

Supporting information

Identification of C₂-C₅ products from CO₂ hydrogenation over PdZn/TiO₂-ZSM-5 hybrid catalysts.

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1. Commercial ZSM-5 zeolites characterisation

1.1 Powder X-ray diffraction (XRD) characterisation

ZSM-5 zeolites with different Si:Al ratio (23, 50 and 80) were purchased from Alfa Aesar in their NH_4^+ form. Prior to use or characterisation, the activated H^+ -ZSM-5 form was obtained by annealing in static air ($550\text{ }^\circ\text{C}$, $10\text{ }^\circ\text{C}\cdot\text{min}^{-1}$, 6 h). Obtained XRD patterns (Figure S1) correlated with the MFI morphology of ZSM-5 zeolites (PDF 00-89-1421).

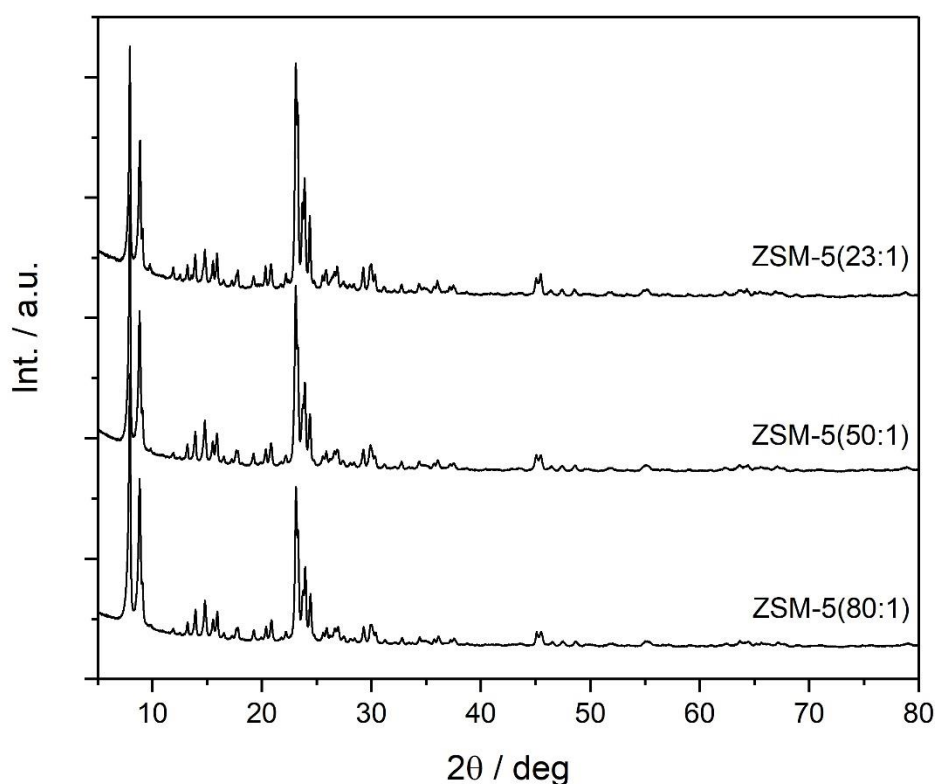


Figure S1. XRD patterns recorded for commercial ZSM-5 zeolites after annealing in static air ($550\text{ }^\circ\text{C}$, $10\text{ }^\circ\text{C}\cdot\text{min}^{-1}$, 6 h).

1.2 Pore size and BET surface area

Pore size and surface area of annealed ZSM-5 commercial zeolites were obtained from N_2 absorption isotherms at 77 K on a 3-flex micromeritics instrument. Prior to analysis, ZSM-5 zeolites were degassed *in situ* under vacuum at $250\text{ }^\circ\text{C}$ for 10 h. A DFT model assuming cylindrical pores and oxide surface was used to obtain the pore size, BET surface areas were obtained on the linear region of the isotherm below at $P/P^0 < 0.3$.¹ As shown in Table S1, no significant changes in pore size neither BET surface area were observed between commercial ZSM-5 zeolites.

