Table S1: Coefficients of the one-dimensional Fourier expansion for the potential energy curves calculated using different methods in combination with the basis set 6-311++G(d,p) given in Figure 2. The potential is expanded as $V(\varphi) = \sum_{i=0}^{6} a_i f_i$.

		MF	2	B3LYP	-D3BJ	M06-22	x
i	f _i	a; / Hartree	a _i / cm⁻¹	a _i / Hartree	a _i / cm⁻¹	a; / Hartree	a _i / cm⁻¹
0	1	-743.5311916		-745.1229207		-744.9051433	
1	cos α	0.0028798	632.1	0.0029098	638.6	0.0031160	683.9
2	cos 2α	0.0019198	421.3	0.0014663	321.8	0.0013606	298.6
3	cos 3α	0.0013365	293.3	0.0009516	208.8	0.0012842	281.9
4	cos 4α	-0.0000195	-4.3	-0.0002997	-65.8	-0.0003624	-79.5
5	cos 5α	-0.0001154	-25.3	-0.0002322	-51.0	-0.0002568	-56.4
6	cos 6α	-0.0000843	-18.5	-0.0001263	-27.7	-0.0001612	-35.4

Table S2a: Nuclear coordinates in the principal axis system of *syn*-2PT and *syn*-C₁-2PT calculated at the MP2/6-311++G(d,p) level of theory (for atom numbering see Figure 1).

		S	/n		syr	ı-C 1
	a/Å	b/Å	c/Å	a/Å	b/Å	c/Å
S 1	1.456117	-1.068910	-0.001120	-1.425833	-0.996238	0.254844
C2	0.238294	0.148986	-0.026017	-0.117773	0.040897	-0.169793
C3	0.799023	1.424550	-0.018429	-0.558553	1.346264	-0.383623
C4	2.212207	1.395798	-0.001248	-1.949355	1.490184	-0.179608
C5	2.702798	0.099129	0.010986	-2.547706	0.289409	0.170759
C6	-1.185448	-0.244282	0.007579	1.240941	-0.522254	-0.308733
07	-1.511642	-1.426265	0.005583	1.433700	-1.731191	-0.218555
C 8	-2.210229	0.878001	0.051818	2.385416	0.456373	-0.480162
C9	-3.643985	0.365936	-0.032649	2.767487	1.065373	0.878463
H10	3.738959	-0.215527	0.018085	-3.592871	0.111123	0.391075
H11	2.847947	2.274112	0.001793	-2.496545	2.419991	-0.287911
H12	0.207180	2.333266	-0.025575	0.102771	2.158244	-0.665391
H13	-2.046611	1.439292	0.980700	3.226298	-0.105303	-0.895256
H14	-1.990902	1.571496	-0.768932	2.110935	1.245735	-1.187078
H15	-3.859336	-0.318246	0.790567	3.040577	0.273916	1.582180
H16	-4.347855	1.201449	0.010884	3.622152	1.738740	0.770310
H17	-3.805358	-0.178476	-0.965846	1.933921	1.630514	1.304393

		anti			anti-C₁	
	a/Å	b/Å	c/Å	a/Å	b/Å	c/Å
S 1	1.099446	-1.204830	0.078603	0.950111	-1.140002	-0.345710
C2	0.288352	0.316970	0.037589	0.184278	0.387191	-0.108543
C3	1.199980	1.363632	-0.062459	1.103078	1.343126	0.314990
C4	2.539798	0.918524	-0.087529	2.411701	0.826757	0.431822
C5	2.636546	-0.463186	-0.020129	2.477640	-0.519817	0.105100
C6	-1.188412	0.459930	0.014194	-1.269272	0.614848	-0.297548
07	-1.701405	1.566525	0.118265	-1.722777	1.753125	-0.277448
C 8	-2.014906	-0.800719	-0.177295	-2.170530	-0.597062	-0.419678
C9	-3.510253	-0.560055	-0.003688	-2.534641	-1.118626	0.979733
H10	3.532510	-1.070837	-0.007143	3.348220	-1.163379	0.095270
H11	3.405298	1.568197	-0.155130	3.276633	1.400721	0.745249
H12	0.875141	2.396935	-0.112830	0.804975	2.365382	0.519900
H13	-1.793798	-1.186669	-1.181312	-3.071398	-0.281771	-0.952686
H14	-1.654866	-1.562684	0.525883	-1.681298	-1.386698	-1.000875
H15	-3.863945	0.191879	-0.711809	-3.035041	-0.334200	1.554160
H16	-4.065697	-1.487335	-0.167249	-3.208707	-1.976139	0.905548
H17	-3.728552	-0.195626	1.002962	-1.641039	-1.431822	1.527205

Table S2b: Nuclear coordinates in the principal axis system of *anti*-2PT and *anti*- C_1 -2PT calculated at the MP2/6-311++G(d,p) level of theory (for atom numbering see Figure 1).

Table S3a: Rotational constants and dihedral angles of *syn*-2PT calculated at various levels of theory. The deviations between the calculated and the experimental values are given as ΔA , ΔB and ΔC .

Mathad/Basis Sat	Α/	∆ A /	B/	∆ B /	C/	∆C/	α/	β/
Method/Dasis Set	MHz	MHz	MHz	MHz	MHz	MHz	•	٥
MP2/6-31G(d,p)	3410.4	-17.0	879.3	2.1	705.1	0.2	0.0	180.0
MP2/6-31+G(d,p)	3393.4	-34.0	877.5	0.3	703.6	-1.3	-3.2	174.2
MP2/6-31++G(d,p)	3391.1	-36.3	877.8	0.6	703.8	-1.1	-3.7	172.5
MP2/6-311G(d,p)	3404.6	-22.8	877.6	0.4	703.8	-1.1	0.0	180.0
MP2/6-311+G(d,p)	3396.0	-31.4	876.8	-0.4	703.1	-1.8	-2.4	175.9
MP2/6-311++G(d,p)	3394.9	-32.5	877.0	-0.2	703.1	-1.8	-2.6	175.2
MP2/6-311G(df,pd)	3429.5	2.1	883.0	5.8	708.3	3.4	0.0	180.0
MP2/6-311+G(df,pd)	3418.4	-9.0	882.1	4.9	707.5	2.6	-3.5	174.5
MP2/6-311++G(df,pd)	3418.3	-9.1	882.2	5.0	707.6	2.7	-3.5	174.1
MP2/6-311G(3df,3pd)	3442.3	14.9	885.9	8.7	710.7	5.8	0.0	180.0
MP2/6-311+G(3df,3pd)	3432.6	5.2	885.4	8.2	709.9	5.0	0.0	180.0
MP2/6-311++G(3df,3pd)	3432.7	5.3	885.4	8.2	709.9	5.0	0.0	-180.0
MP2/cc-pVDZ	3370.3	-57.1	870.7	-6.5	698.0	-6.9	0.0	180.0
MP2/cc-pVTZ	3423.4	-4.0	883.9	6.7	708.6	3.7	0.0	180.0
MP2/aug-cc-pVDZ	3351.6	-75.8	869.8	-7.4	696.6	-8.3	0.0	180.0
MP2/aug-cc-pVTZ	3419.5	-7.9	883.9	6.7	708.4	3.5	0.0	180.0

