## Supporting Information

## Constructing and controlling of ruthenium active phases for acetylene hydrochlorination

Bolin Wang,<sup>a, b, ‡</sup> Yuxue Yue,<sup>a, ‡</sup> Saisai Wang,<sup>a</sup> Zhi Chen,<sup>a</sup> Lu Yu,<sup>a</sup> Shujuan Shao,<sup>a</sup>

Guojun Lan,<sup>a</sup> Zhiyan Pan,<sup>b</sup> Jia Zhao<sup>a,\*</sup> and Xiaonian Li<sup>a,\*</sup>

<sup>a</sup> Industrial Catalysis Institute of Zhejiang University of Technology, Hangzhou,
 310014, People's Republic of China

<sup>b</sup> College of Environment of Zhejiang University of Technology, Hangzhou, 310014,

People's Republic of China

<sup>‡</sup> These authors contributed equally.

\* Corresponding author. Tel: +86 571 88871656. E-mail address: jiazhao@zjut.edu.cn (Jia Zhao)

\* Corresponding author. Tel: +86 571 88320002. E-mail: xnli@zjut.edu.cn (Xiaonian

Li)

### **1. Experimental**

#### **1.1 Catalyst Preparation**

Ru<sup>0</sup>/C: In a typical experiment, a solution of RuCl<sub>3</sub> (0.5 mmol) precursor was dissolved in 1-butyl-3-methylimidazolium bis ((trifluoromethyl) sulfonyl) imide BMIM-NTf<sub>2</sub> (10 mL) via syringe under an argon (Ar) flow, resulting in a turbid dispersion. Then activated carbon (C, NORIT, ROX 0.8) carrier was added to the above solution under 50 °C and hydrogen (4 bar) conditions for 18 h. Subsequently, the prepared sample was thermally activated at 500 °C for 2h.

RuO<sub>2</sub>/C: In a Fischer-Porter bottle, a solution of RuCl<sub>3</sub> (0.5 mmol) was dissolved in 10 mL of 1-butyl-3-methylimidazolium hexafluorophosphate BMIM-PF<sub>6</sub> by heating (50 °C) and stirring under argon. The resulting solution was cooled to room temperature and added an excess of solid NaBH<sub>4</sub>. Then activated carbon (C) carrier was added to the above solution under 50 °C for 2 h under reduced pressure. Subsequently, the prepared sample was thermally activated at 500 °C for 2h under Ar.

Ru SAC: A solution of RuCl<sub>3</sub> (0.5 mmol) was dissolved in 10 mL of 1-butyl-3methylimidazolium chloride BMIM-Cl by heating (50 °C) and stirring under argon. Then, activated carbon (C) carrier was added to the above solution with agitated stirring. Subsequently, the prepared sample was thermally activated at 400 °C for 2h under Ar.

For Ru-N SAC catalysts, all synthesis steps were similar to Ru SAC except that BMIM-Cl is replaced by 1-butyl-3-methylimidazolium dicyanamide BMIM-N(CN)<sub>2</sub>. Unless specifically mentioned, the mass loading of all Ru-based catalysts (Ru<sup>0</sup>/C, RuO<sub>2</sub>/C, Ru SAC, Ru-N SAC) was maintained at 0.5 wt.%.

**Figure S1** shows the structure of the selected ionic liquids (ILs): (a) 1-butyl-3methylimidazolium bis ((trifluoromethyl) sulfonyl) imide BMIM-NTf<sub>2</sub>; (b) 1-butyl-3methylimidazolium hexafluorophosphate BMIM-PF<sub>6</sub> and (c) 1-butyl-3methylimidazolium chloride BMIM-Cl.



**Figure S1** The structure of the selected ionic liquids (ILs): (a) 1-butyl-3-methylimidazolium bis ((trifluoromethyl) sulfonyl) imide BMIM-NTf<sub>2</sub>; (b) 1-butyl-3-methylimidazolium hexafluorophosphate BMIM-PF<sub>6</sub> and (c) 1-butyl-3-methylimidazolium chloride BMIM-Cl.

