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CRYSCAL version : Sept. 2013 [T. Roisnel (CDIFX / ISCR UMR6226 - Rennes)]

PS143: Crystal structure report

X-ray crystallographic study

($C_{16} H_{16} N_4$); $M = 264.33$. APEXII, Bruker-AXS diffractometer, $Mo - K_{\alpha}$ radiation ($\lambda = 0.71073 \text{ \AA}$), $T = 150(2)K$; triclinic $P\bar{1}$ (I.T.#2), $a = 5.8977(6)$, $b = 7.4177(7)$, $c = 30.865(3) \text{ \AA}$, $\alpha; = 91.949(4)$, $\beta; = 92.578(5)$, $\gamma; = 94.343(4)^\circ$, $V = 1344.1(2) \text{ \AA}^3$, $Z = 4$, $d = 1.306 \text{ g.cm}^{-3}$, $\mu = 0.081 \text{ mm}^{-1}$. The structure was solved by direct methods using the SIR97 program [1], and then refined with full-matrix least-square methods based on F^2 (SHELXL-97) [2] with the aid of the WINGX [3] program. All non-hydrogen atoms were refined with anisotropic atomic displacement parameters. H atoms were finally included in their calculated positions. A final refinement on F^2 with 6089 unique intensities and 365 parameters converged at $\omega R(F^2) = 0.139$ ($RF = 0.0589$) for 4195 observed reflections with ($I > 2\sigma$).

1. A. Altomare, M. C. Burla, M. Camalli, G. Cascarano, C. Giacovazzo, A. Guagliardi, A. G. G. Moliterni, G. Polidori, R. Spagna, J. Appl. Cryst. (1999) 32, 115-119
2. Sheldrick G.M., Acta Cryst. A64 (2008), 112-122
3. L. J. Farrugia, J. Appl. Cryst., 2012, 45, 849-854

Structural data

Empirical formula	$C_{16}H_{16}N_4$
Formula weight	264.33
Temperature	150(2) K
Wavelength	0.71073 Å
Crystal system, space group	triclinic, $P\bar{1}$
Unit cell dimensions	a = 5.8977(6) Å, α = 91.949(4) ° b = 7.4177(7) Å, β = 92.578(5) ° c = 30.865(3) Å, γ = 94.343(4) °
Volume	1344.1(2) Å ³
Z, Calculated density	4, 1.306 ($g.cm^{-1}$)
Absorption coefficient	0.081 mm^{-1}
F(000)	560
Crystal size	0.6 x 0.47 x 0.07 mm
Crystal color	colourless
Theta range for data collection	3.01 to 27.44 °
h_min, h_max	-7, 7
k_min, k_max	-9, 9
l_min, l_max	-39, 39
Reflections collected / unique	16133 / 6089 [R_{int}] = 0.0623]
Reflections [$I > 2\sigma$]	4195
Completeness to theta_max	0.988
Absorption correction type	multi-scan
Max. and min. transmission	0.994, 0.726
Refinement method	Full-matrix least-squares on F^2
Data / restraints / parameters	6089 / 0 / 365
^b Goodness-of-fit	1.029
Final R indices [$I > 2\sigma$]	^c R_1 = 0.0589, ^d wR_2 = 0.139
R indices (all data)	^c R_1 = 0.0884, ^d wR_2 = 0.1541
Largest diff. peak and hole	0.323 and -0.276 $e.\text{Å}^{-3}$

$${}^a R_{int} = \frac{\sum |F_o^2 - \langle F_o^2 \rangle|}{\sum F_o^2}$$

$${}^b S = \left\{ \frac{\sum [w(F_o^2 - F_c^2)^2]}{n-p} \right\}^{1/2}$$

$${}^c R_1 = \frac{\sum |F_o| - |F_c|}{\sum |F_o|}$$

$${}^d wR_2 = \left\{ \frac{\sum [w(F_o^2 - F_c^2)^2]}{\sum [w(F_o^2)^2]} \right\}^{1/2}$$

$$w = 1. / [\sigma(F_o^2) + (aP)^2 + bP] \text{ with } P = [2F_c^2 + \text{Max}(F_o^2, 0)] / 3$$

Atomic coordinates, site occupancy (%) and equivalent isotropic displacement parameters ($\text{Å}^2 \times 10^3$). U(eq) is defined as one third of the trace of the orthogonalized U_{ij} tensor.

