

Supplementary information

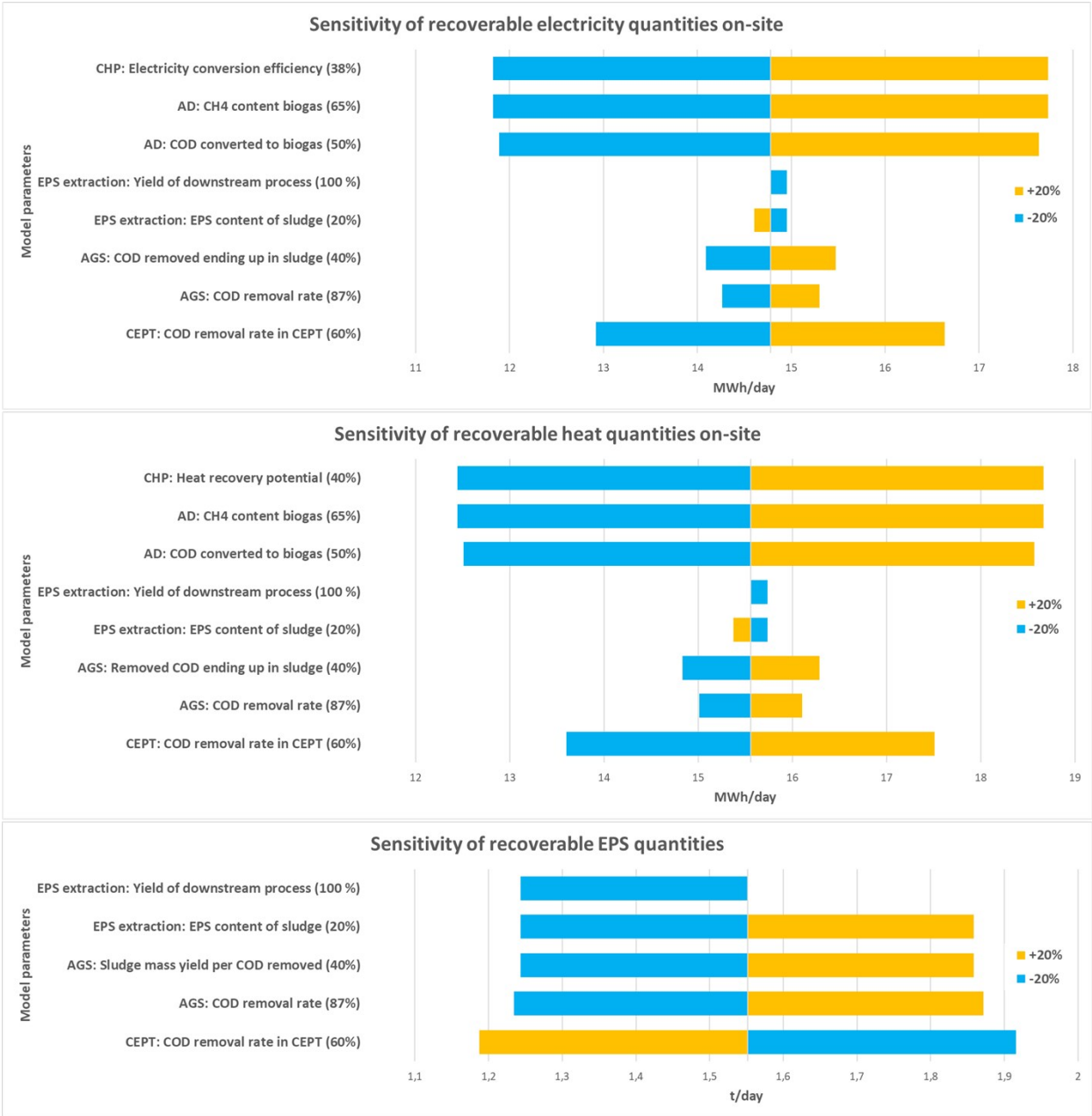
Article: Exploring resource recovery potentials for the aerobic granular sludge process by mass and energy balances - Energy, biopolymer and phosphorous recovery from municipal wastewater