B3LYP-D3/6-31G(d,p)	3395.6	-31.8	870.4	-6.8	698.7	-6.2	0.0 -180.0
B3LYP-D3/6-31+G(d,p)	3385.0	-42.4	868.2	-9.0	696.9	-8.0	0.0 -180.0
B3LYP-D3/6-31++G(d,p)	3385.0	-42.4	868.2	-9.0	696.9	-8.0	0.0 -180.0
B3LYP-D3/6-311G(d,p)	3406.5	-20.9	871.5	-5.7	699.9	-5.0	0.0 180.0
B3LYP-D3/6-311+G(d,p)	3400.3	-27.1	870.5	-6.7	699.0	-5.9	0.0 180.0
B3LYP-D3/6-311++G(d,p)	3400.1	-27.3	870.5	-6.7	699.0	-5.9	0.0 -180.0
B3LYP-D3/6-311G(df,pd)	3416.5	-10.9	873.8	-3.4	701.8	-3.1	0.0 180.0
B3LYP-D3/6-311+G(df,pd)	3410.6	-16.8	872.8	-4.4	700.9	-4.0	0.0 180.0
B3LYP-D3/6-311++G(df,pd)	3410.6	-16.8	872.8	-4.4	700.9	-4.0	0.0 180.0
B3LYP-D3/6-311G(3df,3pd)	3437.9	10.5	876.3	-0.9	704.3	-0.6	0.0 -180.0
B3LYP-D3/6-311+G(3df,3pd)	3429.9	2.5	875.8	-1.4	703.6	-1.3	0.0 -180.0
B3LYP-D3/6-311++G(3df,3pd)	3429.7	2.3	875.8	-1.4	703.6	-1.3	0.0 180.0
B3LYP-D3/cc-pVDZ	3385.4	-42.0	868.5	-8.7	697.2	-7.7	0.0 180.0
B3LYP-D3/cc-pVTZ	3423.8	-3.6	874.6	-2.6	702.6	-2.3	0.0 180.0
B3LYP-D3/aug-cc-pVDZ	3377.9	-49.5	867.3	-9.9	696.0	-8.9	0.0 -180.0
B3LYP-D3/aug-cc-pVTZ	3421.1	-6.3	874.5	-2.7	702.4	-2.5	0.0 180.0
B3LYP-D3BJ/6-31G(d n)	3400 4	-27 0	872 9	_4.3	700.6	-4.3	0.0 180.0
B3I YP-D3B I/6-31+G(d p)	3389.2	-38.2	870.7	-6.5	698.7	-6.2	0.0 -180.0
B31 VP -D3B 1/6-31++G(d p)	3389.2	_38.2	870.7	-6.5	698.7	_6.2	0.0 180.0
B3I VP-D3B I/6-311G(d p)	3410.7	_16.7	874.0	_3.2	701 7	_3.2	0.0 180.0
$B3I VP_D3B I/6_311_+C(d p)$	3/0/ 1	_23.3	873.1	_/ 1	700.8	_/ 1	0.0 -180.0
$B_{21} \times P_{-} D_{3B} = \frac{1}{6} - \frac{311 + 4}{6} (d, p)$	3404.1	-20.0	873.1	-4.1	700.0	-4.1	0.0 180.0
$\frac{D3LTF}{D3D3} = \frac{D3D3}{D3} = \frac{D3D3}{D3}$	2420 5	-23.4	976.2	-4.1	700.0	-4.1	0.0 -180.0
$\begin{array}{c} \text{B3L} F - D3B / O - 3 T \cdot G(u,pu) \\ \text{B3L} V D \cdot D3B / O - 3 T \cdot G(u,pu) \\ \text{C}(df pd) \end{array}$	2/1/ 1	-0.9	975 A	-0.9	703.0	-1.3	0.0 - 180.0
$\begin{array}{c} \text{DSL} I = D \\ \text{DSL} I = D \\$	2414.1	12.0	075.4	-1.0 1 0	702.7	-2.2	0.0 - 180.0
$\begin{array}{c} \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{+} \text{-} \text{-} \text{G}(\text{u},\text{pu}) \\ \text{B3L} \text{I} \text{F} \text{-} \text{D3BJ/0-31} \text{I} \text{-} \text{-} \text{I} \text$	3414.0	14.2	070.4	-1.0	702.7	-2.2	0.0 - 180.0
	3441.7	14.3	0/0.0	1.0	700.0	1.1	0.0 -160.0
$B_{2} = P_{2} = P_{2$	0400.Z	5.0 5.7	070.3	1.1	705.4	0.5	0.0 - 100.0
B3L P - D3BJ/6-3 P + G(301,3p0)	3433.1	5.7	878.4	1.2	705.4	0.5	0.0 -180.0
	3390.4	-37.0	871.0	-0.2	699.0 704 4	-5.9	0.0 180.0
	3427.5	0.1	8//.2	0.0	704.4	-0.5	0.0 -180.0
B3LYP-D3BJ/aug-cc-pVDZ	3382.3	-45.1	869.8	-7.4	697.9	-7.0	0.0 -180.0
	3424.7	-2.7	070.0	-0.1	704.2	-0.7	0.0 -180.0
1000 - 23/0 - 31 G(0,p)	3436.0	8.6	8/8.6	1.4	705.7	0.8	0.0 -180.0
IVIU6-2X/6-31+G(d,p)	3427.5	0.1	8/6./	-0.5	704.2	-0.7	0.0 180.0
MU6-2X/6-31++G(d,p)	3427.5	0.1	876.7	-0.5	704.2	-0.7	0.0 180.0
M06-2X/6-311G(d,p)	3441.7	14.3	879.5	2.3	706.5	1.6	0.0 180.0
M06-2X/6-311+G(d,p)	3437.2	9.8	878.6	1.4	705.8	0.9	0.0 180.0
M06-2X/6-311++G(d,p)	3437.1	9.7	878.6	1.4	705.8	0.9	0.0 180.0
M06-2X/6-311G(df,pd)	3449.4	22.0	881.2	4.0	708.0	3.1	0.0 180.0
M06-2X/6-311+G(df,pd)	3445.3	17.9	880.3	3.1	707.2	2.3	0.0 180.0
M06-2X/6-311++G(df,pd)	3445.2	17.8	880.3	3.1	707.2	2.3	0.0 180.0
M06-2X/6-311G(3df,3pd)	3469.5	42.1	883.3	6.1	710.1	5.2	0.0 180.0
M06-2X/6-311+G(3df,3pd)	3463.1	35.7	882.9	5.7	709.7	4.8	0.0 180.0
M06-2X/6-311++G(3df,3pd)	3463.0	35.6	882.9	5.7	709.6	4.7	0.0 180.0
M06-2X/cc-pVDZ	3427.0	-0.4	877.4	0.2	704.6	-0.3	0.0 180.0
M06-2X/cc-pVTZ	3456.1	28.7	882.6	5.4	709.1	4.2	0.0 180.0
	0400 5	6.0	070 4		702.0	10	0.0 190.0

Experiment	3427.4		877.2		704.9			
CCSD/cc-pVDZ	3372.0	-55.4	863.9	-13.3	693.7	-11.2	0.0	180.0
M06-2X/aug-cc-pVTZ	3454.9	27.5	882.5	5.3	709.0	4.1	0.0	180.0

Table S3b: Rotational constants and dihedral angles of *anti*-2PT calculated at various levels of theory. The deviations between the calculated and the experimental values are given as ΔA , ΔB and ΔC .

