Electronic Supplementary Information (ESI)

An Emerging Air Pollution Mobile Source: Outdoor Plastic Liner Manufacturing Sites Discharge VOCs into Urban and Rural Areas

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S1. INTRODUCTION

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S1. INTRODUCTION

Table S1 List of CIPP associated air contamination incidents found by authors not included in the 59 incidents reported by Teimouri et al. (2017) and 45 incidents reported by Ra et al. (2019) in their Supplementary Information files.

Incident	Styrene	Description of events from reference
Location (Year)		
Philadelphia, PA (2020) ¹	nr	PERSONAL COMMUNICATION: A resident found her house filled with CIPP fumes which entered to the building through the basement. She left the house and contacted the water department and contractors. A water department inspector came to her house but only prepared a report. The resident was a cancer survivor with neuropathy, and that became worse after the incident.
Harrisburg, PA (2020) ^{2,3}	nr	PERSONAL COMMUNICATION: A resident noticed a strong glue-like smell in his basement coming from an underground work in the neighborhood. The resident asked the workers the cause of such smell and they assured him that the smell would vanish and not be as strong as it cures. The resident was concerned because: 1) the incident happened during the winter and they expect residents to open windows to ventilate; 2) it affected those who may be elderly, working remotely or children who may be home schooled or in cyber school; 3) nobody in the City of Harrisburg Codes was too concerned. They also said that there was no oversight from the City government of the process or possible health, safety, welfare of residents; 4) With the population being 25% under the age of 18, any type of chemicals can adversely affect brain development up until 25 years of age; 5) With older houses, many times there are floor drains that may not have a functioning trap as in the case of our house. However, the Capital Region Water released a notice in which they claimed that "the smell released in sewer rehabilitation process is in such small quantities that it does not pose a significant risk to human health, the environment, or the workers who are working on our behalf. It exists briefly in the environment and is destroyed rapidly in the air, disappearing quickly."
Chicago, IL (2020) ⁴	nr	MEDIA REPORT: Sewer pipe repair construction caused a very strong chemical smell adversely impacted business at a bakery in Chicago.
Decatur, IL (2020) ⁵	nr	Cancer Care Center of Decatur was evacuated due to an odor caused by city sewer projects. Decatur Fire Department responded to the incident

Incident	Styrene	Description of events from reference
Location (Year)		
		but did not find anything unsafe.
Seneca Falls, NY	nr	MEDIA REPORT: A teacher and several middle school students in a
(2019) ⁶		classroom became sick because of inhalation of odors caused by sewer
		pipe rehabilitation work at nearby area. Windows of the classroom were
		opened when the rehabilitation work was taking place. Nine students
		went home sick at the incident day. Eight students felt better and returned
		school the next day while one student still felt sick two days later.
		Styrene, as a volatile organic compound, was mixed with the resin to help
		it cure. An engineer for the project from Barton & Loguidice Engineers
		told the reporter that curing of the resin impregnated liner causes odors.
		He also mentioned that results of some studies showed that even though
		odors are a common occurrence in CIPP practices, styrene concentrations
		are less than exposure guidelines and do not lead to health risk. He said
		that individuals have different sensitivities towards styrene odors and can
		be inconvenient to those who are not used to working around it. After
		investigation it was concluded that a combination of weather conditions
		(i.e. breeze and air movement at the incident day) and opened windows
		resulted in increased odors from the CIPP process.
Festus, MO	nr	MEDIA REPORT: Public Works director Matt Clemens announced that
(2019) ⁷		while fabric lining in sewer lines was conducting in Festus, residents may
		notice a strange odor. He said that this process has been conducted every
		other year on a rotating basis and nothing harmful exists in this procedure.
Regina, CAN	nr	MEDIA REPORT: One of the residents found going outside impossible
(2019) ⁸		because of massive maintenance project being conducted nearby her
		house. The noise and fumes from the project have disrupted her daily life.
		Some residents noticed sewer gas smell after steaming the pipe. said some
		people have been put as a result of the project, but only Residents directly
		affected by the noise and fumes were put in hotels while contractor
		decided when a house should be evacuated.
Regina, CAN	nr	PERSONAL COMMUNICATION: Explosion in a basement in sump pit
(2019)9		occurred as a result of fume accumulation during sewer pipe lining. CIPP
		was installed a few months prior the incident. The pit was connected to
		sanitary sewer. During CIPP installation styrene residue settled in pit for

Incident	Styrene	Description of events from reference
Location (Year)		
		4 months and the spark was from the pump and ignited gas.
Herndon, VA (2019) ¹⁰	nr	PERSONAL COMMUNICATION: Residents were concerned about a strong smell assumed to originate from chemical reaction to the epoxy in the sewer pipe. The chemical odor became worse in the past 30 minutes of incident report. It was advised that the odor would dissipate by the morning and was not harmful.
Pitcairn, PA (2019) ¹¹	nr	MEDIA REPORT: Three students and three teachers felt ill after breathing emissions from a sewer project near school. It caused nausea and watery eyes for students and staff. 280 students and staff were vacated from the school and students were sent home an hour later.
Rochelle, IL (2019) ¹²	nr	MEDIA REPORT: Aldi evacuated the building and stayed closed for several hours as a result of smoke coming from restrooms. A strong odor was also noticed in the building and parking area. Sewer pipe rehabilitation work near the area was the reason for smoke and strong smell. Rochelle fire chief explained that they monitored the air nothing harmful, flammable or explosive was found.
Evanston, IL (2019) ¹³	nr	MEDIA REPORT: City officials announced a sewer repair work will be conducted and advised nearby residents not to distress by unpleasant odors caused by heated styrene. The chemical has been commonly used in fiberglass industry and is not dangerous. They also asked the residents to pour a gallon of water into drains to avoid the odor in their home and repeat the process when the water evaporates.
Festus, MO (2019) ¹⁴	nr	MEDIA REPORT: In March, Institutform was awarded \$130,124 by Festus City Council to repair city sewer pipes by CIPP installations. There's no need to worry about steam rising from Festus streets, Public Works Matt Clemens said.
Moncton, CAN (2019) ¹⁵	nr	MEDIA REPORT: An unpleasant glue-like odor came from sewer lining activities and permeated homes in the city's north end. The city declared the smell isn't a public-health risk. However, some residents developed headaches and felt nauseous. One resident rented an industrial fan to force the smell out of his building. A few of them smelt the odor on their cloths, furniture and even bottled water.