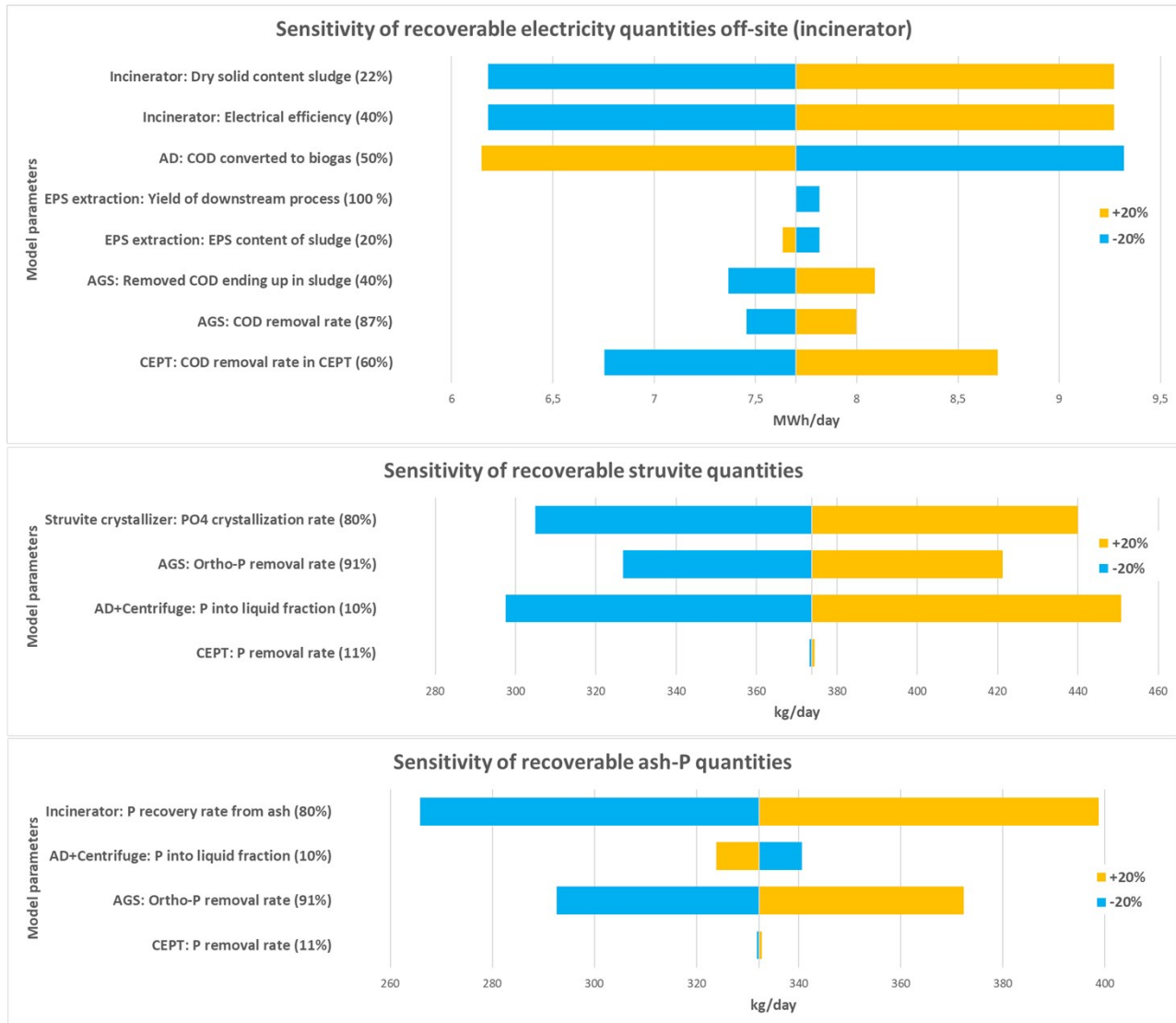
Model parameters

Influent			
Average flow rate	64400	m ³ /d	Personal communication
COD	729,8	mg/l	Personal communication
BOD	287,3	mg/l	Personal communication
TSS	314,4	mg/l	Personal communication
TKN	60,6	mg/l	Personal communication
NH ₄ -N	70	%/TKN	(Hartley, 2013)
Organic-N	30	%/TKN	(Hartley, 2013)
P-total	8,4	mg/l	Personal communication
Ortho-P	67	%/P-total	(Henze and Comeau, 2008)
Organic-P	33	%/P-total	(Henze and Comeau, 2008)
Fe total	1,0	mg/l	(Wilfert et al., 2015)
Fe ³⁺ share	100	%	(Wilfert et al., 2016)
Fe ³⁺ forming vivianite	100	%	(Wilfert et al., 2016)
Energy content COD	17,8	kJ/g COD	(Heidrich et al., 2011)
Coarse screen			
No impacts on any relevant flows are assumed			
CEPT			
Coagulant	Polymer		(Klute and Hahn, 1994)
COD removal	60	%	(Wan et al., 2016)
TKN removal in conventional primary settler (with 40% COD removal, no coagulant)	16,4	%	based on (Hartley, 2013)
P-total removal in conventional primary settler (with 40% COD removal, no coagulant)	11	%	(Cornel and Schaum, 2009)
Effect of coagulation compared to conventional primary settler with 40% COD removal:			
TKN effluent concentration	-9,4	%	based on (Klute and Hahn, 1994)
P-total effluent concentration	-33,3	%	based on (Klute and Hahn, 1994)
AGS			
COD oxidized	60	%	(Winkler, 2012)
COD into sludge	40	%	(Winkler, 2012)
COD removal rate	87	%	based on (Pronk et al., 2015)
Sludge mass yield per COD removed	40	%	Wan et al. 2016
TKN removal rate	94	%	(de Kreuk et al., 2005)
TKN into sludge	20	%	(Matassa et al., 2015)
Organic-N converted to NH ₄	90	%	(Makinia et al., 2011)
Organic-P removal	87	%	based on (Pronk et al., 2015)

