

# How does the ligand affect the sensitivity of luminescent thermometers based on Tb-Eu complexes

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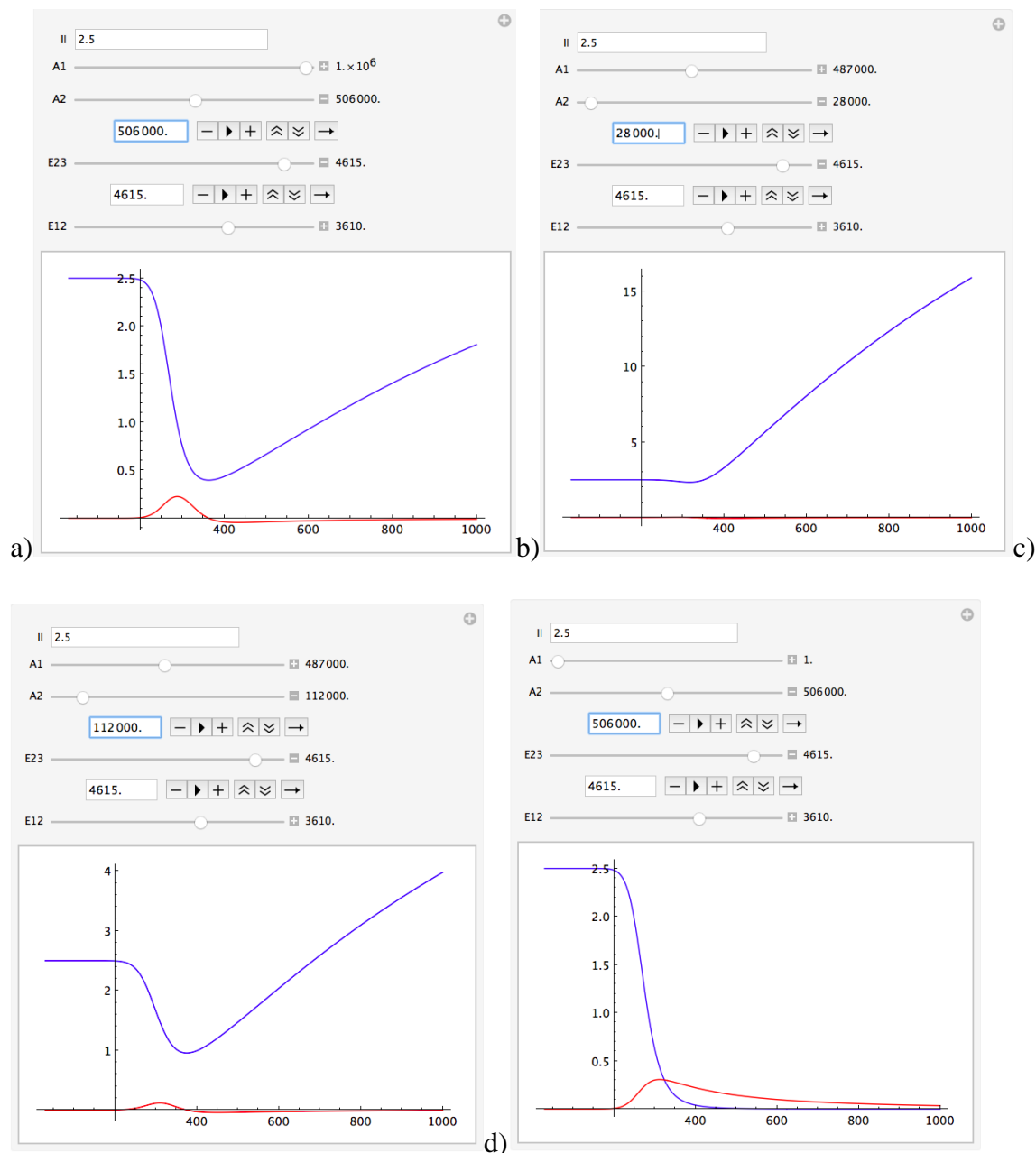
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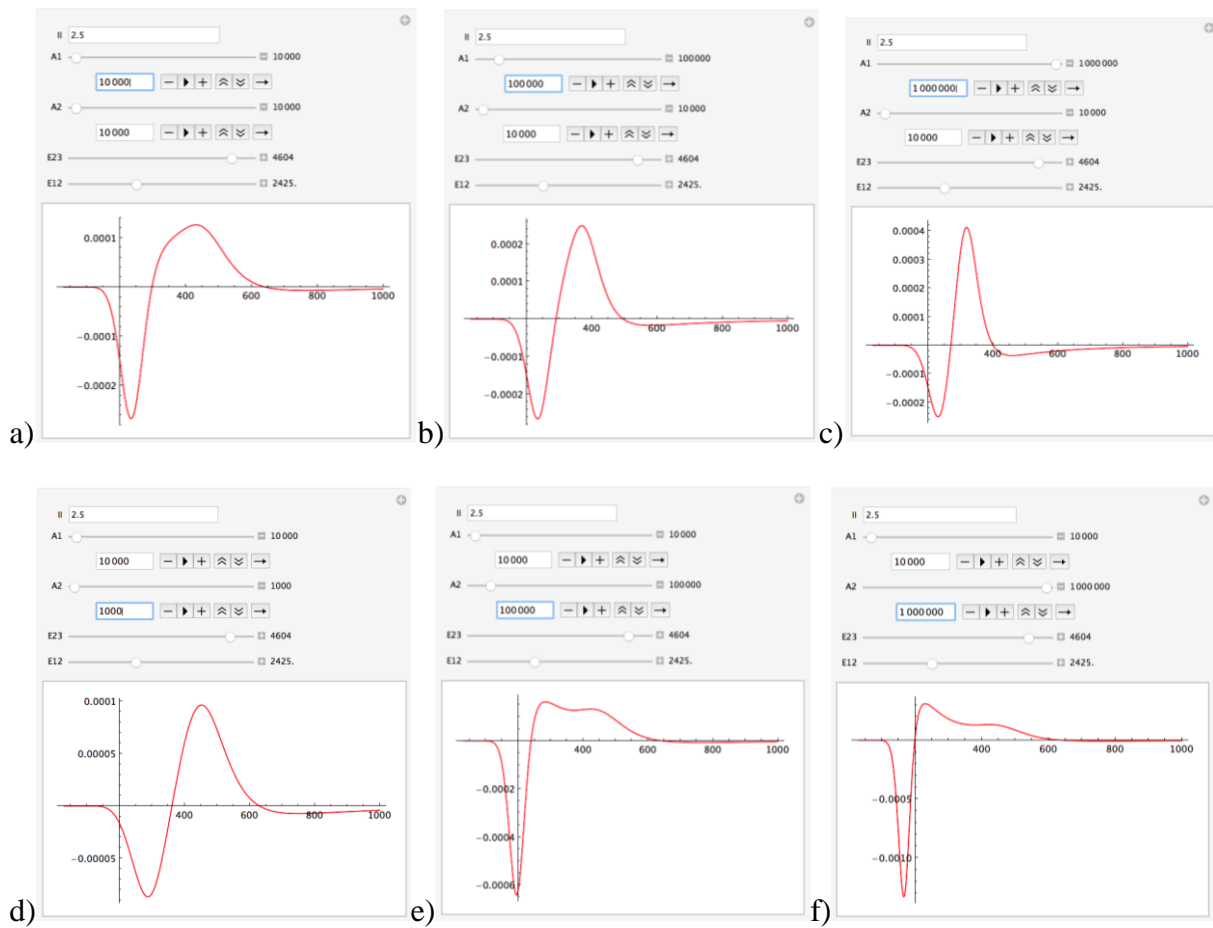
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## LIR and Sr simulation



