## Two-dimensional two-photon absorptions and third-order nonlinear optical properties of I<sub>h</sub> fullerenes and fullerene onions

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20. Fig. S13 The evolution of third-order nonlinear optic properties with electronic spectra for  $C_{60} @C_{240}(I_h) @C_{540}$  (1057) at specific external fields.

1. Fig. S1 Electronic spectra of  $C_{60}@C_{240}(I_h)$  [2117 (46×46) configurations] predicted with optimized geometry predicted with PBE0/6-31G(d) and PBE0-D3/6-31G(d), respectively.



Cartesian coordinates of  $C_{60} @C_{240}(I_h)$  optimized with PBE0/6-31G(d) and PBE0-D3/6-31G(d):

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С	1.16976482	0.38007963	3.31277278	
С	2.29487811	0.74565110	2.58162984	
С	3.01783253	-0.24941029	1.82147058	
С	2.58807749	-1.57206029	1.82147058	
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С	-0.69535826	-2.94720131	1.82147058	
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С	-3.01783253	-0.24941029	1.82147058	
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C	-0.71044924	-3.10288938	4.0431/0/3	C	-0.70930600	-3.09233200	4.03318800
C C	-3.4/593199	-0.00144940	-0.061/4355	C ~	-3.46854300	-5.98908300	-0.06110600
C	-5.90056975	-3.41651720	1.2/043199	C ~	-5.88802900	-3.40988300	1.26/84900
C	-4.63359550	-2.25255698	4.64317673	С	-4.62411700	-2.24827500	4.63318800
C	-1.42592463	-4.11812218	5.39547207	С	-1.42349000	-4.10956200	5.38412600
С	-0.71044924	-6.43506512	2.48767143	C	-0.70930600	-6.42150800	2.48289300
С	-5.62189437	1.82666422	4.30758554	C	-5.62133300	1.82648200	4.30826100

С	-6.33267271	0.84836175	3.56022896	С	-6.33262100	0.84747700	3.56036800
С	-6.77195788	1.45298592	2.35098061	C	-6.77222200	1.45253500	2.35025200
С	-6.33267271	2.80496668	2.35098061	C	-6.33262100	2.80548600	2.35025200
С	-5.62189437	3.03591257	3.56022896	С	-5.62133300	3.03659800	3.56036800
С	-4.58185401	1.48873461	5.15567005	С	-4.57638000	1.48695600	5.14811200
С	-6.02595687	-0.49890244	3.63725046	С	-6.01802200	-0.49729400	3.63228000
С	-6.91846150	0.72952482	1.18039595	С	-6.90900600	0.72904000	1.17961100
С	-6.02595687	3.47637166	1.18039595	С	-6.01802200	3.47120600	1.17961100
С	-4.58185401	3.94558913	3.63725046	С	-4.57638000	3.93962400	3.63228000
С	-6.78183963	-0.70424739	1.27043199	С	-6.76779500	-0.70224300	1.26784900
C	-6.33965150	2.81217298	-0.06174355	C	-6.32640400	2.80651100	-0.06110600
C	-4 35720188	4 78848545	2.48767143	C	-4 34830800	4 77818900	2.48289300
C	-3 57416874	2 49349336	5 39547207	C C	-3 56716800	2 48799900	5 38412600
C	-5 07267727	-0.90120222	4 64317673	C C	-5.06249300	-0.89909500	4 63318800
C	-6 78183963	1 45125792	-0.06174355	C	-6 76779500	1 44805200	-0.06110600
C	-5.07267727	4 55601341	1 270/3199	C C	-5.06249300	4 54613700	1 26784900
c	3 57416874	3 71073280	1.27043177	C	3 56716800	3 70304200	1.20784900
C	4 25720188	0.08256517	5 205 47207	C C	-3.30710800	0.08280500	5 28412600
C	-4.33720188	1.21296711	2 49767142	C	-4.54850800	1.20076500	3.38412000
C	-6.33965150	-1.31280/11	2.48/6/143	ť	-6.32640400	-1.309/6500	2.48289300
C	0.0000000	5.91120954	4.30758554	ť	0.0000000	5.91061900	4.30826100
C	-1.15006352	6.28488785	3.56022896	C	-1.15088900	6.28456600	3.56036800
C	-0.71077835	6.88951201	2.35098061	С	-0.71128800	6.88962400	2.35025200
C	0.71077835	6.88951201	2.35098061	C	0.71128800	6.88962400	2.35025200
C	1.15006352	6.28488785	3.56022896	C	1.15088900	6.28456600	3.56036800
С	0.00000000	4.81764641	5.15567005	С	0.00000000	4.81189100	5.14811200
С	-2.33660749	5.57685620	3.63725046	C	-2.33262600	5.56980700	3.63228000
С	-1.44410285	6.80528345	1.18039595	C	-1.44164200	6.79614100	1.17961100
С	1.44410285	6.80528345	1.18039595	C	1.44164200	6.79614100	1.17961100
С	2.33660749	5.57685620	3.63725046	C	2.33262600	5.56980700	3.63228000
С	1.26697423	4.16976830	5.39547207	C	1.26391200	4.16141200	5.38412600
С	-2.42463773	4.54591597	4.64317673	C	-2.41948700	4.53688100	4.63318800
С	-2.76548276	6.23228832	1.27043199	C	-2.75923700	6.21955000	1.26784900
С	0.71547539	6.89837610	-0.06174355	C	0.71418400	6.88402800	-0.06110600
С	3.20767087	5.62366860	2.48767143	C	3.20062700	5.61202900	2.48289300
С	-0.71547539	6.89837610	-0.06174355	C	-0.71418400	6.88402800	-0.06110600
С	2.76548276	6.23228832	1.27043199	C	2.75923700	6.21955000	1.26784900
С	2.42463773	4.54591597	4.64317673	С	2.41948700	4.53688100	4.63318800
С	-1.26697423	4.16976830	5.39547207	С	-1.26391200	4.16141200	5.38412600
С	-3.20767087	5.62366860	2.48767143	С	-3.20062700	5.61202900	2.48289300
С	5.62189437	1.82666422	4.30758554	С	5.62133300	1.82648200	4.30826100
С	5.62189437	3.03591257	3.56022896	С	5.62133300	3.03659800	3.56036800
С	6.33267271	2.80496668	2.35098061	C	6.33262100	2.80548600	2.35025200
С	6.77195788	1.45298592	2.35098061	C	6.77222200	1.45253500	2.35025200
С	6.33267271	0.84836175	3.56022896	C	6.33262100	0.84747700	3.56036800
С	4.58185401	1.48873461	5.15567005	C	4.57638000	1.48695600	5.14811200
С	4.58185401	3.94558913	3.63725046	С	4.57638000	3.93962400	3.63228000
С	6.02595687	3.47637166	1.18039595	С	6.01802200	3.47120600	1.17961100
С	6.91846150	0.72952482	1.18039595	С	6.90900600	0.72904000	1.17961100
С	6.02595687	-0.49890244	3.63725046	С	6.01802200	-0.49729400	3.63228000
С	4.35720188	0.08356517	5.39547207	С	4.34830800	0.08389500	5.38412600
С	3.57416874	3.71073280	4.64317673	С	3.56716800	3.70304200	4.63318800
С	5.07267727	4.55601341	1.27043199	C	5.06249300	4.54613700	1.26784900
С	6.78183963	1.45125792	-0.06174355	C	6.76779500	1.44805200	-0.06110600
-				C			