Atom	x	y	z	occ.	U(eq)
C1	0.7757(3)	0.1927(3)	-0.02461(6)	1	0.0303(4)
H1	0.6284	0.1374	-0.0202	1	0.036
C2	0.8367(3)	0.2398(3)	-0.06580(6)	1	0.0355(5)
H2	0.7296	0.2185	-0.0897	1	0.043
C3	1.0530(4)	0.3179(3)	-0.07237(6)	1	0.0366(5)
H3	1.0938	0.3501	-0.1007	1	0.044
C4	1.2090(3)	0.3486(3)	-0.03764(7)	1	0.0349(5)
H4	1.3576	0.4012	-0.0422	1	0.042
C5	1.1501(3)	0.3034(3)	0.00388(6)	1	0.0307(4)
H5	1.2575	0.3242	0.0277	1	0.037
C6	0.9324(3)	0.2273(2)	0.01006(6)	1	0.0252(4)
N7	0.8673(2)	0.1835(2)	0.05287(5)	1	0.0251(3)
N8	0.6434(3)	0.1563(2)	0.06108(5)	1	0.0328(4)
N9	0.6320(3)	0.1171(2)	0.10239(5)	1	0.0323(4)
C10	0.8484(3)	0.1203(2)	0.12086(6)	1	0.0242(4)
C11	0.9989(3)	0.1633(2)	0.08935(6)	1	0.0261(4)
H11	1.1603	0.1761	0.0924	1	0.031
C12	0.8916(3)	0.0793(2)	0.16650(6)	1	0.0237(4)
C13	0.7232(3)	-0.0065(2)	0.19056(6)	1	0.0261(4)
H13	0.5775	-0.0393	0.177	1	0.031
C14	0.7626(3)	-0.0452(3)	0.23379(6)	1	0.0277(4)
H14	0.6433	-0.1033	0.2491	1	0.033
C15	0.9750(3)	-0.0001(2)	0.25534(6)	1	0.0246(4)
C16	1.1447(3)	0.0871(3)	0.23113(6)	1	0.0295(4)
H16	1.2905	0.1209	0.2446	1	0.035
C17	1.1023(3)	0.1246(3)	0.18795(6)	1	0.0300(4)
H17	1.2207	0.183	0.1725	1	0.036
N18	1.0180(3)	-0.0441(2)	0.29802(5)	1	0.0340(4)
C19	0.8352(3)	-0.1106(3)	0.32414(6)	1	0.0367(5)
H19A	0.7401	-0.0118	0.3311	1	0.055
H19B	0.8988	-0.1571	0.351	1	0.055
H19C	0.7425	-0.2079	0.308	1	0.055
C20	1.2230(3)	0.0254(3)	0.32158(7)	1	0.0395(5)
H20A	1.3537	0.0104	0.3036	1	0.059
H20B	1.2416	-0.0408	0.3483	1	0.059
H20C	1.2139	0.1542	0.3289	1	0.059
C21	0.3699(3)	0.2054(2)	0.49817(6)	1	0.0273(4)
H21	0.2537	0.1918	0.4757	1	0.033
C22	0.3250(3)	0.1566(3)	0.54023(6)	1	0.0325(5)
H22	0.1767	0.1089	0.5466	1	0.039
C23	0.4950(3)	0.1769(3)	0.57295(6)	1	0.0341(5)
H23	0.4634	0.1419	0.6015	1	0.041
C24	0.7104(3)	0.2480(3)	0.56394(6)	1	0.0330(5)
H24	0.8264	0.2622	0.5864	1	0.04
C25	0.7585(3)	0.2990(3)	0.52215(6)	1	0.0280(4)
H25	0.9059	0.3497	0.516	1	0.034
C26	0.5887(3)	0.2748(2)	0.48971(5)	1	0.0228(4)
N27	0.6414(2)	0.3195(2)	0.44619(5)	1	0.0238(3)
N28	0.8610(3)	0.3281(2)	0.43454(5)	1	0.0325(4)
N29	0.8601(3)	0.3686(2)	0.39333(5)	1	0.0318(4)
C30	0.6413(3)	0.3849(2)	0.37823(6)	1	0.0229(4)
C31	0.4996(3)	0.3520(2)	0.41204(5)	1	0.0234(4)
H31	0.3384	0.3521	0.4115	1	0.028
C32	0.5837(3)	0.4313(2)	0.33338(5)	1	0.0228(4)
C33	0.7279(3)	0.3943(2)	0.30004(6)	1	0.0246(4)
H33	0.8661	0.341	0.3067	1	0.03
C34	0.6731(3)	0.4339(2)	0.25736(6)	1	0.0252(4)