**Fig. S1** The possible LIR and Sr dependencies on T. Illustrations are given for  $E_{12} = 3601$ ,  $E_{23} = 4615$ :

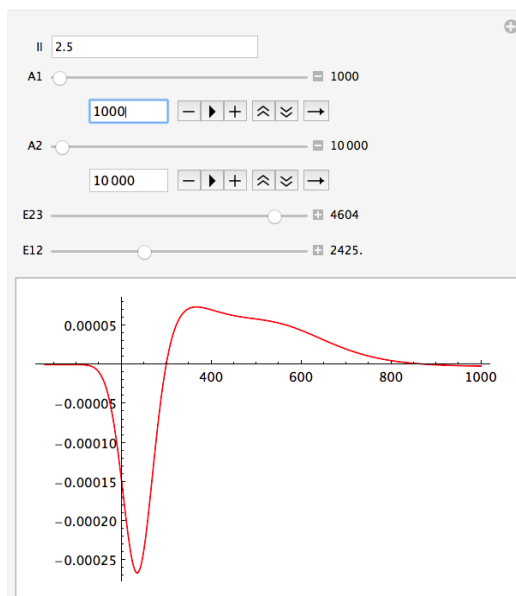
a)  $A_1 = 10^6$ ,  $A_2 = 506000$ , b)  $A_1 = 487000$ ,  $A_2 = 28000$ , c)  $A_1 = 487000$ ,  $A_2 = 112000$ , d)  $A_1 = 1$ ,  $A_2 = 506000$ .



**Fig. S2**  $T_{\max}$  dependence on a-c) A1 value, a,d-f) A2 value



**Fig. S3**  $T_{max}$  dependence on a-d) E23 value, d-h) E12 value



**Fig. S1** Searching for the A2-E12 dependence to give  $T_{maz} = 312K$  at  $E_{23}$  fixed at 4604 K and a voluntarily selected  $A1=1000$

## Case study

### Case (4,5)

$$S_{45} = \frac{A_1(E_{23} - E_{12})}{(A_1 + \exp(E_{12}/T))T^2} = \frac{A_1}{A_1 + \exp(E_{12}/T)} \times S_{55}$$

$$\exp(E_{12}/T) > 0$$

$$A_1 + \exp(E_{12}/T) > A_1$$

$$\frac{A_1}{A_1 + \exp(E_{12}/T)} < 1$$

$$S_{45} < S_{55}$$

### Case (5,4)

$$S_{54} = \frac{A_2(E_{23} - E_{12})}{(A_2 + \exp(E_{23}/T))T^2} = \frac{A_2}{A_2 + \exp(E_{23}/T)} \times S_{55} < S_{55}$$