Incident	Styrene	Description of events from reference
Location (Year)		
Nerroll, CT		MEDIA REPORT: All students' after school activities were canceled due
Norwalk, CT (2019) ¹⁶⁻¹⁸	nr	to an odor from an adjacent construction. The students left the building
(2019).010		by local Fire Department personnel "out of an abundance of caution".
Pitcairn, PA	nr	MEDIA REPORT: Students were sent home after several were sickened
$(2019)^{19}$		by an odor from a nearby sewer lining project. A 5th grade student was
		among the six people taken to the hospital after inhaling the odor.
Ontario, CAN	nr	PERSONAL COMMUNICATION: A resident found their house
$(2019)^{20}$		saturated with a peculiar chemical smell came from sewer pipes working
		in the neighborhood. The odor got into the house through sewer pipes of
		toilets. The house was also filled with a high roaring sound that came
		from some violent action in the toilet bowls. The resident alerted the
		authorities. A group of inspectors/engineers arrived at the incident place
		and after investigation they ordered the residents leave the house as the
		gas concentrations were beyond an acceptable level. The residents stayed
		at hotel overnight until the house is properly ventilated. In the incident
		place, windows were opened, and a large number of fans were installed
		to ventilate. Project engineers claimed that this has never happened before
		and then modified to a chance of one in a million.
Warsaw, IN	nr	PERSONAL COMMUNICATION: Several residents were concerned
$(2019)^{21}$		and complained about glue like odor in their homes as a result of sewer
		pipe lining conducted in their neighborhood. Wastewater Treatment
		Utility Plant responded to the residents by saying that the odor is not toxic
		and residents can avoid it by pouring water to their plumbing traps.
Deerfield beach,	nr	MEDIA REPORT: Individual reported that emissions entered a single-
FL (2019) ²²		family home during sanitary sewer CIPP installation in front of the house.
		When she arrived, she opened the door, smelled a glue-like odor in the
		house, and found 2 adults unconscious. The individual then called 911.
Jersey City, NJ	nr	PERSONAL COMMUNICATION: The resident found the CIPP odor
$(2019)^{23}$		overwhelming and noticeable in his second floor apartment. The city
		never notified residents of this project.
Warrnambool,	nr	MEDIA REPORT: Warrnambool residents were told that a strong plastic-
AU (2018) ²⁴		like smell originating from an innovative sewer repair project and
		persisting in parts of the city was not toxic and disappeared very quickly.

nr = *not reported in the reference*

S2. MATERIALS AND METHODS

S2.1. Analytical standards for liquid-solid extraction samples

Different analytical standards were used to confirm and quantify some compounds identified by GC/MS. They include: butyl hydroxytoluene (BHT) (CAS# 128-37-0, Supelco), benzaldehyde (CAS# 100-52-7, Sigma-Aldrich), benzoic acid (CAS# 65-85-0, Supelco), 1- tetradecanol (CAS#112-72-1, Sigma-Aldrich), , chlorobenzene-d5 (CAS# 3114-55-4, Supelco), styrene oxide 97% (CAS# 96-09-3, Sigma-Aldrich), hydroquinone (CAS# 123-31-9, Sigma-Aldrich), 3-ethyl-1-methylbenzene (CAS# 620-14-4, Sigma-Aldrich), 2-ethylhexanoic acid (CAS# 149-57-5, Supelco), 2-propenylbenzene (CAS# 300-57-2, Sigma-Aldrich), *N*-propylbenzene (CAS# 103-65-1, Supelco), 1,3,5-trimethylbenzene (CAS# 108-67-8, Supelco), 1,2,4-trimethylbenzene (CAS# 95-63-6, Sigma-Aldrich) and styrene \geq 99% that contained 4-tert-butylcatechol stabilizer (CAS# 100-42-5, Sigma-Aldrich).

Calibration curves were developed for methylene chloride extracts: styrene ($R^2 = 0.991$, 0.992) benzaldehyde ($R^2 = 0.998$), 1,3,5-trimethylbenzene ($R^2 = 0.985$, 0.998), 1,2,4-trimethylbenzene ($R^2 = 0.991$), benzoic acid ($R^2 = 0.998$), 1-tetradecanol ($R^2 = 0.995$), *N*-propylbenzene ($R^2 = 0.999$, 0.998), 2-propenylbenzene ($R^2 = 1$), styrene oxide ($R^2 = 0.997$), 3-ethyl-1-methylbenzene ($R^2 = 0.998$), 0.980), 2-ethylhexanoic acid ($R^2 = 0.999$, 0.961), hydroquinone ($R^2 = 0.998$) and BHT ($R^2=0.995$).

Calibration curves were also created for hexane extracts and were for: styrene (R^2 = 0.996, 0.999), benzaldehyde (R^2 = 0.999, 0.998), 1,3,5-trimethylbenzene (R^2 = 0.999, 0.991, 0.980), 1,2,4-trimethylbenzene (R^2 = 0.998, 0.997), benzoic acid (R^2 = 0.980, 0.950), 1-tetradecanol (R^2 = 0.982), *N*-propylbenzene (R^2 = 0.999, 0.997), 2-propenylbenzene ((R^2 = 0.999), styrene oxide (R^2 = 0.995), 3-ethyl-1-methylbenzene (R^2 = 0.994), 2-ethylhexanoic acid (R^2 = 0.996), hydroquinone (R^2 = 0.999) and BHT (R^2 = 0.999).



Fig. S1 Experimental setup for capturing post-cured chemical air emissions from cured composites: (a) inside the ETC; (b) enclosed ETC; (c) sampling ports connected to the ETC; (d) entire set-up

S3. RESULTS AND DISCUSSION

		Reported CIPP Information								
Year	Resin Type	Resin Weight (kg)	Application	Monomer	Curing Method	mass of resin lost if heating was applied for each CIPP application described the reference (kg)				
2019 27	-	2.72×10 ⁵	Storm sewer	-	-	2.41×10 ⁴				
2018 28	Isophthalic polyester	6.12×10 ⁴	Sanitary sewer	Styrene	-	5.43×10 ³				
2014 29	Vinyl ester	7.94×10 ⁴	Sewer	Styrene	-	7.04×10 ³				
2013 30	Unsaturated polyester	1.22×10 ⁸	Sanitary and Storm	-	-	1.09×10 ⁷				
2012 31	Isophthalic polyester	4.54×10 ⁵	-	-	Thermal	4.02×10 ⁴				
2012 32	Styrene- free vinyl	6.80×10 ⁴	Storm sewer	-	-	6.04×10 ³				
2009 33	Vinyl ester	3.47×10 ⁵	Sanitary sewer	Styrene	Hot water	3.08×10 ⁴				

Table S2 Estimated mass of resin lost into atmosphere during CIPP manufacture

Estimated mass of resin lost is equal to resin weight for each CIPP incidents reported in this Table times the average resin lost obtained in the present study when no vacuum was applied (8.87%).

