

## **Supporting Information**

# **Unveiling the reaction mechanism of novel copper N-alkylated tetra-azacyclophanes with outstanding superoxide dismutase activity**

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## I. Experimental section

### 2.1 Synthesis of L1 and L2

All reagents were obtained from commercial sources and used as received. Solvents used for the chemical synthesis were of analytical grade and used without further purification.

**Synthesis of 6-(*N*-methyl)-3,6,9-triaza-1(2,6)-pyridinecyclodecaphane (L2).** The synthesis of the starting material 6-(*N*-methyl)-3,9-(*p*-tolylsulfonyl)-3,6,9-triaza-1(2,6)-pyridinecyclodecaphane was carried out following a procedure described previously in the literature.<sup>[1]</sup> 6-(*N*-methyl)-3,9-(*p*-tolylsulfonyl)-3,6,9-triaza-1(2,6)-pyridinecyclodecaphane (0.79 g, 1.49 mmol) and phenol (3.41 g, 35.72 mmol) were suspended in HBr-AcOH 33% (36 cm<sup>3</sup>). The mixture was stirred at 90 °C for further 24 h and cooled. The resulting suspension was filtered and washed several times with EtOH anhydrous to give the product L2 in a salt form (0.45 g, 65%). Characterization data of the compound are included in the supplementary materials (Figures S1-S4). <sup>1</sup>H NMR (300 MHz, D<sub>2</sub>O), δ (ppm): 7.99 (t, J=7.84 Hz, 1H), 7.51 (d, J=7.81 Hz, 2H), 4.63 (m, 4H), 3.32 (m, 4H), 2.66 (t, J=5.53 Hz, 4H), 2.45 (s, 3H). <sup>13</sup>C NMR (75.43 MHz, D<sub>2</sub>O) δ (ppm): 149.76, 140.15, 122.73, 52.99, 50.49, 46.19, 42.20. Anal. Calc. for C<sub>18</sub>H<sub>32</sub>N<sub>4</sub>·3HBr·0.3H<sub>2</sub>O·0.05(C<sub>4</sub>H<sub>8</sub>O<sub>2</sub>): C 31.0 %, H 5.1 %, N 11.8 %. Found: C 31.0 %, H 4.6%, N 11.7%. MS (ESI) m/z 221.2 [M + H]<sup>+</sup>.

The synthesis of **6-(*N*-methyl)-3,9-(*N*-isopropyl)-3,6,9-triaza-1(2,6)-pyridinecyclodecaphane hydrochloride (L1)** has been carried out as previously described in bibliography.<sup>[2]</sup> Characterization data of the compound are included in the supplementary materials (Figures S5-S8). <sup>1</sup>H NMR (300 MHz, D<sub>2</sub>O), δ (ppm): 8.01 (t, J=7.8 Hz, 1H), 7.53 (d, J=7.8 Hz, 2H), 4.83 (s, 2H), 4.59 (s, 2H), 3.96 (hept, J=6.7 Hz,

2H), 3.55 (s, 4H), 2.71 (s, 2H), 2.43 (s, 3H), 3.05-2.00 (m, 2H), 1.48 (s, 6H), 1.46 (s, 6H).  $^{13}\text{C}$  NMR (75.43 MHz,  $\text{D}_2\text{O}$ )  $\delta$  (ppm): 150.5, 140.6, 122.9, 60.5, 54.9, 53.2, 51.6, 40.3, 16.7. Anal. Calc. for  $\text{C}_{18}\text{H}_{32}\text{N}_4 \cdot 3.3\text{HCl} \cdot 4\text{H}_2\text{O} \cdot 0.4(\text{C}_4\text{H}_8\text{O}_2)$ : C 44.2 %, H 8.8 %, N 10.5 %. Found: C 44.4 %, H 8.5 %, N 10.6 %. MS (ESI)  $m/z$  305.1  $[\text{M} + \text{H}]^+$ .

## 2.2 *In vitro* McCord-Fridovich SOD activity assays

SOD-like activity of the Cu-based complexes was determined by measuring the amount of blue formazane that is produced by reduction of nitro blue tetrazolium (NBT) after reaction with  $\text{O}_2^-$  in the presence of the tested inhibitor.<sup>[3-7]</sup> A reproducible and constant flux of superoxide anions was generated using xanthine ( $1.5 \times 10^{-4}$  M) and xanthine oxidase (50 mM in TRIS pH=7.4). The rate of reduction of NBT ( $5.6 \times 10^{-5}$  M) to blue formazane was followed spectrophotometrically at 560 nm. Data in the absence of the complex were used as reference. The rate of NBT reduction was progressively inhibited after the addition of the complex solutions at increasing concentrations prepared in 50 mM Tris buffer, pH 7.4. Thus, the percentage of inhibition of the NBT reduction was used as a measure of the SOD activity of the tested compounds. The half maximum inhibitory concentration ( $\text{IC}_{50}$ ) was determined from a plot of percentage inhibition versus complex concentration. The  $\text{IC}_{50}$  data have been calculated from the mean values of three independent measurements. The catalytic constant was calculated from  $\text{IC}_{50}$  values using the equation  $k_{cat} = k_{NBT} [\text{NBT}] / \text{IC}_{50}$  where  $k_{NBT} = (5.9 \pm 0.5) \times 10^5 \text{ M}^{-1} \text{ s}^{-1}$ .<sup>[8-10]</sup>

## 2.3 Quantum mechanical calculations

The available crystal structure of  $[\text{Cu}(\text{C}_{18}\text{H}_{32}\text{N}_4)(\text{OH}_2)]^{2+}$  (Figure 1) in the Cambridge Crystal Database (CCD id. 1827336) was used as starting geometry for the ground state geometry optimization. As initial benchmarking, the GGA functional BP86,<sup>[11,12]</sup> the

Becke three-parameter Lee-Yang-Parr hybrid functional (B3LYP),<sup>[11,13,14]</sup> and the meta-hybrid GGA functional M06<sup>[15]</sup> of Truhlar and Zhao were tested. The influence of the dispersion was also taken into account by means of the Grimme's dispersion (D3) correction.<sup>[16]</sup> All the gas-phase optimizations were carried out using the Ahlrichs' basis set def2-SV(P)<sup>[17]</sup> for all atoms except for copper for which we used the MDF10 Stuttgart-Dresden effective core potential.<sup>[18]</sup> A larger basis set (def2-TZV(P)) for all atoms except copper was also tested to check its influence over the geometry. Vibrational frequencies were computed on each stationary point for identification as either a transition state (TS) (single imaginary frequency) or an intermediate (all frequencies positive) on the potential energy surface. The zero-point correction was calculated and applied to all the stationary structures. The atomic polar tensor (APT) charges and the spin density were also computed for each stationary structure in order to elucidate the oxidation state of the metal ion and the dioxygen molecules. Finally, the energies were recalculated taking into account the effect of the polarizable solvent (water) by using the default SCRF method of the Polarizable Continuum Model.<sup>[19]</sup> gMolden<sup>[20]</sup> and PyMOL<sup>[21]</sup> were used for visual inspection and to create the molecular graphics. Computations were carried out using the program Gaussian09 E.01.<sup>[22]</sup>

#### **2.4 Hybrid quantum mechanics/molecular dynamics (QM/MD) simulation**

The QM-optimized geometry of 1 was embedded in a box of 4175 TIP3P water molecules<sup>[23]</sup> that extended 20 Å away from any solute atom and two Cl<sup>-</sup> ions were added to ensure electrical neutrality. The system was relaxed by energy minimization in three consecutive steps (3x5000 cycles) in which after the first 1000 cycles the minimization method was switched from steepest descent to conjugate gradient. The resulting system was heated from 100 to 300 K during 20 ps with the position of the solute atoms were restrained (20 kcal mol<sup>-1</sup> Å<sup>-2</sup>) using the weak-coupled algorithm for

the temperature regulation and with fixed volume (NVT ensemble). These harmonic restraints were gradually reduced in five steps (5 x 20 ps) until they were completely removed. In the latter equilibrating step, the pressure was fixed (NPT ensemble). The system was further simulated under the same conditions up to a total time of 200 ps with a time step of 2 fs. System coordinates were printed every 10 ps for further analysis. The step time used for the minimizations, as well as for the heating and the equilibration steps, was fixed in 1 fs. The cutoff distance for the non-bonded interactions was 10 Å and periodic boundary conditions were used. Electrostatic interactions were treated by using the smooth particle mesh Ewald (PME) method<sup>[24]</sup> with a grid spacing of 1 Å. The SHAKE algorithm<sup>[25]</sup> was applied to all bonds involving hydrogen atoms in the classical region. The molecular dynamics (MD) simulation protocol made use of the pmemd\_cuda.SPFP module in the AMBER16 suite of programs.<sup>[26]</sup> All the MD simulations were performed using one NVIDIA GPU.

The square pyramid coordination sphere of 1 and 2 was described using the Metal Centre Parameter Builder (MCPB)<sup>[27]</sup> module within Amber16. Briefly, the force field parameters (bond, angle, dihedral, electrostatic, van der Waals terms) were obtained at the B3LYP/6-31G\*<sup>[28]</sup> level of theory and the ESP punctual charges were derived by fitting the electrostatic potential according to the Merz-Singh-Kollman<sup>[29,30]</sup> scheme. Some additional parameters for the coordination sphere of 1 and 2 were taken from previous works.<sup>[31-33]</sup>

The final equilibrated snapshots of 1 and 2 within the box of TIP3P water molecules obtained in the former MD simulation step were subjected to a hybrid quantum mechanics/molecular mechanics molecular dynamics (QM/MM-MD) simulation. All the QM/MM-MD calculations were performed within the *sander* module of AMBER16, which also includes a complete treatment of long-range electrostatic interactions. The

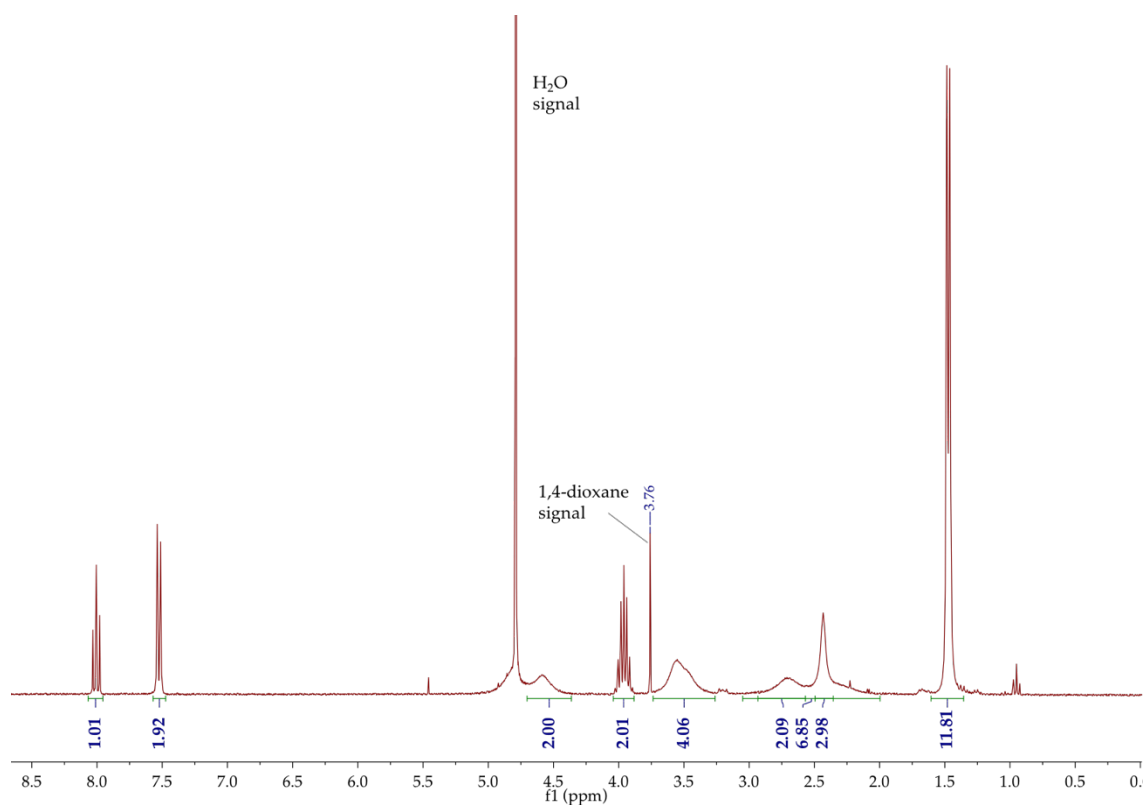
external ORCA package<sup>[34]</sup> was used for the quantum mechanical calculations. The QM region encompassed the complex and the different diatomic oxygen species ( $O_2^-$  for steps *b* and *d*,  $O_2$  for step *c* and  $O^{2-}$  for step *e*), whereas the MM region included all the remaining solvent and counter ions. Therefore, no covalent bond had been cut when defining the QM/MM-MD boundary. The inner QM region was treated at the B3LYP-D3/def2-SV(P) level of theory. A cutoff of 10 Å was employed for the evaluation of the electrostatic interactions within the MM-MD region and of 10 Å for the QM region. All the simulations were run up to 2 ps (2000 steps, 1 fm/step) at 300 K. The system coordinates were printed every 10 steps for further analysis. The MD and QM/MM-MD simulation trajectories were analysed using the cpptraj module<sup>[35]</sup> within AmberTools17.

## 2.5 Crystal structure determination

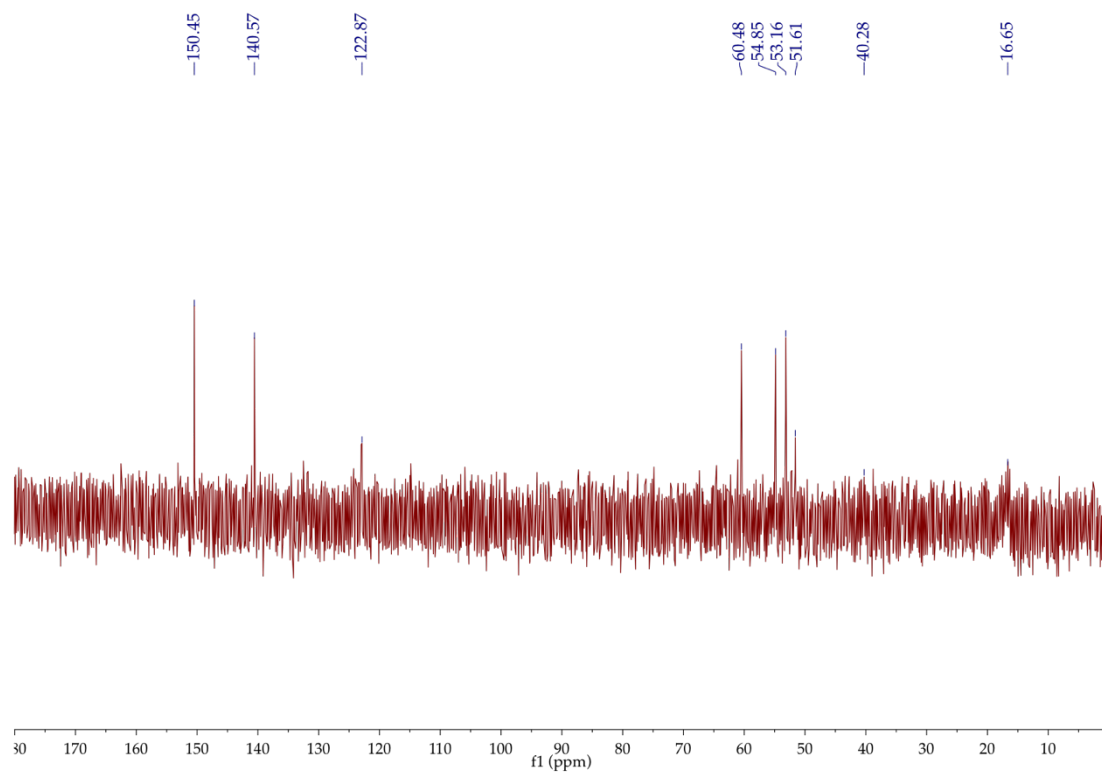
$3.6 \cdot 10^{-3}$  mmol of  $[CuL1(H_2O)]^{2+}$  and  $18 \cdot 10^{-3}$  mmol of  $NaN_3$  were dissolved in pure water and, after slow evaporation, green crystals suitable for X-ray diffraction were obtained. The crystals were measured in a Bruker D8 Venture X-ray diffractometer using  $MoK\alpha$  radiation ( $\lambda=0.71073$  Å) equipped with an Oxford low temperature unit operating at 120 K. Indexing, strategy and data collection were performed with APEX3 software suite. OLEX2 was used as frontend for solving and refining.<sup>[36]</sup> The initial structure was solved with direct methods using SHELXS.<sup>[37]</sup> The resulting structure was refined using SHELXL2014.<sup>[38]</sup> Initially, an isotropic refinement was performed on the non-hydrogen atoms and then anisotropic refinement was introduced. The hydrogen atoms were found in the Fourier map and positions and isotropic thermal factors were left free to refine.