#### **1.2 Catalyst Characterization and Computational Details**

The atomic-resolution images were obtained by a JEOL JEM-ARM 200F aberrationcorrected scanning transmission electron microscopy (AC-STEM) operating at 200 kV in high-angle annular dark-field (HAADF) mode. The carbon powder was dispersed dry onto holey-carbon coated copper grids. Scanning electron microscopy (SEM) morphology was evaluated with a Philips XL-30 scanning electron microscope. Nitrogen adsorption/desorption isotherms (BET) is acquired from a Micromeritics ASAP 2020. The X-ray absorption (EXAFS) experiments were carried out at the XAS station (BL14W1) of the Shanghai Synchrotron Radiation Facility (SSRF). The electron storage ring was operated at 3.5 GeV. Si (311) double-crystal was used as the monochromator, and the data was collected using solid-state detector under ambient conditions. The beam size was limited by the horizontal and vertical slits with a surface area of 1×4 mm<sup>2</sup> during XAS measurements. The X-ray absorption of Ru foil at Ru Kedge was measured for energy calibration. The obtained XAFS data was processed in Athena (version 0.9.25) for background, pre-edge line and post-edge line calibrations. Then Fourier transformed fitting was carried out in Artemis (version 0.9.25). The  $k_2$ weighting, k-range of ~3-12 Å and R range of 1-3 Å were used. The four parameters, coordination number, bond length, Debye-Waller factor and  $E^0$  shift (CN, R,  $\sigma^2$ ,  $\Delta E^0$ ) were fitted without anyone was being fixed, constrained, or correlated. X-ray photoelectron spectroscopy (XPS) was conducted by a Kratos AXIS Ultra DLD spectrometer. The solids were analyzed at the electron take-off angle of  $45^{\circ}$  and the pass energy of 46.95 eV. Temperature-programmed desorption (TPD) measurements is conducted with an Omnistar GSD320 mass spectrometer. All density functional theory (DFT) calculations were carried out using the Cambridge Sequential Total Energy Package known as CASTEP. Information regarding to the electron-electron interaction can be obtained from the exchange-correlation function under the generalized gradient approximation (GGA) with norm-conserving pseudopotentials and Perdew-Burke-Ernzerhof functional. The geometry optimization and electronic structure calculation were carried out using the Monkhorst-Pack special k-point meshes of  $10 \times 10 \times 10$  with a kinetic energy cut-off at 750 eV. During the geometry optimization, all atoms were allowed to relax without any constraints until the convergence thresholds of maximum displacement were reached, maximum force and energy were smaller than 0.001 Å,

0.03 eV/Å and  $1.0 \times 10^{-5}$  eV/atom, respectively.

#### **1.3 Catalyst Testing**

Catalytic performance of acetylene hydrochlorination was carried out in a fixed bed glass reactor (i.d. 10 mm, **Figure S2**). Firstly, the reactor containing catalyst was flushed using nitrogen gas (N<sub>2</sub>) for 0.5 h at 160 °C. Then, reaction gas mixture of C<sub>2</sub>H<sub>2</sub> and HCl was fed into the cleaned reactor at a gas hourly space velocity of C<sub>2</sub>H<sub>2</sub> (GHSV) of 1000 h<sup>-1</sup>, C<sub>2</sub>H<sub>2</sub> : HCl ratio was kept constant at a value of 1 : 1.2. The exitting gas from the reactor was passed through a saturated NaOH solution in an absorption bottle to remove any unreacted HCl before it was sent to be analyzed by an online gas chromatography (GC 9790, Zhejiang Fuli Analytical Instruments Co., Ltd.). The catalytic activity is presented as the conversion of acetylene,  $X_{(C2H2)}$ , calculated according to Eq. 1,

$$X_{C2H2} = \frac{n(C_2H_2)^{\text{intlet}} - n(C_2H_2)^{\text{outlet}}}{n(C_2H_2)^{\text{intlet}}} \times 100\%$$
Eq.1

Where  $n(C_2H_2)^{intlet}$  and  $n(C_2H_2)^{outtlet}$  denote the respective molar flows of C<sub>2</sub>H<sub>2</sub> at the reactor outlet and inlet.