H34	0.7747	0.4073	0.2354	1	0.03
C35	0.4706(3)	0.5124(2)	0.24598(5)	1	0.0226(4)
C36	0.3259(3)	0.5510(2)	0.27979(6)	1	0.0255(4)
H36	0.1883	0.6058	0.2734	1	0.031
C37	0.3826(3)	0.5099(2)	0.32220(6)	1	0.0254(4)
H37	0.2816	0.5359	0.3443	1	0.03
N38	0.4147(3)	0.5512(2)	0.20346(5)	1	0.0306(4)
C39	0.5673(3)	0.5147(3)	0.16927(6)	1	0.0351(5)
H39A	0.71	0.5907	0.1743	1	0.053
H39B	0.496	0.5418	0.1412	1	0.053
H39C	0.5993	0.387	0.1692	1	0.053
C40	0.1986(3)	0.6154(3)	0.19099(6)	1	0.0359(5)
H40A	0.0761	0.5294	0.1997	1	0.054
H40B	0.1876	0.627	0.1594	1	0.054
H40C	0.1846	0.7337	0.2053	1	0.054

Anisotropic displacement parameters (\AA^2)

The anisotropic displacement factor exponent takes the form: $-2\pi[h^2a^{*2}U_{11} + \dots + 2hka^*b^*U_{12}]$