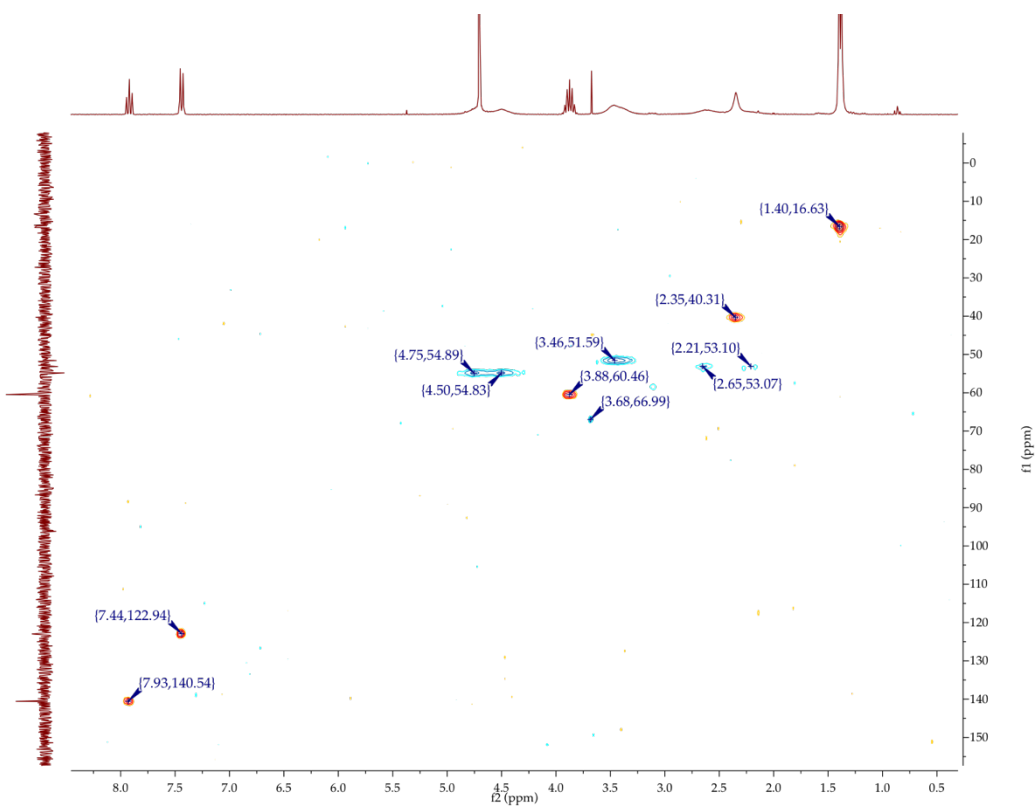
## II. Figures



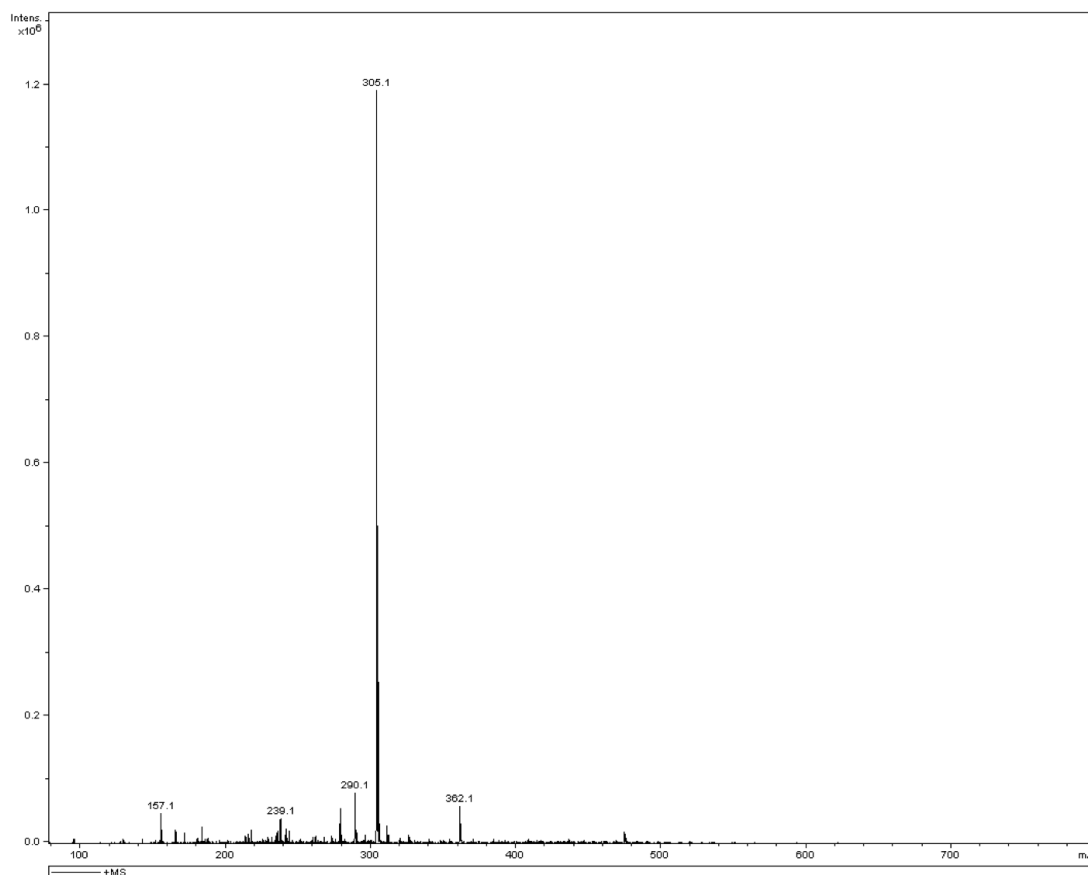
**Figure S1.**  $^1\text{H-NMR}$  spectrum of **L1** in  $\text{D}_2\text{O}$  at 298 K.



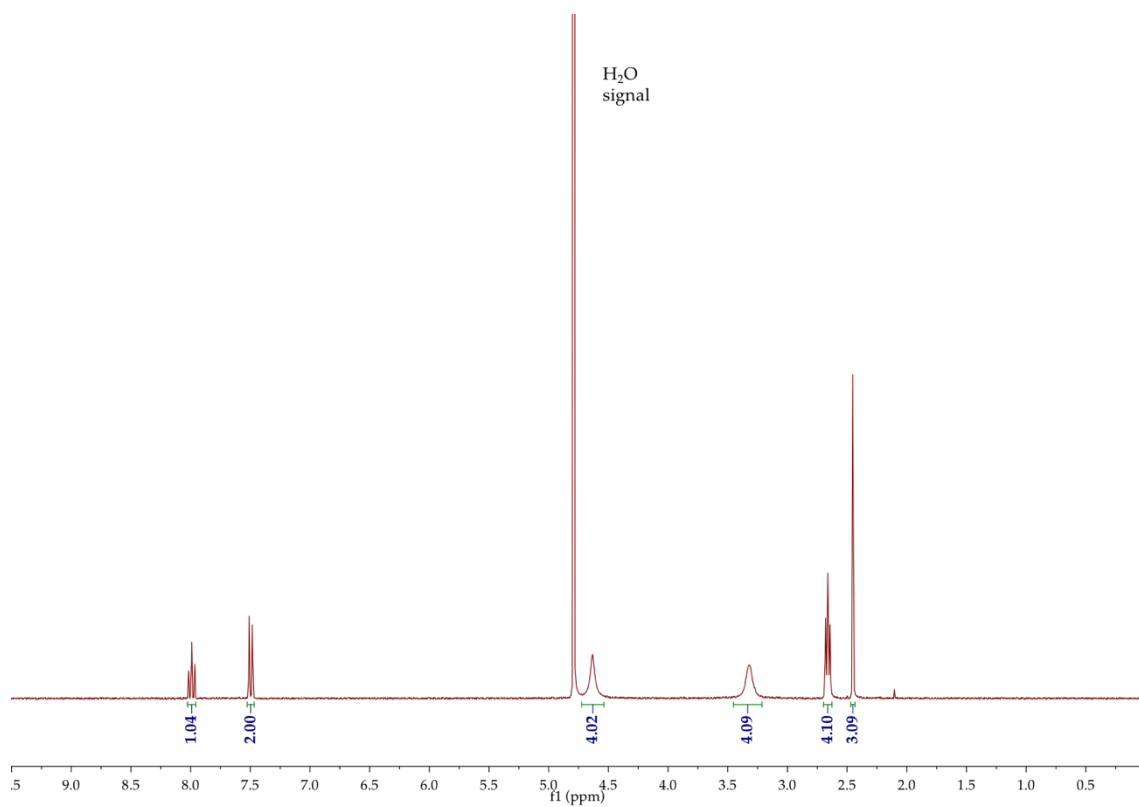
**Figure S2.**  $^{13}\text{C-NMR}$  spectrum of **L1** in  $\text{D}_2\text{O}$  at 298 K.



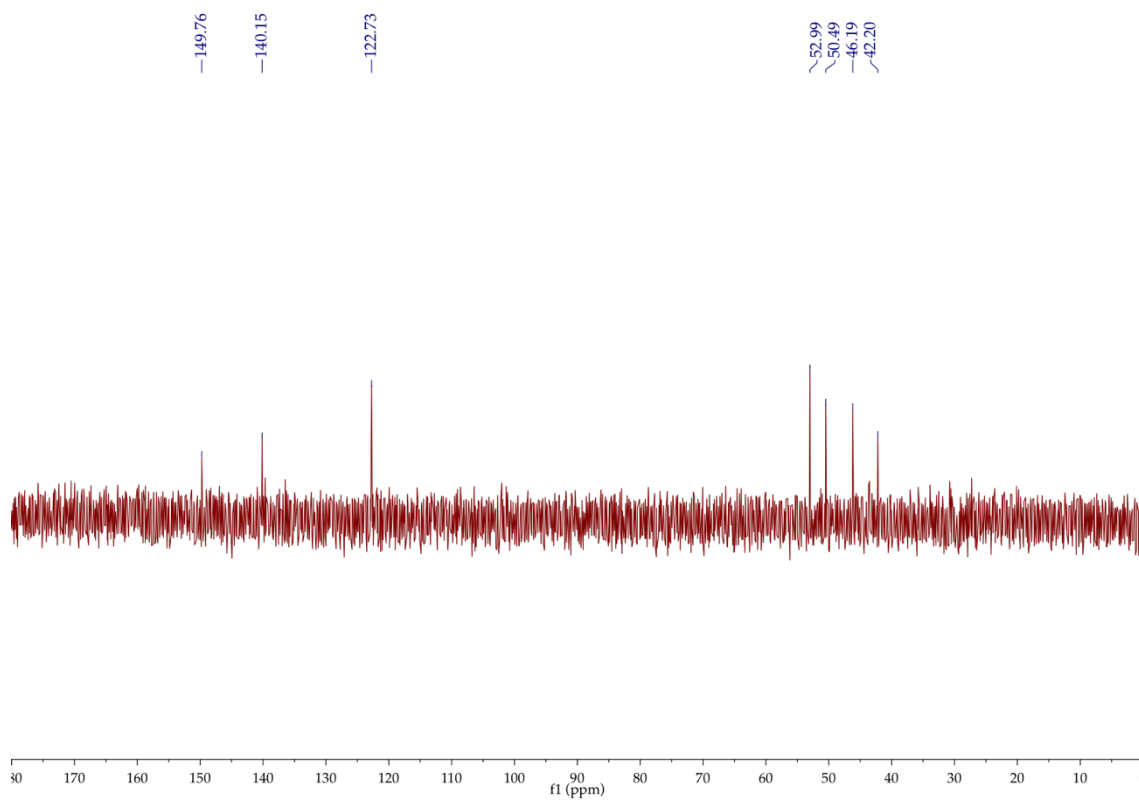
**Figure S3.** 2D  $^1\text{H}$ - $^{13}\text{C}$  HSQC-NMR spectrum of **L1** in  $\text{D}_2\text{O}$  at 298 K.



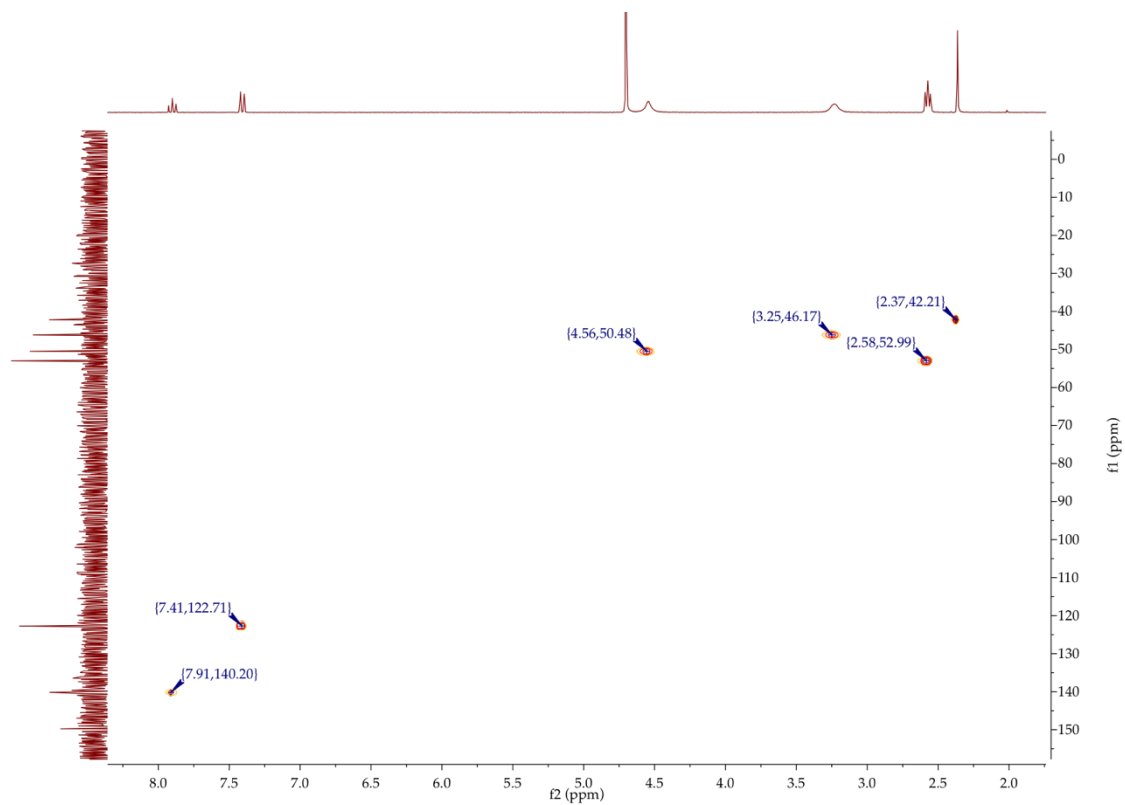
**Figure S4.** LC-MS (ESI/APCI-TOF) of **L1** in  $\text{H}_2\text{O}$ .



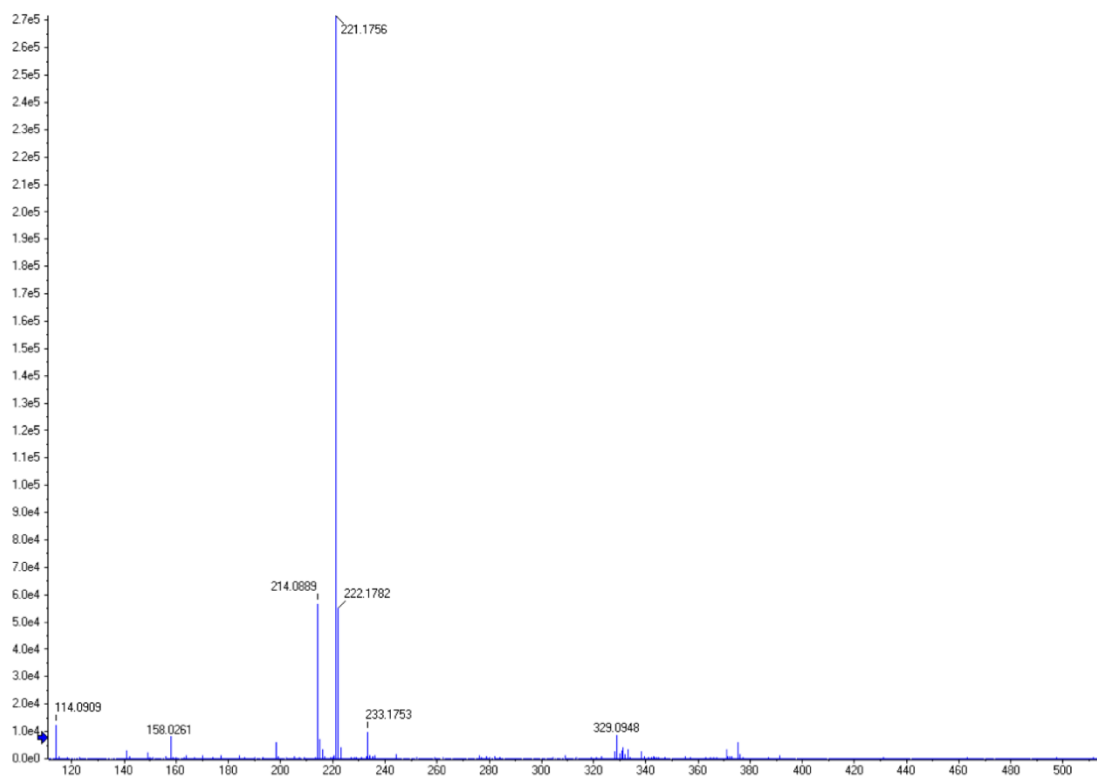
**Figure S5.**  $^1\text{H-NMR}$  spectrum of L2 in  $\text{D}_2\text{O}$  at 298 K.



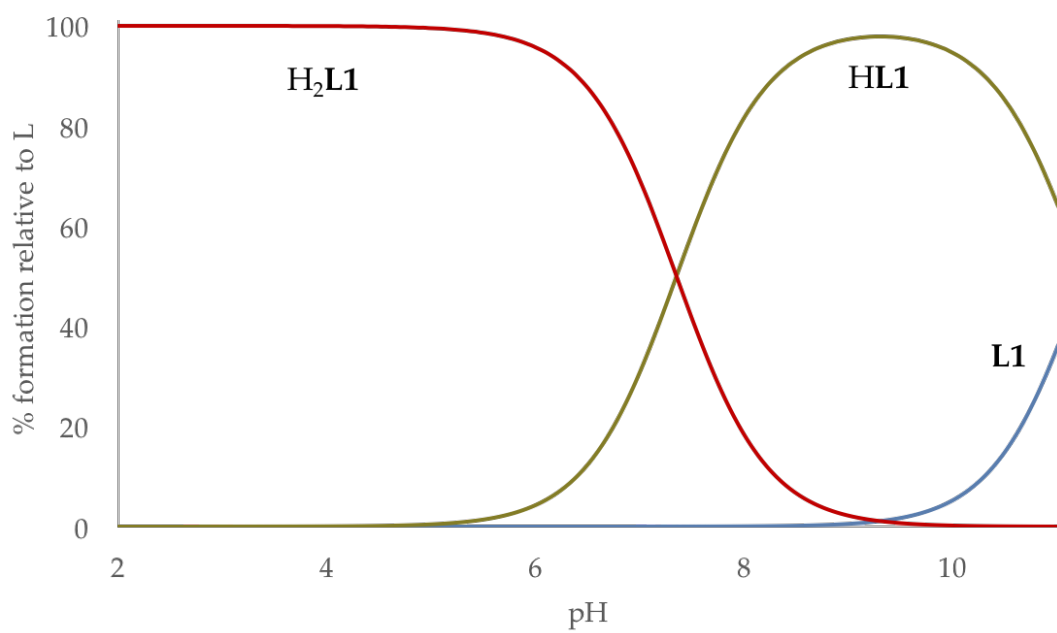
**Figure S6.**  $^{13}\text{C-NMR}$  spectrum of L2 in  $\text{D}_2\text{O}$  at 298 K.



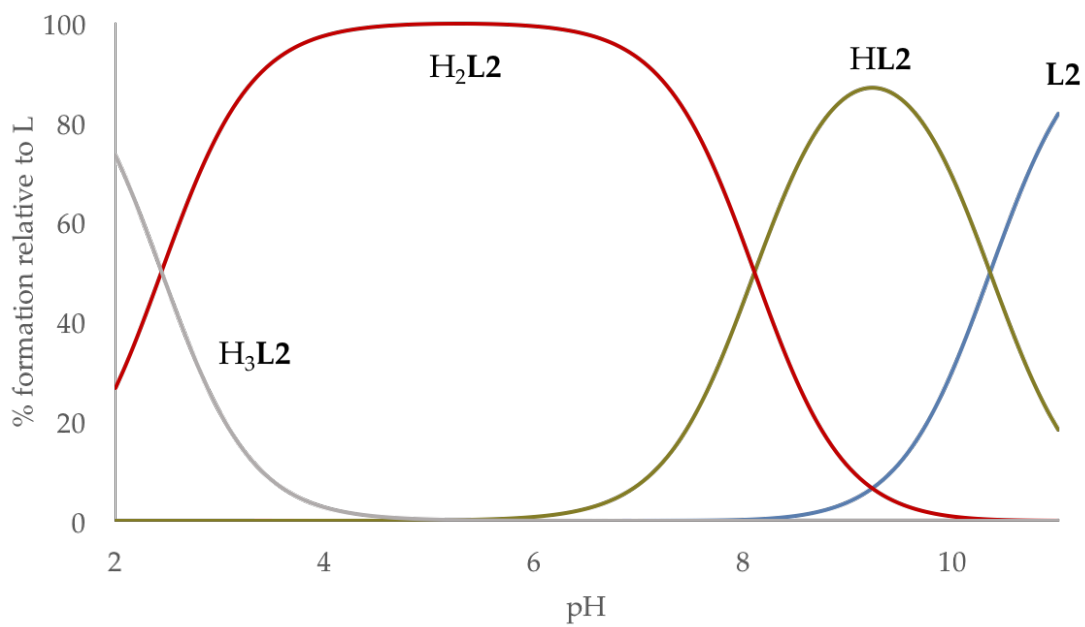
**Figure S7.** 2D  $^1\text{H}$ - $^{13}\text{C}$  HSQC-NMR spectrum of L2 in  $\text{D}_2\text{O}$  at 298 K.