Table S3 List of some tentatively identified compounds detected in uncured resin dissolved in methylene chloride with no dilution

Retention Time	Tentatively	IM	m/z	%Area (Average, STDEV)		
Ketention 1 mie	identified compound	LIVI		Methylene chloride	Hexane	
3.929, 3.933	Benzene, methyl-	3	1	3 replicates shown intensity < 5.00×10 ⁴	2.85×10 ⁻² , 1.20×10 ⁻¹ 1 replicate shown intensity < 5.00×10 ⁴	
4.415, 4.418, 4.20, 4.395, 4.396, 4.397	1,3-Dioxolane, 2- ethyl-4-methyl-	5	7	$1.26 \times 10^{-1} \pm 7.64 \times 10^{-3}$	2.70×10 ⁻¹ ± 1.80×10 ⁻¹	
4.617, 4.618, 4.621, 4.636, 4.638, 4.639	1,3-Dioxolane, 2- ethyl-4-methyl-	3	7	9.81×10 ⁻² ± 8.61×10 ⁻³	1.90×10 ⁻¹ ± 1.20×10 ⁻¹	
6.176, 6.177, 6.179, 6.192	Benzene, ethyl-	9	1	$5.76 \times 10^{-1} \pm 3.43 \times 10^{-2}$	1.68 ± 1.12	
6.381	o-Xylene	4	1	3 replicates shown intensity < 5.00×10 ⁴	2.82×10 ⁻¹ , 5.90×10 ⁻²	
6.44, 6.449, 6.467	Maleic anhydride	5	4	$2.06 \times 10^{-1} \pm 1.25 \times 10^{-1}$	3 replicates shown intensity < 5.00×10 ⁴	
7.526, 7.528, 7.529, 7.54, 7.546, 7.551	Benzene, (1- methylethyl)-	7	05	1.30 ± 1.43	1.92 ± 1.21	
7.785, 7.793. 7.797	Cyclooctane, ethyl-	4	9	$1.26 \times 10^{-1} \pm 1.11 \times 10^{-2}$	2 replicates shown intensity < 5.00×10 ⁴	
7.906, 7.907, 7.909, 7.912, 7.919, 7.923	Benzene, 2-propenyl-	6	17	2.87×10 ⁻¹ ± 2.84×10 ⁻²	5.30×10 ⁻¹ ± 3.40×10 ⁻¹	
8.04, 8.043, 8.044, 8.046, 8.054, 8.057	Benzene, propyl-	8	1	$2.57 \pm 3.09 \times 10^{-1}$	4.74 ± 2.97	
8.182, 8.185, 8.186, 8.189, 8.196, 8.2	Benzene, 1-ethyl-3- methyl-	7	05	12.8 ± 1.93	22.6 ± 14.1	
8.297, 8.301,8.303, 8.311, 8.314	Mesitylene	7	05	$3.54 \pm 4.60 \times 10^{-1}$	4.33 ± 2.74	
8.494, 8.499, 8.5, 8.507, 8.51	Benzene, 1-ethyl-3- methyl-	6	05	$3.20 \pm 3.02 \times 10^{-1}$	4.19 ± 2.62	
8.534, 8.535, 8.539, 8.547, 8.549	Benzene, (1- methylethenyl)-	7	18	$6.53 \times 10^{-1} \pm 1.38 \times 10^{-1}$	$1.17 \pm 7.2 \times 10^{-1}$	

Retention Time	Tentatively	IM	m/z	%Area (Average, STDEV)		
Retention Time	identified compound	IIVI	III/Z	Methylene chloride	Hexane	
8.589, 8.597, 8.599	Cyclohexane, 1- methyl-4-(1- methylethyl)-, trans-	4	5	$3.14 \times 10^{-2} \pm 4.33 \times 10^{-3}$	3 replicates shown intensity < 5.00×10 ⁴	
8.723, 8.728, 8.729, 8.73, 8.738, 8.741	Mesitylene	7	05	13.5 ± 1.99	21.9 ± 13.7	
8.824, 8.829, 8.83, 8.837	Decane	3	7	$2.75 \times 10^{-1} \pm 6.34 \times 10^{-2}$	$3.10 \times 10^{-1} \pm 2.0 \times 10^{-1}$	
8.959, 8.964, 8.965, 8.971, 8.973	Benzene, (2- methylpropyl)-	1	1	$1.07 \times 10^{-1} \pm 1.78 \times 10^{-2}$	$\frac{1.30 \times 10^{-1}}{8.00 \times 10^{-2}} \pm$	
9.013, 9.018, 9.019, 9.025, 9.027	Benzene, (1-methyl- 4-propyl)-	0	05	$9.53E \times 10^{-2} \pm 1.56 \times 10^{-2}$	1.20×10 ⁻¹ ± 8.00×10 ⁻²	
9.199, 9.203, 9.204, 9.205, 9.211, 9.214	Benzene, 1,3,5- trimethyl-	4	05	$2.89 \pm 4.43 \times 10^{-1}$	3.53 ± 2.21	
9.354, 9.355	Cyclohexane, butyl-	8	3	2.28×10 ⁻² , 2.83×10 ⁻² , 1 replicate shown intensity < 5.00×10 ⁴	3 replicates shown intensity < 5.00×10 ⁴	
9.412, 9.417, 9.418, 9.419, 9.424, 9.427	Indane	5	17	3.50×10 ⁻¹ ± 5.11×10 ⁻²	6.60×10 ⁻¹ ± 4.20×10 ⁻¹	
9.654, 9.659, 9.666, 9.668	Benzene, 1-methyl-3- propyl-	4	05	4.91×10 ⁻¹ ± 7.46×10 ⁻²	$6.30 \times 10^{-1} \pm 4.0 \times 10^{-1}$	
9.764, 9.769, 9.77, 9.776, 9.778	Benzene, 1-ethyl-3,5- dimethyl-	4	19	2.50×10 ⁻¹ ± 4.13×10 ⁻²	2.10×10 ⁻¹ ± 1.40×10 ⁻¹	
9.840	Decane, 2-methyl-	8	7	$4.44 \times 10^{-2} \pm 1.13 \times 10^{-2}$	3 replicates shown intensity < 5.00×10 ⁴	
9.875	Oxirane, phenyl-	4	1	$2.95 \times 10^{-2} \pm 4.47 \times 10^{-3}$	2.46×10 ⁻¹ , 2 replicates shown intensity < 5.00×10 ⁴	
9.968, 9.978	1,2-Propanedione, 1- phenyl-	4	05	3.56×10 ⁻² , 7.45×10 ⁻² , 1 replicate shown < 5.00×10 ⁴	3 replicates shown intensity < 5.00×10 ⁴	
10.052, 10.058, 10.061	Benzene, 2-ethyl-1,4- dimethyl-	9	19	1.13×10 ⁻¹ ± 8.07×10 ⁻²	9.49×10 ⁻² , 9.69×10 ⁻²	