С	6.33965150	-1.31286711	2.48767143	С	6.32640400	-1.30976500	2.48289300
С	6.33965150	2.81217298	-0.06174355	C	6.32640400	2.80651100	-0.06110600
С	6.78183963	-0.70424739	1.27043199	С	6.76779500	-0.70224300	1.26784900
С	5.07267727	-0.90120222	4.64317673	С	5.06249300	-0.89909500	4.63318800
С	3.57416874	2.49349336	5.39547207	С	3.56716800	2.48799900	5.38412600
С	4.35720188	4.78848545	2.48767143	С	4.34830800	4.77818900	2.48289300
С	-3.47452181	4.78226900	-4.30758554	С	-3.47417500	4.78179200	-4.30826100
С	-2.76374346	5.76057146	-3.56022896	С	-2.76288700	5.76079600	-3.56036800
С	-3.47452181	5.99151732	-2.35098061	С	-3.47417500	5.99190800	-2.35025200
C	-4.62458533	5.15594729	-2.35098061	C	-4.62506400	5,15573800	-2.35025200
C	-4 62458533	4 40859071	-3 56022896	C	-4 62506400	4 40784500	-3 56036800
c	-2 83174151	3 89755782	-5 15567005	C C	-2 82835800	3 89290100	-5 14811200
c	-1 38763866	5 88519487	-3 63725046	C	-1 38671600	5 87715200	-3 63228000
C	-2.83174151	6 35441232	-1 18039595	C	-2 82835800	6 34557000	-1 17961100
c	5 16834000	4 65676761	1 18030505	C	5 16008500	4 65081800	1 17961100
C	-5.16834900	4.03070701	-1.18039393	C	-5.10098500	3 13408500	-1.17901100
C	-5.10854900	5.13854802	-3.03723040	C	-3.10098300	5.13498500	-3.03228000
C	-1.42392403	5.16025762	-1.2/043199	C	-1.42349000	5.14050800	-1.26/84900
C	-4.63359550	5.16035763	0.06174355	ť	-4.62411/00	5.14950800	0.06110600
C	-5.90056975	2.66422186	-2.48/6/143	C	-5.88802900	2.65894500	-2.48289300
c	-3.47593199	2.628/0465	-5.39547207	C	-3.46854300	2.62374400	-5.38412600
С	-0.71044924	5.10288958	-4.64317673	С	-0.70930600	5.09255200	-4.63318800
С	-3.47593199	6.00144940	0.06174355	С	-3.46854300	5.98908300	0.06110600
С	-5.90056975	3.41651720	-1.27043199	C	-5.88802900	3.40988300	-1.26784900
С	-4.63359550	2.25255698	-4.64317673	C	-4.62411700	2.24827500	-4.63318800
С	-1.42592463	4.11812218	-5.39547207	C	-1.42349000	4.10956200	-5.38412600
С	-0.71044924	6.43506512	-2.48767143	C	-0.70930600	6.42150800	-2.48289300
С	-5.62189437	-1.82666422	-4.30758554	C	-5.62133300	-1.82648200	-4.30826100
С	-6.33267271	-0.84836175	-3.56022896	C	-6.33262100	-0.84747700	-3.56036800
С	-6.77195788	-1.45298592	-2.35098061	C	-6.77222200	-1.45253500	-2.35025200
С	-6.33267271	-2.80496668	-2.35098061	C	-6.33262100	-2.80548600	-2.35025200
С	-5.62189437	-3.03591257	-3.56022896	C	-5.62133300	-3.03659800	-3.56036800
С	-4.58185401	-1.48873461	-5.15567005	С	-4.57638000	-1.48695600	-5.14811200
С	-6.02595687	0.49890244	-3.63725046	С	-6.01802200	0.49729400	-3.63228000
С	-6.91846150	-0.72952482	-1.18039595	С	-6.90900600	-0.72904000	-1.17961100
С	-6.02595687	-3.47637166	-1.18039595	C	-6.01802200	-3.47120600	-1.17961100
С	-4.58185401	-3.94558913	-3.63725046	C	-4.57638000	-3.93962400	-3.63228000
С	-6.78183963	0.70424739	-1.27043199	С	-6.76779500	0.70224300	-1.26784900
С	-6.33965150	-2.81217298	0.06174355	С	-6.32640400	-2.80651100	0.06110600
С	-4.35720188	-4.78848545	-2.48767143	C	-4.34830800	-4.77818900	-2.48289300
С	-3.57416874	-2.49349336	-5.39547207	С	-3.56716800	-2.48799900	-5.38412600
С	-5.07267727	0.90120222	-4.64317673	С	-5.06249300	0.89909500	-4.63318800
С	-6.78183963	-1.45125792	0.06174355	С	-6.76779500	-1.44805200	0.06110600
С	-5.07267727	-4.55601341	-1.27043199	С	-5.06249300	-4.54613700	-1.26784900
С	-3.57416874	-3.71073280	-4.64317673	С	-3.56716800	-3.70304200	-4.63318800
С	-4.35720188	-0.08356517	-5.39547207	С	-4.34830800	-0.08389500	-5.38412600
С	-6.33965150	1.31286711	-2.48767143	С	-6.32640400	1.30976500	-2.48289300
С	-0.00000000	-5.91120954	-4.30758554	С	0.00000000	-5.91061900	-4.30826100
С	-1.15006352	-6.28488785	-3.56022896	C	-1.15088900	-6.28456600	-3.56036800
С	-0.71077835	-6.88951201	-2.35098061	C	-0.71128800	-6.88962400	-2,35025200
С	0.71077835	-6.88951201	-2.35098061	C C	0.71128800	-6.88962400	-2.35025200
C	1 15006352	-6 28488785	-3 56022896	C C	1 15088900	-6 28456600	-3 56036800
C	-0.00000000	-4 81764641	-5 15567005	C C	0.00000000	-4 81189100	-5 14811200
c	-2.33660749	-5.57685620	-3.63725046	C C	-2.33262600	-5.56980700	-3.63228000
-		2.2.200020	2.22.200.0	C		2.2.2.2.007.00	2.22 - 200000

С	-1.44410285	-6.80528345	-1.18039595	C	-1.44164200	-6.79614100	-1.17961100
С	1.44410285	-6.80528345	-1.18039595	С	1.44164200	-6.79614100	-1.17961100
С	2.33660749	-5.57685620	-3.63725046	С	2.33262600	-5.56980700	-3.63228000
С	-2.76548276	-6.23228832	-1.27043199	С	-2.75923700	-6.21955000	-1.26784900
С	0.71547539	-6.89837610	0.06174355	С	0.71418400	-6.88402800	0.06110600
С	3.20767087	-5.62366860	-2.48767143	С	3.20062700	-5.61202900	-2.48289300
С	1.26697423	-4.16976830	-5.39547207	С	1.26391200	-4.16141200	-5.38412600
С	-2.42463773	-4.54591597	-4.64317673	С	-2.41948700	-4.53688100	-4.63318800
С	-0.71547539	-6.89837610	0.06174355	С	-0.71418400	-6.88402800	0.06110600
С	2.76548276	-6.23228832	-1.27043199	С	2.75923700	-6.21955000	-1.26784900
С	2.42463773	-4.54591597	-4.64317673	С	2.41948700	-4.53688100	-4.63318800
С	-1.26697423	-4.16976830	-5.39547207	С	-1.26391200	-4.16141200	-5.38412600
C	-3 20767087	-5 62366860	-2.48767143	C	-3 20062700	-5 61202900	-2.48289300
c	5 62189437	-1 82666422	-4 30758554	C	5 62133300	-1 82648200	-4 30826100
c	5 62189437	-3.03591257	-3 56022896	C C	5 62133300	-3.03659800	-3 56036800
c	6 33267271	-2 80496668	-2 35098061	C C	6 33262100	-2 80548600	-2 35025200
c	6 77195788	-1 45298592	-2 35098061	e C	6 77222200	-1.45253500	-2.35025200
c	6 33267271	-0.84836175	-3 56022896	e C	6 33262100	-0.84747700	-3 56036800
c	4 58185401	1 48873461	5 15567005	C C	4 57638000	1 48605600	5 14811200
C	4.58185401	2 0/558012	-3.13307003	C C	4.57638000	-1.48093000	3 63228000
c	4.58185401	-3.94538915	-3.03723040	c	4.37038000	-3.33902400	-3.03228000
C	6.012393087	-3.47037100	-1.18039393	C	6.00000600	-3.47120000	-1.17901100
C	6.91840130	-0.72932482	-1.18039393	C	6.90900600	-0.72904000	-1.1/901100
c	0.02393087	0.49890244	-5.05725040	C	0.01802200	0.49729400	-3.03228000
C	4.35720188	-0.08356517	-5.39547207	C	4.34830800	-0.08389500	-5.38412600
C	3.5/4168/4	-3./10/3280	-4.6431/6/3	C	3.56/16800	-3.70304200	-4.63318800
C	5.0/26/727	-4.55601341	-1.2/043199	C	5.06249300	-4.54613700	-1.26/84900
C	6.78183963	-1.45125792	0.061/4355	C	6.76779500	-1.44805200	0.06110600
C	6.33965150	1.31286/11	-2.48/6/143	C	6.32640400	1.309/6500	-2.48289300
C	6.33965150	-2.8121/298	0.061/4355	C	6.32640400	-2.80651100	0.06110600
C	6.78183963	0.70424739	-1.2/043199	C	6.76779500	0.70224300	-1.26/84900
C	5.07267727	0.90120222	-4.64317673	C	5.06249300	0.89909500	-4.63318800
С	3.57416874	-2.49349336	-5.39547207	С	3.56716800	-2.48799900	-5.38412600
С	4.35720188	-4.78848545	-2.48767143	С	4.34830800	-4.77818900	-2.48289300
С	3.47452181	4.78226900	-4.30758554	С	3.47417500	4.78179200	-4.30826100
С	4.62458533	4.40859071	-3.56022896	С	4.62506400	4.40784500	-3.56036800
С	4.62458533	5.15594729	-2.35098061	C	4.62506400	5.15573800	-2.35025200
С	3.47452181	5.99151732	-2.35098061	C	3.47417500	5.99190800	-2.35025200
С	2.76374346	5.76057146	-3.56022896	C	2.76288700	5.76079600	-3.56036800
С	2.83174151	3.89755782	-5.15567005	C	2.82835800	3.89290100	-5.14811200
С	5.16834900	3.13834802	-3.63725046	C	5.16098500	3.13498500	-3.63228000
С	5.16834900	4.65676761	-1.18039595	С	5.16098500	4.65081800	-1.17961100
С	2.83174151	6.35441232	-1.18039595	С	2.82835800	6.34557000	-1.17961100
С	1.38763866	5.88519487	-3.63725046	С	1.38671600	5.87715200	-3.63228000
С	1.42592463	4.11812218	-5.39547207	С	1.42349000	4.10956200	-5.38412600
С	4.63359550	2.25255698	-4.64317673	C	4.62411700	2.24827500	-4.63318800
С	5.90056975	3.41651720	-1.27043199	C	5.88802900	3.40988300	-1.26784900
С	3.47593199	6.00144940	0.06174355	С	3.46854300	5.98908300	0.06110600
С	0.71044924	6.43506512	-2.48767143	С	0.70930600	6.42150800	-2.48289300
С	4.63359550	5.16035763	0.06174355	С	4.62411700	5.14950800	0.06110600
С	1.42592463	6.66753719	-1.27043199	С	1.42349000	6.65356000	-1.26784900
С	0.71044924	5.10288958	-4.64317673	С	0.70930600	5.09255200	-4.63318800
С	3.47593199	2.62870465	-5.39547207	С	3.46854300	2.62374400	-5.38412600
С	5.90056975	2.66422186	-2.48767143	С	5.88802900	2.65894500	-2.48289300