The turnover frequency (TOF) is calculated according to Eq.2,

$$TOF = \frac{n(C_2H_2)^{\text{intlet}} - n(C_2H_2)^{\text{outlet}}}{mol_{Ru} \cdot h}$$
Eq.2

The error of the carbon balance is presented as  $\varepsilon_C$ , calculated according to Eq. 3.<sup>[9]</sup> Where  $n(VCM)^{outlet}$  denote the respective molar flows of VCM at the reactor outlet.

$$\varepsilon_{\rm C} = \frac{n(C_2H_2)^{\rm intlet} - n(C_2H_2)^{\rm outlet} + n(VCM)^{\rm outlet}}{n(C_2H_2)^{\rm intlet}}$$
Eq.3

The carbon balance is  $\geq 98\%$  in all experiments.

All catalytic data points were determined as an average of at least two measurements. According to Weisz-Prater Criterion and Mears Criterion <sup>[10]</sup> (Section 2 of *Supporting Information*), the internal and external mass transfer limitations are insignificant in the evaluation system of this work.

# 2. Absence of mass transport and heat transfer during kinetic measurements

#### 2.1 Internal and external diffusion

The absence of mass transport resistances was checked by Weisz-Prater criterion ( $C_{WP}$ ) for internal diffusion and Mears' criterion ( $C_M$ ) for external diffusion.

$$C_{WP} = \frac{r_{obs}\rho_b R_p^2}{D_{eff} c_s} < 1$$
 Eq.4

$$C_M = \frac{r_{obs}\rho_b R_P n}{k_c c_s} < 0.15$$
 Eq.5

Where  $r_{obs} = \frac{n(C_2H_2)^{inlet} - n(C_2H_2)^{outlet}}{m_{Cat} \cdot S}$ , observed reaction rate: 0.082 mol/kg<sub>cat</sub>·s

n= reaction order, estimated at a maximum value of 2

 $R_p$ = catalyst particle radius: 6.25 · 10<sup>-5</sup> m

 $\rho_b$  = bulk density of catalyst bed: 430 kg·m<sup>-3</sup>

 $D_{eff}$  = effective diffusivity, estimated at a value of 8.9×10<sup>-6</sup> m<sup>2</sup>/s

 $C_s$  = gas concentration at the external surface of the catalyst: 14 mol·m<sup>-3</sup>

 $k_c$  = external mass transfer coefficient, estimated at a value of 0.142 m/s

$$C_{WP} = \frac{r_{obs}\rho_b R_p^2}{D_{eff} c_s}$$
 Eq.6

 $= [(0.082 \ mol/kg_{cat} \cdot s) \times (430 \ kg/m^3) \times (6.25 \times 10^{-5} \ m)^2] \ / \ [(8.9 \times 10^{-6} \ m^2/s) \times (14 \ mol \ /m^3)]$ 

$$= 1.7 \times 10^{3} << 1$$

$$C_{M} = \frac{r_{obs}\rho_{b}R_{P}n}{k_{c}C_{s}}$$
Eq.7

$$= [(0.082 \text{ mol/kg}_{cat} \cdot \text{s}) \times (430 \text{ kg/m}^3) \times (6.25 \times 10^{-5} \text{ m}) \times (2)] / [(0.142 \text{ m/s}) \times (14 \text{ mol}) / \text{m}^3)] = 2.2 \times 10^{-3} << 0.15$$

Therefore, internal and external diffusion effects could be neglected during the kinetic experiments.

