Electronic Supplementary Information

A Novel Nitrogen-Doped KFeS₂/C Composites for Efficient Removal of Cr(VI)

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Analyses of the adsorption data

The equilibrium adsorption capacity (q_e , mg g⁻¹) was calculated by Eq. (1):

$$q_e = \frac{V \cdot (C_0 - C_e)}{m} \tag{1}$$

where $C_0 \text{ (mg L}^{-1)}$ and $C_e \text{ (mg L}^{-1)}$ represent the initial and equilibrium concentrations of Cr(VI) in solutions respectively, V (L) and m (g) represent volume and mass, respectively.

The study of adsorption kinetics is of great significance for the objective evaluation of Cr(VI) adsorption rate. The kinetics of adsorption of Cr(VI) on NSC-1.3 was analyzed by using pseudo-first-order and pseudo-second-order models, which were expressed as Eq. (2) and Eq. (3), respectively:¹

$$log(q_e - q_t) = logq_e - \frac{tk_1}{2.3303}$$
(2)
$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e}$$
(3)

where $q_e \pmod{g^{-1}}$ and $q_t \pmod{g^{-1}}$ represent the adsorption capacity at equilibrium and time *t*, respectively, $k_1 \pmod{k_2} \pmod{g^{-1}}$ represent the corresponding rate constants, respectively.

In order to evaluate the adsorption capacity of NSC-1.3 for Cr(VI), the Langmuir and Freundlich isothermal adsorption model was used to fit the experimental data at three temperatures. The models were expressed as Eq. (4) and Eq. (5), respectively:²

$$\frac{C_e}{q_e} = \frac{l}{q_m K_L} + \frac{C_e}{q_m} \tag{4}$$

$$logq_e = \frac{l}{n} logC_e + logK_F$$
⁽⁵⁾

Where $C_e \text{ (mg L}^{-1)}$ represents the equilibrium concentration, and $q_e \text{ (mg g}^{-1)}$ and $q_m \text{ (mg g}^{-1)}$ represent the equilibrium adsorption capacity and the maximum adsorption capacity, respectively, K_L (L mg $^{-1}$) is Langmuir equilibrium constant, K_F (mg g $^{-1}$) represents an adsorption coefficient, and n is the index coefficient.

The study of thermodynamic parameters such as Gibbs free energy change (ΔG°), enthalpy (ΔH°), and entropy change (ΔS°) has profound significance to the specific adsorption process. These parameter values can be calculated by *Eq.* (6), *Eq.*(7) and *Eq.*(8), respectively:³

$$\Delta G^{\circ} = -RT ln K_d \tag{6}$$

$$K_d = \frac{q_e}{C_e} \tag{7}$$

$$lnK_{d} = \frac{\Delta S^{\Box}}{R} - \frac{\Delta H^{\Box}}{RT}$$
(8)

Where K_d is the thermodynamic equilibrium constant, R (8.314 J mol⁻¹ K⁻¹) is the gas constant, and *T*(K) is the experimental temperature.

DFT simulation details

The density functional theory (DFT) was used for all calculations implemented in Dmol3 code.^{4,5} The generalized-gradient approximation (GGA) of Perdew-Burke-Ernzerhof (PBE) functional⁶ was utilized for all geometry optimization and electronic properties calculations. In intermolecular interactions long-range dispersion-correction was set by applying the Grimme's DFT-D correction.^{7,8} Double numerical pluspolarization (DNP) basis set and DFT semicore pseudopotenitals (DSPPs) were used for all the calculations.⁹ While The thermal smearing was set to 0.005 au while the basis set cutoff was set to 4.6 Å. The convergence tolerance for geometries optimization was set to 10⁻⁵ Ha, 0.001 Ha/ Å for the energy while 0.005 Å for force and displacement. The KFeS₂ structure was modeled according to the recently reported literature¹⁰ which is depicted in Fig. S1. Then we selected single layer 1 x 5 x 1 non-periodic single layer to reduce the computational simulations cost and just to check the N doping effects on the KFeS₂ structure and there adsorption behaviors towards the Cr(VI).



Fig. S1 Graphical representation of the KFeS₂ supercell structure.

The formation energy (E_f) for N doped system was calculated as:

$$E_f = E_{N \text{ KFeS}_2} - (E_{n \text{ N}} + E_{\text{KFeS}_2} - E_{n \text{S}})$$
(9)

where, E_{NKFeS2} and E_{KFeS2} are the total energy of the N doped KFeS₂ layer and undoped KFeS₂ layer while the E_{nN} and E_{nS} are the total energies of the isolated N and S atoms, respectively. The adsorption energy (E_{ad}) was computed using the following equation:

$$E_{ad} = E_{complex} - (E_{Ml} + E_{M2})$$
⁽¹⁰⁾

here, E_{complex} is the total energy of the complex system (H₂CrO₄ adsorbed over the pure or N doped KFeS₂ layer) while E_{M1} and E_{M2} are the total energy of the individual monomers (isolated pure KFeS₂, N-doped KFeS₂ layer and H₂CrO₄).



