## Supporting Information

# Molecular dynamics simulation of rupture mechanism in nanorod filled polymer 

 nanocompositesYangyang Gao ${ }^{1,2}$, Jun Liu ${ }^{1,2^{*}}$, Jianxiang Shen ${ }^{1}$, Liqun Zhang ${ }^{1,2^{*}}$
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Fig. S1 Stress versus strain curves using different strain rates.


Fig. S2 The maximum void size versus strain.

We examined further the structural properties of polymer nanocomposites by calculating their orientational order parameter. The order parameter is defined by $S=0.5\left(3 \cos ^{2} \theta-1\right)$, where $\theta$ is the angle between the bond vector and the tensile direction. Its lower bound is $\mathrm{S}=-0.5$ and corresponds to an ensemble of chains whose bonds vector are all perpendicular to the tensile direction. The upper bound $\mathrm{S}=1$ corresponds to a perfectly stretched sample along the tensile direction, while $\mathrm{S}=0$ for a random, isotropic arrangement. Fig. S3(a) showed the order parameter S as a function of the strain for all polymer bonds, the polymer bonds near the voids and other polymer bonds. At first, the bonds exhibit random distribution. With the increase of the strain, the polymers are stretched along the tensile direction and the value of S increases. Further separation of material leads to a higher orientation until the big voids appear. Accordingly, the order parameter $S$ reaches a maximum and then decreases. It is interesting to find that the peak of $S$ of the polymer bonds near the voids is roughly close to that of radius of gyration $\left\langle R_{g}\right\rangle$, while the peak of S of other polymer bonds is consistent with that of VDWL energy. When small voids grow and merge into big voids, the inner chains begin to contract, which leads to the decrease of S of other polymer bonds. And when the material completely ruptures, namely the polymer bundles begin to get separated, the chains near the voids begin to contract, leading to the decrease of S of the polymer bonds near the voids. The number of bonds near the void is less compared with the total number of bonds, so the bond orientation of S of all polymer bonds is similar to that of other polymer bonds.

The rupture behavior can be understood better by analyzing the various energy
contributions inside our system. The total kinetic energy comprises kinetic contributions of all individual beads, which is constant during the simulation because of the thermostating. The evolution of the energy (total potential energy, VDWL energy, bond energy and angle energy) during the rupture process was presented in Fig. S3(b) as a function of the strain. The bond and angle energies are roughly constant since bonds and angles cannot break in our model. The VDWL energy dominates the process.



Fig. S3(a) The order parameter $S$ for all polymer bonds, the polymer bonds near the voids and other polymer bonds. (b) The energy change (total potential energy, VDWL energy, bond energy and angle energy) as a function of strain.


Fig. S4 Distribution of all beads along the tensile direction ( $L$ is the length of box along the tensile direction) at strain $=\mathbf{0 . 5}$.



Fig. S5(a) Stress-strain curves obtained for different simulated temperatures ( $\varepsilon_{n p}=3.0$ ). (b) The order parameter $S$ as a function of the strain for different rod lengths.


Fig. S6 The snapshots at strain $=\mathbf{0 . 5 , 0 . 9}$ and 2.0 for three types of chain lengths.


Fig. S7 (a) The order parameter $S$ as a function of the strain for different chain lengths. (b) The snapshots for a bridging cluster of nanorods via one polymer layer. The red beads denote one polymer chain and other color beads denote nanorods.



Fig. S8 (a) The number of broken bonds and (b) the order parameter $S$ as a function of the strain for different cross-linking density $\mathbf{n}$.


Fig. S9 The number of broken bonds as a function of the strain for different interfacial chemical bonds $m$.

Table I. All simulated systems

| System | Chain |  | Interaction strength | Temperatur <br> e | Nanorod |  | Equilibration times $\tau$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Number | length |  |  | Number | length |  |
| 1 | 600 | 30 |  | 1.0 | 0 | 0 | 50000 |
| 2 | 600 | 30 | 1.0 | 1.0 | 800 | 6 | 50000 |
| 3 | 600 | 30 | 1.5 | 1.0 | 800 | 6 | 50000 |
| 4 | 600 | 30 | 2.0 | 1.0 | 800 | 6 | 50000 |
| 5 | 600 | 30 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 6 | 600 | 30 | 5.0 | 1.0 | 800 | 6 | 50000 |
| 7 | 600 | 30 | 8.0 | 1.0 | 800 | 6 | 50000 |
| 8 | 600 | 30 | 3.0 | 0.1 | 800 | 6 | 50000 |
| 9 | 600 | 30 | 3.0 | 0.2 | 800 | 6 | 50000 |
| 10 | 600 | 30 | 3.0 | 0.3 | 800 | 6 | 50000 |
| 11 | 600 | 30 | 3.0 | 0.4 | 800 | 6 | 50000 |
| 12 | 600 | 30 | 3.0 | 0.5 | 800 | 6 | 50000 |
| 13 | 600 | 30 | 3.0 | 0.6 | 800 | 6 | 50000 |
| 14 | 600 | 30 | 3.0 | 0.7 | 800 | 6 | 50000 |
| 15 | 600 | 30 | 3.0 | 0.8 | 800 | 6 | 50000 |
| 16 | 600 | 30 | 3.0 | 0.9 | 800 | 6 | 50000 |
| 17 | 600 | 30 | 3.0 | 1.0 | 2400 | 2 | 50000 |
| 18 | 600 | 30 | 3.0 | 1.0 | 1200 | 4 | 50000 |
| 19 | 600 | 30 | 3.0 | 1.0 | 600 | 8 | 50000 |


| 20 | 600 | 30 | 3.0 | 1.0 | 480 | 10 | 50000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 600 | 30 | 3.0 | 1.0 | 400 | 12 | 50000 |
| 22 | 600 | 30 | 3.0 | 1.0 | 343 | 14 | 50000 |
| 21 | 600 | 30 | 3.0 | 1.0 | 300 | 16 | 50000 |
| 22 | 1800 | 10 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 23 | 360 | 50 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 24 | 180 | 100 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 25 | 90 | 200 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 26 | 45 | 400 | 3.0 | 1.0 | 800 | 6 | 50000 |
| 27 | 600 | 30 | 3.0 | 1.0 | 200 | 6 | 50000 |
| 28 | 600 | 30 | 3.0 | 1.0 | 500 | 6 | 50000 |
| 28 | 600 | 30 | 3.0 | 1.0 | 1600 | 6 | 50000 |
| 29 | 600 | 30 | 3.0 | 1.0 | 2000 | 6 | 50000 |
| 30 | 600 | 30 | 3.0 | 1.0 | 2800 | 6 | 50000 |


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