### 2.2 Heat transfer

The absence of heat transfer was checked by Mears' criterion.

$$C_M = \left| \frac{-\Delta H r_{obs} \rho_b R_p E}{h T^2 R_g} \right|$$
 Eq.8

Where  $\Delta H$ = heat of reaction: -98.9 kJ/mol

robs=0.082 mol/kgcat·s

 $\rho_b$  = bulk density of catalyst bed: 430 kg·m<sup>-3</sup>

 $R_b$  = catalyst particle radius:  $6.25 \cdot 10^{-5}$  m

E= activation energy, estimated at a value of 42 kJ/mol

h=heat transfer coefficient between gas and pellet, estimated at a value of  $8.3 \times 10^{-2}$ 

$$kJ/m^2 \cdot s \cdot K$$

 $R_g$ = gas constant: 8.314× 10<sup>-3</sup> kJ/mol·K

T = reaction temperature, 433.15 K

$$C_M = \left| \frac{-\Delta H r_{obs} \rho_b R_p E}{h T^2 R_g} \right|$$
 Eq.9

= [(98.9 kJ/mol)×(0.082 mol/kg<sub>cat</sub>·s)×(430 kg/m<sup>3</sup>)×(6.25×10<sup>-5</sup> m)×42 kJ/mol] /

$$[(8.3 \times 10^{-2} \text{ kJ/m}^2 \cdot \text{s} \cdot \text{K}) \times (433.15 \text{ K})^2 \times 8.314 \times 10^{-3} \text{ kJ/mol} \cdot \text{K}] = 0.069 \ll 0.15$$

Therefore, heat transfer effect during the kinetic experiment could be neglected.



**Figure S2**. Schematic representation of the experimental rig as applied in the here reported continuous flow, gas phase acetylene hydrochlorination experiments [1].

Sample	Scattering path	CN <sup>a</sup>	R (Å) <sup>b</sup>	$\sigma^{2}\times10^{3}(\text{\AA}^{2})^{c}$	$\Delta E (eV)^d$	R factor
Ru foil	Ru-Ru	12	2.67±0.004	3.3±0.5	-4.3±0.8	0.008
RuCl <sub>3</sub>	Ru-Cl	2.9±0.4	2.33±0.01	5.2±2.5	-1.9±0.7	0.007
Ru SAC	Ru-Cl	2.7±0.5	2.33±0.01	5.1±2.2	-1.2±2.0	0.010
Ru-N SAC	Ru-Cl Ru-N	2.2±0.4 1.1±0.4	2.33±0.01 2.02±0.03	5.1±2.0	-0.6±1.7	0.009

Table S1 Fitting parameters from the EXAFS spectra of selected Ru-based catalysts.

<sup>a</sup>Coordination number. <sup>b</sup>Coordination shell distance. <sup>c</sup>Debye-Waller factor. <sup>d</sup>Energy shift.

Catalyst	Temperature °C	GHSV h <sup>-1</sup>	TOF h <sup>-1</sup>	Reference
Ru/SAC	170	1080	319	2
Ru/SAC-C200	170	1080	434	2
Ru/SAC-C300	170	1080	778	2
Ru/SAC-C400	170	1080	310	2
Ru/SAC-R300	170	1080	347	2
Ru/SAC-R400	170	1080	409	2
Ru/SAC-R500	170	1080	367	2
Ru-10%DMPU/AC	170	900	1590	3
Ru/AC	170	900	114	3
Ru1Co3/AC	170	900	29	3
Ru/3AC-N700	170	900	360	3
Ru/in-CNT	170	900	240	3
Ru/AC-NHN	170	900	110	3
Ru/AC-C300	170	900	612	3
Ru1K1/AC	170	900	65	3
Ru1Co3Cu1/AC	170	900	55	4
Hg/AC	170	900	12	5
Ru-N SAC <sup>a</sup>	160	6000	5263	This work
Ru SAC <sup>a</sup>	160	6000	2969	This work
RuO <sub>2</sub> /C <sup>a</sup>	160	6000	329	This work
Ru <sup>0</sup> /C <sup>a</sup>	160	6000	9	This work

 Table S2 TOF of different Ru-based catalysts.

