>Te<sub>3</sub>-based alloys is  $1.1 \times 10^{-3} \Omega\text{-cm}$ . The dimension of thermoelectric leg is  $1.35 \text{ mm} \times 1.35 \text{ mm} \times 1.65 \text{ mm}$ .  $R_{TE-i} = 0.01 \Omega$ .

We further assume that the ratio of contact resistance to the resistance of thermoelectric leg is

$R_{cx} / R_{TE-i} = \alpha$ , so that Eq. (S1) can be rewritten as,

$$\chi = \frac{1.5+2\alpha}{1+0.02} \quad (S2)$$

Based on the data of  $\chi$ , the  $\alpha$  and  $R_{cx}$  can be calculated as a function of time. The specific contact resistance ( $\Omega\text{-cm}^2$ ) can be estimated by  $R_{cx}$  timing contact area (1.35mm x 1.35mm). For example, if  $\alpha = 5\%$ , the specific contact resistance of  $9 \times 10^{-6} \Omega\text{-cm}^2$  can be obtained.