Retention Time	Tentatively	IM	m/z	%Area (Average, STDEV)		
Retention Time	identified compound	IIVI	III/Z	Methylene chloride	Hexane	
10.167, 10.172, 10.173, 10.179, 10.181	Benzene, 1-ethyl-3,5- dimethyl-	3	19	1.68×10 ⁻¹ ± 3.49×10 ⁻²	1.90×10 ⁻¹ ± 1.10×10 ⁻¹	
10.351,10.355, 10.361, 10.363	Undecane	0	7	$8.10 \times 10^{-2} \pm 3.72 \times 10^{-3}$	2.76×10 ⁻² , 2 replicates shown < 5.00×10 ⁴	
10.568, 10.572, 10.575 10.657, 10.688, 10.689	Hexanoic acid, 2- ethyl-	5	3	$3.02 \pm 2.96 \times 10^{-1}$	5.20×10 ⁻¹ ± 3.30×10 ⁻¹	
10.74, 10.769, 10.786	Phosphoric acid, triethyl ester	5	9	$2.90 \times 10^{-2} \pm 7.86 \times 10^{-3}$	1 replicate shown intensity < 5.00×10 ⁴	
11.14, 11.16, 11.182, 11.21	Benzoic acid	6	05	$3.47 \times 10^{-2} \pm 2.01 \times 10^{-2}$	3 replicates shown intensity < 5.00×10 ⁴	
12.29	Ethanedione, diphenyl-	9	05	6.00×10 ⁻² ± 1.00×10 ⁻²	3 replicates shown intensity < 5.00×10 ⁴	
12.565, 12.654, 12.706	Hydroquinone	3	10	$5.05 \times 10^{-1} \pm 1.46 \times 10^{-1}$	3 replicates shown intensity $< 5.00 \times 10^4$	
12.76, 12.763	4,7-Methano-1H- indenol, hexahydro-	1	6	3.96×10 ⁻² , 3.06×10 ⁻²	3 replicates shown intensity < 5.00×10 ⁴	
13.035, 13.064, 13.084	1,2-Ethanediol, 1- phenyl-	9	07	$7.32 \times 10^{-2} \pm 1.12 \times 10^{-2}$	3 replicates shown intensity < 5.00×10 ⁴	
13.214, 13.224, 13.231	1,2- Benzenedicarboxylic acid	4	04	4.99 ± 5.59×10 ⁻¹	3 replicates shown intensity < 5.00×10 ⁴	
15.294, 15.306, 15.318	p-tertButylcatechol	9	91	$1.41 \times 10^{-1} \pm 2.12 \times 10^{-2}$	3 replicates shown intensity < 5.00×10 ⁴	
15.313, 15.314	2,4-Di-tert- butylphenol	0	91	1.57×10-1	9.77×10 ⁻² ± 6.58×10 ⁻²	
15.37, 15.379, 15.38, 15.382, 15.384	2,6-bis (1,1- dimethylethyl)-4- methyl-phenol	2	05	1.51 ± 1.70×10 ⁻¹	1.80×10 ⁻¹ ± 1.20×10 ⁻¹	

*Results shown only represent chromatogram signals greater than 50,000 a.u.; Styrene is not mentioned because it was excluded from MS program to protect MS from saturation and contamination due to very high concentration in the solution.

S3.1. Volatile content in the cured composite cured at 65.5°C for 25 min

For the composite cured at Condition B (65.5°C / 25 min), the amount of volatile residual remained on the surface $(2.63 \pm 0.24 \%)$ and in the depth $(2.96 \pm 0.13 \%)$ was statistically similar to volatile content existed on the surface and in the depth of composites cured at Conditions A, C and D.

Table S4 The magnitude of volatile material that was released from cured composites during manufacture

Material description	Volatile material emitted during manufacture							
Composite	Condition A	Condition B	Condition C	Condition A				
manufacture conditions	50 min, 65.5 °C	25 min, 65.5 °C	100 min, 65.5 °C	50 min, 93.3 °C				
	Weight	loss due to manufac	ture†, wt%					
Manufacture [†] , N	No vacuum ^{††}							
	8.87 ± 1.67							
Manufacture, V	acuum applied							
	26.43 ± 1.73	25.87, 11.56*	21.95 ± 8.85	23.55 ± 3.77				

[†] Weight loss due to manufacture is equal to the difference between weight of resin mixture and two felts prior to curing and weight of composite obtained from the same materials after curing; * Weight loss was conducted for three replicate cured composites except for this condition where two replicates were measured; ^{††} Weight loss at ambient conditions (no vacuum) was only measured at 65.5 °C for 50 min.

	Table S5 Density and porosity results of cured composites							
		Curing conditions (Average =	± STD)					
	50 min at 65.5°C	100 min at 65.5°C	50 min at 93.3 °C					
Density	R_1 : 1.19 ± 1.00×10 ⁻² ,	R_1 : 1.15 ± 5.38×10 ⁻³ ,	R_1 : 1.14 ± 4.04×10 ⁻² ,					
(g/cm ³)	R_2 : 1.16, 1.17 [£]	R ₂ : $1.17 \pm 7.44 \times 10^{-3}$	$R_2: 1.10^{\$}$					
Porosity	$R_1: 3.44 \times 10^{-1} \pm 2.03 \times 10^{-1},$	$R_1: 3.14 \times 10^{-1} \pm 1.63 \times 10^{-1},$	$R_1:6.04 \times 10^{-1} \pm 5.51 \times 10^{-1}$,					
(%)	$R_2: 2.52 \times 10^{\text{-1}} \pm 1.56 \times 10^{\text{-1}}$	$R_2: 5.70 \times 10^{\text{-1}} \pm 3.40 \times 10^{\text{-1}}$	R_2 : 1.27 ± 4.79×10 ⁻¹					

R is replicate; STD = standard deviation; ^f Each cured composite replicate (i.e. R_1 and R_2) contained three replicate cubes to undergo density measurements except for this condition where two replicate cubes were measured; §Each cured composite replicate (i.e. R_1 and R_2) contained three replicate cubes to undergo density measurements except for this condition where one replicate cube was measured.