<sup>a</sup> The catalysts developed in this work. Reaction conditions: 160 °C,  $C_2H_2$  GHSV = 18000 h<sup>-1</sup>, V(HCl)/V( $C_2H_2$ ) = 1.2.

RuO <sub>2</sub> /C			
Step	Description		
Ads.	$* + HCl \leftrightarrow *HCl$		
TS	$^{*}\mathrm{HCl} + \mathrm{C}_{2}\mathrm{H}_{2} \leftrightarrow \mathrm{HCl}^{*}\mathrm{C}_{2}\mathrm{H}_{2}$		
Rea.	$HCl^*C_2H_2 \leftrightarrow C_2H_3Cl^*$		
Dea.	$C_2H_3Cl^{\boldsymbol{*}} \leftrightarrow C_2H_3Cl + \boldsymbol{*}$		

**Table S3.** Reaction schemes of acetylene hydrochlorination on RuO<sub>2</sub>/C and Ru SAC. Corresponding to the energy profiles shown in Figure 3a and Figure 3b.

\* adsorption sites.

Table S4. Reaction schemes of acetylene hydrochlorination on Ru SAC. Corresponding to the

energy profiles shown in Figure 3b.

Ru SAC			
Step	Description		
Ads.	$^{\boldsymbol{*}}+C_{2}H_{2} \leftrightarrow ^{\boldsymbol{*}}C_{2}H_{2}$		
TS	$^{*}C_{2}H_{2} + HCl \leftrightarrow HCl^{*}C_{2}H_{2}$		
Rea.	$HCl^*C_2H_2 \leftrightarrow C_2H_3Cl^*$		
Dea.	$C_2H_3Cl^* \leftrightarrow C_2H_3Cl + *$		

\* adsorption sites for Ru SAC.

Table S5. Reaction schemes of acetylene hydrochlorination on Ru-N SAC. Corresponding to the

energy profiles shown in Figure 3c.

Ru-N SAC			
Step	Description		
Ads.	$^{*}+C_{2}H_{2}\leftrightarrow ^{*}C_{2}H_{2}$		
	$* + \text{HCl} \leftrightarrow * \text{HCl}$		
TS	$^{*}C_{2}H_{2} + ^{*}HCl \leftrightarrow ^{*}HCl^{*}C_{2}H_{2}$		
Rea.	$^{\ast}HCl^{\ast}C_{2}H_{2}\leftrightarrow C_{2}H_{3}Cl^{\ast}+^{\ast}$		
Dea.	$C_2H_3Cl^* \leftrightarrow C_2H_3Cl + *$		

\* adsorption sites for Ru-N SAC.

Sample	С	N(O)	Cl	Ru	Cl/C
Sample	wt.%	wt.%	wt.%	wt.%	
RuO <sub>2</sub> /C	0.9.1	1.1(0)	0.1	0.7	0.001
Fresh	98.1	1.1(0)	0.1	0.7	0.001
RuO <sub>2</sub> /C	04.0	0.0(0)	25	0.7	0.04
Used	94.9	0.9(0)	3.3	0.7	0.04
Ru-N SAC					
400 °C	95.3	3.2	0.9	0.6	0.009
Fresh					
Ru-N SAC					
400 °C	95.2	2.9	1.2	0.7	0.01
Used					

Table S6. Element contents determined by XPS analysis over selected Ru-N SAC.

**Table S7**. Impurities in industrial grade and laboratory level of reaction gases.

Impurity	Industrial grade (ppm)	Laboratory level (ppm)
Moisture	10	1.5
$O_2$	125	1
$N_2$	500	2
$CO_2$	15	5
$H_2$	350	/
$H_2S$	250	/



Figure S3 Ru 3p3 XPS spectra of RuO<sub>2</sub>.