Mathad/Basis Sat	Α/	∆ A /	B/	∆ B /	C/	∆C/	α/	βΙ
Method/Basis Set	MHz	MHz	MHz	MHz	MHz	MHz	o	o
MP2/6-31G(d,p)	3268.9	-5.1	903.6	-2.1	714.1	-2.1	-180.0	180.0
MP2/6-31+G(d,p)	3242.8	-31.2	904.3	-1.5	715.3	-1.0	172.8	171.7
MP2/6-31++G(d,p)	3241.1	-32.9	904.5	-1.2	715.5	-0.8	172.8	171.4
MP2/6-311G(d,p)	3267.4	-6.6	902.9	-2.8	713.7	-2.6	-180.0	-180.0
MP2/6-311+G(d,p)	3247.0	-27.0	904.6	-1.1	715.7	-0.5	173.3	172.7
MP2/6-311++G(d,p)	3245.4	-28.6	904.8	-1.0	716.0	-0.2	172.8	172.5
MP2/6-311G(df,pd)	3290.8	16.8	909.1	3.4	718.7	2.4	178.8	178.1
MP2/6-311+G(df,pd)	3266.8	-7.2	910.7	5.0	720.9	4.7	172.5	172.1
MP2/6-311++G(df,pd)	3265.7	-8.3	910.8	5.0	721.1	4.9	172.1	172.0
MP2/6-311G(3df,3pd)	3302.2	28.2	913.2	7.5	721.7	5.4	-180.0	180.0
MP2/6-311+G(3df,3pd)	3293.8	19.8	913.7	7.9	721.6	5.3	-180.0	180.0
MP2/6-311++G(3df,3pd)	3293.9	19.9	913.7	7.9	721.6	5.3	-180.0	180.0
MP2/cc-pVDZ	3231.7	-42.3	895.7	-10.1	707.5	-8.7	-180.0	180.0
MP2/cc-pVTZ	3284.1	10.1	911.2	5.4	719.5	3.3	-180.0	180.0
MP2/aug-cc-pVDZ	3215.3	-58.7	897.6	-8.2	707.9	-8.3	-180.0	180.0
B3LYP-D3/6-31G(d,p)	3249.9	-24.1	894.7	-11.1	707.6	-8.6	-180.0	-180.0
B3LYP-D3/6-31+G(d,p)	3240.8	-33.2	893.9	-11.9	706.7	-9.5	-180.0	180.0
B3LYP-D3/6-31++G(d,p)	3240.7	-33.3	893.9	-11.8	706.7	-9.5	-180.0	-180.0
B3LYP-D3/6-311G(d,p)	3260.1	-13.9	895.9	-9.8	708.9	-7.3	-180.0	-180.0
B3LYP-D3/6-311+G(d,p)	3253.6	-20.4	896.4	-9.4	708.9	-7.4	-180.0	180.0
B3LYP-D3/6-311++G(d,p)	3253.4	-20.6	896.4	-9.3	708.9	-7.3	-180.0	180.0
B3LYP-D3/6-311G(df,pd)	3269.7	-4.3	898.7	-7.1	711.1	-5.2	-180.0	-180.0
B3LYP-D3/6-311+G(df,pd)	3263.5	-10.5	899.1	-6.6	711.0	-5.2	-180.0	180.0
B3LYP-D3/6-311++G(df,pd)	3263.3	-10.7	899.1	-6.6	711.0	-5.2	-180.0	180.0
B3LYP-D3/6-311G(3df,3pd)	3291.7	17.7	901.6	-4.1	713.9	-2.3	-179.9	180.0
B3LYP-D3/6-311+G(3df,3pd)	3284.1	10.1	902.3	-3.5	714.0	-2.3	-180.0	180.0
B3LYP-D3/6-311++G(3df,3pd)	3284.0	10.0	902.3	-3.5	714.0	-2.3	-180.0	180.0
B3LYP-D3/cc-pVDZ	3239.1	-34.9	892.9	-12.8	706.1	-10.1	180.0	-180.0
B3LYP-D3/cc-pVTZ	3276.8	2.8	900.6	-5.1	712.6	-3.7	-180.0	180.0
B3LYP-D3/aug-cc-pVDZ	3233.5	-40.5	893.6	-12.1	706.3	-10.0	-180.0	180.0
B3LYP-D3/aug-cc-pVTZ	3274.2	0.2	901.0	-4.7	712.7	-3.5	-180.0	180.0
B3LYP-D3BJ/6-31G(d,p)	3247.0	-27.0	899.1	-6.7	710.2	-6.0	180.0	-180.0
B3LYP-D3BJ/6-31+G(d,p)	3237.7	-36.3	898.4	-7.4	709.4	-6.9	-180.0	-180.0
B3LYP-D3BJ/6-31++G(d,p)	3237.7	-36.3	898.4	-7.4	709.4	-6.9	-180.0	180.0
B3LYP-D3BJ/6-311G(d,p)	3256.8	-17.2	900.4	-5.4	711.5	-4.7	180.0	180.0
B3LYP-D3BJ/6-311+G(d,p)	3250.0	-24.0	901.0	-4.8	711.6	-4.7	-180.0	180.0

M06-2X/6-311++G(d,p) 3288.0 14.0 906.5 0.8 716.8 0.6 -180. M06-2X/6-311G(df,pd) 3301.1 27.1 908.2 2.4 718.5 2.2 -180. M06-2X/6-311+G(df,pd) 3296.3 22.3 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/c-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311++G(d n) 3288.0						
M06-2X/6-311G(df,pd) 3301.1 27.1 908.2 2.4 718.5 2.2 -180. M06-2X/6-311+G(df,pd) 3296.3 22.3 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/c-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/c-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	0200.0	14.0	906.5	0.8	716.8	0.6 -180.0	-180.0
M06-2X/6-311+G(df,pd) 3296.3 22.3 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311G(df.pd) 3301.1	27.1	908.2	2.4	718.5	2.2 -180.0	-180.0
M06-2X/6-311+G(dr,pd) 3296.3 22.3 908.6 2.8 718.5 2.3 -179. M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311+G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/c-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	$V_{0} = 2X/6 - 311G(at,pa)$ 3301.1	27.1	908.2	2.4	/18.5	2.2 -180.0	-180.0
M06-2X/6-311++G(df,pd) 3296.2 22.2 908.6 2.8 718.5 2.3 -179. M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311+G(df,pd) 3296.3	22.3	908.6	2.8	718.5	2.3 –179.9	180.0
M06-2X/6-311F+G(al,pd) 3230.2 22.2 900.0 2.0 718.5 2.3 -179.5 M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180.5 M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180.5 M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180.5 M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180.5 M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180.5 M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.5	$M06_2X/6_311_{\pm\pm}C(df nd) = 3290.3$	22.3	008 6	∠.0 2.9	718.5	2.3 -179.9	180.0
M06-2X/6-311G(3df,3pd) 3321.5 47.5 911.0 5.2 721.2 4.9 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311++G(df,pd) 3296.2	22.2	908.6	2.8	718.5	2.3 –179.9	180.0
M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311G(3df.3pd) 3321.5	47.5	911.0	5.2	721.2	4.9 -180.0	180.0
M06-2X/6-311+G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/6-311++G(3df,3pd) 3315.4 41.4 911.5 5.7 721.2 5.0 -180. M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311G(3dt,3pd) 3321.5	47.5	911.0	5.2	721.2	4.9 –180.0	180.0
M06-2X/6-311++G(3df,3pd)3315.441.4911.55.7721.25.0-180.M06-2X/cc-pVDZ3278.74.7903.5-2.2714.6-1.6-180.M06-2X/cc-pVTZ3307.733.7910.85.0720.44.2-180.M06-2X/aug-cc-pVDZ3274.70.7903.9-1.8714.7-1.6-180.	M06-2X/6-311+G(3df,3pd) 3315.4	41.4	911.5	5.7	721.2	5.0 -180.0	180.0
M06-2X/cc-pVDZ 3278.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/6-311++G(3df 3pd) 3315.4	41 4	911.5	57	721.2	5.0 -180.0	180.0
MU6-2X/cc-pVDZ 32/8.7 4.7 903.5 -2.2 714.6 -1.6 -180. M06-2X/cc-pVTZ 3307.7 33.7 910.8 5.0 720.4 4.2 -180. M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	1000 - 27/0 - 311 + + + + + + + + + + + + + + + + + +	41.4	911.5	5.7	721.2	5.0 -180.0	180.0
M06-2X/cc-pVTZ3307.733.7910.85.0720.44.2-180.M06-2X/aug-cc-pVDZ3274.70.7903.9-1.8714.7-1.6-180.	M06-2X/cc-pVDZ 3278.7	4.7	903.5	-2.2	714.6	–1.6 –180.0	180.0
M06-2X/aug-cc-pVDZ 3274.7 0.7 903.9 -1.8 714.7 -1.6 -180.	M06-2X/cc-pVTZ 3307.7	33.7	910.8	5.0	720.4	4.2 -180.0	180.0
viuo-z/aug-uu-pvuz 32/4./ U./ 903.9 -1.0 /14./ -1.0 -180.	$\frac{100}{2} \frac{2}{100} \frac{1}{2} \frac{1}{100} \frac{1}{1$	07	002.0	1.0	7117	4.2 -100.0	100.0
	v106-2X/aug-cc-pVDZ 3274.7	0.7	903.9	-1.8	714.7	-1.6 -180.0	180.0
M06-2X/aug-cc-pVTZ 3306.6 32.6 911.1 5.4 720.6 4.4 –180.	M06-2X/aug-cc-pVTZ 3306.6	32.6	911.1	5.4	720.6	4.4 -180.0	180.0
CCSD/6-311++G(d.p) 3244.2 -29.8 897.9 -7.8 711.0 -5.3 173	CCSD/6-311++G(d.p) 3244 2	-29.8	897.9	-7.8	711.0	-5.3 173.6	174.6
2222.0 51.0	2CSD/cc p/DZ = 2222.0	£3.0	007.0	15.0	702 5	12.9 190.0	100.0
-100 - 100		-51.0	009.0	-15.9	103.5	-12.0 -100.0	100.0



Figure S1: The potential energy curves of *syn*-2PT obtained by rotating the methyl group around the C8–C9 bond in 10° steps calculated at the different levels of theory with the 6-311++G(d,p) basis set. The predicted rotational barriers are 929.3 cm⁻¹ (MP2), 823.8 cm⁻¹ (M06-2X) and 764.5 cm⁻¹ (B3LYP-D3BJ). The Fourier coefficients of the parameterized potential are given in Table S4.