### Case (4,4)

$$S_{44} = \frac{A_1 A_2 (E_{23} - E_{12})}{(A_2 + \exp(E_{23}/T))(A_1 + \exp(E_{12}/T))T^2} = \frac{A_1 A_2}{(A_2 + \exp(E_{23}/T))(A_1 + \exp(E_{12}/T))} \times S_{55} < S_{55}$$

### Case (3,5)

$$S_{34} = \frac{A_1(E_{23} - E_{12})}{\exp(E_{12}/T)T^2} = \frac{A_1}{\exp(E_{12}/T)} \times S_{55} < S_{55}$$

### Case (5,3)

$$S_{43} = \frac{A_2(E_{23} - E_{12})}{\exp(E_{23}/T)T^2} = \frac{A_2}{\exp(E_{23}/T)} \times S_{55} < S_{55}$$

**Case (3,4)**

$$S_{34} = \frac{A_1 A_2 (E_{23} - E_{12})}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} = \frac{A_1 A_2}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)} \times S_{55} < S_{55}$$

**Case (4,3)**

$$S_{43} = \frac{A_1 A_2 (E_{23} - E_{12})}{(A_1 + \exp(E_{12}/T)) \exp(E_{23}/T) T^2} = \frac{A_1 A_2}{(A_1 + \exp(E_{12}/T)) \exp(E_{23}/T)} \times S_{55} < S_{55}$$

**Case (5,2)**

$$S_{25} = \frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2}$$

**1)  $E_{23} \geq E_{12}$**

$$1a) \frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2} > 0$$

$$\frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2} > \frac{(E_{23} - E_{12})}{T^2}$$

$$A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2) > E_{23} \exp(E_{23}/T) - E_{12} \exp(E_{23}/T)$$

$$A_2 (E_{23} - E_{12}) > E_{23} \exp(E_{23}/T)$$

$$(E_{23} - E_{12})/E_{23} > \exp(E_{23}/T)/A_2$$

$$1 - E_{12}/E_{23} > \exp(E_{23}/T)/A_2$$

Since  $A_1 \gg \exp(E_{12}/T)$  and  $A_2 \sim \exp(-E_{23}/T) \ll \exp(E_{23}/T)$

$$\exp(E_{23}/T)/A_2 \sim 0$$

Thus  $S_{25} > S_{55}$  requires

$$\begin{cases} E_{12} \approx E_{23} \\ \exp(-E_{23}/T) \approx 0 \end{cases}$$

$$1b) \frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2} < 0$$

$$\frac{E_{12} (\exp(-E_{23}/T) + A_2) - A_2 E_{23}}{\exp(E_{23}/T) T^2} > \frac{(E_{23} - E_{12})}{T^2}$$

$$E_{12} (\exp(-E_{23}/T) + A_2) - A_2 E_{23} > (E_{23} \exp(E_{23}/T) - E_{12} \exp(E_{23}/T))$$

$$E_{12} \exp(-E_{23}/T) > (E_{23} - E_{12}) (\exp(E_{23}/T) - A_2) \approx (E_{23} - E_{12}) \exp(E_{23}/T)$$

$$\exp(-2E_{23}/T) > \frac{E_{23}}{E_{12}} - 1$$

Thus  $S_{25} > S_{55}$  requires  $E_{12} \approx E_{23}$

$$E_{23} \leq E_{12}$$

$$2a) \frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2} < 0$$

$$A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2) > (E_{23} - E_{12}) \exp(E_{23}/T)$$

$$A_2 (E_{23} - E_{12}) - E_{12} \exp(-E_{23}/T) > (E_{12} - E_{23}) \exp(E_{23}/T)$$

$$(E_{23} - E_{12}) (A_2 + \exp(E_{23}/T)) > E_{12} \exp(-E_{23}/T)$$



$$(E_{23} - E_{12}) \exp(E_{23}/T) > E_{12} \exp(-E_{23}/T)$$

$$\frac{E_{23}}{E_{12}} - 1 > \exp(-2E_{23}/T)$$

Thus  $S_{25} > S_{55}$  requires

$$\begin{cases} E_{12} \approx E_{23} \\ \exp(-E_{23}/T) \approx 0 \end{cases}$$

$$2b) \frac{A_2 E_{23} - E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) T^2} < 0$$

$$E_{12} (\exp(-E_{23}/T) + A_2) - A_2 E_{23} > (E_{23} - E_{12}) \exp(E_{23}/T)$$

$$A_2 (E_{12} - E_{23}) > -E_{23} \exp(-E_{23}/T)$$

$$A_2 (E_{23} - E_{12}) < \exp(-E_{23}/T)$$

$$1 - \frac{E_{12}}{E_{23}} < \exp(-E_{23}/T) / A_2$$

Thus  $S_{25} > S_{55}$  requires  $E_{12} \approx E_{23}$

$$\mathbf{E_{23} \leq E_{12}}$$

Thus  $S_{25} > S_{55}$  only if  $E_{12} = E_{23}$ . Let's consider this case.