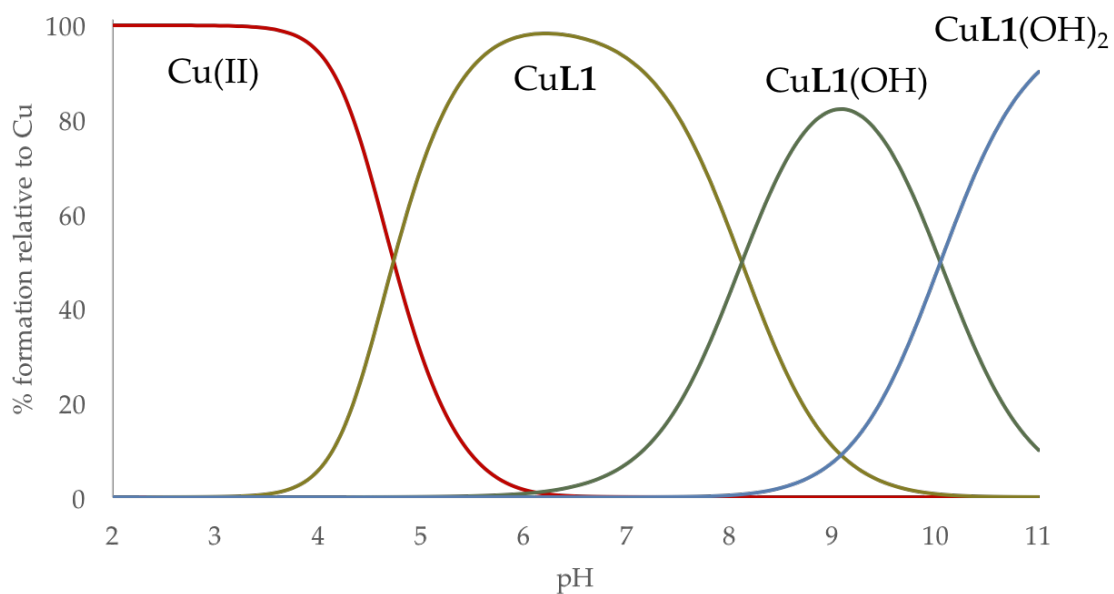
**Figure S8.** LC-MS (ESI/APCI-TOF) of L2 in  $\text{H}_2\text{O}$ .



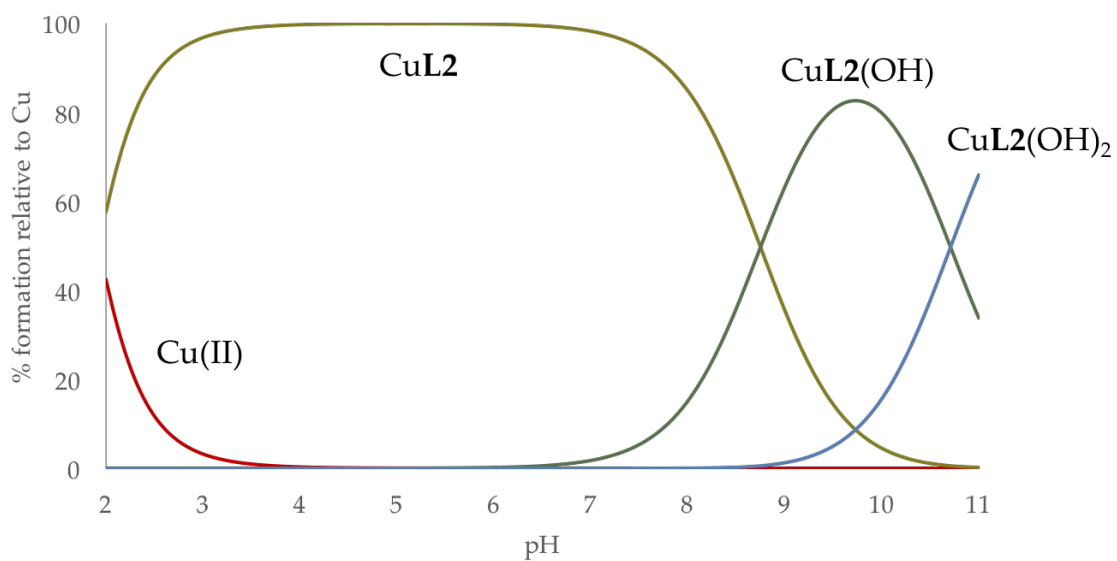
**Figure S9.** Distribution diagram of **L1** as a function of the pH in aqueous solution.



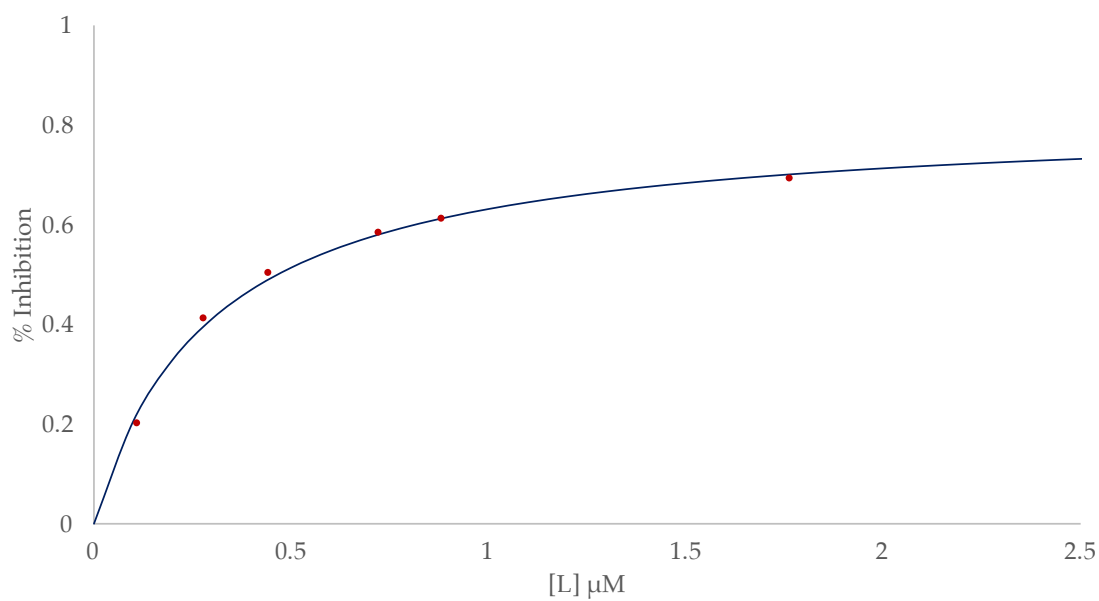
**Figure S10.** Distribution diagram of **L2** as a function of the pH in aqueous solution.



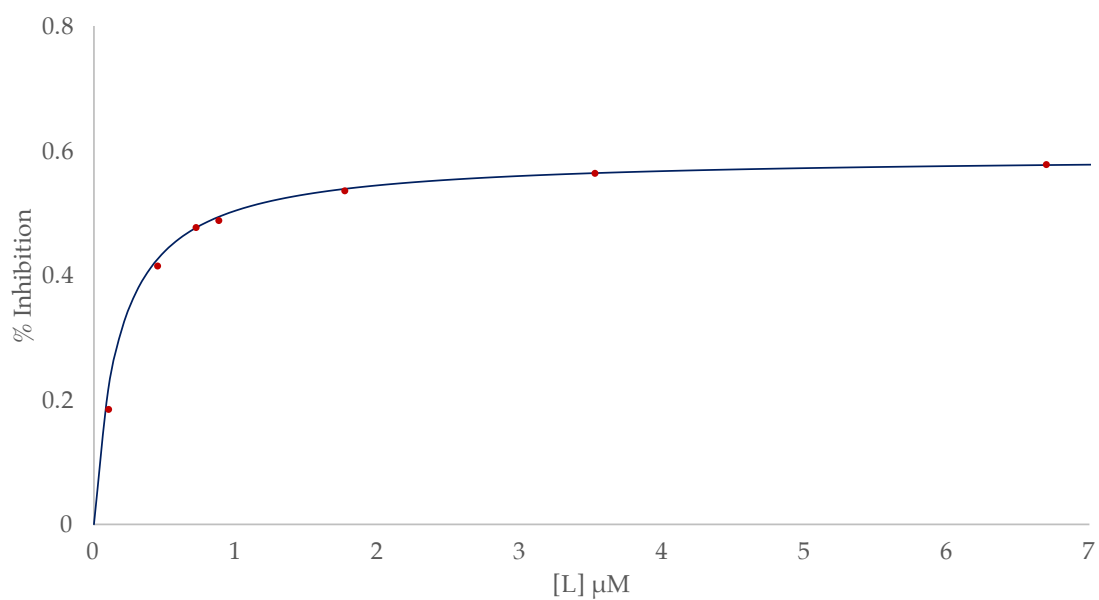
**Figure S11.** Distribution diagram of the  $\text{Cu}^{2+}:\text{L1}$  system as a function of the pH in aqueous solution.



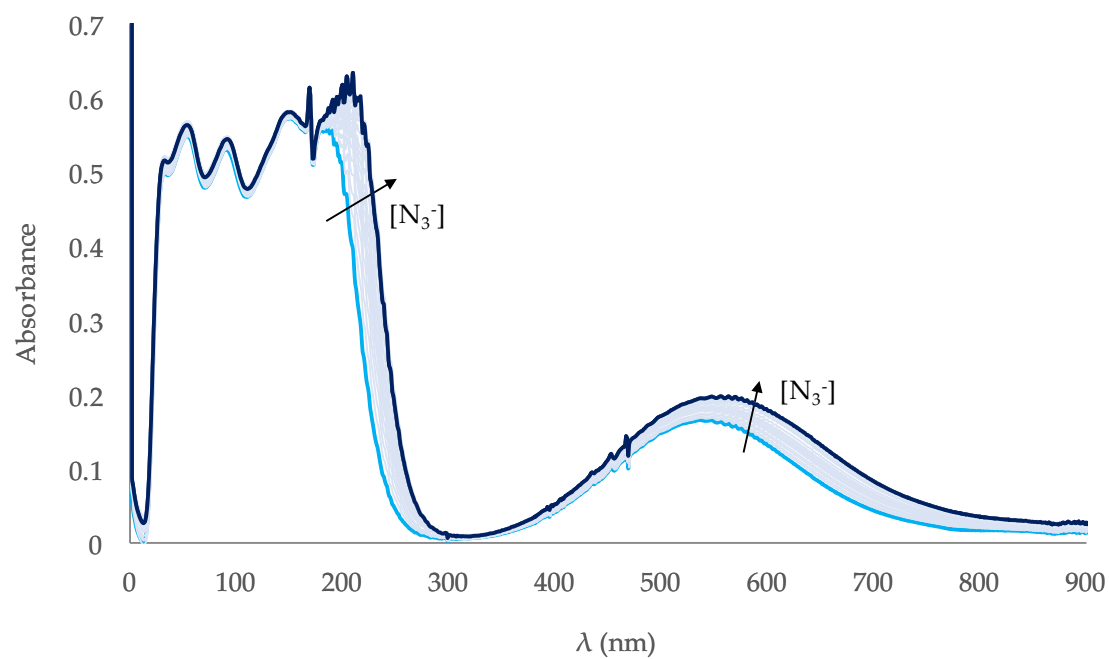
**Figure S12.** Distribution diagram of the  $\text{Cu}^{2+}:\text{L2}$  system as a function of the pH in aqueous solution.



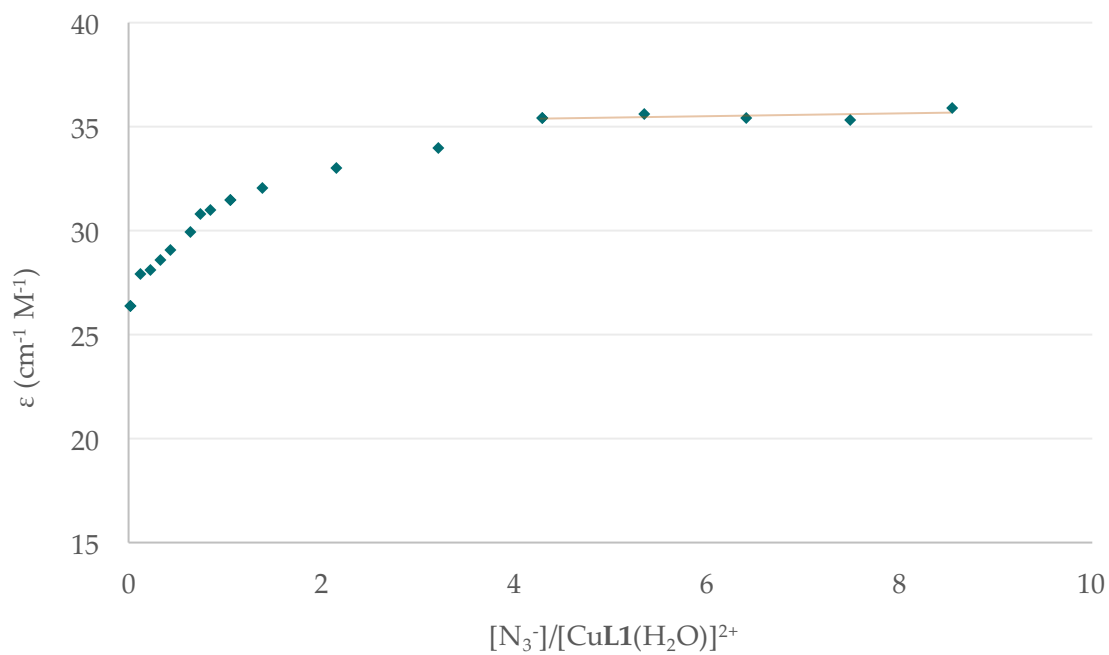
**Figure S13.** Fitting of the SOD activity data obtained by the McCord-Fridovich method for the system Cu-L1-N<sub>3</sub><sup>-</sup>, 1:1:1 molar ratio.



**Figure S14.** Fitting of the SOD activity data obtained by the McCord-Fridovich method for the system Cu-L1-N<sub>3</sub><sup>-</sup>, 1:1:6 molar ratio.