Table S4: Coefficients of the one-dimensional Fourier expansion for the potential energy curve of *syn*-2PT given in Figure S1 calculated using different methods in combination with the basis set 6-311++G(d,p). The potential is expanded as $V(\varphi) = \sum_{i=0}^{2} a_i f_i$.

		М	2	B3LYP	-D3BJ	M06-2>	(
i	f _i	a _i / Hartree	a _i / cm⁻¹	a; / Hartree	a _i / cm⁻¹	a; / Hartree	a _i / cm⁻¹
0	1	-743.591750		-745.1212221		-744.9032898	
1	cos 3α	0.0021111	463.3	0.0017355	380.9	0.0018733	411.1
2	cos 6α	0.0000805	17.7	0.0000429	9.4	0.0000232	5.1

Kc J Ka Kc J Ka Vobs Vobs-Vcalc Species No. upper level lower level MHz kHz 3155.7033 А -0.3 4712.5964 А -0.2А 6245.1040 -0.2 7747.4055 А -0.1 А 9217.1304 -0.3 10656.5614 -0.7 А А 12072.2521 -0.5 A 13472.8402 -0.3 10 А 14866.3298 0.2

Table S5: Observed frequencies v_{obs} of 201 rotational transitions of *syn*-2PT with $v_{obs}-v_{calc}$ values obtained from a fit with the program *XIAM*.

10	11	0	11	10	0	10	А	16258.3959	-0.1
11	12	0	12	11	0	11	А	17652.1589	-0.2
12	13	0	13	12	0	12	А	19048.8281	0.7
13	14	0	14	13	0	13	А	20448.5041	-0.1
14	16	0	16	15	0	15	А	23255.1592	0.6
15	4	0	4	3	1	3	А	4088.6400	2.1
16	5	0	5	4	1	4	А	5868.4507	1.2
17	6	0	6	5	1	5	А	7640.2300	1.5
18	7	0	7	6	1	6	А	9381.8094	3.4
19	8	0	8	7	1	7	А	11078.0117	1.9
20	9	0	9	8	1	8	А	12722.2717	0.8
21	10	0	10	9	1	9	А	14315.5702	1.0
22	11	0	11	10	1	10	А	15863.7818	-0.5
23	12	0	12	11	1	11	А	17374.9293	0.8
24	13	0	13	12	1	12	А	18857.1752	-0.4
25	14	0	14	13	1	13	А	20317.7589	0.3
26	15	0	15	14	1	14	А	21762.5782	1.3
27	2	1	1	2	0	2	А	2903.2592	-2.4
28	3	1	2	3	0	3	А	3189.8822	-2.4
29	4	1	3	4	0	4	А	3599.9412	-0.8
30	5	1	4	5	0	5	А	4153.8831	4.6
31	7	1	6	7	0	7	А	5764.5981	3.9
32	9	1	8	9	0	9	А	8074.3749	3.8
33	12	1	11	12	0	12	А	12500.6450	3.1
34	13	1	12	13	0	13	А	14093.0648	1.2
35	14	1	13	14	0	14	А	15689.6540	2.6
36	2	1	2	1	0	1	А	5542.1227	-3.7
37	3	1	3	2	0	2	А	6869.0581	-4.8
38	4	1	4	3	0	3	А	8124.0624	2.1
39	4	1	4	3	0	3	Е	8124.0531	-3.0
40	5	1	5	4	0	4	А	9324.3027	-5.1
41	6	1	6	5	0	5	А	10491.8819	-4.9
42	7	1	7	6	0	6	А	11650.8002	-4.7

43	8	1	8	7	0	7	А	12822.8173	-4.9
44	9	1	9	8	0	8	А	14023.6003	-0.6
45	10	1	10	9	0	9	А	15260.9402	-3.1
46	11	1	11	10	0	10	А	16535.6252	-1.4
47	12	1	12	11	0	11	А	17843.8116	0.6
48	13	1	13	12	0	12	А	19179.5728	-0.3
49	14	1	14	13	0	13	А	20536.7220	0.2
50	16	1	16	15	0	15	А	23294.2702	-0.6
51	2	1	1	1	1	0	А	3336.4190	-0.4
52	3	1	2	2	1	1	А	4999.2197	0.1
53	4	1	3	3	1	2	А	6655.1615	-0.2
54	5	1	4	4	1	3	А	8301.3421	0.1
55	6	1	5	5	1	4	А	9934.3305	0.7
56	7	1	6	6	1	5	А	11550.0786	-0.1
57	8	1	7	7	1	6	А	13143.9449	-0.2
58	9	1	8	8	1	7	А	14710.9244	-0.5
59	10	1	9	9	1	8	А	16246.2460	-1.4
60	11	1	10	10	1	9	А	17746.4094	-0.6
61	12	1	11	11	1	10	А	19210.4969	-1.2
62	3	1	3	2	1	2	А	4482.6395	-0.5
63	4	1	4	3	1	3	А	5967.5940	0.0
64	5	1	5	4	1	4	А	7445.3513	-0.4
65	6	1	6	5	1	5	А	8914.9840	-0.6
66	7	1	7	6	1	6	А	10376.0476	-1.3
67	8	1	8	7	1	7	А	11828.5789	-0.4
68	9	1	9	8	1	8	А	13273.0309	-0.4
69	10	1	10	9	1	9	А	14710.1827	-0.2
70	11	1	11	10	1	10	А	16141.0128	-0.1
71	12	1	12	11	1	11	А	17566.5806	0.2
72	13	1	13	12	1	12	А	18987.9215	0.3
73	14	1	14	13	1	13	А	20405.9769	0.8
74	15	1	15	14	1	14	А	21821.5508	1.0
75	8	1	7	7	2	6	А	7510.1492	-3.1
76	8	1	7	7	2	6	Е	7510.1669	3.1
77	9	1	8	8	2	7	А	9666.8532	-2.1
78	9	1	8	8	2	7	Е	9666.8696	3.4
79	10	1	9	9	2	8	А	11824.3636	-2.7
80	10	1	9	9	2	8	Е	11824.3775	1.0
81	11	1	10	10	2	9	А	13958.9940	-1.9
82	11	1	10	10	2	9	Е	13959.0059	0.7
83	12	1	11	11	2	10	А	16046.7625	-2.1
84	12	1	11	11	2	10	E	16046.7749	2.0
85	13	1	12	12	2	11	А	18066.7423	-2.3
86	13	1	12	12	2	11	Е	18066.7515	-0.2
87	2	2	0	1	1	1	Ā	11167.9304	2.7
88	2	2	0	2	1	1	A	7659.2230	-5.6
89	3	2	1	3	1	2	A	7439.8230	-6.0

