# Supporting Information Design the co-symbiotic Fe<sub>x</sub>Mn<sub>y</sub>O catalysts for NO reduction by CO

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Fig. S1 SEM image of sample  $Fe_{0.1}Mn_{0.9}O$ 



Fig. S2 SEM image of sample  $Fe_{0.2}Mn_{0.8}O$ 



Fig. S3 SEM images of sample  $Fe_{0.25}Mn_{0.75}O$ 



Fig. S4 SEM images of sample  $Fe_{0.35}Mn_{0.65}O$ 



Fig. S5 the HRTEM image of  $Fe_{0.3}Mn_{0.7}O$  at 200 nm



Fig. S6 the N<sub>2</sub> sorption isotherms and pore size distribution curves of Fe<sub>x</sub>Mn<sub>y</sub>O samples.



Fig. S7 the CO conversion of the Fe<sub>x</sub>Mn<sub>y</sub>O catalysts. (Reaction condition: 50 mg of catalyst,

5 vol% NO/He+10 vol% CO/He, 1 bar, GHSV=24 000 mL $\cdot$ g<sub>cat</sub>-1·h-1)

As can be seen from Fig. S7, the CO conversion rate was significantly increased after FeO<sub>x</sub> was added. At low temperature, the CO conversion rate was about 15 %. With the temperature rising to 300 °C, the curve rose rapidly, which may be the result of the rapid adsorption and activation of the reaction gas on the catalyst at this temperature. At 300 °C, the CO conversion rate reached 50 %, while the NO conversion rate reached 100 %, indicating that NO and CO were basically in dynamic equilibrium state on the catalyst. As the temperature rises further, it can be found that the CO conversion rate of the catalyst exceeds 50 %. This may be because the temperature rise leads to the reduction of the surface of the catalyst Fe<sub>x</sub>Mn<sub>y</sub>O, which then leads to the CO conversion rate exceeding 50 %.



Fig. S8 The results of H<sub>2</sub>O or/and SO<sub>2</sub> resistance test of the Fe<sub>0.3</sub>Mn<sub>0.7</sub>O catalysts at 300 °C

 $(10 \text{ vol}\% \text{ H}_2\text{O}, 500 \text{ ppm SO}_2 \text{ and } 10 \text{ vol}\% \text{ H}_2\text{O} + 500 \text{ ppm SO}_2).$ 

Fig. S8 is the test result of water resistance and sulfur resistance of  $Fe_{0.3}Mn_{0.7}O$  catalyst at 300 °C. It can be seen from the figure that the NO conversion rate of the catalyst is basically unaffected after water is poured, indicating that the catalyst has good water resistance. When SO<sub>2</sub> is injected, NO conversion of the catalyst decreases obviously, but when SO<sub>2</sub> is shut down, NO conversion of the catalyst increases. When H<sub>2</sub>O and SO<sub>2</sub> were injected simultaneously, the NO conversion rate of the catalyst showed the same trend as that of sulfur alone, but its decline was larger. This indicates that the influence of SO<sub>2</sub> on the catalyst is greater than that of H<sub>2</sub>O, and the sulfur resistance of the catalyst is not very good. This may be due to the formation of sulfate on the surface of the catalyst by SO<sub>2</sub>, which occupies the active part of the catalyst, leading to the degradation of the performance of the catalyst <sup>[6]</sup>.



Fig. S9 The activity stability test of the Fe<sub>0.3</sub>Mn<sub>0.7</sub>O catalysts at 300 °C

(Reaction condition: 50 mg of catalyst, 5 vol% NO/He+10 vol% CO/He, 1 bar, GHSV=24

 $000 \text{ mL} \cdot g_{cat}^{-1} \cdot h^{-1})$ 

The stability of the sample test data, are also supporting material supplement, specific content is as follows: the stability of the catalyst is the key factor in its catalytic application, so we passed in 300 °C, the GHSV = 24 000 mL·g<sub>cat</sub><sup>-1</sup>·h<sup>-1</sup> 8 hours pass into the CO-SCR reaction, can be found from figure integrated under 300 °C Fe<sub>0.3</sub>Mn<sub>0.7</sub>O NO conversion and N<sub>2</sub> selectivity of catalysts basic did not change, only fell by about 2 %, this shows that the catalyst has good activity stability.