Figure S4 Ru 3p3 XPS spectra of Ru<sup>0</sup>.



Figure S5 SEM image and elemental mapping of Ru<sup>0</sup>/C.



Figure S6 SEM image and elemental mapping of RuO<sub>2</sub>/C.



Figure S7 SEM image and elemental mapping of Ru SAC.



Figure S8 Ex situ Ru K edge-normalized XANES spectra of Ru SAC.



Figure S9 Ex situ Ru K edge-normalized XANES spectra of Ru foil.



Figure S10 FT-EXAFS spectra of RuCl<sub>3</sub>.



Figure S11 C<sub>2</sub>H<sub>2</sub> Conversion of different Ru-based catalysts. Reaction conditions: 160 °C, C<sub>2</sub>H<sub>2</sub>

GHSV = 1000 h<sup>-1</sup>, V(HCl)/V(C<sub>2</sub>H<sub>2</sub>) = 1.2.



Figure S12  $C_2H_2$  and HCl TPD of Ru<sup>0</sup>/C under individual gas ( $C_2H_2$  or HCl). For C carrier, only

acetylene signal is detected.



Figure S13  $C_2H_2$  and HCl TPD of RuO<sub>2</sub>/C under individual gas ( $C_2H_2$  or HCl) and gas mixture of  $[C_2H_2 + HCl]$ .

The TPD results showed that large amount of HCl and  $C_2H_2$  could be adsorbed on RuO<sub>2</sub>/C when HCl and  $C_2H_2$  were passed over the catalyst bed individually. However, when RuO<sub>2</sub>/C was pretreated by the gas mixture of [ $C_2H_2 + HCl$ ],  $C_2H_2$  adsorbed contents was significantly reduced, suggesting competitive adsorption of HCl and  $C_2H_2$  on Ru sites. HCl is preferentially adsorbed when the reactants flows through RuO<sub>2</sub>/C catalyst.



**Figure S14** The adsorption  $C_2H_2$  and HCl at sites on  $RuO_2/C$  sample. Adsorption sites 1 (a and c) and 2 (b and d) are different sites for  $C_2H_2$  and HCl adsorbed on  $RuO_2/C$ . The red, gray (carrier), black ( $C_2H_2$ ), green, white and yellow balls represent O, C (carrier and  $C_2H_2$ ), Cl, H and Ru atoms, respectively.



**Figure S15** The adsorption  $C_2H_2$  and HCl on Ru SAC sample at site 1 and site 2. Adsorption sites 1 (a and c) and 2 (b and d) are different sites for  $C_2H_2$  adsorbed on RuCl<sub>3</sub> of Ru SAC. In this case, the adsorption energy is -101 kJ·mol<sup>-1</sup>. The red, gray (carrier), black ( $C_2H_2$ ), green, white and yellow balls represent O, C (carrier and  $C_2H_2$ ), Cl, H and Ru atoms, respectively.



Figure S16 The adsorption energies of C<sub>2</sub>H<sub>2</sub> and HCl on different Ru sites (Figure S14-S15).



Figure S17 C<sub>2</sub>H<sub>2</sub> and HCl TPD of Ru SAC under individual gas (C<sub>2</sub>H<sub>2</sub> or HCl).

The adsorption amount of  $C_2H_2$  on RuCl<sub>3</sub> in Ru SAC was higher than that of HCl (Figure 2b), and the HCl-TPD profiles for the catalysts and rare activated carbon carrier were very similar (Figure S17), suggesting the dominant adsorption properties of  $C_2H_2$  on RuCl<sub>3</sub>.



Figure S18 STEM images and elemental mapping of Ru-N SAC.



Figure S19 Ex situ Ru K edge-normalized XANES spectra of Ru-N SAC.



Figure S20 N1s XPS spectra of Ru-N SAC catalysts.