In this case  $S_{55} = 0$  and

$$\begin{aligned}\max(S_{25}) &= \max\left(\frac{E_{23} (\exp(-E_{12}/T) + A_1) - A_1 E_{12}}{\exp(E_{12}/T) T^2}\right) = \max\left(\frac{E_{12} (\exp(-E_{12}/T) + A_1) - A_1 E_{12}}{\exp(E_{12}/T) T^2}\right) \\ &= \max\left(\frac{E_{12} \exp(-E_{12}/T)}{\exp(E_{12}/T) T^2}\right) = \max\left(\frac{E_{12} \exp(-2E_{12}/T)}{T^2}\right)\end{aligned}$$

$$\exp(-2E_{12}/T) < 1 \Rightarrow$$

$$\max(S_{25}) < \frac{E_{12}}{T^2} = S_{55} (\text{at } E_{23} = 0)$$

So looking for the highest  $S_T$  we should not consider this either.

### Case (2,5)

Similarly,

$$\max(S_{25}) < \max(S_{55})$$

unless  $E_{12} = E_{23}$ , which does not lead to the high sensitivity.

### Case (3,3)

$$S_{33} = \frac{A_1 A_2 (E_{23} - E_{12})}{\exp((E_{12} + E_{23})/T) T^2} = \frac{A_1 A_2}{\exp((E_{12} + E_{23})/T)} \times S_{55} < S_{55}$$

### Case (2,4)

$$S_{24} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2}$$

Let's consider if it is possible that  $S_{24} > S_{55}$ .

- 1) Both are positive. For that

$$\left\{ \begin{array}{l} E_{12} < E_{23} \\ E_{23} (\exp(-E_{12}/T) + A_1) > A_1 E_{12} \end{array} \right.$$

$$\left\{ \begin{array}{l} E_{23} > E_{12} \\ E_{23} > \frac{A_1}{(\exp(-E_{12}/T) + A_1)} E_{12} \end{array} \right.$$

Thus the latter is automatically true if the former is, and the only condition is  $E_{23} > E_{12}$ .

$$S_{24} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} > \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

$$\begin{aligned} A_2 (\exp(-E_{12}/T) + A_1) E_{23} + (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) E_{12} \\ > A_1 A_2 E_{12} + (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) E_{23} \end{aligned}$$

$$\begin{aligned} E_{23} (A_2 (\exp(-E_{12}/T) + A_1) - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \\ > E_{12} (A_1 A_2 - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \end{aligned}$$

As  $A_2 \sim (A_2 + \exp(E_{23}/T))$  and  $(\exp(-E_{12}/T) + A_1) \ll \exp(E_{12}/T)$ ,

$$A_2 (\exp(-E_{12}/T) + A_1) - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \approx -(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)$$

And as  $(A_2 + \exp(E_{23}/T)) \sim A_2$  and  $\exp(E_{12}/T) \gg A_1$

$$A_1 A_2 - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \approx -(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)$$

From that

$$\begin{aligned} E_{23} (A_2 (\exp(-E_{12}/T) + A_1) - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \\ > E_{12} (A_1 A_2 - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \end{aligned}$$

is equal to

$$\mathbf{E}_{23}(- (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) > \mathbf{E}_{12}(- (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T))$$

$$\mathbf{E}_{23}(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) < \mathbf{E}_{12}(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)$$

Meaning that  $\mathbf{S}_{24} > \mathbf{S}_{55} \Leftrightarrow \mathbf{E}_{12} > \mathbf{E}_{23}$ , which contradicts the condition.

2) **Both are negative: For that  $\mathbf{E}_{23} < \mathbf{E}_{12} \frac{A_1}{(\exp(-E_{12}/T) + A_1)}$  (and automatically  $< \mathbf{E}_{12}$ )**

$$\mathbf{S}_{24} = \frac{A_1 A_2 \mathbf{E}_{12} - A_2 \mathbf{E}_{23} (\exp(-E_{12}/T) + A_1)}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} > \frac{(\mathbf{E}_{12} - \mathbf{E}_{23})}{T^2} = \mathbf{S}_{55}$$

$$\begin{aligned} A_1 A_2 \mathbf{E}_{12} + \mathbf{E}_{23} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \\ > A_2 \mathbf{E}_{23} (\exp(-E_{12}/T) + A_1) + \mathbf{E}_{12} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \end{aligned}$$

$$\begin{aligned} \mathbf{E}_{12} (A_1 A_2 - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \\ > \mathbf{E}_{23} (A_2 (\exp(-E_{12}/T) + A_1) - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \end{aligned}$$

Again, this is equal to

$$\mathbf{E}_{12} (- (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) > \mathbf{E}_{23} (- (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T))$$

$$\mathbf{E}_{12} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) < \mathbf{E}_{23} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)$$

$$\mathbf{E}_{12} < \mathbf{E}_{23}$$

which contradicts to the conditions.