2. **Table S1** The longest and shortest interlayer distances of  $C_{60} @C_{240}(I_h)$  and  $C_{60} @C_{240}(I_h) @C_{540}$  and the radius of  $C_{60}$ ,  $C_{240}$ ,  $C_{540}$ ,  $C_{60} @C_{240}(I_h)$ , and  $C_{60} @C_{240}(I_h) @C_{540}$  at the PBE0/6-31G(d) level of theory. Three digitals after decimal point for shell distances are kept for comparison.

Incluted full man on and Onione	Distan	ces (Å)	Radius (Å)			
Isolated fullerenes and Onions	longest	shortest	longest	shortest		
C <sub>60</sub>	—	—	3.53	6 (C <sub>60</sub> )		
C240	_	_	7.318 (C <sub>240</sub> )	6.926 (C <sub>240</sub> )		
C540	_	_	11.321 (C540)	10.197 (C540)		
			3.53	3.534 (C <sub>60</sub> )		
	3.901 (C <sub>60</sub> -C <sub>240</sub> )	3.551 (C <sub>60</sub> -C <sub>240</sub> )	3.544	$4 (C_{60})^a$		
$C_{60}(\underline{w}C_{240}(I_{h}))$	3.892 (C <sub>60</sub> -C <sub>240</sub> ) <sup>a</sup>	3.528 (C <sub>60</sub> -C <sub>240</sub> ) <sup>a</sup>	7.314 (C <sub>240</sub> )	6.936 (C <sub>240</sub> )		
			7.314 (C <sub>240</sub> ) <sup>a</sup>	6.921 (C <sub>240</sub> ) <sup>a</sup>		
	3.896 (C60-C240)	3.524 (C60-C240)	3.53	3 (C <sub>60</sub> )		
$C_{60} @C_{240} (I_h) @C_{540}$	4.042 (C <sub>240</sub> -C <sub>540</sub> )	3.389 (C <sub>240</sub> -C <sub>540</sub> )	7.308 (C <sub>240</sub> )	6.908 (C <sub>240</sub> )		
			11.314 (C540)	10.249 (C540)		

<sup>a</sup> The distances and radius of C<sub>60</sub>@C<sub>240</sub>(I<sub>h</sub>) are predicted with PBE0-D3/6-31G(d).

3. **Fig. S2** The frontier molecular orbitals (five degenerate HOMO and three degenerate LUMO) of a)  $C_{60}$ , b)  $C_{240}$ , c)  $C_{60}@C_{240}(I_h)$ , d)  $C_{540}$ , and e)  $C_{60}@C_{240}(I_h)@C_{540}$ . (single-point computation from zindo). The m in HOMO(m) [LMUMO(m)] stand for the numbering of degenerate orbitals. The number in square brackets is the orbital energy. All HOMOs are five-fold degenerate and all LUMOs are three-fold degenerate.









LUMO(1)

LUMO(2)

LUMO(3) [-2.01 eV]

c) C<sub>60</sub>@C<sub>240</sub>(I<sub>h</sub>)











HOMO(1) C<sub>240</sub>+C<sub>60</sub>(minor)

HOMO(2)

HOMO(3)

HOMO(4)

HOMO(5) [-6.30 eV]







LUMO(1)

LUMO(2)

LUMO(3) [-2.02 eV] C<sub>240</sub>

d) Cs40 HOMO(1) HOMO(2) HOMO(3) HOMO(4) HOMO(4) HOMO(4) HOMO(5) [-5.89 eV] LUMO(1) LUMO(1) LUMO(1) LUMO(2) L



4. Fig. S3 Electronic spectra of  $C_{60}$  with 197 (14×14), 347 (196 single-electron excitation and 150 double-electron excitation), and 931(31×30) configurations. f is the oscillator strength. The numbers in blue are the predicted highest electron transition energies.



5. Fig. S4 Electronic spectra of  $C_{240}$  [2545 (48×53) configurations],  $C_{540}$  [2500 (49×51) configurations],  $C_{60}@C_{240}(I_h)$  [2551 (50×51) configurations], and  $C_{60}@C_{240}(I_h)@C_{540}$  [2916 (55×53) configurations]. f is the oscillator strength. The numbers in blue are the predicted highest electron transition energies.



Molecules	signs <sup>a</sup>	λ/nm (eV)	$\mathbf{f}_{total}$	f		Transition nature	$<\gamma_0>_{contribution}$	$<\gamma_0>_{total}$
C <sub>60</sub> (931)	6а	376.3		0.006	$S_0 \rightarrow S_{28}$	$H(4) \rightarrow L+3(3)(15.16\%)H(3) \rightarrow L+3(1)(15.08\%)H(1) \rightarrow L+1(1)(12.82\%)$	0.00	-10.00
( )		376.3	0.018	0.006	$S_0 \rightarrow S_{29}$	H(2)→L+3(4)(10.90%)	0.00	
		376.3		0.006	$S_0 \rightarrow S_{30}$	NO	0.00	
		(3.29 eV)					$\begin{array}{c c} & -0.34 \\ & -0.52 \\ & -0.71 \end{array}$ $\overline{}$ $\overline{}$ $-1(4) \rightarrow L+2(2)(11.09\%) & 0.00 \\ 0.00 \\ 1)(10.96\%) & 0.00 \\ \hline 1)(19.72\%) & -1.01 \\ & -1.14 \\ \hline 4.71\%) & -0.55 \\ & -0.57 \\ 0.83\%) & -0.58 \\ \end{array}$	
	_	238.3		3.016	$S_0 \rightarrow S_{193}$	NO	-0.34	
		238.3	9.048	3.016	$S_0 \rightarrow S_{194}$	NO	-0.52	
		238.3		3.016	$S_0 \rightarrow S_{195}$	NO	-0.71	
		(5.20 eV)						
	6в	235.5		0.000	$S_0 \rightarrow S_{209}$	$H-1(5) \rightarrow L+2(3)(23.63\%)H-1(3) \rightarrow L+2(2)(21.74\%)H-1(5) \rightarrow L+2(1)(18.04\%)H-1(4) \rightarrow L+2(2)(18.03\%)H-1(4) \rightarrow L+2(2)(18.03\%)H-1(4) \rightarrow L+2(2)(18.03\%)H-1(4) \rightarrow L+2(2)(18.03\%)H-1(4) \rightarrow L+2(2)(18.03\%)H-1(4) \rightarrow L+2(2)(18.04\%)H-1(4) \rightarrow L+2(2)(18.04\%)H-1$	0.00	
		235.5	0.000	0.000	$S_0 \rightarrow S_{210}$	$H-1(4) \rightarrow L+2(1)(32.56\%)H-1(2) \rightarrow L+2(3)(30.14\%)$	0.00	
		235.5	0.000	0.000	$S_0 \rightarrow S_{211}$	$H-1(1) \rightarrow L+2(3)(28.20\%)H-1(3) \rightarrow L+2(2)(21.86\%)H-1(5) \rightarrow L+2(1)(12.64\%)H-1(4) \rightarrow L+2(2)(11.09\%)H-1(4) \rightarrow L+2(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1(2)(11.09\%)H-1($	0.00	
		235.5		0.000	$S_0 \rightarrow S_{212}$	$H-1(1) \rightarrow L+2(2)(35.57\%)H-1(2) \rightarrow L+2(1)(30.54\%)H-1(3) \rightarrow L+2(1)(10.96\%)$	0.00	
		(5.26 eV)						
	6с	222.7		2.181	$S_0 \rightarrow S_{256}$	$H-2(4) \rightarrow L+2(1)(38.78\%)H-2(3) \rightarrow L+2(2)(19.65\%)$	-0.88	
		222.7	6.543	2.181	$S_0 \rightarrow S_{257}$	$H-2(3) \rightarrow L+2(2)(25.72\%)H-2(2) \rightarrow L+2(3)(21.41\%)H-2(2) \rightarrow L+2(1)(19.72\%)$	-1.01	
		222.7		2.181	$S_0 \rightarrow S_{258}$	$H-2(1) \rightarrow L+2(3)(41.37\%)H-2(2) \rightarrow L+2(2)(10.15\%)$	-1.14	
		(5.57 eV)						
	_	200.1		1.151	$S_0 \rightarrow S_{305}$	$H-6(5) \rightarrow L(1)(14.93\%)H-6(4) \rightarrow L(2)(14.72\%)H-6(1) \rightarrow L(3)(14.71\%)$	-0.55	
		200.1	3.453	1.151	$S_0 \rightarrow S_{306}$	$H-6(4) \rightarrow L(1)(16.10\%)H-6(2) \rightarrow L(2)(12.24\%)$	-0.57	
		200.1		1.151	$S_0 \rightarrow S_{307}$	$H-6(5) \rightarrow L(3)(16.23\%)H-6(1) \rightarrow L(1)(16.10\%)H-6(3) \rightarrow L(2)(10.83\%)$	-0.58	
		(6.19 eV)						
	_	142.5		3.373	$S_0 \rightarrow S_{663}$	H−4(5)→L+5(1)(11.93%)	-0.76	
		142.5	10.119	3.373	$S_0 \rightarrow S_{664}$	NO	-0.78	
		142.5		3.373	$S_0 \rightarrow S_{665}$	$H-4(3) \rightarrow L+5(2)(11.11\%)H-4(1) \rightarrow L+5(1)(11.10\%)H-6(2) \rightarrow L+4(2)(11.07\%)H-6(2) \rightarrow L+4(2)(11.07\%)H-6(2)($	-0.80	
		(8.70 eV)						
C <sub>240</sub> (1600)	_	425.8		2.242	$S_0 \rightarrow S_{40}$	$H(2) \rightarrow L+1(2)(16.39\%)H(4) \rightarrow L+1(3)(14.90\%)H(1) \rightarrow L+1(1)(13.00\%)$	-1.69	-332.43
()		425.8	6.726	2.242	$S_0 \rightarrow S_{41}$	$H(3) \rightarrow L+1(2)(21.22\%)H(2) \rightarrow L+1(1)(16.57\%)H(5) \rightarrow L+1(3)(16.57\%)$	-3.93	
		425.8		2.242	$S_0 \rightarrow S_{42}$	$H(5) \rightarrow L+1(2)(16.39\%)H(1) \rightarrow L+1(3)(12.75\%)$	-6.18	
		(2.91 eV)						
		327.6		6.461	$S_0 \rightarrow S_{144}$	H(5)→L+2(2)(16.75%)	-27.45	
		327.6	19.383	6.461	$S_0 \rightarrow S_{145}$	NO	-32.49	
		327.6		6.461	$S_0 \rightarrow S_{146}$	$H(2) \rightarrow L+2(5)(13.96\%)H(3) \rightarrow L+2(1)(13.68\%)$	-37.54	
		(3.78 eV)						