90 3 2 1 3 1 2 E 7439.8154 -2.3 91 4 2 2 4 1 3 E 7189.5319 1.7 92 5 2 3 5 1 4 A 6942.6837 3.2 94 8 2 6 8 1 7 A 6606.4561 1.5 95 8 2 6 8 1 7 A 6606.4361 1.5 95 8 2 6 8 1 7 E 6606.4430 -1.3 96 2 2 1 2 I 2 E 8167.6285 -2.2 99 3 2 2 3 1 3 B 8431.1837 -0.2 100 4 2 3 4 1 4 A 8785.3091 -3.9 101 4 2 3 1 5 E 971.0678 -7.4 102 5										
91 4 2 2 4 1 3 E 7189.5319 1.7 92 5 2 3 5 1 4 A 6942.6665 -2.0 93 5 2 3 5 1 4 E 6942.6665 -2.0 94 8 2 6 8 1 7 A 6606.4631 1.5 95 8 2 6 8 1 7 E 6606.4631 -5.8 97 2 2 1 2 1 2 E 8167.6122 0.9 98 3 2 2 3 4 1 4 A 8785.3091 -3.9 101 4 2 3 4 1 4 E 8785.2966 -3.0 102 5 6 1 6 E 9771.0678 -7.4 104 6 2 5 6 1 6 E 9771.0575 -2.4 105 7 </th <th>90</th> <th>3</th> <th>2</th> <th>1</th> <th>3</th> <th>1</th> <th>2</th> <th>E</th> <th>7439.8154</th> <th>-2.3</th>	90	3	2	1	3	1	2	E	7439.8154	-2.3
92 5 2 3 5 1 4 A 6942.6837 3.2 93 5 2 3 5 1 4 E 6942.6665 -2.0 94 8 2 6 8 1 7 A 6606.4561 1.5 95 8 2 6 8 1 7 E 6606.4430 -1.3 96 2 2 1 2 1 2 A 8167.6122 0.9 97 2 2 1 2 1 2 E 8167.6122 0.9 98 3 2 2 3 4 1 4 E 8785.2966 -3.0 100 4 2 3 4 1 4 E 8785.2966 -3.0 102 5 6 1 6 A 9771.0578 -7.4 104 6 2 5 6 1 6 E 9771.0595 -2.4 105 7 <th>91</th> <th>4</th> <th>2</th> <th>2</th> <th>4</th> <th>1</th> <th>3</th> <th>Е</th> <th>7189.5319</th> <th>1.7</th>	91	4	2	2	4	1	3	Е	7189.5319	1.7
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125 8 2 7 7 1 6 A 18188.0177 2.9 126 9 2 8 8 1 7 A 19132.8082 2.1 127 9 2 8 8 1 7 E 19132.7901 -3.6 128 10 2 9 9 1 8 A 20033.6647 3.2 129 10 2 9 9 1 8 E 20033.6479 -1.6 130 11 2 10 10 1 9 A 20910.1484 4.9 131 11 2 10 10 1 9 E 20910.1318 -0.2 132 2 2 0 3 1 3 A 3693.4207 -6.7 133 3 2 1 2 2 0 A 4779.8172 -2.8 134 4 2 2 3 4 2 2 A 8054.4797 -0.6 </th <th>124</th> <th>7</th> <th>2</th> <th>6</th> <th>6</th> <th>1</th> <th>5</th> <th>E</th> <th>17183.8549</th> <th>-3.9</th>	124	7	2	6	6	1	5	E	17183.8549	-3.9
126 9 2 8 8 1 7 A 19132.8082 2.1 127 9 2 8 8 1 7 E 19132.7901 -3.6 128 10 2 9 9 1 8 A 20033.6647 3.2 129 10 2 9 9 1 8 E 20033.6479 -1.6 130 11 2 10 10 1 9 A 20910.1484 4.9 131 11 2 10 10 1 9 E 20910.1318 -0.2 132 2 2 0 3 1 3 A 3693.4207 -6.7 133 3 2 1 2 2 0 A 4779.8172 -2.8 134 4 2 2 3 4 2 2 3 A 9729.5416 -0.6 136 6 2 4 5 2 3 A 9729.5416	125	8	2	7	7	1	6	А	18188.0177	2.9
127 9 2 8 8 1 7 E 19132.7901 -3.6 128 10 2 9 9 1 8 A 20033.6647 3.2 129 10 2 9 9 1 8 E 20033.6479 -1.6 130 11 2 10 10 1 9 A 20910.1484 4.9 131 11 2 10 10 1 9 E 20910.1318 -0.2 132 2 2 0 3 1 3 A 3693.4207 -6.7 133 3 2 1 2 2 0 A 4779.8172 -2.8 134 4 2 2 3 2 1 A 6404.8735 -1.4 135 5 2 3 4 2 2 A 8054.4797 -0.6 136 6 2 4 5 2 3 A 9729.5416 -0.5 <	126	9	2	8	8	1	7	А	19132.8082	2.1
128 1029918A20033.6647 3.2 129 1029918E20033.6479 -1.6 130 112101019A20910.14844.9 131 112101019E20910.1318 -0.2 132 220313A 3693.4207 -6.7 133 321220A 4779.8172 -2.8 134 422321A 6404.8735 -1.4 135 523422A 8054.4797 -0.6 136 624523A 9729.5416 -0.5	127	9	2	8	8	1	7	Е	19132.7901	-3.6
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130 11 2 10 10 1 9 A 20910.1484 4.9 131 11 2 10 10 1 9 E 20910.1318 -0.2 132 2 2 0 3 1 3 A 3693.4207 -6.7 133 3 2 1 2 2 0 A 4779.8172 -2.8 134 4 2 2 3 2 1 A 6404.8735 -1.4 135 5 2 3 4 2 2 3 A 9729.5416 -0.5	129	10	2	9	9	1	8	F	20033 6479	_1.6
131 11 2 10 10 1 9 E 20910.1318 -0.2 132 2 2 0 3 1 3 A 3693.4207 -6.7 133 3 2 1 2 2 0 A 4779.8172 -2.8 134 4 2 2 3 2 1 A 6404.8735 -1.4 135 5 2 3 4 2 2 3 A 9729.5416 -0.5	130	11	2	10	10	1	a	Δ	20000.0470	4.0
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135 5 2 3 4 2 2 A 8054.4797 -0.6 136 6 2 4 5 2 3 A 9729.5416 -0.5	134	4	2	2	3	2	1	A	6404.8735	-1.4
136 6 2 4 5 2 3 A 9729.5416 -0.5	135	5	2	3	4	2	2	А	8054.4797	-0.6
	<u>13</u> 6	6	2	4	5	2	3	А	9729.5416	-0.5