3)  $\mathbf{S}_{55} < 0 < \mathbf{S}_{24}$ . For that

$$E_{12} > E_{23} > E_{12} \frac{A_1}{(\exp(-E_{12}/T) + A_1)}$$

The conditions of  $S_{24} < S_{55}$  is

$$S_{24} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} > \frac{(E_{12} - E_{23})}{T^2} = S_{55}$$

$$\begin{aligned} E_{23} (A_2 (\exp(-E_{12}/T) + A_1) + (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \\ > ((A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) + A_1 A_2) E_{12} \end{aligned}$$

Similarly equal to

$$E_{23} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) > (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) E_{12}$$

$$E_{23} > E_{12}$$

which contradicts to the conditions.

**Case (4,2)**

Similarly, always

$$S_{42} = \frac{A_1 A_2 E_{23} - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{23}/T) (A_1 + \exp(E_{12}/T)) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (1,5)**

$$\begin{aligned} S_{15} - S_{55} &= \frac{E_{23} \exp(-E_{12}/T) - A_1 E_{12}}{\exp(E_{12}/T) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\ &= \frac{1}{\exp(E_{12}/T) T^2} \left( E_{23} (\exp(-E_{12}/T) - \exp(E_{12}/T)) - E_{12} (A_1 - \exp(E_{12}/T)) \right) \\ &\approx \frac{1}{\exp(E_{12}/T) T^2} \left( -E_{23} (\exp(E_{12}/T)) + E_{12} (\exp(E_{12}/T)) \right) = \frac{E_{12} - E_{23}}{T^2} = -S_{55} \\ &< 0 \end{aligned}$$

Thus again it is always that

$$S_{15} = \frac{E_{23} \exp(-E_{12}/T) - A_1 E_{12}}{\exp(E_{12}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (5,1)**

Similarly,

$$S_{51} = \frac{A_2 E_{23} - E_{12} \exp(-E_{23}/T)}{\exp(E_{23}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (1,4)**

$$\begin{aligned}
S_{14} - S_{55} &= \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} \left( E_{23} (A_2 \exp(-E_{12}/T)) \right. \\
&\quad \left. - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) - E_{12} (A_1 A_2 - (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T)) \right) \\
&\approx \frac{1}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} \left( -E_{23} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \right. \\
&\quad \left. + E_{12} (A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) \right) = \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus again it is always that

$$S_{14} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (4,1)**

Similarly,

$$S_{41} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 A_2 E_{12}}{(A_2 + \exp(E_{23}/T)) \exp(E_{12}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case(2,3)**

$$S_{23} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{\exp(E_{12} + E_{23}/T) T^2}$$

$$\begin{aligned}
S_{23} - S_{55} &= \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{\exp(E_{12} + E_{23}/T) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (A_2 \exp(-E_{12}/T) + A_1 A_2 - \exp(E_{12} + E_{23}/T)) \right. \\
&\quad \left. - E_{12} (A_1 A_2 - \exp(E_{12} + E_{23}/T)) \right) \\
&\approx \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (-\exp(E_{12} + E_{23}/T)) - E_{12} (-\exp(E_{12} + E_{23}/T)) \right) \\
&= \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus always

$$S_{23} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 A_2 E_{12}}{\exp(E_{12} + E_{23}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (3,2)**

Similarly,

$$S_{32} = \frac{A_1 A_2 E_{23} - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{12} + E_{23}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (1,3)**

$$S_{13} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 A_2 E_{12}}{(\exp(E_{23} + E_{12}/T)) T^2}$$



$$\begin{aligned}
S_{13} - S_{55} &= \frac{A_2 E_{23} \exp\left(-\frac{E_{12}}{T}\right) - A_1 A_2 E_{12}}{\left(\exp\left(\frac{E_{23} + E_{12}}{T}\right)\right) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{\left(\exp\left(\frac{E_{23} + E_{12}}{T}\right)\right) T^2} \left( E_{23} \left( A_2 \exp\left(-\frac{E_{12}}{T}\right) - \exp\left(\frac{E_{23} + E_{12}}{T}\right) \right) \right. \\
&\quad \left. - E_{12} \left( A_1 A_2 - \exp\left(\frac{E_{23} + E_{12}}{T}\right) \right) \right) \\
&\approx \frac{1}{\left(\exp\left(\frac{E_{23} + E_{12}}{T}\right)\right) T^2} \left( E_{23} \left( -\exp\left(\frac{E_{23} + E_{12}}{T}\right) \right) - E_{12} \left( -\exp\left(\frac{E_{23} + E_{12}}{T}\right) \right) \right) \\
&= \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus

$$S_{13} = \frac{A_2 E_{23} \exp\left(-\frac{E_{12}}{T}\right) - A_1 A_2 E_{12}}{\left(\exp\left(\frac{E_{23} + E_{12}}{T}\right)\right) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (3,1)**