6. Table S2 The transition nature of the major electron excitations in  $C_{60}$ ,  $C_{240}$ ,  $C_{60}$ ,  $C_{240}$ ,  $C_{540}$ , and  $C_{60}$ ,  $C_{240}$ ,  $I_h$ ,  $C_{540}$ . The numbering of molecular orbitals is in Fig. S4.

		224.7		2.231	S0→S777	NO	-6.36	
		224.7	6.693	2.231	$S_0 \rightarrow S_{778}$	NO	-6.40	
		224.7		2.231	S <sub>0</sub> →S <sub>779</sub>	NO	-6.44	
		(5.52 eV)						
	_	209.1		3.958	S0→S938	$H-9(3) \rightarrow L+5(13.54\%)H-5(2) \rightarrow L+8(2)(13.47\%)H-5(3) \rightarrow L+8(1)(13.47\%)$	-12.13	_
		209.1	11.874	3.958	S <sub>0</sub> →S <sub>939</sub>	$H-5(3) \rightarrow L+8(3)(15.63\%)H-9(2) \rightarrow L+5(13.41\%)H-5(1) \rightarrow L+8(3)(12.84\%)$	-12.33	
		209.1		3.958	S <sub>0</sub> →S <sub>940</sub>	$H-5(2) \rightarrow L+8(3)(15.63\%)H-9(1) \rightarrow L+5(13.41\%)H-5(1) \rightarrow L+8(1)(12.83\%)$	-12.53	
		(5.93 eV)						_
	2 <sub>A</sub>	203.8		2.665	$S_0 \rightarrow S_{1027}$	H−3(3)→L+6(4)(21.96%)	-8.35	_
		203.8	7.995	2.665	$S_0 \rightarrow S_{1028}$	H−3(1)→L+6(2)(23.11%)	-8.54	
		203.8		2.665	$S_0 \rightarrow S_{1029}$	$H-3(2) \rightarrow L+6(3)(14.18\%)H-3(2) \rightarrow L+6(1)(11.39\%)$	-8.74	
		(6.08 eV)						
		197.2		4.677	$S_0 \rightarrow S_{1138}$	NO	-15.68	_
		197.2	14.031	4.677	$S_0 \rightarrow S_{1139}$	NO	-15.88	
		197.2		4.677	$S_0 \rightarrow S_{1140}$	NO	-16.09	9
		(6.29 eV)						
	2 <sub>B</sub>	187.5		0.007	$S_0 \rightarrow S_{1317}$	H−7(1)→L+7(5)(13.10%)	0.01	
		187.5	0.021	0.007	$S_0 \rightarrow S_{1318}$	H−7(3)→L+7(4)(10.44%)	0.01	
		187.5		0.007	$S_0 \rightarrow S_{1319}$	$H-7(1) \rightarrow L+7(1)(12.87\%)H-7(2) \rightarrow L+7(2)(10.06\%)$	0.01	
		(6.61 eV)						
	2c	187.1		0.000	$S_0 \rightarrow S_{1332}$	NO	0.00	
		187.1		0.000	$S_0 \rightarrow S_{1333}$	$H-6(1) \rightarrow L+7(1)(14.33\%)H-6(4) \rightarrow L+7(5)(13.86\%)$	0.00	
		187.1	0.000	0.000	$S_0 \rightarrow S_{1334}$	H−6(1)→L+7(2)(10.16%)	0.00	
		187.1		0.000	$S_0 \rightarrow S_{1335}$	NO	0.00	
		187.1		0.000	$S_0 \rightarrow S_{1336}$	$H-6(1) \rightarrow L+7(4)(12.13\%)H-6(2) \rightarrow L+7(2)(12.01\%)$	0.00	
		(6.63 eV)						
C <sub>60</sub> @C <sub>240</sub> (I <sub>h</sub> ) (2117)	_	469.1		0.701	$S_0 \rightarrow S_{56}$	$H-1(5)(C_{60}) \rightarrow L+1(3)(C_{240})(11.23\%)H(4)(C_{60} \text{ and } C_{240}) \rightarrow L+1(2)(C_{240})(10.48\%)$	0.37	-306.17
		469.1	2.103	0.701	$S_0 \rightarrow S_{57}$	$\begin{array}{l} H(3)(C_{60} \text{ and } C_{240}) \rightarrow L+1(1)(C_{240})(13.15\%)H(1)(C_{60} \text{ and } C_{240}) \rightarrow L+1(3)(C_{240})(11.57\%) \\ H(5)(C_{60} \text{ and } C_{240}) \rightarrow L+1(2)(C_{240})(11.57\%) \end{array}$	-0.05	
		469.1		0.701	$S_0 \rightarrow S_{58}$	$H-1(3)(C_{60}) \rightarrow L+1(3)(C_{240})(15.17\%)$	-0.47	
		(2.64 eV)						
	6@2	430.0		1.876	$S_0 \rightarrow S_{85}$	$H-1(2)(C_{60}) \rightarrow L+1(1)(C_{240})(14.18\%)$	-4.43	_
	$\smile$	430.0	5.628	1.876	$S_0 \rightarrow S_{86}$	NO	-6.26	
		430.0		1.876	$S_0 \rightarrow S_{87}$	$H-1(3)(C_{60}) \rightarrow L+1(3)(C_{240})(13.13\%)$	-8.10	
		(2.88 eV)						
		347.3	5.056	1.692	$S_0 \rightarrow S_{198}$	$H(4)(C_{60} \text{ and } C_{240}) \rightarrow L+3(1)(C_{240})(18.08\%)H(2)(C_{60} \text{ and } C_{240}) \rightarrow L+3(2)(C_{240})(14.98\%)$	-6.32	_
		347.3	5.076	1.692	$S_0 \rightarrow S_{199}$	$H(5)(C_{60} \text{ and } C_{240}) \rightarrow L+3(4)(C_{240})(18.95\%)H(4)(C_{60} \text{ and } C_{240}) \rightarrow L+3(5)(C_{240})(11.48\%)$	-6.91	