Atom	U11	U22	U33	U23	U13	U12
C1	0.0284(10)	0.0308(11)	0.0313(10)	0.0016(8)	-0.0001(8)	0.0010(8)
C2	0.0380(12)	0.0389(12)	0.0296(10)	0.0009(9)	-0.0029(9)	0.0051(9)
C3	0.0421(13)	0.0394(12)	0.0303(11)	0.0072(9)	0.0069(9)	0.0099(9)
C4	0.0293(11)	0.0362(12)	0.0409(11)	0.0106(9)	0.0070(9)	0.0066(9)
C5	0.0252(10)	0.0317(11)	0.0357(11)	0.0046(8)	-0.0016(8)	0.0044(8)
C6	0.0263(10)	0.0223(10)	0.0277(9)	0.0023(7)	0.0017(7)	0.0065(7)
N7	0.0202(8)	0.0265(8)	0.0284(8)	0.0019(6)	-0.0009(6)	0.0021(6)
N8	0.0225(9)	0.0441(10)	0.0315(9)	0.0020(7)	0.0010(7)	0.0019(7)
N9	0.0251(9)	0.0441(10)	0.0273(8)	0.0025(7)	-0.0018(7)	0.0014(7)
C10	0.0219(9)	0.0223(10)	0.0279(9)	-0.0025(7)	0.0002(7)	0.0014(7)
C11	0.0215(9)	0.0259(10)	0.0307(10)	0.0025(8)	-0.0014(7)	0.0017(7)
C12	0.0226(9)	0.0216(9)	0.0272(9)	-0.0006(7)	0.0005(7)	0.0037(7)
C13	0.0196(9)	0.0286(10)	0.0290(9)	-0.0023(8)	-0.0020(7)	-0.0028(7)
C14	0.0218(10)	0.0294(10)	0.0313(10)	0.0036(8)	0.0025(7)	-0.0035(7)
C15	0.0245(9)	0.0199(9)	0.0299(9)	0.0029(7)	0.0002(7)	0.0050(7)
C16	0.0201(10)	0.0308(11)	0.0363(11)	0.0041(8)	-0.0055(8)	-0.0034(8)
C17	0.0214(10)	0.0321(11)	0.0361(10)	0.0084(8)	0.0012(8)	-0.0041(8)
N18	0.0234(9)	0.0468(11)	0.0313(9)	0.0094(8)	-0.0016(7)	-0.0012(7)
C19	0.0305(11)	0.0455(13)	0.0333(11)	0.0114(9)	-0.0024(8)	-0.0050(9)
C20	0.0332(12)	0.0464(13)	0.0369(11)	0.0124(10)	-0.0099(9)	-0.0079(9)
C21	0.0249(10)	0.0302(10)	0.0275(9)	0.0049(8)	-0.0003(7)	0.0050(8)
C22	0.0292(11)	0.0354(12)	0.0351(11)	0.0106(9)	0.0085(8)	0.0093(8)
C23	0.0405(12)	0.0414(12)	0.0229(9)	0.0066(8)	0.0055(8)	0.0141(9)
C24	0.0363(12)	0.0398(12)	0.0239(10)	0.0008(8)	-0.0026(8)	0.0113(9)
C25	0.0259(10)	0.0296(10)	0.0286(10)	0.0023(8)	-0.0012(8)	0.0036(8)
C26	0.0252(9)	0.0226(9)	0.0214(9)	0.0029(7)	0.0004(7)	0.0060(7)
N27	0.0192(8)	0.0275(8)	0.0247(8)	0.0034(6)	-0.0011(6)	0.0012(6)
N28	0.0209(8)	0.0496(11)	0.0271(8)	0.0071(7)	-0.0001(6)	0.0016(7)
N29	0.0234(9)	0.0453(11)	0.0266(8)	0.0065(7)	-0.0009(6)	0.0012(7)
C30	0.0199(9)	0.0220(9)	0.0267(9)	0.0025(7)	-0.0006(7)	0.0009(7)
C31	0.0205(9)	0.0245(10)	0.0251(9)	0.0034(7)	-0.0017(7)	0.0022(7)
C32	0.0210(9)	0.0224(9)	0.0245(9)	0.0038(7)	-0.0014(7)	-0.0014(7)
C33	0.0191(9)	0.0247(10)	0.0303(10)	0.0038(8)	0.0003(7)	0.0024(7)
C34	0.0234(10)	0.0275(10)	0.0246(9)	0.0009(7)	0.0041(7)	-0.0001(7)
C35	0.0205(9)	0.0229(9)	0.0237(9)	0.0020(7)	-0.0014(7)	-0.0028(7)
C36	0.0199(9)	0.0286(10)	0.0279(9)	0.0020(8)	-0.0009(7)	0.0028(7)
C37	0.0234(9)	0.0270(10)	0.0261(9)	0.0004(7)	0.0041(7)	0.0020(7)
N38	0.0215(8)	0.0483(11)	0.0219(8)	0.0038(7)	-0.0010(6)	0.0023(7)
C39	0.0304(11)	0.0511(14)	0.0246(10)	0.0042(9)	0.0025(8)	0.0058(9)
C40	0.0325(11)	0.0461(13)	0.0308(10)	0.0090(9)	0.0015(8)	0.0105(9)

Bond length [Å]