N1s XPS spectra showed that three possible types of N species were present (Figure S20): pyridinic N at around 398.6 eV, pyrrolic N at around 400.5 eV and graphitic N at around 401.3 eV <sup>[6-8]</sup>. We found that the binding energy of pyridinic-N species positively shifted from the standard 398.3 eV to 398.6 eV. Except for pyridinic-N, no similar phenomenon was found in the binding energy of pyridinic-N. In XPS analysis technology,  $\pm 0.2$  eV is considered as the system error range. Therefore, this result indicates that a strong interaction has occurred between the Ru atom and the pyridinic-N species.



Figure S21 Schematic representation of the investigated Ru species adsorbed on distinct N sites. The gray, white, blue, light green and dark green balls represent C, H, N, Cl and Ru atoms, respectively.



Figure S22 The adsorption energies of Ru species on distinct N sites.



Figure S23 C<sub>2</sub>H<sub>2</sub>-TPD spectra of Ru-N SAC under individual gas (C<sub>2</sub>H<sub>2</sub>) and gas mixture [C<sub>2</sub>H<sub>2</sub> +

HCl].



Figure S24 HCl-TPD spectra of Ru-N SAC under individual gas (HCl) and gas mixture  $[C_2H_2 + HCl$ 



Figure S25 Pretreatment effects of  $C_2H_2$  and HCl on the catalytic performance of Ru-N SAC in acetylene hydr ochlorination. The catalyst was pre-treated with the individual components at 160 °C for 2 h. Reaction conditions: 160 °C,  $C_2H_2$  GHSV = 1000 h<sup>-1</sup>, V(HCl)/V( $C_2H_2$ ) = 1.2.



Figure S26 TOF values of Ru SAC and Ru-N SAC. Reaction conditions: 160 °C, C<sub>2</sub>H<sub>2</sub> GHSV =

 $18000 h^{-1}$ , V(HCl)/V(C<sub>2</sub>H<sub>2</sub>) = 1.2.



Figure S27 Long-term stability of Ru-N SAC catalyst. Reactions were carried out at 160  $^{\circ}$ C, a space velocity GHSV (C<sub>2</sub>H<sub>2</sub>) of 50 h<sup>-1</sup>, V(HCl)/V(C<sub>2</sub>H<sub>2</sub>) = 1.2, and reaction gas mixture with 250 ppm H<sub>2</sub>S and 350 ppm H<sub>2</sub>.



Figure S28 TPR profiles of fresh and Spent Ru-N SAC.



**Figure S29** HAADF-STEM images for Ru-N SAC with 0.5 wt.% Ru mass loading. The atom density is expressed as the number of atoms in a unit region (atoms nm<sup>-2</sup>). The average ruthenium atom density on the surface of the catalyst calculated from Figures a and b is 0.874 atoms nm<sup>-2</sup>.



**Figure S30** HAADF-STEM images for Ru-N SAC with 2.0 wt.% Ru mass loading. The atom density is expressed as the number of atoms in a unit region (atoms nm<sup>-2</sup>). The average ruthenium atom density on the surface of the catalyst calculated from Figures a and b is 2.626 atoms nm<sup>-2</sup>.



**Figure S31** HAADF-STEM images for Ru-N SAC with 4.0 wt.% Ru mass loading. The atom density is expressed as the number of atoms in a unit region (atoms nm<sup>-2</sup>). The average ruthenium atom density on the surface of the catalyst calculated from Figures a and b is 4.454 atoms nm<sup>-2</sup>.



Figure S32 TOF of Ru-N SAC with different Ru mass loading. Reaction conditions: 160 °C,  $C_2H_2$ GHSV = 18000 h<sup>-1</sup>, V(HCl)/V( $C_2H_2$ ) = 1.2.



Figure S33 The apparent activation energy (Ea) of Ru-N SAC with different Ru mass loading. Reaction conditions:  $C_2H_2$  GHSV = 18000 h<sup>-1</sup>, V(HCl)/V( $C_2H_2$ ) = 1.2. In order to circumvent the influence of catalyst deactivation, each point was obtained in a single experiment.

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