					$H(3)(C_{60} \text{ and } C_{240}) \rightarrow L+3(5)(C_{240})(10.50\%)$	
	347.3		1.692	$S_0 \rightarrow S_{200}$	$H(3)(C_{60} \text{ and } C_{240}) \rightarrow L+3(3)(C_{240})(17.65\%)H(1)(C_{60} \text{ and } C_{240}) \rightarrow L+3(2)(C_{240})(16.17\%)$	-7.49
	(3.57 eV)					
_	331.2		1.063	$S_0 \rightarrow S_{258}$	$H-1(2)(C_{60}) \rightarrow L+3(1)(C_{240})(12.89\%)H-1(3)(C_{60}) \rightarrow L+3(2)(C_{240})(10.40\%)$	-6.28
	331.2	2 1 9 0	1.063	$S_0 \rightarrow S_{259}$	$H-1(5)(C_{60}) \rightarrow L+3(3)(C_{240})(12.56\%)H-1(1)(C_{60}) \rightarrow L+3(2)(C_{240})(10.75\%)$	-6.46
	221.2	5.169	1.062	So Seco	$H-1(4)(C_{60}) \rightarrow L+3(4)(C_{240})(21.61\%)H-1(2)(C_{60}) \rightarrow L+3(5)(C_{240})(14.32\%)$	6 62
	551.2		1.005	S0→S260	$H-1(3)(C_{60}) \rightarrow L+3(3)(C_{240})(12.42\%)$	-0.03
	(3.74 eV)					
6 <sub>A</sub>	326.6		0.000	$S_0 \rightarrow S_{285}$	$H-1(2)(C_{60}) \rightarrow L+12(1)(C_{60})(15.25\%)H-1(5)(C_{60}) \rightarrow L+12(2)(C_{60})(14.71\%)$	0.00
	326.6	0.000	0.000	$S_0 \rightarrow S_{286}$	$H-1(4)(C_{60}) \rightarrow L+12(3)(C_{60})(14.17\%)$	0.00
	326.6	0.000	0.000	$S_0 {\rightarrow} S_{287}$	$H-1(3)(C_{60}) \rightarrow L+12(5)(C_{60})(11.53\%)H-1(4)(C_{60}) \rightarrow L+12(2)(C_{60})(10.99\%)$	0.00
	326.6		0.000	$S_0 \rightarrow S_{288}$	$H-1(1)(C_{60}) \rightarrow L+12(5)(C_{60})(18.28\%)H-1(3)(C_{60}) \rightarrow L+12(3)(C_{60})(13.70\%)$	0.00
	(3.80 eV)					
бв	247.1		0.793	$S_0 \rightarrow S_{1002}$	$H-6(3)(C_{60}) \rightarrow L+10(1)(C_{60})(10.99\%)H-6(4)(C_{60}) \rightarrow L+10(1)(C_{60})(10.21\%)$	-1.33
	247.1	2.379	0.793	$S_0 \rightarrow S_{1003}$	H−6(5)(C <sub>60</sub> )→L+10(2)(C <sub>60</sub> )(14.55%)	-1.34
	247.1		0.793	$S_0 \rightarrow S_{1004}$	H−6(2)(C <sub>60</sub> )→L+10(3)(C <sub>60</sub> )(15.82%)	-1.36
	(5.02 eV)					
5с	230.4		0.000	$S_0 \rightarrow S_{1263}$	$H-7(4)(C_{60}) \rightarrow L+10(2)(C_{60})(12.95\%)H-7(2)(C_{60}) \rightarrow L+10(1)(C_{60})(12.94\%)$	0.00
	230.4	0.000	0.000	$S_0 \rightarrow S_{1264}$	$H-7(4)(C_{60}) \rightarrow L+10(3)(C_{60})(12.18\%)$	0.00
	230.4	0.000	0.000	$S_0 \rightarrow S_{1265}$	$H-7(2)(C_{60}) \rightarrow L+10(3)(C_{60})(12.18\%)$	0.00
	230.4		0.000	$S_0 \rightarrow S_{1266}$	$H-7(2)(C_{60}) \rightarrow L+10(2)(C_{60})(12.95\%)H-7(4)(C_{60}) \rightarrow L+10(1)(C_{60})(12.94\%)$	0.00
	(5.38 eV)					
2 <sub>A</sub>	200.3		0.749	$S_0 \rightarrow S_{1866}$	$H-4(3)(C_{240}) \rightarrow L+8(1)(C_{240})(30.02\%)H-4(2)(C_{240}) \rightarrow L+8(3)(C_{240})(11.79\%)$	-1.41
	200.3		0.740	So-Sierz	$H-4(1)(C_{240}) \rightarrow L+8(2)(C_{240})(23.82\%)H-4(3)(C_{240}) \rightarrow L+8(3)(C_{240})(11.92\%)$	1.44
	200.5	2.247	0.749	50-5186/	$H-8(2)(C_{240}) \rightarrow L+11(2)(C_{240})(11.81\%)$	-1.44
	200.3		0 749	So-Siece	$H-4(2)(C_{240}) \rightarrow L+8(4)(C_{240})(26.53\%)H-8(3)(C_{240}) \rightarrow L+11(2)(C_{240})(11.81\%)$	_1.48
	200.5		0.777	50 , 51909	$H-4(1)(C_{240}) \rightarrow L+8(3)(C_{240})(10.35\%)$	-1.40
	(6.19 eV)					
	192.1		1 065	S0→S19 71	$H-9(4)(C_{240}) \rightarrow L+12(1)(C_{60})(20.31\%)H-9(2)(C_{240}) \rightarrow L+12(5)(C_{60})(12.13\%)$	-1 73
	1/2.1		1.005	50 51771	$H-9(3)(C_{240}) \rightarrow L+12(4)(C_{60})(10.46\%)$	1.75
	192.1	3.195	1.065	$S_0 \rightarrow S_{1972}$	$H-9(5)(C_{240}) \rightarrow L+12(3)(C_{60})(28.90\%)H-9(2)(C_{240}) \rightarrow L+12(1)(C_{60})(21.68\%)$	-1.76
	192.1		1.065	$S_0 \rightarrow S_{1973}$	$H-9(1)(C_{240}) \rightarrow L+12(2)(C_{60})(27.08\%)H-9(3)(C_{240}) \rightarrow L+12(4)(C_{60})(19.32\%)$	-1 80
				~~ ~1775	$H-9(4)(C_{240}) \rightarrow L+12(3)(C_{60})(10.37\%)$	1.50
	(6.45 eV)					
2 <sub>B</sub>	190.0		2.189	$S_0 \rightarrow S_{2031}$	$H-10(2)(C_{240}) \rightarrow L+9(2)(C_{240})(33.01\%)H-10(1)(C_{240}) \rightarrow L+9(1)(C_{240})(14.04\%)$	-3.59
	190.0	6.567	2.189	$S_0 \rightarrow S_{2032}$	$H-10(3)(C_{240}) \rightarrow L+9(5)(C_{240})(31.12\%)H-10(1)(C_{240}) \rightarrow L+9(1)(C_{240})(26.95\%)$	-3.61
	190.0		2.189	S <sub>0</sub> →S <sub>2033</sub>	$H-10(3)(C_{240}) \rightarrow L+9(4)(C_{240})(27.69\%)H-10(1)(C_{240}) \rightarrow L+9(3)(C_{240})(21.66\%)$	-3.63
				$H-10(2)(C_{240}) \rightarrow L+9(5)(C_{240})(12.82\%)$		