Fig. S10 The NO conversions in Fe<sub>x</sub>Mn<sub>y</sub>O catalysts, reaction conditions: 10 vol. % CO (10 vol. % CO and 90 vol. % He), 5 vol. % NO (5 vol. % NO and 95 vol. % He), 10 vol% H<sub>2</sub>O(10 vol. % H<sub>2</sub>O and 90 vol. % He), 1 vol. % O<sub>2</sub> (1 vol. % O<sub>2</sub> and 99 vol. % He), GHSV = 24000 mL·g<sub>cat</sub><sup>-1</sup>·h<sup>-1</sup>.

Catalytic property of these synthesized samples for  $NO_x$  reduction in presence of  $H_2O$  and  $O_2$  are explored at 100–400 °C, as observed in Fig. S10. It can be seen from Fig. S10(a) that the conversion rate of NO after adding water is basically unchanged, indicating that the water resistance of the catalyst is good. According to Fig. S10(b),

the optimal activity of all catalysts decreased significantly to about 65 % after  $O_2$  was added, which indicated that the oxygen resistance of the catalyst was poor, and the addition of  $O_2$  obviously inhibited the transformation of NO and reduced the NO conversion rate of the catalyst. However, it is worth noting that with the increase of temperature, the catalytic performance of catalyst  $Fe_{0.3}Mn_{0.7}O$  still the best, which further proves that doping appropriate amount of Fe can effectively improve the performance of catalyst. However, the poor catalytic performance of the catalyst due to the addition of  $O_2$  is also of concern. This is because our preparation  $Fe_xMn_yO$ catalyst is mainly applied to gasoline vehicles, a better general performance after oxygen catalyst is mainly used in diesel type of car, this is also a point, we should continue to further study for research that can have good oxygen resistance, and can be widely used in the gasoline cars of the catalyst.







Fig. S11 the *in situ* DRIFTS spectra of NO (5.0 % in volume) + CO (10.0 % in volume) at different temperatures (a)  $Fe_{0.1}Mn_{0.9}O$ , (b)  $Fe_{0.2}Mn_{0.8}O$ , (c)  $Fe_{0.25}Mn_{0.75}O$  (d)  $Fe_{0.35}Mn_{0.65}O$ , (e)  $Fe_{0.4}Mn_{0.6}O$ 

Fig. S11 (a), (b), (c), (d), and (e) are respectively *in situ* DRIFTS spectra of NO+CO adsorption by catalyst Fe<sub>0.1</sub>Mn<sub>0.9</sub>O, Fe<sub>0.2</sub>Mn<sub>0.8O</sub>, Fe<sub>0.25</sub>Mn<sub>0.75</sub>O, Fe<sub>0.35</sub>Mn<sub>0.65</sub>O, Fe<sub>0.4</sub>Mn<sub>0.6</sub>O at different temperatures. As can be seen from the Fig. S11, at lower temperatures (<100 °C), according to the literature,<sup>[1-4]</sup> bridging bidentate nitrate (1583-1637 cm<sup>-1</sup>), bidentate nitrate (1510-1543 cm<sup>-1</sup>) and linear nitrite (1239-1513 cm<sup>-1</sup>), NO gaseous peak (1849 and 1909 cm<sup>-1</sup>), and infrared peak of N<sub>2</sub>O absorption peak (2202 and 2238 cm<sup>-1</sup>) appeared, but the peak of carbon adsorbent species is not detected. This indicates that NO<sub>x</sub> preferentially adsorbs to the catalyst surface.<sup>[4, 5]</sup>

With the increase of temperature, NO species gradually decreased, indicating that the thermal stability of NO species in the catalytic reaction atmosphere is very poor. In addition, it can be seen that the infrared peaks of gaseous  $CO_2$  (2337 and 2371 cm<sup>-1</sup>)

are enhanced as the temperature increases. This illustrates that the weak reaction of  $CO + M^{n+} \rightarrow CO_2 + M^{(n-1)+}$  occurs under reaction atmosphere. On the other hand, this result also demonstrates that [O] species in  $CO + [O] \rightarrow CO_2$  reaction are mainly stemmed from the transformation of  $NO \rightarrow [O] + [N]$  rather than the reduction of high valence  $M^{n+}$  species. Therefore, we speculate that NO molecule is reacted preferentially with surface active O species to form NO<sub>x</sub> species and surface oxygen vacancies (i.e.  $Fe^{x+}-\Box-Mn^{y+}$  species (x=2 or 3 and y=3 or 4)). With increasing the reaction temperature, the adsorbed NO<sub>x</sub> species are increasingly dissociated into [N] and [O] over the  $Fe^{x+}-\Box-Mn^{y+}$  species, and then [N] is transferred into N<sub>2</sub> via reacting with other [N] and partial [O] reacts with CO into  $CO_2$ .<sup>[3]</sup> In addition, other [O] species convert to reactive oxygen species, activating NO molecules in the next catalytic cycle. This is consistent with the analysis conclusion in Fig. 9. Therefore, we explored the reaction mechanism of the catalyst in the original text according to the *in-situ* infrared results.