The single composite cured at ambient pressure showed no exothermic peak on the surface. No endothermic or exothermic peak was found on the second heating scan exhibiting no volatile residual and resin/initiator remained.

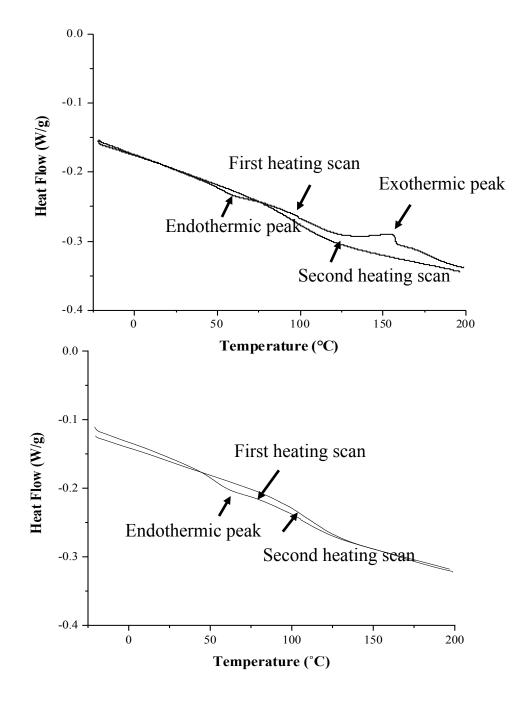


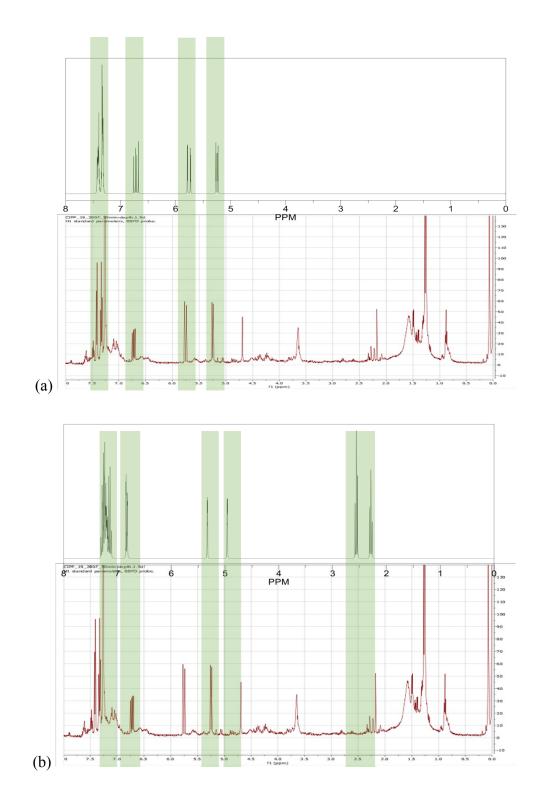
Fig. S2 DSC thermograms of cured composites cured at: (a) 65.5°C/50 min from surface; and (b) 93.3°C/50min from depth.

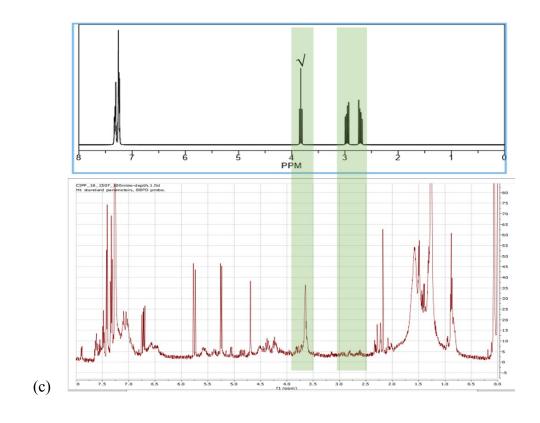
Chemical		Under Vacuum				No Vacuum	Studies in the Literature	
Detected	Resin			100 min at 65.5 °C	50 min at 93.3°C	50 min at 65.5°C	CIPP	Resin Tube
Hexane						,		
							(5.63×10 ² -	(5.72×10 ³ -
Styrene CAR,	$2.34 \times 10^{5} \pm$	$1.02{ imes}10^4$ \pm	$1.20 \times 10^{3} \pm$	$1.06 \times 10^{3} \pm$	$1.26 \times 10^{3} \pm$	$5.22 \times 10^{2} \pm$	1.47×10 ⁴) ²⁵ ,	1.68×10 ⁵) ²⁵ ,
EDR, HAP	2.91×10 ⁴	2.20×10 ²	2.73×10^{2}	4.41×10 ²	3.05×10 ²	1.81×10 ²	(3.20×10 ¹ –	(4.45×10 ⁴ –
							9.30×10 ¹) ²⁶	6.14×10 ⁴) ²⁶
Styrene oxide ^{CAR,} HAP	-	$3.45 \times 10^{1} \pm 2.24 \times 10^{1}$	$1.61 \times 10^{1} \pm 0.94$	2.05×10 ¹ ± 7.55	$1.68 \times 10^{1} \pm 4.93$	$4.40 \times 10^{1} \pm 3.65 \times 10^{1}$	(1.10×10 ¹ - 3.90×10 ¹) ²⁵	(2.20×10 ¹ - 5.50×10 ¹) ²⁵
Benzaldehy		$4.91 \times 10^{1} \pm$	3.18×10 ¹ ±	7.58×10 ¹ ±	2.06×10 ¹ ±	1.14×10 ¹ ±	(1.40×10 ¹ –	
de	-	3.32×10 ¹	3.34×10 ¹	2.89×10 ¹	2.45×10 ¹	8.54×10 ¹	9.40×10 ¹) ²⁶	-
1,3,5-TMB	$2.27 \times 10^{1} \pm 4.00$	3.35 ± 0.87	2.96 ± 0.48	3.61 ± 1.06	3.26 ± 0.58	7.13×10 ¹	(1.70-2.40) ²⁵	(5.10- 5.40×10 ¹) ²⁵
1.0.4 TM	$1.07 \times 10^{2} \pm$	$1.54{ imes}10^1$ ±	$1.83 \times 10^{1} \pm$	$1.94 \times 10^{1} \pm$	$1.70 \times 10^2 \pm$	0.00 + 4.11	(2.20.1.20101)25	(1.10×10 ¹ -
1,2,4 - TMB	2.52×10 ¹	4.44	3.15	5.86	5.16	9.08 ± 4.11	$(2.30-1.20\times10^{1})^{25}$	1.88×10 ²) ²⁵
Benzoic Acid	1 replicate shown<5.0 0×10 ⁴ & SIM<90	$1.51 \times 10^{2} \pm$ 5.37×10 ¹	$1.41 \times 10^2 \pm 1.25 \times 10^1$	$1.80 \times 10^2 \pm 2.17 \times 10^1$	$1.68 \times 10^2 \pm$ 2.74×10 ¹	$1.10 \times 10^{2} \pm$ 2.59×10 ¹	-	-
1-		2.88×102±	3.14×102 ±	3.49×102 ±	3.38×102 ±	3.04×102 ±	(4.33×10 ² -	
tetradecanol	-	2.93×101	2.99×101	1.30×102	5.26×101	6.07×101	8.72×10 ²) ²⁶	