Similarly,

$$S_{31} = \frac{A_1 A_2 E_{23} - A_1 E_{12} \exp\left(-\frac{E_{23}}{T}\right)}{\exp\left(\frac{E_{12} + E_{23}}{T}\right) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (2,2)**

$$S_{22} = \frac{A_2 E_{23} \left( \exp\left(-\frac{E_{12}}{T}\right) + A_1 \right) - A_1 E_{12} \left( \exp\left(-\frac{E_{23}}{T}\right) + A_2 \right)}{\exp\left(\frac{E_{12} + E_{23}}{T}\right) T^2}$$

$$\begin{aligned}
S_{22} - S_{55} &= \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{12} + E_{23}/T) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (A_2 (\exp(-E_{12}/T) + A_1) - \exp(E_{12} + E_{23}/T)) \right. \\
&\quad \left. - E_{12} (A_1 (\exp(-E_{23}/T) + A_2) - \exp(E_{12} + E_{23}/T)) \right) \\
&\approx \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (-\exp(E_{12} + E_{23}/T)) - E_{12} (-\exp(E_{12} + E_{23}/T)) \right) \\
&= \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus it is always that

$$S_{22} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{\exp(E_{12} + E_{23}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (1,2)**

$$S_{12} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{(\exp(E_{23} + E_{12}/T)) T^2}$$

$$\begin{aligned}
S_{12} - S_{55} &= \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{(\exp(E_{23} + E_{12}/T)) T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (A_2 \exp(-E_{12}/T) - \exp(E_{12} + E_{23}/T)) \right. \\
&\quad \left. - E_{12} (A_1 (\exp(-E_{23}/T) + A_2) - \exp(E_{12} + E_{23}/T)) \right) \\
&\approx \frac{1}{\exp(E_{12} + E_{23}/T) T^2} \left( E_{23} (-\exp(E_{12} + E_{23}/T)) - E_{12} (-\exp(E_{12} + E_{23}/T)) \right) \\
&= \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus it is always that

$$S_{12} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} (\exp(-E_{23}/T) + A_2)}{(\exp(E_{23} + E_{12}/T)) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (2,1)**

Similarly,

$$S_{21} = \frac{A_2 E_{23} (\exp(-E_{12}/T) + A_1) - A_1 E_{12} \exp(-E_{23}/T)}{\exp(E_{12} + E_{23}/T) T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

**Case (1,1)**

$$S_{11} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} \exp(-E_{23}/T)}{(\exp(E_{23} + E_{12}/T)) T^2}$$

$$\begin{aligned}
S_{11} - S_{55} &= \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} \exp(-E_{23}/T)}{(\exp(E_{23} + E_{12}/T))T^2} - \frac{(E_{23} - E_{12})}{T^2} \\
&= \frac{1}{\exp(E_{12} + E_{23}/T)T^2} \left( E_{23} (A_2 \exp(-E_{12}/T) - \exp(E_{12} + E_{23}/T)) \right. \\
&\quad \left. - E_{12} (A_1 \exp(-E_{23}/T) - \exp(E_{12} + E_{23}/T)) \right) \\
&\approx \frac{1}{\exp(E_{12} + E_{23}/T)T^2} \left( E_{23} (-\exp(E_{12} + E_{23}/T)) - E_{12} (-\exp(E_{12} + E_{23}/T)) \right) \\
&= \frac{E_{12} - E_{23}}{T^2} = -S_{55} < 0
\end{aligned}$$

Thus again always

$$S_{11} = \frac{A_2 E_{23} \exp(-E_{12}/T) - A_1 E_{12} \exp(-E_{23}/T)}{(\exp(E_{23} + E_{12}/T))T^2} < \frac{(E_{23} - E_{12})}{T^2} = S_{55}$$

## Detailed study of literature $\text{Eu}_x\text{Tb}_{1-x}\text{L}$ systems

Table S1 Relative thermometer sensitivity of some  $\text{Eu}_x\text{Tb}_{1-x}\text{L}$  systems and triplet state energy of L ligands.

№	link	$\text{Eu}_x\text{Tb}_{1-x}\text{L}$	$E(T_1)$ , $\text{cm}^{-1}$	T, K	$S_r, \%K^{-1}$			$\text{Exp}(E_2$ $_{3/T})$	$A_2$	$\text{Exp}(E_{12}/$ $T)$	$A_1$	Case
					exp	$\frac{E_{12}}{T^2}$	$\frac{E_{23} - E_{12}}{T^2}$					
1	28	pdms-eddpo(1%)- [Tb <sub>0,90</sub> Eu <sub>0,10</sub> (bzac) <sub>3</sub> ](0,25%)	23058	203	<b>11,05</b>	<b>11,17232</b>	<b>1,89315</b>	1,52E8	8,85E8	7,07E9	4,13E10	<b>5,5</b>
2	28	pdms-eddpo(1%)- [Tb <sub>0,95</sub> Eu <sub>0,05</sub> (bzac) <sub>3</sub> ](0,25%)		188	<b>9,22</b>	<b>13,02626</b>	<b>2,2073</b>	6,81E8	2,84E9	4,32E10	1,80E11	<b>5,5</b>
3	28	pdms-eddpo(1%)- [Tb <sub>0,99</sub> Eu <sub>0,01</sub> (bzac) <sub>3</sub> ](0,25%)		203	<b>7,87</b>	<b>11,17232</b>	<b>1,89315</b>	1,52E8	6,30E8	7,07E9	2,94E10	<b>4,5</b>
4	28	pdms-eddpo(1%)- [Tb <sub>0,995</sub> Eu <sub>0,005</sub> (bzac) <sub>3</sub> ](0,25%)		203	<b>7,72</b>	<b>11,17232</b>	<b>1,89315</b>	1,52E8	6,18E8	7,07E9	2,88E10	<b>4,5</b>
5	29	Eu <sub>0,088</sub> Tb <sub>0,2287</sub> (phen)(btc)(dmf)·dmf	22075 (phen)	393	<b>2,37</b>	<b>2,98092</b>	<b>1,42085</b> <b>(0,37284)</b>	2,82E4	1,80E5	1,22E5	7,78E5	<b>3,4</b>