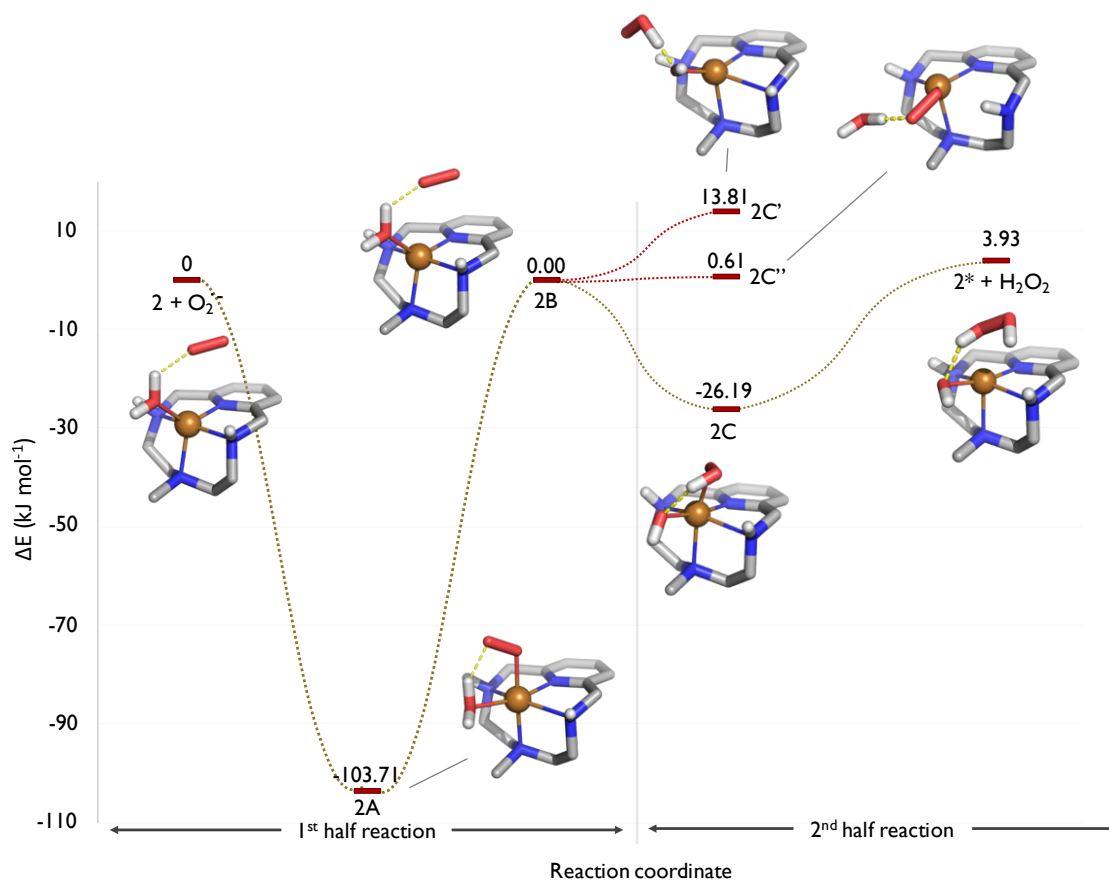


**Figure S15.** UV Vis spectra of  $[\text{CuL1}(\text{H}_2\text{O})]^{2+}$  versus  $[\text{N}_3^-]$ .

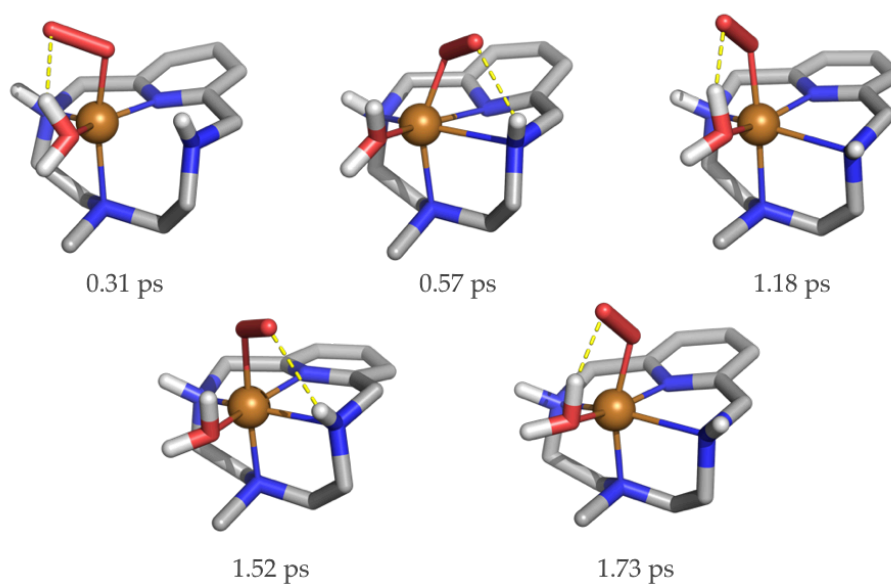


**Figure S16** Absorbance at 573 nm versus  $[\text{N}_3^-]/[\text{CuL1}(\text{H}_2\text{O})]^{2+}$  ratio.

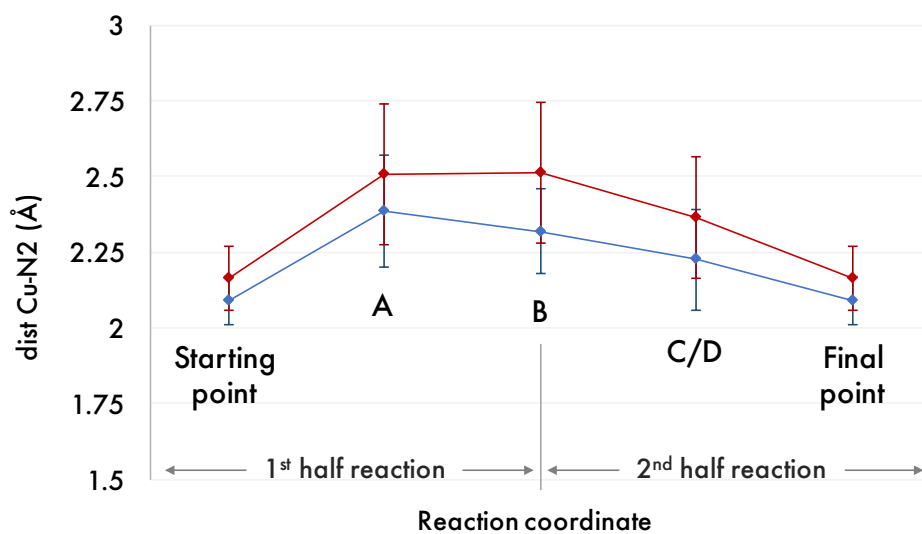




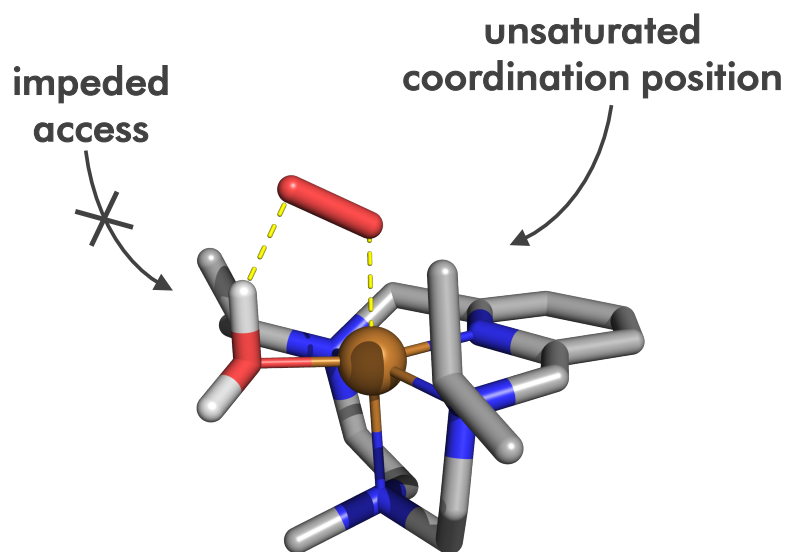
**Figure S17.** Energy profile (kJ mol<sup>-1</sup>, B3LYP-D3/def2-svp/Cu(MDF10)) for the reaction mechanism of the catalytic oxidation and reduction of two species of superoxide by complex **2**. Structure **2\*** corresponds to the hydroxylated form of **2**.



**Figure S18.** Representation of the different conformations adopted by adduct **2A** all along the QM/MM MD modelling. Structures taken at 0.31, 0.57, 1.18, 1.52 and 1.73 ps since the starting of the calculation.



**Figure S19.** Distance Cu-N2 (Å) for complex **1** (red line) and **2** (blue line) along the catalytic mechanism.



**Figure S20.** Entering of the superoxide into **1**. The water molecule prevents the entering by face A but orientates the entrance by a hydrogen-bond with the superoxide.

### III. Tables

**Table S1.** Stepwise protonation logarithm constants for **L1** and **L2** measured in 0.15 M NaClO<sub>4</sub> at 298.1 K.

Reaction <sup>a</sup>	log K <sub>a</sub> ( <b>L1</b> )	log K <sub>a</sub> ( <b>L2</b> )
H + L ⇌ HL	11.25(1)	10.35(1) <sup>b</sup>
H + HL ⇌ H <sub>2</sub> L	7.345(7)	8.09(2)
H + H <sub>2</sub> L ⇌ H <sub>3</sub> L	-	2.47(6)

a) Charges omitted. b) Values in parenthesis are standard deviations in the last significant figure.

**Table S2.** Distribution of the Cu(II)-N and Cu(II)-O distances (Å) in complexes **1** and **2** along QM/MM-MD trajectories in the absence of superoxide. The variation between the values of the two complexes (noted as  $\Delta d$ ) is shown.

cmp	value	distance (Å)				
		Cu-N1	Cu-N2	Cu-N3	Cu-N4	Cu-O5
<b>1</b>	mean	1.97 ± 0.13	2.28 ± 0.17	2.19 ± 0.15	2.16 ± 0.19	2.02 ± 0.12
<b>2</b>	mean	1.97 ± 0.12	2.19 ± 0.16	2.08 ± 0.16	1.97 ± 0.19	2.04 ± 0.11
	$\Delta d^*$	<b>0.00</b>	<b>-0.09</b>	<b>-0.11</b>	<b>-0.19</b>	<b>0.02</b>
<b>1</b>	width**	0.66	1.21	1.23	0.78	0.82
<b>2</b>	width**	0.63	0.99	0.44	0.52	0.64
	$\Delta width$	<b>-0.03</b>	<b>-0.22</b>	<b>-0.79</b>	<b>-0.26</b>	<b>-0.18</b>

(\*)  $\Delta d$  is defined as the difference between the distance found in **2** and **1**.

(\*\*) Difference between maximum and minimum value of the distribution.

**Table S3.** Crystal data and structure refinement for [CuL1(N<sub>3</sub><sup>-</sup>)](ClO<sub>4</sub>).

	[CuL1(N <sub>3</sub> <sup>-</sup> )](ClO <sub>4</sub> )
<b>Empirical formula</b>	C <sub>18</sub> H <sub>32</sub> ClCuN <sub>7</sub> O <sub>4</sub>
<b>Formula weight</b>	509.49
<b>Temperature/K</b>	120.0(1)
<b>Crystal system</b>	monoclinic
<b>Space group</b>	Cc
<b>a/Å</b>	9.682(2)
<b>b/Å</b>	18.886(6)
<b>c/Å</b>	24.789(7)
<b>α/°</b>	90
<b>β/°</b>	99.902(11)
<b>γ/°</b>	90
<b>Volume/Å<sup>3</sup></b>	4465(2)
<b>Z</b>	8
<b>d(calc) /g cm<sup>-3</sup></b>	1.516
<b>μ/mm<sup>-1</sup></b>	1.138
<b>F(000)</b>	2136.0
<b>2θ range</b>	2.400 to 36.327
<b>Radiation</b>	0.71073
<b>Refl. collected</b>	118824
<b>Independent refl.</b>	21612
<b>R<sub>int</sub></b>	0.0365
<b>restraints/param</b>	2/803
<b>GOF</b>	1.037
<b>R<sub>1</sub>, wR<sub>2</sub>[I&gt;=2σ (I)]</b>	0.0276, 0.0615
<b>R<sub>1</sub>, wR<sub>2</sub>[all data]</b>	0.0349, 0.0654

## IV.- Gas phase geometry optimization

An initial small benchmarking for the ground state geometry optimization of complex 1 was carried out using three different functionals (BP86, B3LYP and M06). The most relevant geometrical parameters are shown in Tables S5 and S6. All the geometries were compared with the crystal structure of 1.

For the smallest basis set, all the computed geometries are in reasonably good agreement with the experimental structure obtained by X-Ray analysis (RMSd values < 0.20). The distances Cu-alkylated nitrogens (N2-N4) in all the computed structures differ less than a 3 % from the experimental model. In contrast, the distance Cu-pyridine nitrogen deviates less than a 1 % from the experimental data. Larger differences were found for the distance Cu-O (up to a 8 %) that could be due to the crystal packing effect. The geometry index ( $\tau_5$ )<sup>[39]</sup> defines the trigonal bipyramidal/square pyramid molecular geometry of the coordination sphere. The closer to 0 the value of  $\tau_5$ , the more trigonal bipyramidal the geometry is. On the other side, a closer value to 1 corresponds to square pyramid geometry. 1 has a distorted square pyramidal molecular geometry in the solved crystal structure ( $\tau_5 = 0.24$ ) like in all the optimized geometries. However, the use of the hybrid functionals B3LYP and M06 give results more in consonant with the crystallographic data (Tables S5 and S6).

**Table S4.** Measured Cu(II)-N and Cu(II)-O distances (Å) in the optimized ground state geometries of 1 at different levels of theory and deviation from the X-Ray structure values (%). Deviations higher than 1 % are highlighted in red.

	X-Ray	BP86		M06		B3LYP		B3LYP-D3 (SVP)		B3LYP-D3 (TZVP)	
	d (Å)	d (Å)	% desv.	d (Å)	% desv.	d (Å)	% desv.	d (Å)	% desv.	d (Å)	% desv.
Cu-N1	1.935	1.955	1.03	1.952	0.88	1.958	1.19	1.954	0.98	1.948	0.67
Cu-N2	2.102	2.167	3.09	2.117	0.71	2.151	2.33	2.131	1.38	2.119	0.81
Cu-N3	2.191	2.186	-0.23	2.163	-1.28	2.203	0.55	2.184	-0.32	2.174	-0.78
Cu-N4	2.103	2.165	2.95	2.114	0.52	2.151	2.28	2.129	1.24	2.119	0.76
Cu-O	1.977	2.138	8.14	2.123	7.38	2.125	7.49	2.103	6.37	2.128	7.64
RMSd (Å)	-	0.201		0.174		0.184		0.170		0.155	

**Table S5.** Measured angles ( $^{\circ}$ ), geometry index in the optimized ground state geometries of 1 at different levels of theory and deviation from the X-Ray structure values (%). Deviations higher than 1 % are highlighted in red.

	X-Ray	BP86		M06		B3LYP		B3LYP-D3 (def2-SVP)		B3LYP-D3 (def2-TZVP)	
	Angle ( $^{\circ}$ )	Angle ( $^{\circ}$ )	% desv	Angle ( $^{\circ}$ )	% desv	Angle ( $^{\circ}$ )	% desv	Angle ( $^{\circ}$ )	% desv	Angle ( $^{\circ}$ )	% desv
N1-Cu-N2	82.48	82.78	0.36	82.78	0.36	82.68	0.24	82.83	0.42	83.00	0.63
N1-Cu-N3	100.03	104.44	4.41	104.36	4.33	104.12	4.09	103.42	3.39	104.29	4.26
N1-Cu-N4	82.39	82.79	0.49	82.86	0.57	82.68	0.35	82.89	0.61	83.00	0.74
N1-Cu-O	160.68	157.54	-1.95	159.47	-0.75	159.26	-0.88	160.69	0.01	159.83	-0.53
N2-Cu-N3	86.66	87.56	1.04	87.55	1.03	87.56	1.04	87.64	1.13	87.73	1.23
N2-Cu-N4	162.14	163.18	0.64	163.24	0.68	162.94	0.49	163.55	0.87	163.73	0.98
N2-Cu-O	99.23	100.35	1.13	99.23	0.00	98.35	-0.89	98.85	-0.38	98.01	-1.23
N3-Cu-N4	86.70	87.71	1.16	87.68	1.13	87.56	0.99	87.78	1.25	87.74	1.20
N3-Cu-O	99.29	97.93	-1.37	96.14	-3.17	96.62	-2.69	95.88	-3.43	95.88	-3.43
N4-Cu-O	98.20	111.17	13.21	97.25	-0.97	98.45	0.25	97.33	-0.89	97.99	-0.21
$\tau$	0.024	0.094	-	0.063	-	0.061	-	0.048	-	0.065	-

We also expanded the size of the basis set and we introduced the Grimm's dispersion correction.<sup>[16]</sup> For the latter case, the deviation respect to the crystal structure is reduced up to a 50% using B3LYP-D3/def2-SVP. As example, the deviation distances Cu-N2 and Cu-N4 with respect to the X-Ray structure decreases from 0.049 Å to 0.026 Å, respectively. These observations are in accordance to previous works which show an insufficiently account for dispersion for the B3LYP functional.<sup>[40]</sup> On the other hand, the inclusion of the extra valence basis (triple zeta) in the basis set<sup>[17,41-43]</sup> shows a marginal influence on the optimized geometries since we are using in all case an ECP for the copper atom. Thus, as result of our benchmarking, we chose B3LYP-D3/def2-SVP as method for the following computations.

## V.- Geometries and energies of the optimized structures

Geometry and energy of **1** + O<sub>2</sub><sup>-</sup> structure in z-matrix format.

Energy = -1346.985569 Hartrees

Geometry:

```
C
C 1 r2
C 2 r3 1 a3
C 2 r4 1 a4 3 d4
C 2 r5 1 a5 3 d5
C 3 r6 2 a6 1 d6
C 1 r7 2 a7 3 d7
C 7 r8 1 a8 2 d8
C 1 r9 2 a9 3 d9
C 2 r10 1 a10 3 d10
C 4 r11 2 a11 1 d11
C 4 r12 2 a12 1 d12
C 8 r13 7 a13 1 d13
C 9 r14 1 a14 2 d14
C 3 r15 2 a15 1 d15
C 10 r16 2 a16 1 d16
C 7 r17 1 a17 2 d17
C 9 r18 1 a18 2 d18
O 14 r19 9 a19 1 d19
N 4 r20 2 a20 1 d20
N 17 r21 7 a21 1 d21
N 5 r22 2 a22 1 d22
N 11 r23 4 a23 2 d23
H 15 r24 3 a24 2 d24
H 15 r25 3 a25 2 d25
H 17 r26 7 a26 1 d26
H 18 r27 9 a27 1 d27
H 17 r28 7 a28 1 d28
H 18 r29 9 a29 1 d29
H 17 r30 7 a30 1 d30
H 19 r31 14 a31 9 d31
H 19 r32 14 a32 9 d32
H 5 r33 2 a33 1 d33
H 3 r34 2 a34 1 d34
H 5 r35 2 a35 1 d35
H 6 r36 3 a36 2 d36
H 6 r37 3 a37 2 d37
H 6 r38 3 a38 2 d38
```

H 7 r39 1 a39 2 d39  
H 7 r40 1 a40 2 d40  
H 8 r41 7 a41 1 d41  
H 8 r42 7 a42 1 d42  
H 9 r43 1 a43 2 d43  
H 10 r44 2 a44 1 d44  
H 11 r45 4 a45 2 d45  
H 11 r46 4 a46 2 d46  
H 1 r47 2 a47 3 d47  
H 1 r48 2 a48 3 d48  
H 12 r49 4 a49 2 d49  
H 13 r50 8 a50 7 d50  
H 13 r51 8 a51 7 d51  
H 14 r52 9 a52 1 d52  
H 14 r53 9 a53 1 d53  
H 14 r54 9 a54 1 d54  
H 15 r55 3 a55 2 d55  
H 16 r56 10 a56 2 d56  
H 18 r57 9 a57 1 d57  
C 20 r58 4 a58 2 d58  
O 52 r59 14 a59 9 d59  
O 59 r60 52 a60 14 d60

Variables:

r2= 3.2196  
r3= 5.4259  
a3= 86.46  
r4= 2.3320  
a4= 113.86  
d4= 23.71  
r5= 1.5216  
a5= 47.31  
d5= 236.71  
r6= 1.5304  
a6= 85.73  
d6= 250.33  
r7= 1.5349  
a7= 76.33  
d7= 298.62  
r8= 2.4460  
a8= 143.80  
d8= 67.41  
r9= 2.4588  
a9= 82.29  
d9= 88.49



r10= 1.3971  
a10= 126.93  
d10= 135.33  
r11= 1.5200  
a11= 146.81  
d11= 312.98  
r12= 1.3974  
a12= 91.57  
d12= 131.99  
r13= 1.5345  
a13= 144.04  
d13= 1.04  
r14= 1.5314  
a14= 144.50  
d14= 329.05  
r15= 1.5348  
a15= 131.31  
d15= 135.66  
r16= 1.3961  
a16= 118.95  
d16= 237.52  
r17= 2.4384  
a17= 102.01  
d17= 122.27  
r18= 1.5349  
a18= 97.38  
d18= 112.27  
r19= 3.3503  
a19= 80.09  
d19= 301.97  
r20= 1.3428  
a20= 29.75  
d20= 309.62  
r21= 1.4655  
a21= 34.02  
d21= 244.47  
r22= 1.4652  
a22= 114.34  
d22= 34.29  
r23= 1.4676  
a23= 114.44  
d23= 33.30  
r24= 1.1001  
a24= 110.33

d24= 161.58  
r25= 1.1017  
a25= 111.18  
d25= 42.59  
r26= 1.0978  
a26= 90.51  
d26= 11.52  
r27= 1.1002  
a27= 110.37  
d27= 145.88  
r28= 1.1082  
a28= 94.47  
d28= 120.49  
r29= 1.1007  
a29= 112.17  
d29= 26.12  
r30= 1.0981  
a30= 144.00  
d30= 250.95  
r31= 0.9700  
a31= 47.79  
d31= 215.47  
r32= 0.9683  
a32= 150.75  
d32= 188.24  
r33= 1.1003  
a33= 106.46  
d33= 153.86  
r34= 1.1040  
a34= 109.81  
d34= 356.87  
r35= 1.1066  
a35= 108.78  
d35= 267.98  
r36= 1.1001  
a36= 112.57  
d36= 284.58  
r37= 1.1015  
a37= 109.71  
d37= 165.90  
r38= 1.0998  
a38= 111.18  
d38= 45.37  
r39= 1.1085

a39= 108.00  
d39= 212.95  
r40= 1.0988  
a40= 109.25  
d40= 328.13  
r41= 1.0982  
a41= 80.03  
d41= 251.85  
r42= 1.1087  
a42= 102.05  
d42= 147.11  
r43= 1.1034  
a43= 82.63  
d43= 219.85  
r44= 1.0928  
a44= 120.09  
d44= 56.80  
r45= 1.1004  
a45= 106.40  
d45= 273.72  
r46= 1.1065  
a46= 108.77  
d46= 159.46  
r47= 1.1080  
a47= 97.76  
d47= 192.71  
r48= 1.0998  
a48= 152.07  
d48= 43.67  
r49= 1.0923  
a49= 120.10  
d49= 181.52  
r50= 1.1002  
a50= 109.13  
d50= 85.11  
r51= 1.1079  
a51= 107.22  
d51= 199.49  
r52= 1.1006  
a52= 111.34  
d52= 329.53  
r53= 1.1011  
a53= 109.84  
d53= 208.31

r54= 1.1008  
a54= 112.64  
d54= 89.58  
r55= 1.1006  
a55= 112.02  
d55= 281.37  
r56= 1.0922  
a56= 120.47  
d56= 179.86  
r57= 1.1020  
a57= 111.20  
d57= 264.91  
r58= 2.0305  
a58= 117.87  
d58= 158.46  
r59= 2.5610  
a59= 139.26  
d59= 115.28  
r60= 1.2029  
a60= 156.81  
d60= 288.96

Geometry and energy of **1A** structure in z-matrix format.  
Energy = -1346.998916 Hartrees

Geometry:

N  
C 1 r2  
C 2 r3 1 a3  
C 3 r4 2 a4 1 d4  
C 4 r5 3 a5 2 d5  
C 1 r6 2 a6 3 d6  
C 2 r7 1 a7 3 d7  
N 7 r8 2 a8 1 d8  
C 1 r9 2 a9 3 d9  
O 9 r10 1 a10 2 d10  
O 10 r11 9 a11 1 d11  
C 6 r12 1 a12 2 d12  
N 12 r13 6 a13 1 d13  
C 13 r14 12 a14 6 d14  
C 14 r15 13 a15 12 d15

N 15 r16 14 a16 13 d16  
C 16 r17 15 a17 14 d17  
C 16 r18 15 a18 14 d18  
C 8 r19 7 a19 2 d19  
C 8 r20 7 a20 2 d20  
C 20 r21 8 a21 7 d21  
C 20 r22 8 a22 7 d22  
C 13 r23 12 a23 6 d23  
C 23 r24 13 a24 12 d24  
C 23 r25 13 a25 12 d25  
O 9 r26 1 a26 2 d26  
H 24 r27 23 a27 13 d27  
H 24 r28 23 a28 13 d28  
H 17 r29 16 a29 15 d29  
H 21 r30 20 a30 8 d30  
H 17 r31 16 a31 15 d31  
H 21 r32 20 a32 8 d32  
H 17 r33 16 a33 15 d33  
H 26 r34 9 a34 1 d34  
H 26 r35 9 a35 1 d35  
H 7 r36 2 a36 1 d36  
H 23 r37 13 a37 12 d37  
H 7 r38 2 a38 1 d38  
H 25 r39 23 a39 13 d39  
H 25 r40 23 a40 13 d40  
H 25 r41 23 a41 13 d41  
H 18 r42 16 a42 15 d42  
H 18 r43 16 a43 15 d43  
H 15 r44 14 a44 13 d44  
H 15 r45 14 a45 13 d45  
H 20 r46 8 a46 7 d46  
H 3 r47 2 a47 1 d47  
H 12 r48 6 a48 1 d48  
H 12 r49 6 a49 1 d49  
H 19 r50 8 a50 7 d50  
H 19 r51 8 a51 7 d51  
H 5 r52 4 a52 3 d52  
H 14 r53 13 a53 12 d53  
H 14 r54 13 a54 12 d54  
H 22 r55 20 a55 8 d55  
H 22 r56 20 a56 8 d56  
H 22 r57 20 a57 8 d57  
H 24 r58 23 a58 13 d58  
H 4 r59 3 a59 2 d59

H 21 r60 20 a60 8 d60

Variables:

r2= 1.3363

r3= 1.4001

a3= 120.50

r4= 1.3947

a4= 118.79

d4= 0.05

r5= 1.3986

a5= 119.55

d5= 0.66

r6= 1.3421

a6= 121.89

d6= 359.17

r7= 1.5258

a7= 118.80

d7= 182.34

r8= 1.4648

a8= 116.06

d8= 339.50

r9= 2.0396

a9= 120.64

d9= 186.46

r10= 2.0069

a10= 92.62

d10= 260.58

r11= 1.2635

a11= 120.13

d11= 334.23

r12= 1.5203

a12= 117.74

d12= 178.93

r13= 1.4714

a13= 115.48

d13= 35.20

r14= 1.4746

a14= 112.92

d14= 72.44

r15= 1.5283

a15= 114.64

d15= 278.92

r16= 1.4795

a16= 113.95

d16= 309.46

r17= 1.4712  
a17= 111.65  
d17= 288.62  
r18= 1.4799  
a18= 110.13  
d18= 164.22  
r19= 1.4699  
a19= 113.20  
d19= 272.61  
r20= 1.5005  
a20= 113.93  
d20= 144.95  
r21= 1.5359  
a21= 113.52  
d21= 65.40  
r22= 1.5277  
a22= 112.74  
d22= 298.55  
r23= 1.5020  
a23= 112.77  
d23= 198.81  
r24= 1.5350  
a24= 113.51  
d24= 306.30  
r25= 1.5262  
a25= 112.88  
d25= 74.45  
r26= 2.1741  
a26= 166.85  
d26= 309.99  
r27= 1.1001  
a27= 109.92  
d27= 190.81  
r28= 1.1015  
a28= 111.56  
d28= 72.06  
r29= 1.0966  
a29= 109.85  
d29= 179.04  
r30= 1.1007  
a30= 109.91  
d30= 177.04  
r31= 1.1064  
a31= 111.65

d31= 300.03  
r32= 1.1001  
a32= 112.78  
d32= 57.51  
r33= 1.0979  
a33= 109.93  
d33= 60.49  
r34= 0.9729  
a34= 103.10  
d34= 315.80  
r35= 0.9684  
a35= 120.19  
d35= 199.30  
r36= 1.0995  
a36= 105.67  
d36= 99.81  
r37= 1.1024  
a37= 104.06  
d37= 189.67  
r38= 1.1075  
a38= 108.19  
d38= 212.65  
r39= 1.0996  
a39= 112.76  
d39= 298.12  
r40= 1.1000  
a40= 109.48  
d40= 178.43  
r41= 1.0976  
a41= 111.05  
d41= 58.58  
r42= 1.1066  
a42= 110.43  
d42= 79.84  
r43= 1.0979  
a43= 107.75  
d43= 324.19  
r44= 1.0971  
a44= 109.81  
d44= 70.10  
r45= 1.1069  
a45= 108.43  
d45= 186.06  
r46= 1.1022



a46= 103.81  
d46= 183.02  
r47= 1.0919  
a47= 120.21  
d47= 179.78  
r48= 1.1012  
a48= 105.80  
d48= 276.11  
r49= 1.1052  
a49= 108.29  
d49= 161.38  
r50= 1.1086  
a50= 111.80  
d50= 307.93  
r51= 1.0995  
a51= 107.43  
d51= 191.61  
r52= 1.0916  
a52= 120.97  
d52= 178.91  
r53= 1.0997  
a53= 107.53  
d53= 157.41  
r54= 1.1074  
a54= 111.94  
d54= 41.57  
r55= 1.0974  
a55= 111.89  
d55= 311.18  
r56= 1.0996  
a56= 109.19  
d56= 190.95  
r57= 1.1013  
a57= 112.54  
d57= 72.92  
r58= 1.1009  
a58= 112.25  
d58= 310.35  
r59= 1.0924  
a59= 120.26  
d59= 179.86  
r60= 1.1018  
a60= 111.30  
d60= 295.63

Geometry and energy of **1B** structure in z-matrix format.

Energy = -1346.985562 Hartrees

Geometry:

```
C
C 1 r2
C 2 r3 1 a3
N 3 r4 2 a4 1 d4
C 4 r5 3 a5 2 d5
C 1 r6 2 a6 3 d6
C 3 r7 2 a7 1 d7
N 7 r8 3 a8 2 d8
C 8 r9 7 a9 3 d9
C 9 r10 8 a10 7 d10
C 4 r11 3 a11 2 d11
O 11 r12 4 a12 3 d12
C 5 r13 4 a13 3 d13
N 13 r14 5 a14 4 d14
C 14 r15 13 a15 5 d15
C 15 r16 14 a16 13 d16
C 8 r17 7 a17 3 d17
C 17 r18 8 a18 7 d18
N 18 r19 17 a19 8 d19
C 19 r20 18 a20 17 d20
C 14 r21 13 a21 5 d21
C 19 r22 18 a22 17 d22
C 15 r23 14 a23 13 d23
C 9 r24 8 a24 7 d24
O 4 r25 3 a25 2 d25
O 25 r26 4 a26 3 d26
H 24 r27 9 a27 8 d27
H 24 r28 9 a28 8 d28
H 22 r29 19 a29 18 d29
H 23 r30 15 a30 14 d30
H 22 r31 19 a31 18 d31
H 23 r32 15 a32 14 d32
H 22 r33 19 a33 18 d33
H 12 r34 11 a34 4 d34
H 12 r35 11 a35 4 d35
H 13 r36 5 a36 4 d36
H 9 r37 8 a37 7 d37
H 13 r38 5 a38 4 d38
H 10 r39 9 a39 8 d39
H 10 r40 9 a40 8 d40
```

H 10 r41 9 a41 8 d41  
H 20 r42 19 a42 18 d42  
H 20 r43 19 a43 18 d43  
H 18 r44 17 a44 8 d44  
H 18 r45 17 a45 8 d45  
H 15 r46 14 a46 13 d46  
H 6 r47 1 a47 2 d47  
H 7 r48 3 a48 2 d48  
H 7 r49 3 a49 2 d49  
H 21 r50 14 a50 13 d50  
H 21 r51 14 a51 13 d51  
H 2 r52 1 a52 3 d52  
H 17 r53 8 a53 7 d53  
H 17 r54 8 a54 7 d54  
H 16 r55 15 a55 14 d55  
H 16 r56 15 a56 14 d56  
H 16 r57 15 a57 14 d57  
H 24 r58 9 a58 8 d58  
H 1 r59 2 a59 3 d59  
H 23 r60 15 a60 14 d60

Variables:

r2= 1.3968  
r3= 1.3975  
a3= 118.88  
r4= 1.3428  
a4= 121.24  
d4= 359.29  
r5= 1.3421  
a5= 120.59  
d5= 2.88  
r6= 1.3965  
a6= 119.10  
d6= 358.60  
r7= 1.5195  
a7= 121.60  
d7= 180.09  
r8= 1.4677  
a8= 114.36  
d8= 214.52  
r9= 1.4925  
a9= 113.63  
d9= 208.72  
r10= 1.5299  
a10= 112.18

d10= 65.86  
r11= 2.0317  
a11= 117.69  
d11= 161.32  
r12= 2.1231  
a12= 156.64  
d12= 109.84  
r13= 1.5213  
a13= 117.29  
d13= 178.03  
r14= 1.4655  
a14= 114.35  
d14= 326.73  
r15= 1.4907  
a15= 114.32  
d15= 147.88  
r16= 1.5323  
a16= 112.05  
d16= 298.83  
r17= 1.4740  
a17= 113.27  
d17= 79.36  
r18= 1.5349  
a18= 114.99  
d18= 282.54  
r19= 1.4723  
a19= 114.05  
d19= 303.49  
r20= 1.4728  
a20= 112.38  
d20= 157.90  
r21= 1.4707  
a21= 113.65  
d21= 278.50  
r22= 1.4659  
a22= 112.40  
d22= 285.62  
r23= 1.5346  
a23= 113.92  
d23= 65.69  
r24= 1.5358  
a24= 113.84  
d24= 298.43  
r25= 3.1319

a25= 103.99  
d25= 241.45  
r26= 1.2028  
a26= 79.22  
d26= 26.00  
r27= 1.1005  
a27= 110.31  
d27= 186.00  
r28= 1.1019  
a28= 111.18  
d28= 67.00  
r29= 1.0979  
a29= 110.06  
d29= 173.95  
r30= 1.1007  
a30= 110.34  
d30= 176.53  
r31= 1.1089  
a31= 112.07  
d31= 295.31  
r32= 1.1011  
a32= 112.11  
d32= 56.87  
r33= 1.0979  
a33= 110.12  
d33= 56.25  
r34= 0.9689  
a34= 115.58  
d34= 22.58  
r35= 0.9684  
a35= 117.80  
d35= 256.85  
r36= 1.1001  
a36= 106.52  
d36= 86.40  
r37= 1.1041  
a37= 104.18  
d37= 181.22  
r38= 1.1076  
a38= 108.77  
d38= 200.43  
r39= 1.1010  
a39= 112.50  
d39= 288.96

r40= 1.1003  
a40= 109.78  
d40= 170.25  
r41= 1.0999  
a41= 111.12  
d41= 49.64  
r42= 1.1087  
a42= 111.05  
d42= 80.58  
r43= 1.0985  
a43= 107.86  
d43= 324.52  
r44= 1.0983  
a44= 109.34  
d44= 64.24  
r45= 1.1089  
a45= 107.93  
d45= 179.44  
r46= 1.1021  
a46= 104.08  
d46= 183.52  
r47= 1.0917  
a47= 120.99  
d47= 182.26  
r48= 1.0999  
a48= 106.48  
d48= 95.02  
r49= 1.1067  
a49= 108.79  
d49= 340.59  
r50= 1.1083  
a50= 111.73  
d50= 313.07  
r51= 1.0999  
a51= 107.38  
d51= 197.08  
r52= 1.0914  
a52= 120.98  
d52= 179.15  
r53= 1.0994  
a53= 107.47  
d53= 160.86  
r54= 1.1081  
a54= 111.64

d54= 44.96  
r55= 1.1006  
a55= 111.34  
d55= 317.69  
r56= 1.1005  
a56= 109.85  
d56= 196.36  
r57= 1.1014  
a57= 112.62  
d57= 77.68  
r58= 1.0999  
a58= 112.08  
d58= 305.77  
r59= 1.0922  
a59= 120.44  
d59= 180.19  
r60= 1.1017  
a60= 111.25  
d60= 295.63

Geometry and energy of **1C** structure in z-matrix format.  
Energy = -1423.48637 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 2 r5 1 a5 3 d5  
C 3 r6 2 a6 1 d6  
C 1 r7 2 a7 3 d7  
C 7 r8 1 a8 2 d8  
C 1 r9 2 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 4 r11 2 a11 1 d11  
C 4 r12 2 a12 1 d12  
C 8 r13 7 a13 1 d13  
C 9 r14 1 a14 2 d14  
C 3 r15 2 a15 1 d15  
C 10 r16 2 a16 1 d16  
C 8 r17 7 a17 1 d17

C 9 r18 1 a18 2 d18  
O 6 r19 3 a19 2 d19  
O 19 r20 6 a20 3 d20  
O 19 r21 6 a21 3 d21  
N 2 r22 1 a22 3 d22  
N 8 r23 7 a23 1 d23  
N 5 r24 2 a24 1 d24  
N 11 r25 4 a25 2 d25  
C 22 r26 2 a26 1 d26  
H 15 r27 3 a27 2 d27  
H 15 r28 3 a28 2 d28  
H 17 r29 8 a29 7 d29  
H 18 r30 9 a30 1 d30  
H 17 r31 8 a31 7 d31  
H 18 r32 9 a32 1 d32  
H 17 r33 8 a33 7 d33  
H 21 r34 19 a34 6 d34  
H 21 r35 19 a35 6 d35  
H 5 r36 2 a36 1 d36  
H 3 r37 2 a37 1 d37  
H 5 r38 2 a38 1 d38  
H 6 r39 3 a39 2 d39  
H 6 r40 3 a40 2 d40  
H 6 r41 3 a41 2 d41  
H 7 r42 1 a42 2 d42  
H 7 r43 1 a43 2 d43  
H 8 r44 7 a44 1 d44  
H 8 r45 7 a45 1 d45  
H 9 r46 1 a46 2 d46  
H 10 r47 2 a47 1 d47  
H 11 r48 4 a48 2 d48  
H 11 r49 4 a49 2 d49  
H 1 r50 2 a50 3 d50  
H 1 r51 2 a51 3 d51  
H 12 r52 4 a52 2 d52  
H 13 r53 8 a53 7 d53  
H 13 r54 8 a54 7 d54  
H 14 r55 9 a55 1 d55  
H 14 r56 9 a56 1 d56  
H 14 r57 9 a57 1 d57  
H 15 r58 3 a58 2 d58  
H 16 r59 10 a59 2 d59  
H 18 r60 9 a60 1 d60  
O 51 r61 1 a61 2 d61



H 61 r62 51 a62 1 d62

H 61 r63 51 a63 1 d63

Variables:

r2= 3.2268

r3= 5.5551

a3= 84.65

r4= 2.3306

a4= 114.16

d4= 15.13

r5= 1.5204

a5= 46.88

d5= 227.15

r6= 1.5289

a6= 92.77

d6= 257.97

r7= 1.5324

a7= 73.64

d7= 298.09

r8= 2.4281

a8= 143.31

d8= 63.15

r9= 2.4448

a9= 82.70

d9= 99.06

r10= 1.3997

a10= 129.14

d10= 128.78

r11= 1.5162

a11= 147.20

d11= 317.72

r12= 1.3982

a12= 91.44

d12= 135.23

r13= 1.5384

a13= 145.78

d13= 12.12

r14= 1.5307

a14= 147.00

d14= 337.05

r15= 1.5390

a15= 128.32

d15= 138.49

r16= 1.3937

a16= 119.12

d16= 235.64  
r17= 2.4219  
a17= 59.97  
d17= 72.17  
r18= 1.5386  
a18= 94.25  
d18= 115.24  
r19= 3.4980  
a19= 122.29  
d19= 46.41  
r20= 1.3262  
a20= 74.96  
d20= 286.53  
r21= 2.4633  
a21= 73.92  
d21= 20.76  
r22= 1.3431  
a22= 92.54  
d22= 353.65  
r23= 1.4519  
a23= 33.44  
d23= 42.91  
r24= 1.4594  
a24= 114.68  
d24= 34.68  
r25= 1.4551  
a25= 114.30  
d25= 46.25  
r26= 2.0285  
a26= 116.84  
d26= 323.46  
r27= 1.1027  
a27= 111.11  
d27= 49.99  
r28= 1.1013  
a28= 112.21  
d28= 288.90  
r29= 1.0955  
a29= 144.52  
d29= 327.15  
r30= 1.1005  
a30= 109.70  
d30= 150.15  
r31= 1.1142

a31= 93.66  
d31= 96.60  
r32= 1.1000  
a32= 112.75  
d32= 30.70  
r33= 1.1001  
a33= 91.52  
d33= 204.53  
r34= 1.0582  
a34= 10.76  
d34= 100.10  
r35= 0.9644  
a35= 110.56  
d35= 29.29  
r36= 1.1002  
a36= 106.04  
d36= 154.07  
r37= 1.1043  
a37= 108.44  
d37= 6.59  
r38= 1.1101  
a38= 108.43  
d38= 267.95  
r39= 1.1009  
a39= 109.45  
d39= 165.84  
r40= 1.0963  
a40= 111.83  
d40= 45.41  
r41= 1.1020  
a41= 112.34  
d41= 284.26  
r42= 1.1140  
a42= 106.56  
d42= 211.81  
r43= 1.1002  
a43= 109.41  
d43= 325.20  
r44= 1.0968  
a44= 81.56  
d44= 259.58  
r45= 1.1165  
a45= 101.32  
d45= 155.37

r46= 1.0991  
a46= 83.91  
d46= 223.19  
r47= 1.0928  
a47= 119.71  
d47= 55.04  
r48= 1.1010  
a48= 106.51  
d48= 287.21  
r49= 1.1113  
a49= 107.93  
d49= 172.35  
r50= 1.1101  
a50= 103.49  
d50= 195.27  
r51= 1.0983  
a51= 146.60  
d51= 39.58  
r52= 1.0923  
a52= 119.74  
d52= 181.45  
r53= 1.1000  
a53= 108.35  
d53= 86.99  
r54= 1.1133  
a54= 106.65  
d54= 200.05  
r55= 1.0984  
a55= 112.08  
d55= 320.91  
r56= 1.1001  
a56= 108.95  
d56= 201.70  
r57= 1.1027  
a57= 112.32  
d57= 83.82  
r58= 1.1010  
a58= 110.41  
d58= 168.84  
r59= 1.0932  
a59= 120.62  
d59= 180.14  
r60= 1.1037  
a60= 111.38

d60= 268.71  
r61= 2.2857  
a61= 155.20  
d61= 5.39  
r62= 0.9643  
a62= 138.00  
d62= 93.82  
r63= 0.9879  
a63= 93.29  
d63= 337.91