C1	-	C2	=	1.385(3)
C1	-	C6	=	1.386(3)
C1	-	H1	=	0.95
C2	-	C3	=	1.387(3)
C2	-	H2	=	0.95
C3	-	C4	=	1.382(3)
C3	-	H3	=	0.95
C4	-	C5	=	1.388(3)
C4	-	H4	=	0.95
C5	-	C6	=	1.386(3)
C5	-	H5	=	0.95
C6	-	N7	=	1.433(2)
N7	-	N8	=	1.357(2)
N7	-	C11	=	1.357(2)
N8	-	N9	=	1.321(2)
N9	-	C10	=	1.373(2)
C10	-	C11	=	1.375(2)
C10	-	C12	=	1.466(2)
C11	-	H11	=	0.95
C12	-	C17	=	1.394(2)
C12	-	C13	=	1.395(2)
C13	-	C14	=	1.387(2)
C13	-	H13	=	0.95
C14	-	C15	=	1.404(2)
C14	-	H14	=	0.95
C15	-	N18	=	1.385(2)
C15	-	C16	=	1.407(2)
C16	-	C17	=	1.386(2)
C16	-	H16	=	0.95
C17	-	H17	=	0.95
N18	-	C20	=	1.435(2)
N18	-	C19	=	1.442(2)
C19	-	H19A	=	0.98
C19	-	H19B	=	0.98
C19	-	H19C	=	0.98
C20	-	H20A	=	0.98
C20	-	H20B	=	0.98
C20	-	H20C	=	0.98
C21	-	C22	=	1.391(2)
C21	-	C26	=	1.392(3)
C21	-	H21	=	0.95
C22	-	C23	=	1.387(3)
C22	-	H22	=	0.95
C23	-	C24	=	1.382(3)
C23	-	H23	=	0.95
C24	-	C25	=	1.392(2)
C24	-	H24	=	0.95
C25	-	C26	=	1.381(2)
C25	-	H25	=	0.95
C26	-	N27	=	1.436(2)
N27	-	C31	=	1.355(2)
N27	-	N28	=	1.357(2)
N28	-	N29	=	1.317(2)
N29	-	C30	=	1.368(2)
C30	-	C31	=	1.383(2)
C30	-	C32	=	1.469(2)
C31	-	H31	=	0.95
C32	-	C37	=	1.396(2)
C32	-	C33	=	1.397(2)
C33	-	C34	=	1.389(2)

C33	-	H33	=	0.95
C34	-	C35	=	1.404(2)
C34	-	H34	=	0.95
C35	-	N38	=	1.384(2)
C35	-	C36	=	1.413(2)
C36	-	C37	=	1.386(2)
C36	-	H36	=	0.95
C37	-	H37	=	0.95
N38	-	C40	=	1.435(2)
N38	-	C39	=	1.449(2)
C39	-	H39A	=	0.98
C39	-	H39B	=	0.98
C39	-	H39C	=	0.98
C40	-	H40A	=	0.98
C40	-	H40B	=	0.98
C40	-	H40C	=	0.98

Angles [°]