6	29	Eu <sub>0,174</sub> Tb <sub>0,2188</sub> (phen)(btc)(dmf)·dmf	23200 (btc)		<b>2,71</b>	<b>2,98092</b>	<b>1,42085</b> <b>(0,37284)</b>	2,82E4	2,05E5	1,22E5	8,89E5	<b>3,4</b>
7	30	[Eu <sub>0,53</sub> Tb <sub>0,47</sub> (tfac) <sub>8</sub> ] <sub>2</sub> ·Na <sub>2</sub> <sup>+</sup>	22800	353	<b>2,70</b>	<b>3,69476</b>	<b>0,92398</b>	1,77E4	5,17E4	4,62E5	1,35E6	<b>4,5</b>
8	30	[Eu <sub>0,41</sub> Tb <sub>0,59</sub> (tfac) <sub>8</sub> ] <sub>2</sub> ·Na <sub>2</sub> <sup>+</sup>	22800	315	<b>1,33</b>	<b>4,63996</b>	<b>1,16035</b>	5,76E4	6,59E4	2,22E6	2,55E6	<b>4,4</b>
9	31	Tb <sub>0,9</sub> Eu <sub>0,1</sub> PIA	25866	300	<b>3,53</b>	5,12	<b>3,62</b>	7,95E2	2,65E4	2,46E11	8,2E12	<b>5,5</b>
10	32	Eu <sub>0,0069</sub> Tb <sub>0,9931</sub> -DMBDC	23306	200	<b>1,15</b>	11,51	<b>1,06</b>	9,95E5	8,5E7	2,04E6	9&65E9	<b>5,5</b>
11	19	d-U(600)-Eu <sub>0,25</sub> Tb <sub>0,75</sub> (btfa) <sub>3</sub> (bpeta)	21793	300	<b>3,0</b>	<b>5,11556</b>	<b>2,88915</b>	7,95E2	8,26E2	4,62E6	4,80E6	<b>4,4</b>
12	33	Eu <sub>0,25</sub> Tb <sub>0,75</sub> (btfa) <sub>3</sub> (4,4'-bpy)(EtOH)	22212	225	<b>4,00</b>	<b>9,09432</b>	<b>3,94543</b>	1,07E5	1,09E5	7,70E8	7,81E8	<b>4,4</b>
13	27	[(CH <sub>3</sub> ) <sub>2</sub> NH <sub>2</sub> ]Eu <sub>0,036</sub> Tb <sub>0,964</sub> bpfc	29070	310	<b>9,42</b>	<b>4,79084</b>	<b>8,1893</b>	2,99E1 7	3,44E17	2,82E6	3,24E6	<b>4,4</b>
14	18	[Eu <sub>0,37</sub> Tb <sub>0,63</sub> (btc)H <sub>2</sub> O](H <sub>2</sub> O)(DMF)	23200 (26504) <sup>1</sup>	313	<b>0,68</b>	<b>4,69945</b>	<b>0,58778</b> <b>(4,26457)</b>	1,53E1 2	2,44E11	2,44E6	3,90E5	<b>3,3</b>
15	34	[Tb <sub>2</sub> (bpydc) <sub>3</sub> (H <sub>2</sub> O) <sub>3</sub> ](dmf) <sub>2</sub> @3%Eu(tfac) <sub>3</sub> ·2H <sub>2</sub> O	21505 (bpydc)	225	<b>2,59</b>	<b>9,09432</b>	<b>5,95478</b> <b>(2,27429)</b>	4,62E6	5,25E6	7,70E8	8,77E8	<b>4,4</b>