Table S1. Pore size and BET surface area obtained from commercial ZSM-5 zeolites after annealing in static air (550 °C, 10 °C·min⁻¹, 6 h) through N₂ absorption.

zeolite	Pore size / Å	BET / m ² g ⁻¹
ZSM-5 (80:1)	5.5 ± 1	461 ± 1
ZSM-5 (50:1)	5.4 ± 1	467 ± 1
ZSM-5 (23:1)	5.3 ± 1	460 ± 1

2. Catalytic activity for CO₂ hydrogenation

The use of PdZn/TiO₂-ZSM-5 hybrid catalysts allow the production of olefins and paraffins directly from CO₂ in a single bed reactor. PdZn/TiO₂ was used as a CH₃OH synthesis catalyst, whilst solid acid ZSM-5 catalysts were used for the consecutive CH₃OH dehydration to DME and the further MTH/DMTH conversion to hydrocarbons.

2.1 CO₂ reaction metrics

PdZn/TiO₂ (0.25 g cat. diluted with 0.25 g of SiC) and PdZn/TiO₂-ZSM-5 hybrid catalysts (0.25 g of methanol synthesis catalyst mixed with 0.25 g of activated zeolite, 425-600 µm pellet size) were tested under CO₂ hydrogenation conditions. The methanol synthesis catalyst consisted of 5 wt.% Pd loading and a Pd to Zn molar ratio of 1:5. Reaction temperature was controlled by placing a thermocouple in the middle of the catalyst bed, catalysts were kept in place using quartz wool. Prior to reaction, catalysts were pre-reduced *in situ* with 5 % H₂/He (400 °C, 5 °C min⁻¹, 1 h). The reactor was then allowed to cool down to 50 °C, the gas flow was swap from 5 % H₂ to the reaction mixture (CO₂/H₂/N₂ = 1/3/1, 30 ml min⁻¹), pressured (20 bar) and heated to the reaction temperature (240, 270, 300, 320, 340 and 360 °C, 5 °C min⁻¹, 6 h dwell at each temperature). Post reaction lines were heated at 120 °C using heating tape to avoid product condensation. Reaction products and reagents were measured online *via* GC analysis fitted with an FID and a TCD detector.

The following calculations were used to determine the CO₂ conversion, product selectivity and productivities:

Through the ideal gas law (equation S1) where P is the pressure of the reaction mixture at the mass flow controller (MFC) (1 bar), R is the gas constant (83.15·10⁻³ dm³ bar K⁻¹ mol⁻¹), T is the temperature (298.15 K) and V is the volume (0.03 dm³ min⁻¹ obtained from the flow gas used during the reaction of 30 ml min⁻¹), the total molar gas (n) flow was determined.

$$PV = nRT \quad n = 1.21 \cdot 10^{-3} \text{ CO}_2 \text{ mol min}^{-1} \quad \text{Eq. S1}$$

Nitrogen gas was used as internal standard at a concentration of 20 vol. %. A blank reactor was analysed simultaneously to the CO₂ hydrogenation reaction, CO₂ conversion was calculated according to equation S2.

$$\text{CO}_2 \text{ conv. \%} = \frac{\left(\frac{\left(\frac{\text{Blank } \int \text{CO}_2 / \text{area count}}{\text{Blank } \int \text{N}_2 / \text{area counts}} \right) - \left(\frac{\int \text{CO}_2 / \text{area count}}{\int \text{N}_2 / \text{area counts}} \right)}{\left(\frac{\text{Blank } \int \text{CO}_2 / \text{area count}}{\text{Blank } \int \text{N}_2 / \text{area counts}} \right)} \right) \times 100 \quad \text{Eq S2}$$

Because the number of moles in the gas phase change during the reaction, a compression factor (CF) was introduced (equation S3).

$$\text{CF} = \frac{\int \text{N}_2 / \text{area counts}}{\text{Blank } \int \text{N}_2 / \text{area counts}} \quad \text{Eq S3}$$

Non-reacted CO₂ was calculated according to equation S4.

$$\text{Non-reacted CO}_2 \text{ mol min}^{-1} = \frac{\frac{\int \text{CO}_2 / \text{area counts}}{rF \text{ CO}_2} \times (\text{total gas flow} / \text{mol min}^{-1})}{\text{CF}} \quad \text{Eq S4}$$