		(6.53 eV)						
		187.8		10.463	S <sub>0</sub> →S <sub>2061</sub>	$H-10(1)(C_{240}) \rightarrow L+12(1)(C_{60})(18.65\%)H-10(2)(C_{240}) \rightarrow L+12(3)(C_{60})(12.75\%)$	-19.12	
		187.8	31.387	10.462	$S_0 \rightarrow S_{2062}$	$H-10(3)(C_{240}) \rightarrow L+12(5)(C_{60})(22.57\%)H-10(2)(C_{240}) \rightarrow L+12(3)(C_{60})(12.49\%)$	-19.82	
		187.8		10.462	$S_0 \rightarrow S_{2063}$	$H-10(3)(C_{240}) \rightarrow L+12(2)(C_{60})(17.97\%)H-10(2)(C_{240}) \rightarrow L+12(4)(C_{60})(15.31\%)$	-20.52	
		(6.60 eV)						
		187.2		8.251	$S_0 \rightarrow S_{2071}$	$H-10(1)(C_{240}) \rightarrow L+12(1)(C_{60})(15.43\%)H-8(1)(C_{240}) \rightarrow L+11(3)(C_{240})(10.31\%)$	-18.67	
		187.2	24 752	8.250	$S_0 \rightarrow S_{2072}$	$H-10(3)(C_{240}) \rightarrow L+12(2)(C_{60})(11.77\%)H-10(2)(C_{240}) \rightarrow L+12(4)(C_{60})(10.03\%)$	-19.09	
		187.2	21.752	8.251	$S_0 \rightarrow S_{2073}$	$\begin{array}{c} H-10(3)(C_{240}) \rightarrow L+12(5)(C_{60})(14.09\%)H-10(2)(C_{240}) \rightarrow L+12(3)(C_{60})(12.07\%) \\ H-8(1)(C_{240}) \rightarrow L+11(1)(C_{240})(10.31\%) \end{array}$	-19.50	
		(6.62 eV)						
	$2_{\rm C}$	186.5		13.108	$S_0 \rightarrow S_{2084}$	$H-9(1)(C_{240}) \rightarrow L+9(4)(C_{240})(23.97\%)H-9(3)(C_{240}) \rightarrow L+9(5)(C_{240})(14.64\%)$	-31.95	
		186.4	39.327	13.109	$S_0 \rightarrow S_{2085}$	$H-9(4)(C_{240}) \rightarrow L+9(1)(C_{240})(15.45\%)H-9(3)(C_{240}) \rightarrow L+9(3)(C_{240})(11.61\%)$	-33.50	
		186.4		13.110	$S_0 \rightarrow S_{2086}$	$H-9(5)(C_{240}) \rightarrow L+9(2)(C_{240})(22.30\%)H-9(2)(C_{240}) \rightarrow L+9(1)(C_{240})(14.01\%)$	-35.06	
		(6.65 eV)						
C <sub>540</sub> (1850)	—	523.3	21 224	7.108	$S_0 \rightarrow S_{40}$	$H(2) \rightarrow L+1(1)(21.64\%)H(4) \rightarrow L+1(3)(13.84\%)H(3) \rightarrow L+1(2)(10.83\%)$	-72.60	-3266.74
		523.3	21.324	7.108	$S_0 \rightarrow S_{41}$	H(5)→L+1(2)(10.83%)	-137.54	
		523.3		7.108	$S_0 \rightarrow S_{42}$	$H(1) \rightarrow L+1(2)(13.02\%)H(3) \rightarrow L+1(3)(10.72\%)H(5) \rightarrow L+1(1)(10.72\%)$	-202.47	
		(2.37 eV)						
	—	402.2		10.963	$S_0 \rightarrow S_{137}$	H(2)→L+2(4)(10.74%)	-349.46	
		402.2	32.889	10.963	$S_0 \rightarrow S_{138}$	H(4)→L+2(1)(10.07%)	-389.43	
		402.2		10.963	$S_0 \rightarrow S_{139}$	$H(1) \rightarrow L+2(3)(12.54\%)H(5) \rightarrow L+2(5)(11.70\%)$	-429.40	
		(3.08 eV)						
	5 <sub>A</sub>	319.4		2.709	$S_0 \rightarrow S_{387}$	NO	-64.53	
		319.4	8.127	2.709	$S_0 \rightarrow S_{388}$	H−2(4)→L+3(2)(10.05%)	-65.29	
		319.4		2.709	$S_0 \rightarrow S_{389}$	NO	-66.04	
		(3.88 eV)						_
	—	313.8		3.428	$S_0 \rightarrow S_{430}$	$H-6(1) \rightarrow L+1(1)(12.02\%)H-7(3) \rightarrow L(1)(11.54\%)H-7(2) \rightarrow L(2)(11.43\%)$	-71.59	
		313.8	10.284	3.428	$S_0 \rightarrow S_{431}$	$H-7(1) \rightarrow L(1)(11.54\%)H-7(2) \rightarrow L(3)(11.43\%)$	-72.66	
		313.8		3.428	$S_0 \rightarrow S_{432}$	$H-7(1) \rightarrow L(2)(11.84\%)H-7(3) \rightarrow L(3)(11.84\%)H-6(4) \rightarrow L+1(2)(10.62\%)$	-73.75	
		(3.95 eV)						
	5в	276.2		0.056	$S_0 \rightarrow S_{730}$	H−2(4)→L+4(1)(12.49%)	-1.73	
		276.2	0.168	0.056	$S_0 \rightarrow S_{731}$	NO	-1.73	
		276.2		0.056	$S_0 \rightarrow S_{732}$	H−2(2)→L+4(3)(14.31%)	-1.73	
		(4.49 eV)						
	_	269.1		7.716	$S_0 \rightarrow S_{789}$	NO	-145.42	
		269.1	23.148	7.716	$S_0 \rightarrow S_{790}$	NO	-147.95	
		269.1		7.716	$S_0 \rightarrow S_{791}$	NO	-150.50	

		(4.61 eV)						
		227.3		3.407	$S_0 \rightarrow S_{1331}$	NO	-49.35	_
		227.3	10.221	3.407	$S_0 \rightarrow S_{1332}$	H−5(3)→L+8(4)(11.81%)	-49.56	
		227.3		3.407	$S_0 \rightarrow S_{1333}$	H−5(2)→L +8(2)(13.15%)	-49.78	
		(5.45 eV)						
C60@C240						$H(5)(C_{240} \text{ and } C_{540}) \rightarrow L+1(1)(C_{540})(14.51\%)H(3)(C_{240} \text{ and } C_{540})$		
$(I_h)@C_{540}$		651.0		1.212	$S_0 \rightarrow S_{23}$	$C_{540}) \rightarrow L+1(3)(C_{540})(12.91\%)H-1(5)(C_{540}) \rightarrow L(1)(C_{540})(10.93\%)$	-7.61	-2921.44
(1057)			3 636			$H(4)(C_{240} \text{ and } C_{540}) \rightarrow L+1(2)(C_{540})(10.39\%)$		
		651.0	5.050	1.212	$S_0 \rightarrow S_{24}$	$H(1)(C_{240} \text{ and } C_{540}) \rightarrow L+1(3)(C_{540})(12.91\%)H(2)(C_{240} \text{ and } C_{540}) \rightarrow L+1(2)(C_{540})(12.55\%)$	-12.99	
		651.0		1 212	Sand	$H(1)(C_{240} \text{ and } C_{540}) \rightarrow L+1(2)(C_{540})(12.98\%)H(3)(C_{240} \text{ and } C_{540}) \rightarrow L+1(1)(C_{540})(12.98\%)$	_18.38	
		051.0		1.212	50 7525	$H(2)(C_{240} \text{ and } C_{540}) \rightarrow L+1(3)(C_{540})(11.80\%)$	-10.50	
		(1.90 eV)						
	6@2	429.0		0.420	So-Saza	$H-3(3)(C_{60}) \rightarrow L+3(3)(C_{240})(22.44\%)H-3(2)(C_{60}) \rightarrow L+3(2)(C_{240})(18.75\%)$	-6.22	
	0@2	429.0	429.0	0.420	50 75275	$H-3(5)(C_{60}) \rightarrow L+3(1)(C_{240})(12.50\%)$	-0.22	
		429.0	1 260	0.420	So Soza	$H-3(1)(C_{60}) \rightarrow L+3(2)(C_{240})(18.74\%)H-3(5)(C_{60}) \rightarrow L+3(1)(C_{240})(10.88\%)$	-6.29	
		429.0	1.200	0.420	50 75274	$H-3(4)(C_{60}) \rightarrow L+3(3)(C_{240})(10.47\%)H-3(3)(C_{60}) \rightarrow L+3(1)(C_{240})(10.18\%)$	0.2)	
		429.0		0.420	$S_0 \rightarrow S_{275}$	$H-3(4)(C_{60}) \rightarrow L+3(2)(C_{240})(16.26\%)H-3(2)(C_{60}) \rightarrow L+3(3)(C_{240})(15.57\%)$	-6.37	
		429.0		0.420	50 , 5275	$H-3(1)(C_{60}) \rightarrow L+3(1)(C_{240})(15.56\%)$	0.57	
		(2.89 eV)						
	—	354.7		4.344	$S_0 \rightarrow S_{559}$	$H-4(5)(C_{240}) \rightarrow L+8(1)(C_{60})(12.19\%)H-1(5)(C_{540}) \rightarrow L+8(1)(C_{60}) (11.48\%)$	-68.19	
		354.7	13.032	4.344	$S_0 \rightarrow S_{560}$	$H-4(2)(C_{240}) \rightarrow L+8(3)(C_{60})(10.04\%)$	-71.39	
		354.7		4.344	$S_0 \rightarrow S_{561}$	NO	-74.60	
		(3.50 eV)						
	—	339.1		5.685	$S_0 \rightarrow S_{633}$	NO	-99.91	
		339.1	17.056	5.685	$S_0 \rightarrow S_{634}$	NO	-104.29	
		339.1		5.686	$S_0 \rightarrow S_{635}$	NO	-108.68	
		(3.66 eV)						
	5 <sub>A</sub>	311.9		9.921	$S_0 \rightarrow S_{844}$	$H-5(2)(C_{540}) \rightarrow L+5(2)(C_{540})(18.87\%)H-5(1)(C_{540}) \rightarrow L+5(1)(C_{540})(16.36\%)$	-205.23	
		311.9	29 763	9 921	S <sub>0</sub> →S <sub>845</sub>	$H-5(1)(C_{540}) \rightarrow L+5(5)(C_{540})(15.65\%)H-5(3)(C_{540}) \rightarrow L+5(2)(C_{540})(10.95\%)$	-214.02	
			_,		20 2012	$H-5(4)(C_{540}) \rightarrow L+5(1)(C_{540})(10.68\%)$		
		311.9		9.921	$S_0 \rightarrow S_{846}$	$H-5(4)(C_{540}) \rightarrow L+5(4)(C_{540})(16.64\%)H-5(2)(C_{540}) \rightarrow L+5(3)(C_{540})(10.33\%)$	-222.80	
		(3.98 eV)						_
	_	297.8		5.160	$S_0 \rightarrow S_{926}$	$H-4(5)(C_{240}) \rightarrow L+6(3)(C_{540})(17.94\%)H-4(2)(C_{240}) \rightarrow L+6(1)(C_{540})(11.25\%)$	-117.99	
		297.8	15.479	5.159	$S_0 \rightarrow S_{927}$	$H-4(4)(C_{240}) \rightarrow L+6(1)(C_{540})(22.48\%)H-4(2)(C_{240}) \rightarrow L+6(2)(C_{540})(12.99\%)$	-119.88	
		297.8		5.160	$S_0 \rightarrow S_{928}$	$H-4(1)(C_{240}) \rightarrow L+6(2)(C_{540})(20.11\%)H-4(3)(C_{240}) \rightarrow L+6(3)(C_{540})(11.65\%)$	-121.75	
		(4.16 eV)						_
	5 <sub>B</sub>	286.4	25.413	8.471	$S_0 \rightarrow S_{999}$	$H-5(2)(C_{540}) \rightarrow L+6(1)(C_{540})(33.45\%)H-5(2)(C_{540}) \rightarrow L+6(3)(C_{540})(18.55\%)$	-193.56	
		286.4		8.471	$S_0 \rightarrow S_{1000}$	$H-5(1)(C_{540}) \rightarrow L+6(3)(C_{540})(50.45\%)H-5(3)(C_{540}) \rightarrow L+6(2)(C_{540})(13.37\%)$	-197.74	