16	34	[Tb <sub>2</sub> (bpydc) <sub>3</sub> (H <sub>2</sub> O) <sub>3</sub> ](dmf) <sub>2</sub> @7,3%E u(tfac) <sub>3</sub> ·2H <sub>2</sub> O	22800 (tfac)	325	<b>1,33</b>	<b>4,35882</b>	<b>2,85406</b> <b>(1,09004)</b>	4,10E4	5,01E4	1,42E6	1,73E6	<b>4,4</b>
17	35	Tb <sub>0,995</sub> Eu <sub>0,005</sub> @Al(OH)(bpydc)	21505	333	<b>3,00</b>	<b>4,1519</b>	<b>2,71858</b>	1,18E2	1,30E2	1,01E6	1,11E6	<b>4,4</b>
18	23	Eu <sub>0,01</sub> Tb <sub>0,99</sub> (btc)	23200 (26504) <sup>1</sup>	300	<b>0,42</b>	<b>5,11556</b>	<b>0,63982</b> <b>(4,64217)</b>	5,17E1 2	4,67E11	4,62E6	4,18E5	<b>3,3</b>
19	36	[Tb <sub>0,98</sub> Eu <sub>0,02</sub> (oa) <sub>0,5</sub> (dstp)]·3H <sub>2</sub> O <sup>1</sup>	24570	275	<b>2,4</b>	<b>6,08793</b>	<b>1,84505</b>	8,55E- 4	2,37E-4	1,86E7	5,17E6	<b>4,4</b>
21	37	Tb <sub>0,99</sub> Eu <sub>0,01</sub> (bdc) <sub>1,5</sub> ·(H <sub>2</sub> O) <sub>2</sub>	26211	318	<b>0,31</b>	<b>4,55283</b>	<b>3,71463</b>	2,62E1 1	2,18E10	1,94E6	1,62E5	<b>3,3</b>
22	38	[Tb <sub>0,99</sub> Eu <sub>0,01</sub> (hfa) <sub>3</sub> (dpbp)] <sub>2</sub>	22000 (hfa)	200	<b>0,52</b>	<b>11,51</b>	<b>5,756</b>	9,95E5	8,99E4	9,94E9	8,98E8	<b>3,3</b>
23	39	Tb <sub>0,95</sub> Eu <sub>0,05</sub> HY	26600	4	<b>31</b>	<b>28775</b>	<b>26975,5</b>	∞	∞	∞	∞	--
24	40	cycEu-phTb	20501	298	<b>0,85</b>	<b>5,18445</b>	<b>5,02135</b>	1,62	2,75E-1	5,12E6	8,68E5	<b>4,3</b>
25	41	cycTb-phEu		200	<b>1,86</b>	<b>11,51</b>	<b>11,1479</b>	2,06	3,44E-1	9,94E9	1,66E9	<b>4,3</b>

<sup>1</sup> Two triplets of two metals were listed – 24570 (oa)19050 (dstp). The latter is involved (otherwise Sr = **8,657**)

26		Tb <sub>0,95</sub> Eu <sub>0,05</sub> (btb)	23426	14	<b>2,85</b>	<b>2348,979</b> <b>59</b>	<b>127,8934</b> <b>7</b>	∞	∞	6,62	1,48	<b>4,3</b>
27	<sup>42</sup>	Tb <sub>0,95</sub> Eu <sub>0,05</sub> (pdc)	23809	333	<b>1,37</b>	<b>4,1519</b>	<b>0,27089</b>	2,49E6	1,26E7	1,01E6	5,11E6	<b>3,4</b>
28	<sup>43</sup>	Eu <sub>0,088</sub> Tb <sub>0,912</sub> (ad) <sub>0,5</sub> (phth)(H <sub>2</sub> O) <sub>2</sub>	20833 (phth)	303	<b>0,42</b>	<b>5,01476</b>	<b>4,3367</b>	7,80	7,56E-1	3,97176E	3,85E5	<b>3,3</b>
29	<sup>44</sup>	Ln(ad) <sub>0,5</sub> (phth)(H <sub>2</sub> O) <sub>2</sub> ; Ln = 3Eu <sup>III</sup> :10Tb <sup>III</sup>		303	<b>0,59</b>	<b>5,01476</b>	<b>4,3367</b>	7,80	1,06	3,97E6	5,40E5	<b>3,3</b>
30	<sup>44</sup>	Eu <sub>0,01</sub> Tb <sub>0,99</sub> (bdc-F <sub>4</sub> )	27465	50	<b>0,75</b>	<b>184,16</b>	<b>222,4256</b> <b>8</b>	1,95E8 8	6,56E85	9,77E39	3,29E37	<b>3,3</b>
31	<sup>45</sup>	Eu <sub>0,5</sub> Tb <sub>0,5</sub> (L) <sub>1</sub> @PMMA	22420	77	<b>0,46</b>	<b>77,65222</b>	<b>28,64065</b>	2,45E1 6	3,94E14	9,278E25	1,49E24	<b>3,3</b>
32	<sup>46</sup>	Tb <sub>0,005</sub> Eu <sub>0,995</sub> @UiO-67-bpydc	21505	180	<b>3,01</b>	<b>14,20988</b>	<b>9,30434</b>	6,84E3	2,21E3	1,28E11	4,15E10	<b>4,4</b>
33	<sup>24</sup>	{[Tb <sub>0,9064</sub> Eu <sub>0,0936</sub> (dcptp)(NO <sub>3</sub> )]·(H <sub>2</sub> O)} <sub>2</sub>	25445 (25217) <sup>1</sup>	300	<b>21,5</b>	<b>5,11556</b>	<b>2,94918</b> <b>(2,58469)</b>	1,08E1 0	8,96E10	4,62E6	3,84E7	<b>3,5</b>
34 <sup>&amp;</sup>	<sup>26</sup>	Tb <sub>0,897</sub> Eu <sub>0,103</sub> (tcptpy)	22321	340	<b>8,41</b>	<b>3,9827</b>	<b>1,59217</b>	3,39E3	1,79E4	7,60E5	4,01E6	<b>5,5</b>



& Re-plotted LIR with re-calculated Sr, which only reached 5.55%/K and is similar to the value (5.12%/K), predicted by the theory.