137 7 2 5 6 2 4 A 11426.2378 -0.8 138 8 2 6 7 2 5 A 13136.3442 -2.9 139 3 2 2 2 2 1 A 4746.2100 2.6 140 3 2 2 2 1 E 4746.2157 3.1 141 4 2 3 3 2 2 A 6321.7094 0.5 142 5 2 4 4 2 3 A 7891.5962 0.4 143 6 2 5 5 2 4 A 9454.5026 0.0 144 7 2 6 6 2 5 A 11009.1174 -0.4 145 8 2 7 7 2 6 A 1254.2219 -0.1 144 3 3 1 2 2 0 A 17924.9233 4.1 149	
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143 6 2 5 5 2 4 A 9454.5026 0.0 144 7 2 6 6 2 5 A 11009.1174 -0.4 145 8 2 7 7 2 6 A 12554.2219 -0.1 146 9 2 8 8 2 7 A 14088.7367 0.2 147 10 2 9 9 2 8 A 15611.7805 0.1 148 3 3 1 2 2 0 A 17924.9233 4.1 149 4 3 2 3 2 1 E 19489.4067 1.0 151 5 3 3 4 2 2 A 21021.3322 1.0 152 5 3 3 4 2 2 E 21021.2940 2.0 153 6 3 4 5 2 3 E 22498.6948 2.2	
144 7 2 6 6 2 5 A 11009.1174 -0.4 145 8 2 7 7 2 6 A 12554.2219 -0.1 146 9 2 8 8 2 7 A 14088.7367 0.2 147 10 2 9 9 2 8 A 15611.7805 0.1 148 3 3 1 2 2 0 A 17924.9233 4.1 149 4 3 2 3 2 1 A 19489.4967 1.0 151 5 3 3 4 2 2 A 21021.3322 1.0 152 5 3 3 4 2 2 E 21021.2940 2.0 153 6 3 4 5 2 3 E 22498.7213 1.0 154 6 3 4 5 2 3 E 22498.6948 2.2	
145 8 2 7 7 2 6 A 1100000000000000000000000000000000000	
146 9 2 8 8 2 7 A 14088.7367 0.2 147 10 2 9 9 2 8 A 15611.7805 0.1 148 3 3 1 2 2 0 A 17924.9233 4.1 149 4 3 2 3 2 1 A 19489.4971 2.4 150 4 3 2 3 2 1 E 19489.4067 1.0 151 5 3 3 4 2 2 A 21021.3322 1.0 152 5 3 3 4 2 2 E 21021.2940 2.0 153 6 3 4 5 2 3 A 22498.6948 2.2 153 6 3 4 5 2 3 E 22498.6948 2.2 155 3 3 0 2 2 1 E 17933.8408 -4.6	
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147 10 2 9 9 2 8 A 15011.7805 0.1 148 3 3 1 2 2 0 A 17924.9233 4.1 149 4 3 2 3 2 1 A 19489.4971 2.4 150 4 3 2 3 2 1 E 19489.4067 1.0 151 5 3 3 4 2 2 A 21021.3322 1.0 152 5 3 3 4 2 2 E 21021.2940 2.0 153 6 3 4 5 2 3 A 22498.6948 2.2 155 3 0 2 2 1 A 17933.6158 1.4 156 3 0 2 2 1 E 17933.8408 -4.6 157 4 3 1 3 2 2 E 19533.3540 2.5 158 4	
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153 6 3 4 5 2 3 A 22498.7213 1.0 154 6 3 4 5 2 3 E 22498.6948 2.2 155 3 3 0 2 2 1 A 17933.6158 1.4 156 3 3 0 2 2 1 E 17933.8408 -4.6 157 4 3 1 3 2 2 A 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.4011 3.6 159 5 3 2 4 2 3 A 21153.7564 -1.8 160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12790.7184 3.6 162 6 3 3 6 2 4 E 12790.6994 0.7	
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155 3 3 0 2 2 1 A 17933.6158 1.4 156 3 3 0 2 2 1 E 17933.8408 -4.6 157 4 3 1 3 2 2 A 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.4011 3.6 159 5 3 2 4 2 3 A 21153.7564 -1.8 160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12790.7184 3.6 162 6 3 3 6 2 4 E 12790.6994 0.7	
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157 4 3 1 3 2 2 A 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.3540 2.5 158 4 3 1 3 2 2 E 19533.3540 2.5 159 5 3 2 4 2 3 A 21153.7564 -1.8 160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12974.0602 -2.5 162 6 3 3 6 2 4 A 12790.7184 3.6 163 6 3 3 6 2 4 E 12790.6994 0.7 164 8 3 5 8 2 6 A 12179.8775 1.6 165 8 3 5 8 2 6 E 13209.7486 0.7	
158 4 3 1 3 2 2 E 19533.4011 3.6 159 5 3 2 4 2 3 A 21153.7564 -1.8 160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12974.0602 -2.5 162 6 3 3 6 2 4 A 12790.7184 3.6 163 6 3 3 6 2 4 E 12790.6994 0.7 164 8 3 5 8 2 6 A 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8775 1.6 166 4 3 2 4 2 3 A 13209.8354 0.4 167 4 3 2 4 2 3 E 13209.7486 0.7	
159 5 3 2 4 2 3 A 21153.7564 -1.8 160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12974.0602 -2.5 162 6 3 3 6 2 4 A 12790.7184 3.6 163 6 3 3 6 2 4 E 12790.6994 0.7 164 8 3 5 8 2 6 A 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8775 1.6 166 4 3 2 4 2 3 A 13209.8354 0.4 167 4 3 2 4 2 3 E 13209.7486 0.7 168 5 3 3 5 2 4 A 13254.9473 -3.3	
160 3 3 0 3 2 1 E 13145.5850 4.0 161 5 3 2 5 2 3 A 12974.0602 -2.5 162 6 3 3 6 2 4 A 12790.7184 3.6 163 6 3 3 6 2 4 E 12790.6994 0.7 164 8 3 5 8 2 6 A 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8775 1.6 166 4 3 2 4 2 3 A 13209.8354 0.4 167 4 3 2 4 2 3 E 13209.7486 0.7 168 5 3 3 5 2 4 A 13254.9473 -3.3 169 5 3 3 5 2 4 E 13254.9167 4.4 <td></td>	
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163 6 3 3 6 2 4 E 12790.6994 0.7 164 8 3 5 8 2 6 A 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8775 1.6 166 4 3 2 4 2 3 A 13209.8354 0.4 167 4 3 2 4 2 3 E 13209.7486 0.7 168 5 3 3 5 2 4 A 13254.9473 -3.3 169 5 3 3 5 2 4 E 13254.9167 4.4	
164 8 3 5 8 2 6 A 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8988 1.9 165 8 3 5 8 2 6 E 12179.8775 1.6 166 4 3 2 4 2 3 A 13209.8354 0.4 167 4 3 2 4 2 3 E 13209.7486 0.7 168 5 3 3 5 2 4 A 13254.9473 -3.3 169 5 3 3 5 2 4 E 13254.9167 4.4	
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169 5 3 3 5 2 4 E 13254.9167 4.4	
1/0 0 3 4 0 2 5 A 13332.3101 -1.2	
171 b 3 4 b 2 5 E 13332.2930 2.5	
172 / 3 5 / 2 6 A 13452.4578 2.4	
173 7 3 5 7 2 6 E 13452.4332 1.1	
174 8 3 6 8 2 7 A 13626.0119 –0.8	
175 8 3 6 8 2 7 E 13625.9924 1.6	
176 9 3 7 9 2 8 A 13863.2060 -0.6	
177 9 3 7 9 2 8 E 13863.1852 -0.2	
178 4 3 1 4 2 2 A 13086.4264 -1.1	
179 4 3 1 4 2 2 E 13086.4740 2.3	
180 6 3 3 5 2 4 A 22808.3610 4.4	
181 6 3 3 5 2 4 E 22808.3413 0.2	
182 5 3 2 4 3 1 A 7942.1169 1.4	
183 5 3 2 4 3 1 E 7942.0647 _17	

184	6	3	3	5	3	2	А	9546.1950	0.8
185	6	3	3	5	3	2	Е	9546.1807	-2.0
186	7	3	4	6	3	3	А	11161.1629	-2.3
187	5	3	3	4	3	2	А	7936.7101	-1.3
188	5	3	3	4	3	2	Е	7936.7597	-0.6
189	6	3	4	5	3	3	А	9531.8671	-2.3
190	6	3	4	5	3	3	Е	9531.8811	0.5
191	7	3	5	6	3	4	А	11129.2568	0.9
192	8	3	6	7	3	5	А	12727.7789	-0.4
193	4	4	0	4	3	1	А	18438.2480	0.5
194	5	4	1	5	3	2	А	18425.2556	-3.9
195	6	4	2	6	3	3	А	18400.3063	2.4
196	7	4	3	7	3	4	А	18356.0687	-3.0
197	4	4	1	4	3	2	А	18440.0479	-0.7
198	5	4	2	5	3	3	А	18432.4090	-3.3
199	6	4	3	6	3	4	А	18421.5439	-1.6
200	7	4	4	7	3	5	А	18408.4348	-3.5
201	4	4	1	5	3	2	А	10496.1272	1.8

Table S6: Observed frequencies v_{obs} of 135 rotational transitions of *anti*-2PT, with $v_{obs}-v_{calc}$ values obtained from a fit with the program *XIAM*.