Ortho-P removal	91	%	based on (Pronk et al., 2015)
Organic-P converted to PO ₄	90	%	(Krishnaswamy et al., 2011)
Fe-P removed with sludge	100	%	own assumption
EPS extraction			
EPS content of sludge	20	%	(van der Roest et al., 2015)
Yield of downstream process	100	%	own assumption
C content EPS	47,05	wt%	(Felz et al., 2019)
N content EPS	7,61	wt%	(Felz et al., 2019)
P content EPS	2,92	wt%	(Felz et al., 2019)
Anaerobic digester			
COD converted to biogas	50	%	(Khiewwijit et al., 2016)
CH ₄ content biogas	65	%	(Frijns et al., 2013)
Producible amount of CH ₄	0,35	Nm ³ CH ₄ /kg COD	(Frijns et al., 2013)
Calorific value CH ₄	35,9	MJ/Nm ³	(Frijns et al., 2013)
Organic-N converted to NH ₄	100	%	(Mehta et al., 2015)
Organic-P converted to PO ₄	100	%	(Mehta et al., 2015)
Combined heat and power			
Electricity conversion efficiency	38	%	(Verstraete and Vlaeminck, 2011)
Heat recovery potential	40	%	(Verstraete and Vlaeminck, 2011)
Decanter centrifuge			
COD ending in liquid fraction	10	%	(Andreoli et al., 2007)
NH ₄ -N ending in liquid fraction	13	%	(Khiewwijit et al., 2016)
PO ₄ -P ending in liquid fraction	13	%	(Khiewwijit et al., 2016)
Incinerator			
Energy content COD	0,0178	kJ/mgCOD	(Heidrich et al., 2011)
Electrical efficiency	40	%	(Faaij, 2006)
Dry solid content sludge	22	%	(Frijns et al., 2013)
P recovery rate from ash	80	%	(Lundin et al., 2004)
Struvite crystallization			
PO ₄ crystallization rate	80	%	(Martí et al., 2010)
Required molecular ratio of (Mg ²⁺ :NH ₄ ⁺ :PO ₄ ³⁻)	1:1:1		(Verstraete et al., 2009)
O₂ consumption AGS reactor			
COD removal rate	87	%	(Pronk et al., 2015)
COD into CO ₂	60	%	(Winkler, 2012)
NH ₄ per TKN in	70	%	(Hartley, 2013)
Organic-N per TKN in	30	%	(Hartley, 2013)
Organic-N hydrolyzed to NH ₄	90	%	(Makinia et al., 2011)
NH ₄ removal rate	94	%	(de Kreuk et al., 2005)
NH ₄ uptake in AGS	20	%	(Matassa et al., 2015)

Sensitivity analysis





Effluent qualities

All designs would meet the Dutch legal effluent requirements.

Pollutant	Legal (Pronk et al., 2015)	Design					
		Status quo	AD	AD/CEPT	EPS	AD+EPS	AD/CEPT+EPS
COD	125	92,3	95,7	44,0	92,3	94,8	43,6
P-Total	1	0,7	0,8	0,5	0,7	0,8	0,5
TKN	7	5,3	5,9	4,6	5,9	5,9	4,6

Biodegradable-COD:N ratio AGS reactor

To ensure a sufficient denitrification in the AGS reactor it is important to maintain a high enough bCOD:N ratio. During CEPT ca. 60% bCOD (Wan et al., 2016) but only ca. 25% TKN (Hartley, 2013; Klute and Hahn, 1994) can be assumed to be removed before AGS treatment. Therefore, it needs

to be checked if sufficient bCOD is still present in the AGS reactor. Assuming that the total influent-COD consists to 75% of biodegradable COD (bCOD) (Hartley, 2013; Pasztor et al., 2009), a bCOD:N ratio of 4,9 can be expected in those designs with CEPT integration.

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