<sup>a</sup> The numbers 6, 2, 5, and 6@2 stand for C<sub>60</sub>, C<sub>240</sub>, C<sub>540</sub>, and C<sub>60</sub>@C<sub>240</sub>, respectively and subscripts A, B, and C denote three different electronic excitations states of systems.

7. Fig. S5 The molecular orbitals associated with major electron transitions in  $C_{60}$ ,  $C_{240}$ ,  $C_{60}$ ,

1) C<sub>60</sub> (931) (Isosurface value=0.02) [HOMO-6, HOMO-4, HOMO-1, HOMO and LUMO+3 are five-fold degenerate. LUMO, LUMO+1, LUMO+2, and LUMO+5 are three-fold degenerate. HOMO-2 is four-fold degenerate.]

a. The lowest electronic excitation: 6A-Corresponding to the transition at 3.80 eV (326.6 nm) in C60@C240.



 $S_0 \rightarrow S_{30}$ : 376.3 nm (3.29 eV) (NO)









2)  $C_{240}$  (1600) (Isosurface value=0.02) [HOMO-6, HOMO, LUMO+2, and LUMO+7 are five-fold degenerate. HOMO-9, HOMO-7, HOMO-5, HOMO-3, LUMO+1, and LUMO+8 are three-fold degenerate. LUMO+6 is four-fold degenerate. LUMO+5 has no degenerate orbitals.]

a. The lowest electronic excitation:















3)  $C_{60}@C_{240}$  (2117) (Isosurface value=0.02) [HOMO-9, HOMO-6, HOMO-1, HOMO, LUMO+3, LUMO+9, and LUMO+12 are five-fold degenerate. HOMO-10, HOMO-4, LUMO+1, LUMO+10, and LUMO+11 are three-fold degenerate. HOMO-7 and LUMO+8 are four-fold degenerate.]








































## 





















4) C<sub>540</sub> (1850) (Isosurface value=0.02) [HOMO-6, HOMO, LUMO+2, LUMO+3, and LUMO+8 are five-fold degenerate. HOMO-7, HOMO-5, LUMO, LUMO+1, and LUMO+4 are three-fold degenerate. HOMO-2 is four-fold degenerate.]

a. The lowest electronic excitation:















5) C<sub>60</sub>@C<sub>240</sub>@C<sub>540</sub> (1057) (Isosurface value=0.02) [HOMO-4, HOMO-3, HOMO-1, HOMO, and LUMO+5 are five-fold degenerate. LUMO, LUMO+1, LUMO+3, LUMO+6, and LUMO+8 are three-fold degenerate. HOMO-5 is four-fold degenerate.] a. The lowest electronic excitation:

















d. The strongest oscillator strength:  $5_A$ —Corresponding to the transition at 3.86 eV (321.0 nm) in C<sub>540</sub>.  $S_0 \rightarrow S_{844}$ : 311.9 nm (3.98 eV)














8. Fig. S6 Electronic spectra of  $C_{60}@C_{240}$  (I<sub>h</sub>) and  $C_{60}@C_{240}$  (D<sub>5d</sub>) with 2117 (46×46) configurations. f is the oscillator strength. The numbers are the predicted highest electron transition energies.



9. Fig. S7 The truncation scheme of excited states which is tested with the  $\langle \gamma_0 \rangle$  of C<sub>240</sub> and C<sub>60</sub>@C<sub>240</sub>.



 $\begin{aligned} & \text{Full CIS } \left[ (M, P) \rightarrow (O, P) \right] & \text{Truncated CIS } \left[ (M, N) \rightarrow (O, P) \right] & \text{Missed CIS } \left[ (N+1, P) \rightarrow (N+1, P) \right] \\ & \text{a) The truncation scheme of excited states, where } O \geq M \text{ and } P \geq N. \end{aligned}$ 



b) The truncation scheme in a) is tested with the  $\langle \gamma_0 \rangle$  of C<sub>240</sub> and C<sub>60</sub>@C<sub>240</sub>. The truncated upper starting excited state is the 42<sup>th</sup>, 146<sup>th</sup>, 940<sup>th</sup>, and 1140<sup>th</sup> excited state for C<sub>240</sub>, respectively. The truncated upper starting excited state is the 87<sup>th</sup>, 260<sup>th</sup>, 1211<sup>th</sup>, and 1624<sup>th</sup> excited state for C<sub>60</sub>@C<sub>240</sub>, respectively.

10. Fig. S8 Two-dimensional two-photon absorption spectrum (negative response region) of  $C_{240}$ .



Processes	External Field/eV (λ/nm)	Responses	Major Electronic Excitation Contribution
	5.20 (238.3)	497407	5.20 eV(238.3 nm) (501694)
SIPA	5.55 (223.4)	224667	5.57 eV(222.7 nm) (304389)
0(-w, w, -w, w)	5.05 (245.5)	-259395	5.20 eV(238.3 nm) (-96138); 5.57 eV(222.7 nm) (-96523)
DFWM	5.15 (240.7)	9873	5.20 eV(238.3 nm) (5554); 5.57 eV(222.7 nm) (2668)
γ(-w; w, -w, w)	5.65 (219.4)	-4011	5.57 eV(222.7 nm) (-4731)
THG	5.20 (238.3)	780	5.20 eV(238.3 nm) (390); 5.57 eV(222.7 nm) (70)
γ(-3w; w, w, w)	5.55 (223.4)	318	5.57 eV(222.7 nm) (239)
EFISH	5.35 (231.7)	612	5.20 eV(238.3 nm) (85); 5.47 eV(226.8 nm) (133); 5.59 eV(221.9 nm) (160)
γ(-2w; w, w, 0)	5.10 (243.1)	-294	5.57 eV(222.7 nm) (-104); 5.59 eV(221.9 nm) (-125)

11. Table S3 The strong response and corresponding major electronic excitation contribution of dynamic third-order nonlinear optic process for C<sub>60</sub> (931).





## EFISH: a) EFISH-5.35 eV

b) EFISH-5.10 eV



13. Table S4 The strong response and corresponding major electronic excitation contribution of dynamic third-order nonlinear optic process for  $C_{240}$  (1600).