Fig. S2 (a) Adsorption properties of various adsorbents under the same conditions (m = 4 mg, V = 30 mL, T = 298 K, $C_0 = 50 \text{ mg L}^{-1}$), (b) impact of pH values (m = 4 mg, V = 30 mL, T = 298 K, $C_0 = 50 \text{ mg L}^{-1}$), the insertion diagram is chromium concentration at different pH conditions, (c) pH value changes before and after Cr(VI) adsorption, (d) Zeta potentials of NSC-1.3 in aqueous solution at different pH values, (e) impact of coexisting ions on Cr(VI) removal by NSC-1.3 (m = 4 mg, V = 30 mL, pH = 2, T = 298 K, $C_0 = 30 \text{ mg L}^{-1}$), (f) impact of time on Cr(VI) removal by NSC-1.3 (m = 33.3 mg, V = 250 mL, pH = 2, T = 298 K, $C_0 = 50 \text{ mg L}^{-1}$).



Fig. S3 (a) Pseudo first-order, (b) Pseudo second-order kinetic fitting of NSC-1.3 (m = $33.3 \text{ mg}, \text{V} = 250 \text{ mL}, \text{pH} = 2, \text{T} = 298 \text{ K}, \text{C}_0 = 50 \text{ mg } \text{L}^{-1}$).



Fig. S4 (a) Effect of initial concentration and temperature, (b) Langmuir isotherm, (c) Freundlich isotherm fitting of NSC-1.3 at different temperatures (m = 4 mg, V = 30 mL, pH = 2, $C_0 = 30 - 300$ mg L⁻¹).



Fig. S5 Plot of $\ln K_d$ against 1/T for Cr(VI) removal on NSC-1.3 (m = 4 mg, V = 30 mL, pH = 2, C₀ = 50 mg L⁻¹, T = 298 - 318 K.



Fig. S6 Regeneration experiment of NSC-1.3 (pH = 2, $C_0 = 50 \text{ mg } L^{-1}$, No. 1: m = 4 mg,

V = 30 mL, No. 2: m = 2.7 mg, V = 20 mL, No. 3: m = 2 mg, V = 15 mL).



Fig. S7 (a) SEM image of primary NSC-1.3, (b) SEM image of NSC-1.3 after Cr(VI) adsorption, (c) SEM of NSC-1.3 after regeneration, (d) the diameter of nanoparticles from (c).



Fig. S8 (a) C 1s XPS spectra of NSC-1.3 before and after adsorption, (b) the percentage of Cr species after the reaction with Cr(VI).

Absorbents	$q_{\rm max}$ (mg g ⁻¹)	pН	References
HAB-derived Fe/C	165.00	2	11
Fe/FeS	69.70	5	12
AMGO	123.40	2	13
NZVI/Fe ₃ O ₄ /graphene	101.00	3	14
Fe@PC	10.07	15	
Corn cob-derived magnetic AC	125.00	2	16
Iron doped ordered mesoporous carbon	257.00	5	17
MAC-800	66.35	4	18
NDCS	432	3	19
N-doped carbon spheres	181.82	2	20
HA-N-MPC	130.5	2	21
N-doped porous carbon(Ni)	96.27	2.5	22
NSC-1.3	326.80	2	This work

Table S1 Comparison of removal properties of adsorbents for Cr(VI).

Table S2 Thermodynamic parameters of Cr(VI) removal on NSC-1.3.

ΔH° (kJ mol ⁻¹)	$\Delta S^{\circ}(\text{J mol}^{-1} \text{ K}^{-1})$	$\Delta G^{\circ}(\text{kJ mol}^{-1})$			
		298 K	308 K	318 K	
59.6868	231.4532	-9.2863	-11.6088	-13.9153	

Table S3 The content of different chemical states of N 1s and S 2p in NSC-1.3

	Sulphur content (%)			Nitrogen content (%)						
	Total	S_n^2 -	S ₈	S(VI)	Total	N(I)	N(II)	N(III)	N(IV)	N(V)
Before	8.5	45.1	31.8	23.1	3.01	19.9	19.9	20.0	20.1	20.1
adsorption										
After	7.1	39.5	28.1	32.4	2.98	33.9	11.2	28.9	18.3	7.7

adsorption

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