No	J	Ka	Kc	J	Ka	Kc	Snacias	Vobs	Vobs-Vcalc
140.	upp	oer le	vel	low	er le	evel	opecies	MHz	kHz
1	2	0	2	1	0	1	А	3233.0313	-0.9
2	3	0	3	2	0	2	А	4822.4766	-0.3
3	4	0	4	3	0	3	А	6380.7904	-0.7
4	5	0	5	4	0	4	А	7901.5837	0.0
5	6	0	6	5	0	5	А	9384.0023	0.5
6	7	0	7	6	0	6	А	10833.7562	0.5
7	8	0	8	7	0	7	А	12261.1817	0.2
8	9	0	9	8	0	8	А	13677.2371	0.0
9	10	0	10	9	0	9	А	15090.2141	0.6
10	12	0	12	11	0	11	А	17922.7399	0.3
11	13	0	13	12	0	12	А	19344.2815	0.8
12	14	0	14	13	0	13	А	20768.8765	0.1
13	15	0	15	14	0	14	А	22195.8273	0.0
14	16	0	16	15	0	15	А	23624.4912	1.1
15	3	0	3	2	1	2	А	2632.7742	-0.4
16	3	0	3	2	1	2	Е	2632.7765	-0.6
17	4	0	4	3	1	3	А	4438.5437	3.1
18	4	0	4	3	1	3	Е	4438.5395	-3.5
19	5	0	5	4	1	4	А	6251.9501	-0.3
20	6	0	6	5	1	5	А	8043.6780	0.2
21	7	0	7	6	1	6	А	9791.0736	-1.1
22	8	0	8	7	1	7	А	11482.1107	-0.3

23	9	0	9	8	1	8	А	13115.3559	-0.1
24	9	0	9	8	1	8	Е	13115.3605	3.6
25	10	0	10	9	1	9	А	14696.7963	-1.1
26	10	0	10	9	1	9	Е	14696.7991	1.1
27	11	0	11	10	1	10	А	16235.8761	0.3
28	12	0	12	11	1	11	А	17742.4807	0.2
29	13	0	13	12	1	12	А	19225.3272	0.6
30	14	0	14	13	1	13	А	20691.3810	0.2
31	15	0	15	14	1	14	А	22145.8753	-2.0
32	5	1	4	5	0	5	А	4172.0012	0.8
33	5	1	4	5	0	5	Е	4171.9960	-2.1
34	6	1	5	6	0	6	А	4989.6610	1.7
35	6	1	5	6	0	6	Е	4989.6548	-2.3
36	11	1	10	11	0	11	А	11653.7128	-1.0
37	11	1	10	11	0	11	Е	11653.7101	-1.0
38	2	1	2	1	0	1	А	5422.7354	0.9
39	2	1	2	1	0	1	Е	5422.7290	-3.0
40	3	1	3	2	0	2	А	6764.7284	1.1
41	3	1	3	2	0	2	Е	6764.7230	-1.8
42	4	1	4	3	0	3	А	8030.4244	0.0
43	4	1	4	3	0	3	Е	8030.4186	-3.2
44	5	1	5	4	0	4	А	9241.9082	0.5
45	5	1	5	4	0	4	Е	9241.9051	-0.2
46	6	1	6	5	0	5	А	10426.6839	1.1
47	6	1	6	5	0	5	Е	10426.6790	-1.4
48	7	1	7	6	0	6	А	11612.8290	2.7
49	7	1	7	6	0	6	Е	11612.8241	0.0
50	8	1	8	7	0	7	А	12823.0596	-3.0
51	9	1	9	8	0	8	А	14070.6551	1.9
52	9	1	9	8	0	8	Е	14070.6431	-8.5
53	10	1	10	9	0	9	А	15359.1143	0.0
54	11	1	11	10	0	10	А	16685.0363	0.7
55	11	1	11	10	0	10	Е	16685.0289	-5.6
56	13	1	13	12	0	12	А	19421.7763	-0.1
57	14	1	14	13	0	13	А	20818.8259	-0.5
58	15	1	15	14	0	14	А	22227.7322	-1.5
59	16	1	16	15	0	15	А	23644.7147	0.4
60	2	1	1	1	1	0	А	3433.4649	-2.0
61	2	1	1	1	1	0	Е	3433.4680	1.1
62	3	1	2	2	1	1	А	5143.1642	1.1
63	3	1	2	2	1	1	Е	5143.1586	-4.5
64	4	1	3	3	1	2	А	6843.8542	-0.6
65	5	1	4	4	1	3	А	8531.5979	-0.7
66	6	1	5	5	1	4	А	10201.6615	0.9
67	7	1	6	6	1	5	А	11848.4320	0.1
68	8	1	7	7	1	6	А	13465.5925	0.9
69	9	1	8	8	1	7	А	15046.7483	0.9

70	11	1	10	10	1	9	A	18083.6850	1.1
71	12	1	11	11	1	10	А	19540.4734	1.1
72	2	1	2	1	1	1	А	3054.4417	-3.1
73	2	1	2	1	1	1	Е	3054.4448	-0.1
74	3	1	3	2	1	2	А	4575.0247	-0.4
75	4	1	4	3	1	3	А	6088 1737	-0.2
76	5	1	5	1	1	1	Δ	7502 2751	0.2
70	5	1	5	4	1	4		0000 2504	0.7
77	0	I	0	5		5	A	9086.3594	0.7
78	1	1	1	6	1	6	A	10570.1456	0.3
79	8	1	8	7	1	7	A	12043.9926	0.6
80	9	1	9	8	1	8	A	13508.7730	0.9
81	10	1	10	9	1	9	А	14965.6979	-0.3
82	11	1	11	10	1	10	А	16416.1349	0.0
83	13	1	13	12	1	12	А	19302.8228	0.6
84	14	1	14	13	1	13	А	20741.3308	0.1
85	2	2	0	1	1	1	A	10738 7473	_1 0
86	2	2	n N	1	1	1	F	10738 7/02	_2 3
97	2	2	1	י ר	1	י ר	^	12502 6040	-2.5
01	3	2	ן ג	2	ן ג	2		12090.0940	4.Z
88	3	2	1	2	1	2	E	12593.6757	-1.1
89	4	2	2	3	1	3	A	14605.1746	2.0
90	4	2	2	3	1	3	E	14605.1721	6.9
91	5	2	3	4	1	4	А	16810.8115	1.3
92	7	2	5	6	1	6	А	21950.3955	-1.1
93	3	2	1	3	1	2	А	6881.9978	3.6
94	3	2	1	3	1	2	Е	6881.9837	-3.3
95	4	2	2	4	1	3	А	6624.6432	-3.3
96	5	2	3	5	1	4	Α	6386 8651	57
97	5	2	3	5	1	4	F	6386 8521	-0.1
00	2	2	1	1	4	т 0		10520 2002	-0.1
90	2	2	י ר	י 2	1	4		10000.0000	-5.0
99	3	2	2	2	1	1	A	11970.7775	-0.3
100	3	2	2	2	1	1	E	119/0.//33	3.5
101	4	2	3	3	1	2	A	13307.0155	-1.9
102	4	2	3	3	1	2	Е	13307.0101	0.5
103	5	2	4	4	1	3	А	14548.7730	0.1
104	5	2	4	4	1	3	Е	14548.7617	-3.5
105	6	2	5	5	1	4	А	15699.9803	0.1
106	6	2	5	5	1	4	Е	15699.9710	-1.6
107	7	2	6	6	1	5	А	16767 6598	2.0
108	7	2	e e	e A	1	5	F	16767 6477	_2.5
100	، ٥	2	7	7	1	5	~	17762 0/60	-2.5
109	0	2	1	<i>'</i>	ן ג	0	A ^	7672 2000	J.4
110	2	2	1	2	1	2	A	1013.3808	1.2
111	2	2	1	2	1	2	E	7673.3732	3.0
112	3	2	2	3	1	3	А	7964.2862	0.2
113	4	2	3	4	1	4	А	8355.5172	2.3
114	5	2	4	5	1	5	А	8848.8538	3.1
115	6	2	5	6	1	6	А	9445.3031	5.2
	0	2	Б	6	1	6	F	0445 2860	1 2

117	8	2	7	8	1	8	А	10944.2207	4.4
118	8	2	7	8	1	8	Е	10944.2015	-7.2
119	4	2	2	3	2	1	А	6586.5063	-0.7
120	5	2	3	4	2	2	А	8293.8110	-0.5
121	6	2	4	5	2	3	А	10030.2289	-0.1
122	7	2	5	6	2	4	А	11787.9939	3.3
123	8	2	6	7	2	5	А	13554.4712	1.2
124	4	2	3	3	2	2	А	6479.4045	1.8
125	5	2	4	4	2	3	А	8085.6106	0.3
126	6	2	5	5	2	4	А	9682.8069	1.0
127	7	2	6	6	2	5	А	11269.3384	0.3
128	8	2	7	7	2	6	А	12843.7204	2.8
129	4	3	2	4	2	3	А	12350.9653	-1.6
130	5	3	2	4	3	1	А	8151.6731	-1.4
131	6	3	3	5	3	2	А	9803.2117	4.8
132	8	3	5	7	3	4	А	13156.3934	-1.0
133	5	3	3	4	3	2	А	8143.4489	-0.2
134	5	3	3	4	3	2	Е	8143.4539	-7.0
135	6	3	4	5	3	3	А	9781.4585	3.0

Table S7: Molecular parameters of *syn*-2PT and *anti*-2PT obtained with the program *XIAM* where the angles between the internal rotor axis and the principal axes of inertia are fixed to values predicted at the B3LYP-D3BJ/6-311++G(d,p) level of theory.