Processes	External Field/eV (λ/nm)	Responses	Major Electronic Excitation Contribution
CTD A	2.95 (420.3)	1086560	2.91 eV(425.8 nm) (652461); 3.78 eV(327.6 nm) (202104)
SIPA S(	3.80 (326.3)	5024070	3.78 eV(327.6 nm) (4731332)
O(-W, W, -W, W)	3.65 (339.7)	-1627150	3.78 eV(327.6 nm) (-980366)
DEWM	2.90 (427.5)	66670	2.91 eV(425.8 nm) (24807); 3.78 eV(327.6 nm) (19667)
DF wM	3.75 (330.6)	124464	3.78 eV(327.6 nm) (89526)
$\gamma(-w, w, -w, w)$	3.85 (322.0)	-106723	3.78 eV(327.6 nm) (-127152)
THG	2.90 (427.5)	9593	2.91 eV(425.8 nm) (2849); 3.74 eV(331.6 nm) (2273); 4.49 eV(276.4 nm) (1197)
γ(-3w; w, w, w)	3.80 (326.3)	11075	3.78 eV(327.6 nm) (5275)
FFIGH	2.95 (420.3)	3752	2.91 eV(425.8 nm) (2430)
EFISH	3.85 (322.0)	4285	3.78 eV(327.6 nm) (3208); 3.85 eV(322.0 nm) (1397)
$\gamma(-2w; w, w, 0)$	3.70 (335.1)	-3962	3.78 eV(327.6 nm) (-1275); 3.85 eV(322.0 nm) (-737); 4.37 eV(283.7 nm) (-545)

## 14. **Fig. S10** The evolution of third-order nonlinear optic properties with electronic spectra for $C_{240}$ (1600) at specific external fields. STPA: a) STPA-2.95 eV b) STPA-3.80 eV c) STPA-3.65 eV









c) DFWM-3.85 eV

-0.01-34 -20<sup>-34</sup>esu) (×10<sup>4</sup>)

0.0

10

	External Field/eV (λ/nm)	Responses	Major Electronic Excitation Contribution
	2.40 (516.6)	10620200	2.37 eV(523.3 nm) (8432640); 3.08 eV(402.2 nm) (1123990)
OTD A	3.10 (399.9)	13386900	3.08 eV(402.2 nm) (12437710)
SIPA	3.90 (317.9)	2242480	3.95 eV(313.8 nm) (2282906)
0(-w, w, -w, w)	4.60 (269.5)	3804370	4.61 eV(269.1 nm) (2343120); 4.65 eV(226.4 nm) (1668320)
	2.25 (551.0)	-5155620	2.37 eV(523.3 nm) (-3012840); 3.08 eV(402.2 nm) (-1069630)
	2.35 (527.6)	886669	2.37 eV(523.3 nm) (528872); 3.08 eV(402.2 nm) (184471)
	3.00 (413.3)	479717	3.08 eV(402.2 nm) (401490)
DFWM	3.75 (330.6)	50650	3.88 eV(319.4 nm) (15716); 3.95 eV(313.8 nm) (30054); 4.61 eV(269.1 nm) (8066)
γ(-w; w, -w, w)	4.50 (275.5)	48850	4.61 eV(269.1 nm) (8763); 4.65 eV(226.4 nm) (18218)
	2.45 (506.0)	-472664	2.37 eV(523.3 nm) (-544957)
	3.15 (393.6)	-452904	3.08 eV(402.2 nm) (-554948)
	2.35 (527.6)	102868	2.37 eV(523.3 nm) (40065); 2.97 eV(417.1 nm) (27121)
THG	3.10 (399.9)	52896	3.08 eV(402.2 nm) (27777)
γ(-3w; w, w, w)	3.90 (317.9)	9184	3.88 eV(319.4 nm) (1858); 3.95 eV(313.8 nm) (4227); 4.61 eV(269.1 nm) (1437)
	4.60 (269.5)	4863	4.61 eV(269.1 nm) (3443); 4.65 eV(226.4 nm) (1956)
	2.40 (516.6)	29343	2.37 eV(523.3 nm) (31552);
FFIGU	3.15 (393.6)	14953	3.08 eV(402.2 nm) (15255)
EFISH	4.00 (310.0)	9343	3.95 eV(313.8 nm) (5596)
$\gamma(-2w, w, w, 0)$	4.60 (269.5)	4481	4.61 eV(269.1 nm) (3144); 4.65 eV(226.4 nm) (1449)
	3.00 (413.3)	-14032	3.08 eV(402.2 nm) (-14578)

15. Table S5 The strong response and corresponding major electronic excitation contribution of dynamic third-order nonlinear optic process for C<sub>540</sub> (1850).



d) STPA-4.60 eV



 $\delta(\omega)$  (10<sup>-50</sup> cm<sup>4</sup>s/photon) (×10<sup>7</sup>)





4 6 Energy (eV)

10

8



0

0

2

e) STPA-2.25 eV









d) DFWM-4.50 eV





e) EFISH-3.00 eV





17. Table S6 The strong response and corresponding major electronic excitation contribution of dynamic third-order nonlinear optic process for  $C_{60}@C_{240}(I_b)$  (2117).



19. Table S7 The strong response and corresponding major electronic excitation contribution of dynamic third-order nonlinear optic process for C<sub>60</sub>@C<sub>240</sub>(I<sub>h</sub>)@C<sub>540</sub> (1057).

Processes	External Field/eV (λ/nm)	Responses	Major Electronic Excitation Contribution
STPA δ(-w; w, -w, w)	1.95 (635.8)	656197	1.90 eV(651.0 nm) (107909); 2.26 eV(547.3 nm) (116206)
	2.30 (539.1)	704106	2.26 eV(547.3 nm) (255872)
	3.70 (335.1)	5310810	3.66 eV(339.1 nm) (1165311); 3.72 eV(333.7 nm) (3346949); 3.98 eV(311.9 nm) (1337110)
	4.00 (310.0)	10787400	3.98 eV(311.9 nm) (5049800); 4.09 eV(303.3 nm) (3900620); 4.16 eV(297.8 nm) (3344300)
	4.50 (275.5)	-7206800	4.16 eV(297.8 nm) (-1251560); 4.33 eV(286.4 nm) (-4546350)
DFWM γ(-w; w, -w, w)	1.90 (652.5)	130017	1.90 eV(651.0 nm) (15782); 2.26 eV(547.3 nm) (24085); 3.98 eV(311.9 nm) (12865)
	2.25 (551.0)	82424	2.26 eV(547.3 nm) (7359); 2.63 eV(472.1 nm) (13811); 3.66 eV(339.1 nm) (8036); 3.98 eV(311.9 nm) (9655)
	3.45 (359.4)	226165	3.66 eV(339.1 nm) (88208); 3.72 eV(333.7 nm) (40645); 3.98 eV(311.9 nm) (39074)
	3.90 (317.9)	169832	4.09 eV(303.3 nm) (60975); 4.16 eV(297.8 nm) (77489); 4.33 eV(286.4 nm) (64026)
	4.35 (285.0)	-238711	4.33 eV(286.4 nm) (-222517)
THG	1.90 (652.5)	31628	1.90 eV(651.0 nm) (3222); 2.83 eV(437.7 nm) (5096); 2.92 eV(425.2 nm) (7115); 3.22 eV(385.6 nm) (2976)
γ(-3w; w, w, w)	2.25 (551.0)	14523	2.26 eV(547.3 nm) (3200); 2.92 eV(425.2 nm) (1187); 3.20 eV(387.2 nm) (2364); 3.30 eV(376.2 nm) (1068)

-	3.70 (335.1)	21415	3.66 eV(339.1 nm) (3291); 3.72 eV(333.7 nm) (4935); 3.98 eV(311.9 nm) (8020)
	3.95 (313.9)	25613	3.98 eV(311.9 nm) (12671); 4.09 eV(303.3 nm) (5140); 4.16 eV(297.8 nm) (6099); 4.33 eV(286.4 nm) (4922)
	4.55(272.5)	-9427	3.98 eV(311.9 nm) (-1972); 4.16 eV(297.8 nm) (-1821); 4.33 eV(286.4 nm) (-3290)
EFISH — γ(-2w; w, w, 0) —	2.00 (619.9)	16217	2.01 eV (616.4 nm) (5741); 3.98 eV(311.9 nm) (5031)
	2.35 (527.6)	9775	2.30 eV(538.1 nm) (1265); 2.41 eV(514.5 nm) (984); 4.33 eV(286.4 nm) (2162)
	3.70 (335.1)	13340	3.66 eV(339.1 nm) (1926); 3.72 eV(333.7 nm) (2926); 3.98 eV(311.9 nm) (4916);
	3.95 (313.9)	15438	3.98 eV(311.9 nm) (7521); 4.09 eV(303.3 nm) (3088); 4.16 eV(297.8 nm) (3703); 4.33 eV(286.4 nm) (3083)
	4.55 (272.5)	-5781	3.98 eV(311.9 nm) (-1208); 4.16 eV(297.8 nm) (-1125); 4.33 eV(286.4 nm) (-2059)

20. Fig. S13 The evolution of third-order nonlinear optic properties with electronic spectra for  $C_{60} @C_{240}(I_h) @C_{540}(1057)$  at specific external fields.









e) DFWM-4.35 eV

















1.5 1.0 1.0 1.0 </>→> (10<sup>-34</sup>esu) (×10<sup>4</sup>)

10