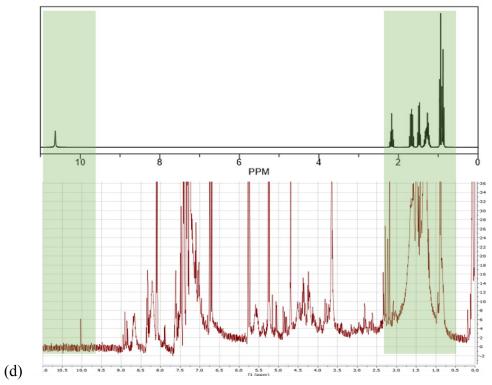
Table S6 Chemical Mass Loading (mg/kg) for the resin and new cured composites manufactured under different conditions in hexane

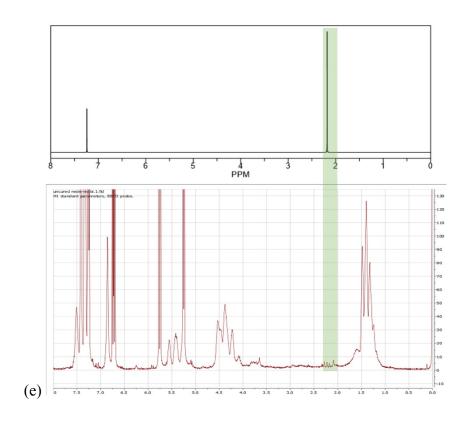
Chemical Resin			Under V	acuum		No Vacuum	Studies in the Literature		
Detected	Kesin	25 min at 65.5°C	50 min at 65.5°C	100 min at 65.5°C	50 min at 93.3 ℃	50 min at 65.5°C	CIPP	Resin Tube	
Hexane							L		
N-	2.03×10 ¹								
Propylbenze	±	3.48 ± 0.80	3.69 ± 0.42	4.03 ± 0.99	3.58 ± 0.94	3.40 ± 0.57	$(0.43 - 1.20 \times 10^{1})^{25}$	$(2.40 \times 10^1 - 4.90 \times 10^1)^{25}$	
ne	5.19								
2-	2.31								
Propenylben	±	-	-	-	-	-	-	-	
zene	5.39×10 ¹								
			1 replicate			2 replicates			
Hydroquino			shown <			shown <			
ne CAR*, HAP	-	-	5.00×10 ⁴ &	-	-	5.00×10 ⁴ &	-	-	
			SIM < 90			SIM < 90			
1 Ed. 1.2	1.07102	3 replicates	3 replicates	3 replicates	3 replicates	3 replicates			
1-Ethyl-3-	1.27×10^{2}	shown >	shown >	shown >	shown >	shown >			
methylbenze	±	5.00×10 ⁴ &	5.00×10 ⁴ &	5.00×10^4 &	5.00×10 ⁴ &	5.00×10^4 &	-	-	
ne	2.84×10^{1}	SIM > 90	SIM > 90	SIM > 90	SIM > 90	SIM > 90			
2-	1.23×10 ¹	2 replicates	3 replicates	3 replicates	3 replicates	3 replicates			
		shown <	shown <	shown <	shown <	shown <			
Ethylhexano	±	5.00×10 ⁴ &	5.00×10 ⁴ &	5.00×10^4 &	5.00×10 ⁴ &	5.00×10^4 &	-	-	
ic acid	2.43	SIM < 90	SIM < 90	SIM < 90	SIM < 90	SIM < 90			
	1.41								
BHT	±	-	-	-	-	-	$(4.90-9.40)^{25}$	$(3.10 \times 10^1 - 8.90 \times 10^1)^{25}$	
	0.24								

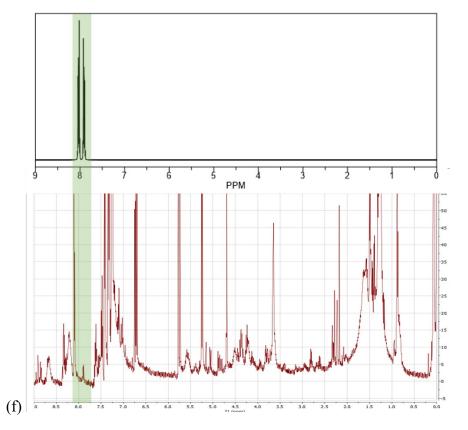
Chemical Detected	Resin	Under Vacuum			No Vacuum	Studies in the Literature		
		25 min at 65.5°C	50 min at 65.5°C	100 min at 65.5°C	50 min at 93.3°C	50 min at 65.5°C	СІРР	Resin Tube
Hexane								
Sum	2.34×10 ⁵	1.57×10 ³	1.73×10 ³	1.72×10 ³	1.82×10 ³	1.07×10 ³	$(6.22 \times 10^2 - 1.47 \times 10^4)^{25},$ $(8.37 \times 10^2 - 1.57 \times 10^3)^{26}$	$(5.98 \times 10^3 - 1.69 \times 10^5)^{25},$ $(4,45 \times 10^4 - 3.20 \times 10^5)^{26}$