Geometry and energy of **1** + HO<sub>2</sub><sup>-</sup> structure in z-matrix format.  
Energy = -1423.492007 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 2 r5 1 a5 3 d5  
C 3 r6 2 a6 1 d6  
C 1 r7 2 a7 3 d7  
C 7 r8 1 a8 2 d8  
C 1 r9 2 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 4 r11 2 a11 1 d11  
C 4 r12 2 a12 1 d12  
C 8 r13 7 a13 1 d13  
C 9 r14 1 a14 2 d14  
C 3 r15 2 a15 1 d15  
C 10 r16 2 a16 1 d16  
C 8 r17 7 a17 1 d17  
C 9 r18 1 a18 2 d18  
O 14 r19 9 a19 1 d19  
O 19 r20 14 a20 9 d20  
O 19 r21 14 a21 9 d21  
N 2 r22 1 a22 3 d22  
N 8 r23 7 a23 1 d23  
N 5 r24 2 a24 1 d24  
N 11 r25 4 a25 2 d25  
C 21 r26 19 a26 14 d26

H 15 r27 3 a27 2 d27  
H 15 r28 3 a28 2 d28  
H 17 r29 8 a29 7 d29  
H 18 r30 9 a30 1 d30  
H 17 r31 8 a31 7 d31  
H 18 r32 9 a32 1 d32  
H 17 r33 8 a33 7 d33  
H 19 r34 14 a34 9 d34  
H 21 r35 19 a35 14 d35  
H 5 r36 2 a36 1 d36  
H 3 r37 2 a37 1 d37  
H 5 r38 2 a38 1 d38  
H 6 r39 3 a39 2 d39  
H 6 r40 3 a40 2 d40  
H 6 r41 3 a41 2 d41  
H 7 r42 1 a42 2 d42  
H 7 r43 1 a43 2 d43  
H 8 r44 7 a44 1 d44  
H 8 r45 7 a45 1 d45  
H 9 r46 1 a46 2 d46  
H 10 r47 2 a47 1 d47  
H 11 r48 4 a48 2 d48  
H 11 r49 4 a49 2 d49  
H 1 r50 2 a50 3 d50  
H 1 r51 2 a51 3 d51  
H 12 r52 4 a52 2 d52  
H 13 r53 8 a53 7 d53  
H 13 r54 8 a54 7 d54  
H 14 r55 9 a55 1 d55  
H 14 r56 9 a56 1 d56  
H 14 r57 9 a57 1 d57  
H 15 r58 3 a58 2 d58  
H 16 r59 10 a59 2 d59  
H 18 r60 9 a60 1 d60  
O 29 r61 17 a61 8 d61  
H 61 r62 29 a62 17 d62  
H 61 r63 29 a63 17 d63

Variables:

r2= 3.2723

r3= 5.4795

a3= 84.56

r4= 2.3272

a4= 114.82

d4= 16.92

r5= 1.5209  
a5= 45.35  
d5= 227.13  
r6= 1.5315  
a6= 90.03  
d6= 255.45  
r7= 1.5356  
a7= 73.99  
d7= 296.89  
r8= 2.4428  
a8= 142.48  
d8= 62.12  
r9= 2.4651  
a9= 80.07  
d9= 93.69  
r10= 1.3994  
a10= 129.46  
d10= 131.27  
r11= 1.5153  
a11= 147.44  
d11= 319.07  
r12= 1.3959  
a12= 91.60  
d12= 135.52  
r13= 1.5399  
a13= 145.82  
d13= 13.43  
r14= 1.5286  
a14= 144.24  
d14= 332.39  
r15= 1.5384  
a15= 131.38  
d15= 136.91  
r16= 1.3932  
a16= 119.45  
d16= 234.84  
r17= 2.4297  
a17= 59.93  
d17= 72.13  
r18= 1.5350  
a18= 97.06  
d18= 114.84  
r19= 3.1535  
a19= 96.93

d19= 265.08  
r20= 1.3155  
a20= 83.91  
d20= 309.81  
r21= 2.4827  
a21= 79.06  
d21= 58.46  
r22= 1.3469  
a22= 92.87  
d22= 355.06  
r23= 1.4609  
a23= 33.52  
d23= 41.98  
r24= 1.4523  
a24= 114.53  
d24= 35.02  
r25= 1.4555  
a25= 113.64  
d25= 41.26  
r26= 1.9477  
a26= 125.27  
d26= 14.58  
r27= 1.1016  
a27= 111.04  
d27= 47.60  
r28= 1.1014  
a28= 112.00  
d28= 286.71  
r29= 1.0951  
a29= 144.32  
d29= 331.63  
r30= 1.1009  
a30= 109.89  
d30= 146.72  
r31= 1.1121  
a31= 91.63  
d31= 98.50  
r32= 1.1007  
a32= 112.13  
d32= 27.37  
r33= 1.0988  
a33= 93.02  
d33= 207.37  
r34= 1.0747



a34= 79.30  
d34= 59.18  
r35= 0.9647  
a35= 109.54  
d35= 160.34  
r36= 1.1006  
a36= 106.40  
d36= 155.16  
r37= 1.1039  
a37= 106.61  
d37= 2.92  
r38= 1.1104  
a38= 108.28  
d38= 268.46  
r39= 1.1021  
a39= 109.41  
d39= 160.98  
r40= 1.0989  
a40= 110.88  
d40= 41.06  
r41= 1.1015  
a41= 112.36  
d41= 279.26  
r42= 1.1114  
a42= 107.73  
d42= 210.02  
r43= 1.1008  
a43= 109.43  
d43= 324.57  
r44= 1.0975  
a44= 81.95  
d44= 260.27  
r45= 1.1140  
a45= 100.22  
d45= 155.39  
r46= 1.0961  
a46= 83.03  
d46= 222.82  
r47= 1.0931  
a47= 119.49  
d47= 54.00  
r48= 1.1003  
a48= 106.83  
d48= 282.26

r49= 1.1107  
a49= 108.35  
d49= 167.41  
r50= 1.1113  
a50= 104.43  
d50= 193.40  
r51= 1.0996  
a51= 144.80  
d51= 38.38  
r52= 1.0915  
a52= 119.69  
d52= 181.83  
r53= 1.1006  
a53= 108.46  
d53= 83.69  
r54= 1.1110  
a54= 106.91  
d54= 197.27  
r55= 1.0995  
a55= 110.84  
d55= 323.88  
r56= 1.0985  
a56= 109.13  
d56= 205.68  
r57= 1.1035  
a57= 112.72  
d57= 86.15  
r58= 1.1016  
a58= 110.47  
d58= 166.74  
r59= 1.0919  
a59= 120.76  
d59= 179.78  
r60= 1.1045  
a60= 111.57  
d60= 265.77  
r61= 2.2177  
a61= 150.96  
d61= 282.87  
r62= 0.9720  
a62= 169.99  
d62= 45.44  
r63= 0.9882  
a63= 72.90

d63= 4.16

Geometry and energy of **1D** structure in z-matrix format.

Energy = -1423.510398 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 2 r5 1 a5 3 d5  
C 3 r6 2 a6 1 d6  
C 1 r7 2 a7 3 d7  
C 7 r8 1 a8 2 d8  
C 1 r9 2 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 4 r11 2 a11 1 d11  
C 4 r12 2 a12 1 d12  
C 8 r13 7 a13 1 d13  
C 9 r14 1 a14 2 d14  
C 3 r15 2 a15 1 d15  
C 10 r16 2 a16 1 d16  
C 8 r17 7 a17 1 d17  
C 9 r18 1 a18 2 d18  
O 6 r19 3 a19 2 d19  
O 19 r20 6 a20 3 d20  
O 19 r21 6 a21 3 d21  
N 2 r22 1 a22 3 d22  
N 17 r23 8 a23 7 d23  
N 5 r24 2 a24 1 d24  
N 11 r25 4 a25 2 d25  
C 20 r26 19 a26 6 d26  
H 15 r27 3 a27 2 d27  
H 15 r28 3 a28 2 d28  
H 17 r29 8 a29 7 d29  
H 18 r30 9 a30 1 d30  
H 17 r31 8 a31 7 d31  
H 18 r32 9 a32 1 d32  
H 17 r33 8 a33 7 d33  
H 19 r34 6 a34 3 d34  
H 21 r35 19 a35 6 d35  
H 5 r36 2 a36 1 d36

H 3 r37 2 a37 1 d37  
H 5 r38 2 a38 1 d38  
H 6 r39 3 a39 2 d39  
H 6 r40 3 a40 2 d40  
H 6 r41 3 a41 2 d41  
H 7 r42 1 a42 2 d42  
H 7 r43 1 a43 2 d43  
H 8 r44 7 a44 1 d44  
H 8 r45 7 a45 1 d45  
H 9 r46 1 a46 2 d46  
H 10 r47 2 a47 1 d47  
H 11 r48 4 a48 2 d48  
H 11 r49 4 a49 2 d49  
H 1 r50 2 a50 3 d50  
H 1 r51 2 a51 3 d51  
H 12 r52 4 a52 2 d52  
H 13 r53 8 a53 7 d53  
H 13 r54 8 a54 7 d54  
H 14 r55 9 a55 1 d55  
H 14 r56 9 a56 1 d56  
H 14 r57 9 a57 1 d57  
H 15 r58 3 a58 2 d58  
H 16 r59 10 a59 2 d59  
H 18 r60 9 a60 1 d60  
O 29 r61 17 a61 8 d61  
H 61 r62 29 a62 17 d62  
H 61 r63 29 a63 17 d63

Variables:

r2= 3.3057  
r3= 5.5623  
a3= 84.46  
r4= 2.3384  
a4= 114.56  
d4= 14.64  
r5= 1.5225  
a5= 44.02  
d5= 223.87  
r6= 1.5280  
a6= 93.67  
d6= 254.72  
r7= 1.5278  
a7= 73.81  
d7= 300.10  
r8= 2.4184

a8= 144.51  
d8= 60.10  
r9= 2.4507  
a9= 80.11  
d9= 97.67  
r10= 1.4030  
a10= 136.65  
d10= 136.04  
r11= 1.5163  
a11= 146.63  
d11= 320.31  
r12= 1.3973  
a12= 91.55  
d12= 144.30  
r13= 1.5335  
a13= 147.95  
d13= 16.51  
r14= 1.5283  
a14= 144.89  
d14= 326.65  
r15= 1.5390  
a15= 128.70  
d15= 134.49  
r16= 1.3926  
a16= 118.91  
d16= 230.64  
r17= 2.4271  
a17= 60.29  
d17= 72.74  
r18= 1.5373  
a18= 97.31  
d18= 111.38  
r19= 3.2824  
a19= 119.38  
d19= 29.97  
r20= 1.4581  
a20= 75.39  
d20= 314.25  
r21= 2.6795  
a21= 76.05  
d21= 37.34  
r22= 1.3346  
a22= 90.01  
d22= 358.20

r23= 1.4696  
a23= 34.47  
d23= 326.88  
r24= 1.4537  
a24= 116.00  
d24= 35.56  
r25= 1.4583  
a25= 114.92  
d25= 44.38  
r26= 1.9234  
a26= 112.66  
d26= 79.79  
r27= 1.1011  
a27= 110.16  
d27= 169.10  
r28= 1.1025  
a28= 110.97  
d28= 50.55  
r29= 1.0937  
a29= 145.14  
d29= 329.24  
r30= 1.1012  
a30= 110.00  
d30= 144.12  
r31= 1.1091  
a31= 90.30  
d31= 95.59  
r32= 1.1018  
a32= 112.46  
d32= 24.58  
r33= 1.0979  
a33= 92.40  
d33= 204.49  
r34= 0.9880  
a34= 84.21  
d34= 56.40  
r35= 0.9664  
a35= 107.71  
d35= 29.19  
r36= 1.1008  
a36= 105.18  
d36= 155.50  
r37= 1.1052  
a37= 106.86

d37= 3.60  
r38= 1.1103  
a38= 108.16  
d38= 268.23  
r39= 1.1022  
a39= 108.64  
d39= 163.77  
r40= 1.0961  
a40= 113.00  
d40= 42.50  
r41= 1.1023  
a41= 111.87  
d41= 281.36  
r42= 1.1077  
a42= 108.43  
d42= 207.74  
r43= 1.1001  
a43= 109.41  
d43= 322.87  
r44= 1.0961  
a44= 81.95  
d44= 261.80  
r45= 1.1106  
a45= 96.76  
d45= 156.49  
r46= 1.0991  
a46= 81.14  
d46= 219.01  
r47= 1.0922  
a47= 119.88  
d47= 50.52  
r48= 1.1016  
a48= 104.61  
d48= 287.45  
r49= 1.1099  
a49= 108.34  
d49= 171.55  
r50= 1.1117  
a50= 104.17  
d50= 196.78  
r51= 1.0983  
a51= 145.20  
d51= 41.83  
r52= 1.0913

a52= 119.98  
d52= 180.35  
r53= 1.0996  
a53= 108.51  
d53= 85.64  
r54= 1.1109  
a54= 107.07  
d54= 199.31  
r55= 1.0970  
a55= 112.16  
d55= 321.46  
r56= 1.1011  
a56= 108.82  
d56= 201.08  
r57= 1.1033  
a57= 112.45  
d57= 83.22  
r58= 1.1016  
a58= 112.75  
d58= 289.20  
r59= 1.0934  
a59= 120.36  
d59= 179.81  
r60= 1.1039  
a60= 111.55  
d60= 262.91  
r61= 2.1964  
a61= 159.01  
d61= 300.51  
r62= 0.9642  
a62= 164.01  
d62= 263.60  
r63= 1.0075  
a63= 72.95  
d63= 347.28

Geometry and energy of **1** + H<sub>2</sub>O<sub>2</sub> structure in z-matrix format.  
Energy = -1499.849477 Hartrees

Geometry:  
C



C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 2 r5 1 a5 3 d5  
C 3 r6 2 a6 1 d6  
C 1 r7 2 a7 3 d7  
C 7 r8 1 a8 2 d8  
C 1 r9 2 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 4 r11 2 a11 1 d11  
C 4 r12 2 a12 1 d12  
C 8 r13 7 a13 1 d13  
C 9 r14 1 a14 2 d14  
C 3 r15 2 a15 1 d15  
C 12 r16 4 a16 2 d16  
C 8 r17 7 a17 1 d17  
C 9 r18 1 a18 2 d18  
O 6 r19 3 a19 2 d19  
O 19 r20 6 a20 3 d20  
O 20 r21 19 a21 6 d21  
N 4 r22 2 a22 1 d22  
N 7 r23 1 a23 2 d23  
N 5 r24 2 a24 1 d24  
N 11 r25 4 a25 2 d25  
C 21 r26 20 a26 19 d26  
H 15 r27 3 a27 2 d27  
H 15 r28 3 a28 2 d28  
H 17 r29 8 a29 7 d29  
H 18 r30 9 a30 1 d30  
H 17 r31 8 a31 7 d31  
H 18 r32 9 a32 1 d32  
H 17 r33 8 a33 7 d33  
H 19 r34 6 a34 3 d34  
H 20 r35 19 a35 6 d35  
H 5 r36 2 a36 1 d36  
H 3 r37 2 a37 1 d37  
H 5 r38 2 a38 1 d38  
H 6 r39 3 a39 2 d39  
H 6 r40 3 a40 2 d40  
H 6 r41 3 a41 2 d41  
H 7 r42 1 a42 2 d42  
H 7 r43 1 a43 2 d43  
H 8 r44 7 a44 1 d44  
H 8 r45 7 a45 1 d45

H 9 r46 1 a46 2 d46  
H 10 r47 2 a47 1 d47  
H 11 r48 4 a48 2 d48  
H 11 r49 4 a49 2 d49  
H 1 r50 2 a50 3 d50  
H 1 r51 2 a51 3 d51  
H 12 r52 4 a52 2 d52  
H 13 r53 8 a53 7 d53  
H 13 r54 8 a54 7 d54  
H 14 r55 9 a55 1 d55  
H 14 r56 9 a56 1 d56  
H 14 r57 9 a57 1 d57  
H 15 r58 3 a58 2 d58  
H 16 r59 12 a59 4 d59  
H 18 r60 9 a60 1 d60  
O 37 r61 3 a61 2 d61  
H 61 r62 37 a62 3 d62  
H 21 r63 20 a63 19 d63  
O 34 r64 19 a64 6 d64  
H 64 r65 34 a65 19 d65  
H 64 r66 34 a66 19 d66

Variables:

r2= 3.2250  
r3= 5.3183  
a3= 85.42  
r4= 2.3343  
a4= 111.79  
d4= 26.73  
r5= 1.5121  
a5= 46.54  
d5= 238.07  
r6= 1.5245  
a6= 81.80  
d6= 242.37  
r7= 1.5419  
a7= 77.68  
d7= 293.50  
r8= 2.4908  
a8= 139.21  
d8= 71.69  
r9= 2.4829  
a9= 80.69  
d9= 83.16  
r10= 1.3958

a10= 132.77  
d10= 141.01  
r11= 1.5082  
a11= 146.68  
d11= 316.65  
r12= 1.3990  
a12= 91.39  
d12= 137.88  
r13= 1.5376  
a13= 138.72  
d13= 358.80  
r14= 1.5283  
a14= 144.51  
d14= 339.18  
r15= 1.5322  
a15= 133.26  
d15= 130.32  
r16= 1.3948  
a16= 118.94  
d16= 0.45  
r17= 2.4269  
a17= 59.40  
d17= 67.44  
r18= 1.5321  
a18= 94.53  
d18= 117.01  
r19= 3.2728  
a19= 118.44  
d19= 74.12  
r20= 1.4467  
a20= 128.81  
d20= 359.03  
r21= 2.5609  
a21= 95.41  
d21= 337.78  
r22= 1.3417  
a22= 29.68  
d22= 316.88  
r23= 1.4607  
a23= 112.02  
d23= 92.17  
r24= 1.4604  
a24= 112.87  
d24= 35.44

r25= 1.4643  
a25= 113.98  
d25= 21.81  
r26= 1.8165  
a26= 118.83  
d26= 322.21  
r27= 1.1006  
a27= 112.40  
d27= 275.10  
r28= 1.1011  
a28= 108.90  
d28= 156.66  
r29= 1.0946  
a29= 143.70  
d29= 323.87  
r30= 1.1004  
a30= 109.50  
d30= 149.89  
r31= 1.1094  
a31= 93.57  
d31= 95.26  
r32= 1.1013  
a32= 112.69  
d32= 30.39  
r33= 1.0994  
a33= 90.48  
d33= 206.67  
r34= 0.9917  
a34= 53.03  
d34= 68.73  
r35= 1.0168  
a35= 99.36  
d35= 335.75  
r36= 1.1006  
a36= 106.68  
d36= 154.83  
r37= 1.0991  
a37= 108.76  
d37= 349.14  
r38= 1.1070  
a38= 109.31  
d38= 269.37  
r39= 1.0991  
a39= 108.67

d39= 159.14  
r40= 1.0997  
a40= 111.08  
d40= 42.20  
r41= 1.1045  
a41= 113.24  
d41= 278.89  
r42= 1.1096  
a42= 107.53  
d42= 215.26  
r43= 1.1000  
a43= 110.09  
d43= 330.69  
r44= 1.1014  
a44= 81.28  
d44= 247.52  
r45= 1.1091  
a45= 106.01  
d45= 143.06  
r46= 1.0986  
a46= 85.15  
d46= 227.15  
r47= 1.0918  
a47= 119.93  
d47= 56.82  
r48= 1.1009  
a48= 106.26  
d48= 262.02  
r49= 1.1065  
a49= 109.20  
d49= 148.09  
r50= 1.1077  
a50= 98.26  
d50= 186.82  
r51= 1.0970  
a51= 149.94  
d51= 39.22  
r52= 1.0912  
a52= 119.75  
d52= 181.04  
r53= 1.1014  
a53= 109.85  
d53= 74.43  
r54= 1.1076

a54= 107.75  
d54= 192.55  
r55= 1.0996  
a55= 112.00  
d55= 321.46  
r56= 1.0972  
a56= 109.10  
d56= 205.61  
r57= 1.1037  
a57= 112.59  
d57= 85.52  
r58= 1.1050  
a58= 112.61  
d58= 37.88  
r59= 1.0931  
a59= 120.39  
d59= 180.20  
r60= 1.1035  
a60= 111.57  
d60= 268.43  
r61= 1.9276  
a61= 159.41  
d61= 21.26  
r62= 0.9666  
a62= 152.26  
d62= 149.63  
r63= 1.0300  
a63= 104.86  
d63= 85.68  
r64= 1.7777  
a64= 154.64  
d64= 230.41  
r65= 0.9689  
a65= 81.79  
d65= 330.93  
r66= 1.0162  
a66= 114.15  
d66= 70.64