# 1. Experimental section 1.1. XRD characterization

XRD patterns of catalysts can be detected by X 'pert PRO at PANalytical. The XRD diffractometer uses a step length of 0.026, a residence time of 25.5 s per step, a scanning range of 5 °- 80 °, an excitation voltage of 40 KV, a tube current of 40 mA, and a scanning rate of 8 ° $\cdot$ min<sup>-1</sup>.

#### 1.2. H<sub>2</sub>-TPR characterization

H<sub>2</sub>-TPR is performed by a FINESORB-3010 automated chemisorption apparatus (Finetec Corporation). For H<sub>2</sub>-TPR, 0.025 g sample is placed in the sample tube, the temperature is programmed to 110 °C, and N<sub>2</sub> with a flow rate of 50 mL·min<sup>-1</sup> was pretreated for 1 h. The water and weak adsorbed gas on the catalyst surface are purged and cooled to room temperature. The gas path is converted into H<sub>2</sub>-Ar mixture with a flow rate of 10 mL·min<sup>-1</sup> (H<sub>2</sub> with a distribution concentration of 7%), which is adsorbed for 30 min, so that the catalyst adsorption reached equilibrium, and then the heating rate of 10 °C·min<sup>-1</sup> is increased from room temperature to the target temperature, and the curve of sample desorption of H<sub>2</sub> is collected by thermal conductivity detector (TCD).

### 1.3. O<sub>2</sub> - TPD characterization

 $O_2$  - TPD is taking 0.1 g sample put in the sample tube, under 200 °C to the flow of 30 mL·min<sup>-1</sup> He for pretreatment for 1 hour, then the cooling gas circuit to 10 mL·min<sup>-1</sup>  $O_2$  for adsorption, adsorption after 30 min, He (30 mL·min<sup>-1</sup>) was used to purge the excess reaction gas in the gas channel. Purging 30 min, The  $O_2$  desorption curves of samples are then collected with a thermal conductivity detector (TCD) from room temperature to target temperature at the rate of 10 °C·min<sup>-1</sup>.

#### 1.4. in situ DRIFTS characterization

The Nicolet iS50 infrared spectrometer from Thermo Fisher is adopted, and the resolution of MCT detector is 4 cm<sup>-1</sup>, and the scanning times are 32. For instantaneous reaction *in situ*, the proper amount of the sample is placed in the small fixed in the sample pool in the crucible, tong N<sub>2</sub> pretreatment for 1 hour under 350 °C, cooling background spectra collected catalyst, then to test the adsorption intensity of reaction gas until the acquisition of the infrared spectrogram without too big change after, will switch to N<sub>2</sub> gas path, the temperature of the heating in the corresponding collection point catalyst response spectra. At last, the infrared diffuse reflection spectrum can be obtained by subtracting the background spectrum.

#### **1.5. BET characterization**

The adsorption–desorption isotherm of  $N_2$  at 77 K is obtained using a Micrometrics TriStar I 3020 analyzer. The pore distribution and specific surface area are calculated from the nitrogen sorption isotherms by the Barrett–Joyner–Halenda and Brunauer–Emmett–Teller (BET) methods, respectively.

#### 1.6. XPS characterization

The X-ray photoelectron spectroscopy (XPS) of the samples are obtained by using an ESCALAB 250Xi multifunctional imaging electron spectrometer (Thermo Fisher Company America), which used monochromatic Al K $\alpha$  radiation (hv = 1486.6 eV) at the power level of 150 W. The electronic binding energy is calibrated on the basis of C 1s (284.8 eV). The irradiated area and detection depth of the samples are 2 mm × 1 mm and 2–5 nm, respectively.

#### 1.7. SEM characterization

Scanning electron microscopy (SEM) measurements are performed with a HITACHI S-3400N electron microscope (Hitachi Company, Japan) at 20 kV. Samples for FESEM are suspended in ethanol and dispersed by ultrasonic, and then dropped onto an aluminium sheet.

# **1.8. TEM characterization**

Transmission electron microscopy (TEM) images are taken on a Tecnai G2 F20 S-TWIN instrument (FEI Company, America) at an acceleration voltage of 200 kV.

# References

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