C2	- C1	- C6	= 119.18(18)
C2	- C1	- H1	= 120.4
C6	- C1	- H1	= 120.4
C1	- C2	- C3	= 120.41(18)
C1	- C2	- H2	= 119.8
C3	- C2	- H2	= 119.8
C4	- C3	- C2	= 119.82(18)
C4	- C3	- H3	= 120.1
C2	- C3	- H3	= 120.1
C3	- C4	- C5	= 120.46(18)
C3	- C4	- H4	= 119.8
C5	- C4	- H4	= 119.8
C6	- C5	- C4	= 119.11(18)
C6	- C5	- H5	= 120.4
C4	- C5	- H5	= 120.4
C1	- C6	- C5	= 120.99(17)
C1	- C6	- N7	= 119.22(16)
C5	- C6	- N7	= 119.80(16)
N8	- N7	- C11	= 110.50(14)
N8	- N7	- C6	= 119.69(14)
C11	- N7	- C6	= 129.80(15)
N9	- N8	- N7	= 107.15(14)
N8	- N9	- C10	= 109.16(15)
N9	- C10	- C11	= 107.93(16)
N9	- C10	- C12	= 122.03(16)
C11	- C10	- C12	= 130.03(16)
N7	- C11	- C10	= 105.26(16)
N7	- C11	- H11	= 127.4
C10	- C11	- H11	= 127.4
C17	- C12	- C13	= 116.82(16)
C17	- C12	- C10	= 121.70(16)
C13	- C12	- C10	= 121.49(16)
C14	- C13	- C12	= 121.81(16)
C14	- C13	- H13	= 119.1
C12	- C13	- H13	= 119.1
C13	- C14	- C15	= 121.36(16)
C13	- C14	- H14	= 119.3
C15	- C14	- H14	= 119.3
N18	- C15	- C14	= 121.65(16)
N18	- C15	- C16	= 121.48(16)
C14	- C15	- C16	= 116.84(16)
C17	- C16	- C15	= 120.99(17)
C17	- C16	- H16	= 119.5
C15	- C16	- H16	= 119.5
C16	- C17	- C12	= 122.18(17)
C16	- C17	- H17	= 118.9
C12	- C17	- H17	= 118.9
C15	- N18	- C20	= 120.93(15)
C15	- N18	- C19	= 120.66(15)
C20	- N18	- C19	= 115.62(16)
N18	- C19	- H19A	= 109.5
N18	- C19	- H19B	= 109.5
H19A	- C19	- H19B	= 109.5
N18	- C19	- H19C	= 109.5
H19A	- C19	- H19C	= 109.5
H19B	- C19	- H19C	= 109.5
N18	- C20	- H20A	= 109.5
N18	- C20	- H20B	= 109.5
H20A	- C20	- H20B	= 109.5
N18	- C20	- H20C	= 109.5

H20A	- C20	- H20C	= 109.5
H20B	- C20	- H20C	= 109.5
C22	- C21	- C26	= 118.55(17)
C22	- C21	- H21	= 120.7
C26	- C21	- H21	= 120.7
C23	- C22	- C21	= 120.57(18)
C23	- C22	- H22	= 119.7
C21	- C22	- H22	= 119.7
C24	- C23	- C22	= 119.90(17)
C24	- C23	- H23	= 120.1
C22	- C23	- H23	= 120.1
C23	- C24	- C25	= 120.47(18)
C23	- C24	- H24	= 119.8
C25	- C24	- H24	= 119.8
C26	- C25	- C24	= 119.01(17)
C26	- C25	- H25	= 120.5
C24	- C25	- H25	= 120.5
C25	- C26	- C21	= 121.48(16)
C25	- C26	- N27	= 118.96(16)
C21	- C26	- N27	= 119.54(15)
C31	- N27	- N28	= 110.88(14)
C31	- N27	- C26	= 129.49(15)
N28	- N27	- C26	= 119.60(14)
N29	- N28	- N27	= 106.94(14)
N28	- N29	- C30	= 109.50(15)
N29	- C30	- C31	= 107.90(15)
N29	- C30	- C32	= 122.71(16)
C31	- C30	- C32	= 129.39(16)
N27	- C31	- C30	= 104.76(15)
N27	- C31	- H31	= 127.6
C30	- C31	- H31	= 127.6
C37	- C32	- C33	= 117.50(16)
C37	- C32	- C30	= 121.77(16)
C33	- C32	- C30	= 120.72(16)
C34	- C33	- C32	= 121.30(16)
C34	- C33	- H33	= 119.3
C32	- C33	- H33	= 119.3
C33	- C34	- C35	= 121.35(16)
C33	- C34	- H34	= 119.3
C35	- C34	- H34	= 119.3
N38	- C35	- C34	= 121.54(16)
N38	- C35	- C36	= 121.19(16)
C34	- C35	- C36	= 117.27(15)
C37	- C36	- C35	= 120.65(17)
C37	- C36	- H36	= 119.7
C35	- C36	- H36	= 119.7
C36	- C37	- C32	= 121.93(16)
C36	- C37	- H37	= 119
C32	- C37	- H37	= 119
C35	- N38	- C40	= 121.77(15)
C35	- N38	- C39	= 120.56(16)
C40	- N38	- C39	= 117.51(15)
N38	- C39	- H39A	= 109.5
N38	- C39	- H39B	= 109.5
H39A	- C39	- H39B	= 109.5
N38	- C39	- H39C	= 109.5
H39A	- C39	- H39C	= 109.5
H39B	- C39	- H39C	= 109.5
N38	- C40	- H40A	= 109.5
N38	- C40	- H40B	= 109.5
H40A	- C40	- H40B	= 109.5
N38	- C40	- H40C	= 109.5
H40A	- C40	- H40C	= 109.5