Par. ^a	Unit	syn	Calc. ^b	anti	Calc. ^b
A_0	MHz	3427.43880(19)	3383.114	3274.03476(39)	3222.920
B_0	MHz	877.177067(48)	866.872	905.747027(78)	895.759
C_0	MHz	704.893296(31)	696.450	716231414 (37)	707.766
D_J	kHz	0.01812(15)	0.0175	0.02330(31)	0.0228
D _{JK}	kHz	0.0749(27)	0.0820	0.0621(69)	0.0419
Dκ	kHz	0.4474(93)	0.4541	1.842(58)	0.4957
d_1	kHz	-0.00370(10)	-0.0039	-0.00639(30)	-0.0056
d ₂	kHz	-0.000275(69)	-0.0004	-0.00138(25)	-0.0004
V_3	cm⁻¹	807.00(54)	764.5	865.4(88)	753.0
∠(i,a)	deg	19.9 ^c	19.9	9.9 ^c	9.9
∠(i,b)	deg	70.2 ^c	70.2	80.1°	80.1
∠(i,c)	deg	90.0 ^c	90.0	90.0 ^c	90.0
N _A /N _E ^d	-	150/51		103/32	
σ^{e}	kHz	2.6		2.5	

^a All parameters refer to the principal axis system. Watson's S reduction and I^r representation were used. ^b Ground state rotational constants and centrifugal distortion constants from anharmonic frequency calculations, all other parameters from optimisations at the B3LYP-D3BJ/6-311++G(d,p) level of theory. ^c Fixed to the values calculated at the B3LYP-D3BJ/6-311++G(d,p) level predicting a planar geometry. ^d Number of A and E species transitions. ^e Standard deviation of the fit.

No	J	Ka	Kc	J	Ka	Kc	Vobs	Vobs-Vcalc
NO.	up	per le	evel	low	er le	evel	MHz	kHz
1	2	0	2	1	0	1	3130.6784	-0.1
2	3	0	3	2	0	2	4674.7172	-1.0
3	4	0	4	3	0	3	6194.0013	-0.3
4	5	0	5	4	0	4	7682.6943	0.5
5	6	0	6	5	0	5	9138.5519	1.6
6	2	1	2	1	0	1	5472.7622	-3.2
7	5	1	5	4	0	4	9219.1284	-1.8
8	6	1	6	5	0	5	10376.0502	-0.8
9	7	1	7	6	0	6	11525.3196	-0.2
10	3	1	3	2	1	2	4445.3162	-0.2
11	4	1	4	3	1	3	5917.6849	-1.1
12	5	1	5	4	1	4	7382.7606	-0.2
13	3	1	2	2	1	1	4961.7111	1.0
14	4	1	3	3	1	2	6604.9657	0.2
15	5	1	4	4	1	3	8238.2752	0.1
16	2	2	0	1	1	1	11009.4573	-3.3
17	3	2	1	2	1	2	12785.4664	-0.5
18	4	2	2	3	1	3	14696.4655	-7.9
19	4	2	3	3	1	2	13536.1898	4.1
20	3	2	1	3	1	2	7307.0851	-10.1
21	6	2	5	5	2	4	9379.2202	0.7
22	3	3	0	2	2	1	17673.5653	6.1
23	3	3	1	2	2	0	17664.7218	5.5

Table S8a: Observed frequencies v_{obs} of 23 rotational transitions of the ³⁴S isotopologue of *syn*-2PT with $v_{obs}-v_{calc}$ values obtained from a fit with the program *XIAM*.

Table S8b: Observed frequencies v_{obs} of 15 rotational transitions of the ¹³C(6) isotopologue (for atom numbering see Figure 1) of *syn*-2PT with v_{obs} - v_{calc} values obtained from a fit with the program *XIAM*.

No	J	Ka	Kc	J	Ka	Kc	V _{obs}	V _{obs} –V _{calc}
140.	up	oer le	vel	low	ver le	evel	MHz	kHz
1	2	0	2	1	0	1	3148.8581	-0.6
2	3	0	3	2	0	2	4702.4997	0.9
3	4	0	4	3	0	3	6231.9455	1.1
4	5	0	5	4	0	4	7731.4034	1.0
5	2	1	2	1	0	1	5536.8014	0.1
6	3	1	3	2	0	2	6861.2767	-4.0
7	4	1	4	3	0	3	8114.0453	-1.3
8	5	1	5	4	0	4	9312.1487	-1.9
9	3	1	3	2	1	2	4473.3385	0.3
10	5	1	5	4	1	4	7430.0502	1.9
11	2	2	0	1	1	1	11162.2901	3.0
12	3	2	1	2	1	2	12945.8286	-4.3
13	4	2	2	3	1	3	14862.9280	-1.0
14	3	2	2	2	1	1	12389.3421	2.0
15	4	2	3	3	1	2	13709.4111	2.5

Table S8c: Observed frequencies v_{obs} of 14 rotational transitions of the ¹³C(8) isotopologue (for atom numbering see Figure 1) of *syn*-2PT, with $v_{obs}-v_{calc}$ obtained from a fit with the program *XIAM*.

No	J	Ka	Kc	J	Ka	Kc	V _{obs}	V _{obs} –V _{calc}
140.	upp	oer le	vel	low	ver le	evel	MHz	kHz
1	3	0	3	2	0	2	4674.5215	0.2
2	4	0	4	3	0	3	6194.9983	-0.9
3	5	0	5	4	0	4	7685.7609	1.6
4	2	1	2	1	0	1	5508.1655	-3.6
5	3	1	3	2	0	2	6824.9792	-0.4
6	4	1	4	3	0	3	8070.5414	2.3
7	5	1	5	4	0	4	9261.7360	-2.2
8	3	1	3	2	1	2	4446.8861	0.4
9	5	1	5	4	1	4	7386.1996	1.2
10	5	1	4	4	1	3	8232.9167	0.8
11	2	2	0	1	1	1	11108.0603	2.8
12	3	2	1	2	1	2	12880.6632	5.2
13	4	2	2	3	1	3	14785.7556	-5.1
14	4	2	3	3	1	2	13640.5904	-1.7

Table S8d: Observed frequencies v_{obs} of 12 rotational transitions of the ¹³C(9) isotopologue (for atom numbering see Figure 1) of *syn*-2PT, with $v_{obs}-v_{calc}$ obtained from a fit with the program *XIAM*.

No	J	Ka	Kc	J	Ka	Kc	V _{obs}	V _{obs} –V _{calc}
NO.	up	per le	evel	low	ver le	evel	MHz	kHz
1	2	0	2	1	0	1	3091.1949	0.5
2	3	0	3	2	0	2	4617.5420	-1.3
3	4	0	4	3	0	3	6121.4372	-0.3
4	2	1	2	1	0	1	5500.6074	-2.6
5	4	1	4	3	0	3	8039.4466	-0.7
6	5	1	5	4	0	4	9220.0956	0.3
7	5	1	5	4	1	4	7302.0868	1.3
8	2	2	0	1	1	1	11139.0376	-1.7
9	3	2	1	2	1	2	12884.8388	0.7
10	4	2	2	3	1	3	14757.6418	-0.1
11	3	2	2	2	1	1	12349.8256	2.6
12	4	2	3	3	1	2	13650.0156	-0.4

Table S8e: Observed frequencies v_{obs} of 4 rotational transitions of the ³⁴S isotopologue of *anti*-2PT, with $v_{obs}-v_{calc}$ obtained from a tentative fit with the program *XIAM*.

No	J	Ka	Kc	J	Ka	Kc	Vobs	Vobs-Vcalc
1	up	ber le	vel	lower level			MHz	kHz
1	2	2	0	1	1	1	10558.2584	-0.2
2	5	1	5	4	0	4	9134.7002	2.1
3	6	0	6	5	0	5	9318.5508	0.0
4	6	1	6	5	0	5	10310.7978	-1.7