Geometry and energy of  $\mathbf{2} + \text{O}_2^-$  structure in z-matrix format.  
Energy = -1111.395403 Hartrees

Geometry:

N  
N 1 r2  
N 1 r3 2 a3  
N 1 r4 2 a4 3 d4  
C 3 r5 1 a5 2 d5  
C 1 r6 2 a6 3 d6  
C 1 r7 2 a7 3 d7  
C 3 r8 1 a8 2 d8  
C 2 r9 1 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 6 r11 1 a11 2 d11  
C 4 r12 1 a12 2 d12  
C 7 r13 1 a13 2 d13  
C 4 r14 1 a14 2 d14  
C 11 r15 6 a15 1 d15  
C 2 r16 1 a16 3 d16  
O 3 r17 1 a17 2 d17  
C 1 r18 2 a18 3 d18  
H 16 r19 2 a19 1 d19  
H 16 r20 2 a20 1 d20  
H 16 r21 2 a21 1 d21  
H 17 r22 3 a22 1 d22  
H 17 r23 3 a23 1 d23  
H 8 r24 3 a24 1 d24  
H 8 r25 3 a25 1 d25  
H 9 r26 2 a26 1 d26  
H 9 r27 2 a27 1 d27  
H 10 r28 2 a28 1 d28  
H 10 r29 2 a29 1 d29  
H 11 r30 6 a30 1 d30  
H 12 r31 4 a31 1 d31  
H 12 r32 4 a32 1 d32  
H 5 r33 3 a33 1 d33  
H 5 r34 3 a34 1 d34  
H 13 r35 7 a35 1 d35  
H 14 r36 4 a36 1 d36  
H 14 r37 4 a37 1 d37  
H 15 r38 11 a38 6 d38  
H 4 r39 1 a39 2 d39  
H 3 r40 1 a40 2 d40  
O 22 r41 17 a41 3 d41  
O 41 r42 22 a42 17 d42  
Variables:  
r2= 3.4182

r3= 2.6836  
a3= 55.68  
r4= 2.6843  
a4= 55.70  
d4= 136.17  
r5= 1.4973  
a5= 119.44  
d5= 320.63  
r6= 1.3411  
a6= 109.34  
d6= 316.72  
r7= 1.3427  
a7= 109.31  
d7= 179.44  
r8= 1.4982  
a8= 63.06  
d8= 213.73  
r9= 1.4890  
a9= 83.20  
d9= 54.64  
r10= 1.4891  
a10= 83.24  
d10= 169.19  
r11= 1.3950  
a11= 119.96  
d11= 227.02  
r12= 1.4963  
a12= 63.07  
d12= 146.27  
r13= 1.3949  
a13= 119.98  
d13= 133.04  
r14= 1.4992  
a14= 119.40  
d14= 39.39  
r15= 1.4008  
a15= 118.29  
d15= 0.75  
r16= 1.4805  
a16= 150.32  
d16= 291.91  
r17= 3.2193  
a17= 78.93  
d17= 74.31



r18= 1.9731  
a18= 35.40  
d18= 68.06  
r19= 1.0980  
a19= 110.60  
d19= 59.77  
r20= 1.1041  
a20= 110.98  
d20= 180.02  
r21= 1.0979  
a21= 110.54  
d21= 300.23  
r22= 0.9706  
a22= 115.35  
d22= 81.59  
r23= 0.9699  
a23= 119.77  
d23= 210.22  
r24= 1.1035  
a24= 107.93  
d24= 249.67  
r25= 1.1012  
a25= 110.60  
d25= 133.72  
r26= 1.1053  
a26= 111.22  
d26= 164.71  
r27= 1.0998  
a27= 108.18  
d27= 47.95  
r28= 1.1000  
a28= 108.18  
d28= 312.14  
r29= 1.1046  
a29= 111.33  
d29= 195.34  
r30= 1.0915  
a30= 120.89  
d30= 180.29  
r31= 1.1023  
a31= 107.95  
d31= 110.30  
r32= 1.1032  
a32= 110.67

d32= 226.30  
r33= 1.1015  
a33= 110.71  
d33= 256.01  
r34= 1.1002  
a34= 107.08  
d34= 140.24  
r35= 1.0913  
a35= 120.93  
d35= 179.65  
r36= 1.1006  
a36= 107.08  
d36= 219.77  
r37= 1.1005  
a37= 110.69  
d37= 104.05  
r38= 1.0944  
a38= 119.78  
d38= 180.04  
r39= 1.0203  
a39= 131.21  
d39= 236.49  
r40= 1.0207  
a40= 131.21  
d40= 123.61  
r41= 1.9792  
a41= 112.45  
d41= 311.61  
r42= 1.2037  
a42= 145.54  
d42= 274.25

Geometry and energy of **2A** structure in z-matrix format.  
Energy = -1111.435292 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
N 3 r4 2 a4 1 d4

C 4 r5 3 a5 2 d5  
C 5 r6 4 a6 3 d6  
C 4 r7 3 a7 2 d7  
O 7 r8 4 a8 3 d8  
C 3 r9 2 a9 1 d9  
N 9 r10 3 a10 2 d10  
C 10 r11 9 a11 3 d11  
C 11 r12 10 a12 9 d12  
N 12 r13 11 a13 10 d13  
C 13 r14 12 a14 11 d14  
C 5 r15 4 a15 3 d15  
N 15 r16 5 a16 4 d16  
C 16 r17 15 a17 5 d17  
C 13 r18 12 a18 11 d18  
O 7 r19 4 a19 3 d19  
O 19 r20 7 a20 4 d20  
H 8 r21 7 a21 4 d21  
H 8 r22 7 a22 4 d22  
H 16 r23 15 a23 5 d23  
H 14 r24 13 a24 12 d24  
H 14 r25 13 a25 12 d25  
H 14 r26 13 a26 12 d26  
H 9 r27 3 a27 2 d27  
H 9 r28 3 a28 2 d28  
H 12 r29 11 a29 10 d29  
H 12 r30 11 a30 10 d30  
H 18 r31 13 a31 12 d31  
H 18 r32 13 a32 12 d32  
H 2 r33 1 a33 3 d33  
H 15 r34 5 a34 4 d34  
H 15 r35 5 a35 4 d35  
H 11 r36 10 a36 9 d36  
H 11 r37 10 a37 9 d37  
H 6 r38 5 a38 4 d38  
H 17 r39 16 a39 15 d39  
H 17 r40 16 a40 15 d40  
H 1 r41 2 a41 3 d41  
H 10 r42 9 a42 3 d42

Variables:

r2= 1.3966

r3= 1.3980

a3= 118.60

r4= 1.3374

a4= 120.66

d4= 359.55  
r5= 1.3365  
a5= 121.77  
d5= 0.93  
r6= 1.3970  
a6= 120.84  
d6= 359.06  
r7= 2.1085  
a7= 119.28  
d7= 185.35  
r8= 2.1154  
a8= 165.37  
d8= 316.44  
r9= 1.5227  
a9= 122.40  
d9= 176.76  
r10= 1.4618  
a10= 113.74  
d10= 157.83  
r11= 1.4660  
a11= 116.95  
d11= 272.13  
r12= 1.5303  
a12= 112.16  
d12= 79.34  
r13= 1.4829  
a13= 112.93  
d13= 57.77  
r14= 1.4753  
a14= 110.97  
d14= 77.40  
r15= 1.5214  
a15= 116.41  
d15= 176.49  
r16= 1.4661  
a16= 113.62  
d16= 27.85  
r17= 1.4685  
a17= 116.54  
d17= 84.72  
r18= 1.4824  
a18= 111.64  
d18= 202.00  
r19= 2.0069

a19= 86.28  
d19= 265.34  
r20= 1.2832  
a20= 116.25  
d20= 163.28  
r21= 1.0019  
a21= 95.18  
d21= 312.78  
r22= 0.9666  
a22= 122.48  
d22= 200.00  
r23= 1.0161  
a23= 109.16  
d23= 210.32  
r24= 1.0956  
a24= 109.98  
d24= 300.84  
r25= 1.1058  
a25= 111.21  
d25= 62.23  
r26= 1.0978  
a26= 109.98  
d26= 182.53  
r27= 1.1025  
a27= 106.69  
d27= 276.47  
r28= 1.1066  
a28= 109.24  
d28= 31.35  
r29= 1.1059  
a29= 109.50  
d29= 181.47  
r30= 1.0986  
a30= 109.16  
d30= 298.03  
r31= 1.0984  
a31= 107.65  
d31= 38.81  
r32= 1.1056  
a32= 110.78  
d32= 282.30  
r33= 1.0923  
a33= 121.03  
d33= 180.05

r34= 1.1021  
a34= 106.79  
d34= 269.62  
r35= 1.1061  
a35= 109.47  
d35= 154.15  
r36= 1.1072  
a36= 112.19  
d36= 317.60  
r37= 1.0994  
a37= 107.56  
d37= 200.52  
r38= 1.0922  
a38= 120.40  
d38= 180.52  
r39= 1.0997  
a39= 107.72  
d39= 156.39  
r40= 1.1065  
a40= 112.07  
d40= 39.61  
r41= 1.0928  
a41= 120.19  
d41= 179.78  
r42= 1.0157  
a42= 110.25  
d42= 144.92

Geometry and energy of **2B** structure in z-matrix format.  
Energy = -1111.395403 Hartrees

Geometry:

N  
N 1 r2  
N 1 r3 2 a3  
N 1 r4 2 a4 3 d4  
C 3 r5 1 a5 2 d5  
C 1 r6 2 a6 3 d6  
C 1 r7 2 a7 3 d7  
C 3 r8 1 a8 2 d8  
C 2 r9 1 a9 3 d9  
C 2 r10 1 a10 3 d10

C 6 r11 1 a11 2 d11  
C 4 r12 1 a12 2 d12  
C 7 r13 1 a13 2 d13  
C 4 r14 1 a14 2 d14  
C 11 r15 6 a15 1 d15  
C 2 r16 1 a16 3 d16  
O 3 r17 1 a17 2 d17  
C 1 r18 2 a18 3 d18  
H 16 r19 2 a19 1 d19  
H 16 r20 2 a20 1 d20  
H 16 r21 2 a21 1 d21  
H 17 r22 3 a22 1 d22  
H 17 r23 3 a23 1 d23  
H 8 r24 3 a24 1 d24  
H 8 r25 3 a25 1 d25  
H 9 r26 2 a26 1 d26  
H 9 r27 2 a27 1 d27  
H 10 r28 2 a28 1 d28  
H 10 r29 2 a29 1 d29  
H 11 r30 6 a30 1 d30  
H 12 r31 4 a31 1 d31  
H 12 r32 4 a32 1 d32  
H 5 r33 3 a33 1 d33  
H 5 r34 3 a34 1 d34  
H 13 r35 7 a35 1 d35  
H 14 r36 4 a36 1 d36  
H 14 r37 4 a37 1 d37  
H 15 r38 11 a38 6 d38  
H 4 r39 1 a39 2 d39  
H 3 r40 1 a40 2 d40  
O 22 r41 17 a41 3 d41  
O 41 r42 22 a42 17 d42

Variables:

r2= 3.4182

r3= 2.6836

a3= 55.68

r4= 2.6843

a4= 55.70

d4= 136.17

r5= 1.4973

a5= 119.44

d5= 320.63

r6= 1.3411

a6= 109.34

d6= 316.72  
r7= 1.3427  
a7= 109.31  
d7= 179.44  
r8= 1.4982  
a8= 63.06  
d8= 213.73  
r9= 1.4890  
a9= 83.20  
d9= 54.64  
r10= 1.4891  
a10= 83.24  
d10= 169.19  
r11= 1.3950  
a11= 119.96  
d11= 227.02  
r12= 1.4963  
a12= 63.07  
d12= 146.27  
r13= 1.3949  
a13= 119.98  
d13= 133.04  
r14= 1.4992  
a14= 119.40  
d14= 39.39  
r15= 1.4008  
a15= 118.29  
d15= 0.75  
r16= 1.4805  
a16= 150.32  
d16= 291.91  
r17= 3.2193  
a17= 78.93  
d17= 74.31  
r18= 1.9731  
a18= 35.40  
d18= 68.06  
r19= 1.0980  
a19= 110.60  
d19= 59.77  
r20= 1.1041  
a20= 110.98  
d20= 180.02  
r21= 1.0979



a21= 110.54  
d21= 300.23  
r22= 0.9706  
a22= 115.35  
d22= 81.59  
r23= 0.9699  
a23= 119.77  
d23= 210.22  
r24= 1.1035  
a24= 107.93  
d24= 249.67  
r25= 1.1012  
a25= 110.60  
d25= 133.72  
r26= 1.1053  
a26= 111.22  
d26= 164.71  
r27= 1.0998  
a27= 108.18  
d27= 47.95  
r28= 1.1000  
a28= 108.18  
d28= 312.14  
r29= 1.1046  
a29= 111.33  
d29= 195.34  
r30= 1.0915  
a30= 120.89  
d30= 180.29  
r31= 1.1023  
a31= 107.95  
d31= 110.30  
r32= 1.1032  
a32= 110.67  
d32= 226.30  
r33= 1.1015  
a33= 110.71  
d33= 256.01  
r34= 1.1002  
a34= 107.08  
d34= 140.24  
r35= 1.0913  
a35= 120.93  
d35= 179.65

r36= 1.1006  
a36= 107.08  
d36= 219.77  
r37= 1.1005  
a37= 110.69  
d37= 104.05  
r38= 1.0944  
a38= 119.78  
d38= 180.04  
r39= 1.0203  
a39= 131.21  
d39= 236.49  
r40= 1.0207  
a40= 131.21  
d40= 123.61  
r41= 1.9792  
a41= 112.45  
d41= 311.61  
r42= 1.2037  
a42= 145.54  
d42= 274.25

Geometry and energy of **2C'** structure in z-matrix format.  
Energy = -1187.927442 Hartrees

Geometry:

N  
N 1 r2  
N 1 r3 2 a3  
N 1 r4 2 a4 3 d4  
C 3 r5 1 a5 2 d5  
C 1 r6 2 a6 3 d6  
C 1 r7 2 a7 3 d7  
C 3 r8 1 a8 2 d8  
C 2 r9 1 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 6 r11 1 a11 2 d11  
C 4 r12 1 a12 2 d12  
C 7 r13 1 a13 2 d13  
C 4 r14 1 a14 2 d14  
C 11 r15 6 a15 1 d15  
C 2 r16 1 a16 3 d16  
O 3 r17 1 a17 2 d17

C 1 r18 2 a18 3 d18  
H 16 r19 2 a19 1 d19  
H 16 r20 2 a20 1 d20  
H 16 r21 2 a21 1 d21  
H 17 r22 3 a22 1 d22  
H 17 r23 3 a23 1 d23  
H 8 r24 3 a24 1 d24  
H 8 r25 3 a25 1 d25  
H 9 r26 2 a26 1 d26  
H 9 r27 2 a27 1 d27  
H 10 r28 2 a28 1 d28  
H 10 r29 2 a29 1 d29  
H 11 r30 6 a30 1 d30  
H 12 r31 4 a31 1 d31  
H 12 r32 4 a32 1 d32  
H 5 r33 3 a33 1 d33  
H 5 r34 3 a34 1 d34  
H 13 r35 7 a35 1 d35  
H 14 r36 4 a36 1 d36  
H 14 r37 4 a37 1 d37  
H 15 r38 11 a38 6 d38  
H 4 r39 1 a39 2 d39  
H 3 r40 1 a40 2 d40  
O 22 r41 17 a41 3 d41  
O 41 r42 22 a42 17 d42

Variables:

r2= 3.4182  
r3= 2.6836  
a3= 55.68  
r4= 2.6843  
a4= 55.70  
d4= 136.17  
r5= 1.4973  
a5= 119.44  
d5= 320.63  
r6= 1.3411  
a6= 109.34  
d6= 316.72  
r7= 1.3427  
a7= 109.31  
d7= 179.44  
r8= 1.4982  
a8= 63.06  
d8= 213.73

r9= 1.4890  
a9= 83.20  
d9= 54.64  
r10= 1.4891  
a10= 83.24  
d10= 169.19  
r11= 1.3950  
a11= 119.96  
d11= 227.02  
r12= 1.4963  
a12= 63.07  
d12= 146.27  
r13= 1.3949  
a13= 119.98  
d13= 133.04  
r14= 1.4992  
a14= 119.40  
d14= 39.39  
r15= 1.4008  
a15= 118.29  
d15= 0.75  
r16= 1.4805  
a16= 150.32  
d16= 291.91  
r17= 3.2193  
a17= 78.93  
d17= 74.31  
r18= 1.9731  
a18= 35.40  
d18= 68.06  
r19= 1.0980  
a19= 110.60  
d19= 59.77  
r20= 1.1041  
a20= 110.98  
d20= 180.02  
r21= 1.0979  
a21= 110.54  
d21= 300.23  
r22= 0.9706  
a22= 115.35  
d22= 81.59  
r23= 0.9699  
a23= 119.77

d23= 210.22  
r24= 1.1035  
a24= 107.93  
d24= 249.67  
r25= 1.1012  
a25= 110.60  
d25= 133.72  
r26= 1.1053  
a26= 111.22  
d26= 164.71  
r27= 1.0998  
a27= 108.18  
d27= 47.95  
r28= 1.1000  
a28= 108.18  
d28= 312.14  
r29= 1.1046  
a29= 111.33  
d29= 195.34  
r30= 1.0915  
a30= 120.89  
d30= 180.29  
r31= 1.1023  
a31= 107.95  
d31= 110.30  
r32= 1.1032  
a32= 110.67  
d32= 226.30  
r33= 1.1015  
a33= 110.71  
d33= 256.01  
r34= 1.1002  
a34= 107.08  
d34= 140.24  
r35= 1.0913  
a35= 120.93  
d35= 179.65  
r36= 1.1006  
a36= 107.08  
d36= 219.77  
r37= 1.1005  
a37= 110.69  
d37= 104.05  
r38= 1.0944

a38= 119.78  
d38= 180.04  
r39= 1.0203  
a39= 131.21  
d39= 236.49  
r40= 1.0207  
a40= 131.21  
d40= 123.61  
r41= 1.9792  
a41= 112.45  
d41= 311.61  
r42= 1.2037  
a42= 145.54  
d42= 274.25