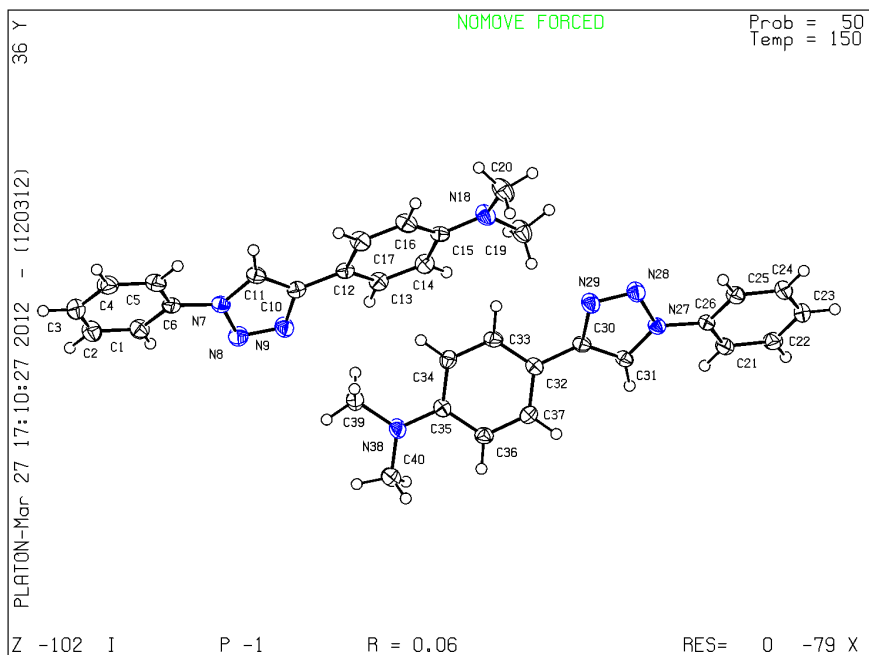
$$H40B - C40 - H40C = 109.5$$

Torsion angles [°]