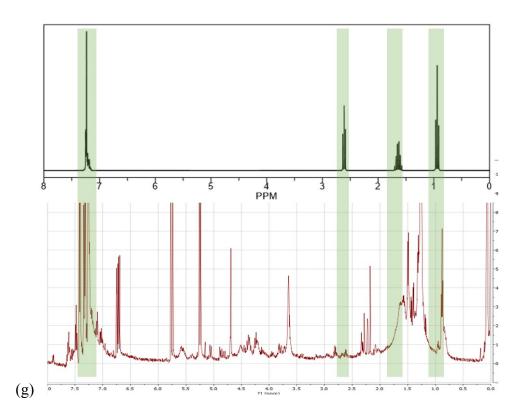
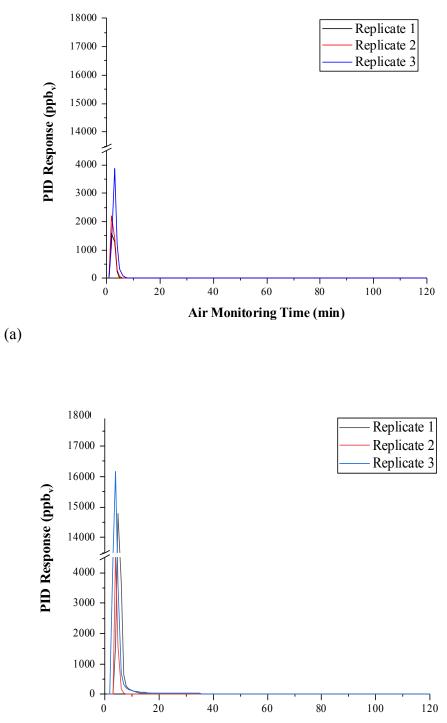


Fig. S3 HNMR images of compounds detected in uncured resin and cured composites at different curing conditions: (a) Styrene, (b) 2,4-diphenyl-1-butene (styrene dimer), (c) styrene oxide, (d) 2-ethylhexanoic acid, (e) 1,3,5-trimethylbenzene, (f) phthalate anhydride, (g) propylbenzene



Air Monitoring Time (min)

(b)

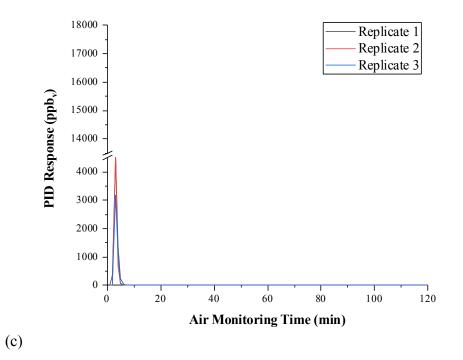


Fig. S4 PID air monitoring results from cured composites (a) 65.5 °C/50 min, (b) 65.5 °C/10 min and (c) 93.3 °C/50 min during 2 hr ventilation.

	Time (min)	Normalized styrene weight (ng/cm ²), Concentration (ppm_v) Average \pm STD					
		65.5 C/50 min	65.5 C/ 100 min	93.3 C/ 50 min			
	0	$1.25 \pm 1.20, 2.19 \pm 1.47$	4.81 ± 3.87, 6.11 ± 4.90	$1.05 \pm 1.63, 1.30 \pm 2.04$			
	5	$5.34 \times 10^{-2} \pm 5.30 \times 10^{-2}$,	$3.26 \times 10^{-2} \pm 1.40 \times 10^{-2}$,	$1.64 \times 10^{-2} \pm 3.75 \times 10^{-3}$,			
		$6.92 \times 10^{-2} \pm 6.93 \times 10^{-2}$	$4.13 \times 10^{-2} \pm 1.77 \times 10^{-2}$	$2.05 \times 10^{-2} \pm 4.53 \times 10^{-3}$			
	10	$9.42 \times 10^{-3} \pm 4.52 \times 10^{-3}$,	$1.49 \times 10^{-2} \pm 1.58 \times 10^{-2}$,	$1.11 \times 10^{-3} \pm 1.92 \times 10^{-3}$,			
		$1.21 \times 10^{-2} \pm 6.01 \times 10^{-3}$	$1.89 \times 10^{-2} \pm 1.98 \times 10^{-2}$	$1.38 \times 10^{-3} \pm 2.38 \times 10^{-3}$			
	20	$6.05 \times 10^{-3} \pm 2.98 \times 10^{-3}$,	$9.30 \times 10^{-3} \pm 9.17 \times 10^{-3}$,	$7.61 \times 10^{-4} \pm 8.90 \times 10^{-4},$			
		$7.79 \times 10^{-3} \pm 3.95 \times 10^{-3}$	$1.18 \times 10^{-2} \pm 1.15 \times 10^{-2}$	$9.46 \times 10^{-4} \pm 1.10 \times 10^{-3}$			
Dynamic	40	$3.54 \times 10^{-3} \pm 2.86 \times 10^{-3}$,	$7.49 \times 10^{-3} \pm 8.42 \times 10^{-3}$,	$1.14 \times 10^{-4} \pm 1.97 \times 10^{-4}$,			
		$4.60 \times 10^{-3} \pm 3.72 \times 10^{-3}$	$9.45 \times 10^{-3} \pm 1.05 \times 10^{-2}$	$1.42{\times}10^{\text{-4}}\pm2.45{\times}10^{\text{-4}}$			
	60	$3.79 \times 10^{-3} \pm 1.02 \times 10^{-3}$,	$8.46 \times 10^{-3} \pm 8.45 \times 10^{-3}$,	$1.14 \times 10^{-4} \pm 1.97 \times 10^{-4}$,			
		$4.87 \times 10^{-3} \pm 1.39 \times 10^{-3}$	$1.07 \times 10^{-2} \pm 1.06 \times 10^{-2}$	$1.42{\times}10^{\text{-4}}\pm2.45{\times}10^{\text{-4}}$			
	80	$2.62 \times 10^{-3} \pm 2.44 \times 10^{-3}$,	$6.81 \times 10^{-3} \pm 7.66 \times 10^{-3},$	$1.14 \times 10^{-4} \pm 1.97 \times 10^{-4}$,			
		$3.39 \times 10^{-3} \pm 3.17 \times 10^{-3}$	$8.59 \times 10^{-3} \pm 9.58 \times 10^{-3}$	$1.42 \times 10^{-4} \pm 2.45 \times 10^{-4}$			
	100	$3.49 \times 10^{-3} \pm 1.27 \times 10^{-3}$,	$6.62 \times 10^{-3} \pm 7.79 \times 10^{-3}$,	$1.14 \times 10^{-4} \pm 1.97 \times 10^{-4}$,			
	100	$4.48 \times 10^{-3} \pm 1.70 \times 10^{-3}$	$8.38 \times 10^{-3} \pm 9.78 \times 10^{-3}$	$1.42 \times 10^{-4} \pm 2.45 \times 10^{-4}$			
	120	$2.35 \times 10^{-3} \pm 1.75 \times 10^{-3}$,	$8.15 \times 10^{-3} \pm 7.82 \times 10^{-3}$,	$1.14 \times 10^{-4} \pm 1.97 \times 10^{-4}$,			
	120	$3.05 \times 10^{-3} \pm 2.29 \times 10^{-3}$	$1.03 \times 10^{-2} \pm 9.83 \times 10^{-3}$	$1.42{\times}10^{\text{-4}}\pm2.45{\times}10^{\text{-4}}$			