Geometry and energy of **2C''** structure in z-matrix format.  
Energy = -1187.932518 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 1 r5 2 a5 3 d5  
C 5 r6 1 a6 2 d6  
C 2 r7 1 a7 3 d7  
C 3 r8 2 a8 1 d8  
C 3 r9 2 a9 1 d9  
C 6 r10 5 a10 1 d10  
C 9 r11 3 a11 2 d11  
C 6 r12 5 a12 1 d12  
O 12 r13 6 a13 5 d13  
O 13 r14 12 a14 6 d14  
O 13 r15 12 a15 6 d15  
N 2 r16 1 a16 3 d16  
N 12 r17 6 a17 5 d17  
N 4 r18 2 a18 1 d18  
H 18 r19 4 a19 2 d19  
N 8 r20 3 a20 2 d20  
H 20 r21 8 a21 3 d21  
C 14 r22 13 a22 12 d22  
H 12 r23 6 a23 5 d23  
H 12 r24 6 a24 5 d24

H 12 r25 6 a25 5 d25  
H 2 r26 1 a26 3 d26  
H 15 r27 13 a27 12 d27  
H 4 r28 2 a28 1 d28  
H 4 r29 2 a29 1 d29  
H 5 r30 1 a30 2 d30  
H 5 r31 1 a31 2 d31  
H 6 r32 5 a32 1 d32  
H 6 r33 5 a33 1 d33  
H 7 r34 2 a34 1 d34  
H 8 r35 3 a35 2 d35  
H 8 r36 3 a36 2 d36  
H 1 r37 2 a37 3 d37  
H 1 r38 2 a38 3 d38  
H 9 r39 3 a39 2 d39  
H 10 r40 6 a40 5 d40  
H 10 r41 6 a41 5 d41  
H 11 r42 9 a42 3 d42  
O 19 r43 18 a43 4 d43  
H 43 r44 19 a44 18 d44  
H 43 r45 19 a45 18 d45

Variables:

r2= 3.3185  
r3= 2.3301  
a3= 113.69  
r4= 1.5227  
a4= 45.69  
d4= 212.97  
r5= 1.5352  
a5= 77.18  
d5= 317.52  
r6= 2.4334  
a6= 142.40  
d6= 60.18  
r7= 1.3990  
a7= 128.85  
d7= 113.69  
r8= 1.5320  
a8= 147.73  
d8= 317.94  
r9= 1.4008  
a9= 91.10  
d9= 134.72  
r10= 1.5468

a10= 147.58  
d10= 14.50  
r11= 1.3955  
a11= 119.34  
d11= 0.31  
r12= 2.4351  
a12= 60.12  
d12= 71.38  
r13= 3.2838  
a13= 107.58  
d13= 251.27  
r14= 1.3294  
a14= 87.76  
d14= 20.76  
r15= 2.5917  
a15= 67.79  
d15= 129.74  
r16= 1.3410  
a16= 92.27  
d16= 338.54  
r17= 1.4644  
a17= 33.86  
d17= 329.41  
r18= 1.4572  
a18= 113.08  
d18= 33.07  
r19= 1.0305  
a19= 110.61  
d19= 142.66  
r20= 1.4368  
a20= 118.45  
d20= 43.89  
r21= 1.0192  
a21= 115.45  
d21= 273.74  
r22= 1.9130  
a22= 117.73  
d22= 39.48  
r23= 1.0959  
a23= 143.84  
d23= 328.14  
r24= 1.1115  
a24= 92.21  
d24= 96.76



r25= 1.0979  
a25= 92.65  
d25= 206.37  
r26= 5.5588  
a26= 41.68  
d26= 307.03  
r27= 0.9657  
a27= 106.36  
d27= 111.91  
r28= 1.1036  
a28= 107.57  
d28= 151.17  
r29= 1.1072  
a29= 109.37  
d29= 266.83  
r30= 1.1112  
a30= 108.67  
d30= 208.45  
r31= 1.1003  
a31= 108.64  
d31= 323.74  
r32= 1.0992  
a32= 82.03  
d32= 261.74  
r33= 1.1133  
a33= 97.89  
d33= 156.31  
r34= 1.0919  
a34= 120.14  
d34= 55.46  
r35= 1.1048  
a35= 106.99  
d35= 282.46  
r36= 1.1068  
a36= 107.10  
d36= 168.84  
r37= 1.1101  
a37= 100.86  
d37= 211.22  
r38= 1.0993  
a38= 145.74  
d38= 64.69  
r39= 1.0926  
a39= 119.77

d39= 181.41  
r40= 1.1025  
a40= 109.18  
d40= 81.71  
r41= 1.1073  
a41= 105.87  
d41= 194.88  
r42= 1.0930  
a42= 120.55  
d42= 180.48  
r43= 1.8686  
a43= 153.86  
d43= 246.26  
r44= 0.9686  
a44= 98.84  
d44= 34.22  
r45= 0.9903  
a45= 87.06  
d45= 292.44

Geometry and energy of **2C** structure in z-matrix format.  
Energy = -1187.942826 Hartrees

Geometry:

C  
C 1 r2  
C 2 r3 1 a3  
C 2 r4 1 a4 3 d4  
C 1 r5 2 a5 3 d5  
C 5 r6 1 a6 2 d6  
C 2 r7 1 a7 3 d7  
C 3 r8 2 a8 1 d8  
C 3 r9 2 a9 1 d9  
C 6 r10 5 a10 1 d10  
C 7 r11 2 a11 1 d11  
C 5 r12 1 a12 2 d12  
O 8 r13 3 a13 2 d13  
O 13 r14 8 a14 3 d14  
O 13 r15 8 a15 3 d15  
N 2 r16 1 a16 3 d16  
N 12 r17 5 a17 1 d17  
N 4 r18 2 a18 1 d18  
H 18 r19 4 a19 2 d19

N 8 r20 3 a20 2 d20  
H 20 r21 8 a21 3 d21  
C 14 r22 13 a22 8 d22  
H 12 r23 5 a23 1 d23  
H 12 r24 5 a24 1 d24  
H 12 r25 5 a25 1 d25  
H 13 r26 8 a26 3 d26  
H 15 r27 13 a27 8 d27  
H 4 r28 2 a28 1 d28  
H 4 r29 2 a29 1 d29  
H 5 r30 1 a30 2 d30  
H 5 r31 1 a31 2 d31  
H 6 r32 5 a32 1 d32  
H 6 r33 5 a33 1 d33  
H 7 r34 2 a34 1 d34  
H 8 r35 3 a35 2 d35  
H 8 r36 3 a36 2 d36  
H 1 r37 2 a37 3 d37  
H 1 r38 2 a38 3 d38  
H 9 r39 3 a39 2 d39  
H 10 r40 6 a40 5 d40  
H 10 r41 6 a41 5 d41  
H 11 r42 7 a42 2 d42  
O 19 r43 18 a43 4 d43  
H 43 r44 19 a44 18 d44  
H 43 r45 19 a45 18 d45

Variables:

r2= 3.3403

r3= 2.3347

a3= 112.90

r4= 1.5267

a4= 44.27

d4= 211.67

r5= 1.5406

a5= 78.32

d5= 319.39

r6= 2.4572

a6= 142.36

d6= 65.00

r7= 1.4001

a7= 138.16

d7= 121.05

r8= 1.5226

a8= 145.58

d8= 319.04  
r9= 1.3972  
a9= 91.58  
d9= 145.00  
r10= 1.5427  
a10= 143.59  
d10= 4.05  
r11= 1.3948  
a11= 118.70  
d11= 232.42  
r12= 2.4237  
a12= 102.52  
d12= 120.95  
r13= 3.4685  
a13= 106.32  
d13= 330.94  
r14= 1.4495  
a14= 65.04  
d14= 356.39  
r15= 2.6386  
a15= 96.17  
d15= 68.31  
r16= 1.3363  
a16= 87.91  
d16= 344.42  
r17= 1.4639  
a17= 34.55  
d17= 247.06  
r18= 1.4390  
a18= 113.99  
d18= 32.74  
r19= 1.0290  
a19= 113.56  
d19= 124.93  
r20= 1.4443  
a20= 113.95  
d20= 33.94  
r21= 1.0170  
a21= 112.38  
d21= 225.82  
r22= 1.9470  
a22= 102.83  
d22= 68.03  
r23= 1.0962

a23= 89.76  
d23= 14.41  
r24= 1.1096  
a24= 93.90  
d24= 123.57  
r25= 1.0971  
a25= 144.47  
d25= 254.24  
r26= 0.9908  
a26= 118.30  
d26= 82.99  
r27= 0.9629  
a27= 130.13  
d27= 88.18  
r28= 1.1037  
a28= 106.26  
d28= 151.27  
r29= 1.1097  
a29= 108.85  
d29= 265.55  
r30= 1.1088  
a30= 109.53  
d30= 210.95  
r31= 1.0999  
a31= 108.48  
d31= 327.05  
r32= 1.0991  
a32= 80.97  
d32= 255.02  
r33= 1.1094  
a33= 100.90  
d33= 149.57  
r34= 1.0928  
a34= 120.01  
d34= 52.35  
r35= 1.1012  
a35= 105.61  
d35= 277.38  
r36= 1.1099  
a36= 109.10  
d36= 161.35  
r37= 1.1107  
a37= 100.77  
d37= 213.81

r38= 1.1001  
a38= 147.12  
d38= 68.03  
r39= 1.0930  
a39= 120.09  
d39= 179.98  
r40= 1.0998  
a40= 109.78  
d40= 83.51  
r41= 1.1108  
a41= 107.21  
d41= 198.57  
r42= 1.0926  
a42= 120.29  
d42= 179.53  
r43= 1.9075  
a43= 149.22  
d43= 274.55  
r44= 0.9800  
a44= 100.72  
d44= 25.22  
r45= 0.9905  
a45= 88.73  
d45= 287.94

Geometry and energy of  $2 + \text{H}_2\text{O}_2$  structure in z-matrix format.  
Energy = -1264.296681 Hartrees

Geometry:

N  
N 1 r2  
N 1 r3 2 a3  
N 1 r4 2 a4 3 d4  
C 3 r5 1 a5 2 d5  
C 1 r6 2 a6 3 d6  
C 1 r7 2 a7 3 d7  
C 3 r8 1 a8 2 d8  
C 2 r9 1 a9 3 d9  
C 2 r10 1 a10 3 d10  
C 6 r11 1 a11 2 d11  
C 4 r12 1 a12 2 d12  
C 7 r13 1 a13 2 d13

C 4 r14 1 a14 2 d14  
C 13 r15 7 a15 1 d15  
C 2 r16 1 a16 3 d16  
O 4 r17 1 a17 2 d17  
O 16 r18 2 a18 1 d18  
O 18 r19 16 a19 2 d19  
O 17 r20 4 a20 1 d20  
O 17 r21 4 a21 1 d21  
C 18 r22 16 a22 2 d22  
H 16 r23 2 a23 1 d23  
H 16 r24 2 a24 1 d24  
H 16 r25 2 a25 1 d25  
H 17 r26 4 a26 1 d26  
H 8 r27 3 a27 1 d27  
H 8 r28 3 a28 1 d28  
H 9 r29 2 a29 1 d29  
H 9 r30 2 a30 1 d30  
H 10 r31 2 a31 1 d31  
H 10 r32 2 a32 1 d32  
H 11 r33 6 a33 1 d33  
H 12 r34 4 a34 1 d34  
H 12 r35 4 a35 1 d35  
H 5 r36 3 a36 1 d36  
H 5 r37 3 a37 1 d37  
H 13 r38 7 a38 1 d38  
H 14 r39 4 a39 1 d39  
H 14 r40 4 a40 1 d40  
H 15 r41 13 a41 7 d41  
H 19 r42 18 a42 16 d42  
H 18 r43 16 a43 2 d43  
H 20 r44 17 a44 4 d44  
H 19 r45 18 a45 16 d45  
H 21 r46 17 a46 4 d46  
H 3 r47 1 a47 2 d47  
H 4 r48 1 a48 2 d48

Variables:

r2= 3.1454

r3= 2.7302

a3= 60.60

r4= 2.7316

a4= 59.79

d4= 136.38

r5= 1.4609

a5= 111.71

d5= 324.99  
r6= 1.3384  
a6= 108.20  
d6= 314.54  
r7= 1.3400  
a7= 108.33  
d7= 180.61  
r8= 1.4527  
a8= 62.43  
d8= 213.77  
r9= 1.4613  
a9= 82.74  
d9= 53.33  
r10= 1.4664  
a10= 82.95  
d10= 169.08  
r11= 1.3965  
a11= 120.82  
d11= 234.77  
r12= 1.4496  
a12= 61.95  
d12= 148.84  
r13= 1.3990  
a13= 120.39  
d13= 125.43  
r14= 1.4544  
a14= 111.78  
d14= 37.60  
r15= 1.3958  
a15= 118.81  
d15= 0.22  
r16= 1.4669  
a16= 148.29  
d16= 291.10  
r17= 3.3240  
a17= 74.71  
d17= 232.81  
r18= 3.0595  
a18= 80.16  
d18= 6.33  
r19= 2.8415  
a19= 68.36  
d19= 246.07  
r20= 2.5244



a20= 51.39  
d20= 164.17  
r21= 1.4471  
a21= 79.91  
d21= 49.53  
r22= 1.8648  
a22= 73.71  
d22= 351.93  
r23= 1.0966  
a23= 109.72  
d23= 56.13  
r24= 1.1101  
a24= 111.10  
d24= 178.20  
r25= 1.0965  
a25= 110.05  
d25= 300.66  
r26= 1.0482  
a26= 54.47  
d26= 164.02  
r27= 1.1024  
a27= 107.99  
d27= 255.18  
r28= 1.1086  
a28= 112.97  
d28= 137.15  
r29= 1.1106  
a29= 111.72  
d29= 160.46  
r30= 1.1012  
a30= 108.24  
d30= 43.43  
r31= 1.1020  
a31= 107.91  
d31= 316.52  
r32= 1.1094  
a32= 111.37  
d32= 199.70  
r33= 1.0924  
a33= 120.21  
d33= 179.24  
r34= 1.1042  
a34= 106.32  
d34= 101.96

r35= 1.1090  
a35= 113.63  
d35= 220.75  
r36= 1.1092  
a36= 111.64  
d36= 249.35  
r37= 1.0984  
a37= 107.23  
d37= 132.28  
r38= 1.0917  
a38= 119.93  
d38= 180.54  
r39= 1.0989  
a39= 106.78  
d39= 224.06  
r40= 1.1105  
a40= 112.14  
d40= 106.86  
r41= 1.0927  
a41= 120.27  
d41= 180.49  
r42= 0.9650  
a42= 110.52  
d42= 238.41  
r43= 0.9784  
a43= 70.35  
d43= 234.79  
r44= 0.9651  
a44= 113.61  
d44= 123.75  
r45= 1.0263  
a45= 82.18  
d45= 135.51  
r46= 0.9981  
a46= 107.23  
d46= 85.43  
r47= 1.0147  
a47= 131.17  
d47= 116.69  
r48= 1.0593  
a48= 131.01  
d48= 241.50

## VI. QM/MM MD simulation in aqueous solution

**Table S6.** Distribution of Cu(II)-N and Cu(II)-O distances (Å) of complexes **1** and **2** along the QM/MM-MD trajectories. The variation between values for the two complexes ( $\Delta$ ) are shown.

Cmp.	Value	Distance ( Å )				
		Cu-N1	Cu-N2	Cu-N3	Cu-N4	Cu-O5
<b>1</b>	Mean	1.97 ± 0.13	2.28 ± 0.17	2.19 ± 0.15	2.16 ± 0.19	2.02 ± 0.12
<b>2</b>	Mean	1.97 ± 0.12	2.19 ± 0.16	2.08 ± 0.16	1.97 ± 0.19	2.04 ± 0.11
	$\Delta$	<b>0.00</b>	<b>-0.09</b>	<b>-0.11</b>	<b>-0.19</b>	<b>0.02</b>
<b>1</b>	Width	0.66	1.21	1.23	0.78	0.82
<b>2</b>	Width	0.63	0.99	0.44	0.52	0.64
	$\Delta$	<b>-0.03</b>	<b>-0.22</b>	<b>-0.79</b>	<b>-0.26</b>	<b>-0.18</b>

(\*\*) Difference btw. max and min value of the distribution.

**Table S7.** Distribution of Cu(I)-N and Cu(I)-O distances (Å) of complexes **1** and **2** along the QM/MM MD trajectories. The variation between values for the two complexes ( $\Delta$ ) are shown.

Cmp.	Value	Distance ( Å )				
		Cu-N1	Cu-N2	Cu-N3	Cu-N4	Cu-O5
<b>1</b>	Mean	1.99 ± 0.13	2.40 ± 0.17	2.21 ± 0.15	2.40 ± 0.19	2.11 ± 0.12
<b>2</b>	Mean	2.03 ± 0.12	2.30 ± 0.16	2.57 ± 0.16	2.03 ± 0.19	2.04 ± 0.11
	$\Delta$	<b>0.04</b>	<b>-0.10</b>	<b>0.36</b>	<b>-0.37</b>	<b>-0.07</b>
<b>1</b>	Width	0.75	1.31	0.82	1.31	0.95
<b>2</b>	Width	0.70	0.90	1.70	0.90	0.66
	$\Delta$	<b>-0.05</b>	<b>-0.41</b>	<b>0.88</b>	<b>-0.41</b>	<b>-0.29</b>

(\*\*) Difference btw. max and min value of the distribution.

**Table S8.** Distribution of Cu(II)-N and Cu(II)-O distances (Å) of complexes **1A** and **2A** along the QM/MM MD trajectories. The variation between values for the two complexes ( $\Delta$ ) are shown.

Cmp.	Value	Distance ( Å )				
		Cu-N1	Cu-N2	Cu-N3	Cu-N4	Cu-O5
<b>1</b>	Mean	2.02 ± 0.10	2.46 ± 0.20	2.21 ± 0.10	2.50 ± 0.23	2.12 ± 0.12
<b>2</b>	Mean	2.14 ± 0.13	2.33 ± 0.16	2.40 ± 0.16	2.45 ± 0.19	2.10 ± 0.11
	$\Delta$	<b>0.12</b>	<b>-0.13</b>	<b>0.19</b>	<b>-0.05</b>	<b>-0.02</b>
<b>1</b>	Width	0.56	1.30	0.65	1.50	0.86
<b>2</b>	Width	0.94	1.02	1.21	1.19	0.67
	$\Delta$	<b>0.38</b>	<b>-0.28</b>	<b>0.56</b>	<b>-0.31</b>	<b>-0.19</b>

**Table S9.** Distribution of Cu(I)-N and Cu(I)-O distances (Å) of complexes **1C** and **2C''** along the QM/MM MD trajectories. The variation between values for the two complexes ( $\Delta$ ) are shown.

Cmp.	Value	Distance ( Å )				
		<b>Cu-N1</b>	<b>Cu-N2</b>	<b>Cu-N3</b>	<b>Cu-N4</b>	<b>Cu-O5</b>
<b>1</b>	Mean	2.07 ± 0.12	2.52 ± 0.16	2.30 ± 0.23	2.55 ± 0.20	2.07 ± 0.80
<b>2</b>	Mean	2.07 ± 0.10	2.36 ± 0.17	2.34 ± 0.14	2.07 ± 0.18	3.04 ± 0.24
	$\Delta$ (%)	<b>0.0</b>	<b>-0.16</b>	<b>0.04</b>	<b>-0.48</b>	<b>0.97</b>
<b>1</b>	Width	0.60	1.25	0.97	1.13	1.32
<b>2</b>	Width	0.87	0.98	1.46	1.14	3.50*
	$\Delta$ (%)	<b>0.27</b>	<b>-0.27</b>	<b>0.49</b>	<b>0.01</b>	<b>2.18</b>

## VII.- References

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