C6	- C1	- C2	- C3	= 1.0(3)
C1	- C2	- C3	- C4	= 0.1(3)
C2	- C3	- C4	- C5	= -0.5(3)
C3	- C4	- C5	- C6	= -0.2(3)
C2	- C1	- C6	- C5	= -1.8(3)
C2	- C1	- C6	- N7	= 178.19(16)
C4	- C5	- C6	- C1	= 1.3(3)
C4	- C5	- C6	- N7	= -178.62(16)
C1	- C6	- N7	- N8	= -17.8(3)
C5	- C6	- N7	- N8	= 162.15(17)
C1	- C6	- N7	- C11	= 162.39(18)
C5	- C6	- N7	- C11	= -17.6(3)
C11	- N7	- N8	- N9	= -0.6(2)
C6	- N7	- N8	- N9	= 179.54(15)
N7	- N8	- N9	- C10	= 0.4(2)
N8	- N9	- C10	- C11	= 0.0(2)
N8	- N9	- C10	- C12	= -179.02(16)
N8	- N7	- C11	- C10	= 0.6(2)
C6	- N7	- C11	- C10	= -179.59(17)
N9	- C10	- C11	- N7	= -0.4(2)
C12	- C10	- C11	- N7	= 178.54(17)
N9	- C10	- C12	- C17	= -164.02(18)
C11	- C10	- C12	- C17	= 17.2(3)
N9	- C10	- C12	- C13	= 15.8(3)
C11	- C10	- C12	- C13	= -162.98(19)
C17	- C12	- C13	- C14	= 0.0(3)
C10	- C12	- C13	- C14	= -179.79(17)
C12	- C13	- C14	- C15	= -0.2(3)
C13	- C14	- C15	- N18	= -177.65(17)
C13	- C14	- C15	- C16	= 0.5(3)
N18	- C15	- C16	- C17	= 177.61(17)
C14	- C15	- C16	- C17	= -0.6(3)
C15	- C16	- C17	- C12	= 0.3(3)
C13	- C12	- C17	- C16	= -0.1(3)
C10	- C12	- C17	- C16	= 179.74(17)
C14	- C15	- N18	- C20	= -170.75(19)
C16	- C15	- N18	- C20	= 11.2(3)
C14	- C15	- N18	- C19	= -10.5(3)
C16	- C15	- N18	- C19	= 171.42(18)
C26	- C21	- C22	- C23	= 0.1(3)
C21	- C22	- C23	- C24	= 0.7(3)
C22	- C23	- C24	- C25	= -0.2(3)
C23	- C24	- C25	- C26	= -1.0(3)
C24	- C25	- C26	- C21	= 1.8(3)
C24	- C25	- C26	- N27	= -177.09(16)
C22	- C21	- C26	- C25	= -1.3(3)
C22	- C21	- C26	- N27	= 177.54(16)
C25	- C26	- N27	- C31	= -161.22(18)
C21	- C26	- N27	- C31	= 19.9(3)
C25	- C26	- N27	- N28	= 21.0(2)
C21	- C26	- N27	- N28	= -157.94(17)
C31	- N27	- N28	- N29	= 1.0(2)
C26	- N27	- N28	- N29	= 179.16(15)
N27	- N28	- N29	- C30	= -0.4(2)
N28	- N29	- C30	- C31	= -0.2(2)
N28	- N29	- C30	- C32	= 179.39(16)
N28	- N27	- C31	- C30	= -1.06(19)
C26	- N27	- C31	- C30	= -179.03(16)
N29	- C30	- C31	- N27	= 0.76(19)
C32	- C30	- C31	- N27	= -178.80(17)

N29	- C30	- C32	- C37	= -156.56(18)
C31	- C30	- C32	- C37	= 22.9(3)
N29	- C30	- C32	- C33	= 24.8(3)
C31	- C30	- C32	- C33	= -155.73(18)
C37	- C32	- C33	- C34	= -0.1(3)
C30	- C32	- C33	- C34	= 178.61(16)
C32	- C33	- C34	- C35	= -0.1(3)
C33	- C34	- C35	- N38	= -179.66(16)
C33	- C34	- C35	- C36	= 0.6(3)
N38	- C35	- C36	- C37	= 179.36(16)
C34	- C35	- C36	- C37	= -0.9(2)
C35	- C36	- C37	- C32	= 0.7(3)
C33	- C32	- C37	- C36	= -0.2(3)
C30	- C32	- C37	- C36	= -178.91(16)
C34	- C35	- N38	- C40	= 173.99(17)
C36	- C35	- N38	- C40	= -6.3(3)
C34	- C35	- N38	- C39	= -1.2(3)
C36	- C35	- N38	- C39	= 178.55(17)

Structure visualisation



This structural report has been created through CRYSCAL (Sept. 2013). Please report bugs and problems to cdifx@univ-rennes1.fr