Table S7 Styrene normalized weight and concentration captured during 2hr dynamic air monitoring

STD = *standard deviation*

S3.2. The most abundant chemical in cured composites

As expected, styrene with the highest loading magnitude $(9.74 \times 10^3 - 2.07 \times 10^4 \text{ mg/Kg})$ constituted a significant portion of cured composites. This compound also showed higher vapor pressure (i.e. 6.40 mmHg at 25 °C) and subsequently, higher volatility compared with other chemicals confirmed in the cured composite extraction. The order of these chemicals with higher vapor pressure (i.e. higher volatility) to lower vapor pressure (i.e. lower volatility) includes: styrene > *N*-propylbenzene > 3-ethyl-1-methylbenzene > 1,3,5-TMB > 1,2,4-TMB > 2-propenylbenzene > benzaldehyde > styrene oxide > 2-ethylhexanoic acid > BHT > benzoic Acid > 1-tetradecanol > hydroquinone. Therefore, it could be assumed that considerable amount of chemicals discharged into air during composite manufacturing contains styrene.

Compound	Chemical Formula	MW, g/mol	Chemical Structure	Vapor Pressure (mmHg 25°C)
Styrene	C_8H_8	104.15		6.40
Styrene oxide	C_8H_8O	120.15		0.30
Benzaldehyde	C ₇ H ₆ O	106.13	O H	1.27
1,3,5-TMB	C ₉ H ₁₂	120.20	H ₃ C CH ₃	2.48

Table S8 Physical and chemical properties of confirmed organic compounds in the uncured resin tube and cured composite

Compound	Chemical Formula	MW, g/mol	Chemical Structure	Vapor Pressure (mmHg 25°C)
1,2,4-TMB	C ₉ H ₁₂	120.20	H ₃ C CH ₃	2.10
Benzoic Acid	$C_7H_6O_2$	122.12		7×10 ⁻⁴
1-Tetradecanol	C ₁₄ H ₃₀ O	214.39	но	1.1×10 ⁻⁴
N-Propylbenzene	C ₉ H ₁₂	120.20		3.42
2-Propenylbenzene	C ₉ H ₁₀	118.18		1.69
Hydroquinone	$C_6H_6O_2$	110.11	çç	1.90×10 ⁻⁵
3-Ethyl-1- methylbenzene	С9Н11	120.19	HSC	3.04
2-Ethylhexanoic acid	C8H16O2	144.214	H ₂ C HO CH ₃	< 7.50×10 ⁻³
ВНТ	C15H24O	220.36	OH K	5.20×10 ⁻³

Table S9 Endothermic/exothermic temperature observed in new cured composites based on
different curing conditions.

	Curing condition and endothermic/exothermic temperature, °C						
Parameter	Condition A	Condition B	Condition C	Condition D			
	50 min, 65.5°C	100 min, 65.5°C	50 min, 93.3°C	25 min, 65.5°C			
	Endothermic/Exothermic	Endothermic/	Endothermic/	Endothermic/			
	Temperature	Exothermic	Exothermic	Exothermic Temperature			
		Temperature	Temperature				
After Manu	facture, No vacuum	L	I	L			
Surface	£ 62°C, 64°C, 65°C / -	-	-	-			
Depth	^{££} 60°C, 63°C, 64°C, 68°C / 153.5°C 154.5°C	-	-	-			
After Manuj	After Manufacture, Vacuum applied						
Surface	€ 58°C, 59°C, 60°C, 64°C, 65°C / 154°C, 154.5°C, 156.5°C, 159°C	<pre>§ 57°C, 58°C, 58.5°C, 64°C / 151.3°C, 153.5°C, 155°C, 155.5°C, 159.5°C</pre>	[¥] 60°C, 61.8°C, 64°C / 154°C, 159.5°C, 164°C, 168°C	t			
Depth	^{€€} 56°C, 59°C, 60°C / 158°C, 160°C, 160.6°C, 161.5°C, 167°C, 168°C	^{§§} 58°C, 59°C, 62°C, 64°C / 158.5°C, 159.5°C, 163°C, 164°C, 165°C	 ^{¥¥} 56.5°C, 58°C, 60°C, 62°C, 64°C / 152°C, 163.5°C, 164°C, 167.5°C, 168.5°C, 172°C 	[‡] 64.5°C, 66°C, 67°C, 68°C / 161°C, 164.5°C			

Initial volatile content of the resin was 39 ± 1.74 %; -: Not measured. The following symbols indicate the number of replicates that showed endothermic peak at approximately 65°C and exothermic peak at 140-160°C per the total number of replicates: e endothermic peak: 8/8, exothermic peak: 0/9; e endothermic peak: 6/9, exothermic peak: 2/9; † endothermic peak:, exothermic peak:; i endothermic peak: 8/9, exothermic peak: 3/9; e endothermic peak: 8/9, exothermic peak: 5/9; ee endothermic peak: 4/9, exothermic peak: 7/9; g endothermic peak: 4/9, exothermic peak: 5/9; g endothermic peak: 3/8, exothermic peak: 7/8; ${}^{\sharp}$ endothermic peak: 5/9, exothermic peak: 4/9; ${}^{\sharp}$ endothermic peak: 6/9

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