CH₃OH productivity was calculated according to equation S5, where rF is the response factor obtained from the calibration (area counts per mol⁻¹).

$$\text{CH}_3\text{OH mol min}^{-1} = \frac{\left(\frac{\int \text{CH}_3\text{OH} / \text{area counts}}{rF \text{ CH}_3\text{OH}} \right) \times \left(\frac{\text{total gas flow} / \text{ml min}^{-1}}{0.25 \text{ ml loop volume}} \right)}{\text{CF}} \quad \text{Eq S5}$$

Productivity for remaining products was obtained following the next calculations (equation S6 representative for CO productivity), where rF is the response factor obtained from the corresponding calibration (area counts per ppm⁻¹).

$$\text{CO mol min}^{-1} = \frac{\frac{\int \text{CO} / \text{area counts}}{rF \text{ CO}} \times (\text{total gas flow} / \text{mol min}^{-1})}{\text{CF}} \quad \text{Eq. S6}$$

The product selectivity based on CO₂ hydrogenation was determined by dividing its productivity times the number of carbons (nC) by the productivities of all the products. For instance, methanol and ethane selectivity was calculated following equation S7 and S8, respectively.

$$\text{CH}_3\text{OH sel. \%} = \left(\frac{\text{CH}_3\text{OH productivity} \times 1C / \text{mol min}^{-1}}{\Sigma \text{ productivities}} \right) \times 100 \quad \text{Eq. S7}$$

$$\text{CH}_3\text{CH}_3 \text{ sel. \%} = \left(\frac{\text{CH}_3\text{CH}_3 \text{ productivity} \times 2C / \text{mol min}^{-1}}{\Sigma \text{ productivities}} \right) \times 100 \quad \text{Eq. S8}$$

Molar productivities obtained in mol min^{-1} could be normalised to the mass of catalysts used during the reaction (0.5 g) and expressed as $\text{mol kg}_{\text{cat}}^{-1} \text{ h}^{-1}$ according to equation S9 as shown for methanol.

$$\text{CH}_3\text{OH prod mol kg}_{\text{cat}}^{-1} \text{ h}^{-1} = \left(\frac{\text{CH}_3\text{OH productivity / mol min}^{-1}}{(\text{catalyst mass g / 1000})} \right) \times 60 \quad \text{Eq. S9}$$

The total CH_3OH productivity, considering that all hydrocarbon except for CO originate from CH_3OH was obtained by adding productivities by the number of carbons (nC) as shown in Eq. S10.

$$\text{CH}_3\text{OH}_{(\text{tot})} \text{ prod mol kg}_{\text{cat}}^{-1} \text{ h}^{-1} = \sum \text{prod.} \times nC \quad \text{Eq. S10}$$

Hydrocarbon selectivity based on MTH/DMTH were calculated by dividing the individual hydrocarbon productivity multiplied by the number of carbons in the molecule, divided by the total hydrocarbon productivity excluding CH_3OH and DME as shown for ethane in equation S11.

$$\text{CH}_3\text{CH}_3_{(\text{CH}_3\text{OH})} \text{ sel.} = \left(\frac{\text{CH}_3\text{CH}_3 \text{ productivity} \times 2C / \text{mol min}^{-1}}{\sum \text{prod. (mol min}^{-1}) \times nC} \right) \quad \text{Eq. S11}$$

2.2 CO_2 hydrogenation over PdZn/TiO_2

Catalytic data for the CO_2 hydrogenation to CH_3OH for 0.25 g of PdZn/TiO_2 catalyst (diluted with 0.25 g of SiC) is shown in Table S2. Increasing the reaction temperature from 240 to 360 $^{\circ}\text{C}$ resulted in an increase in the CO_2 conversion from 6.8 to 31.2 %. However, in agreement with reaction thermodynamics, CH_3OH selectivity decreases with increasing the reaction temperature, whilst CO formation *via* RWGS is favoured.² As observed by the increase in CH_3OH productivity with temperature up to 518 $\text{mmol}_{\text{CH}_3\text{OH}} \text{ kg}_{\text{cat}}^{-1} \text{ h}^{-1}$ at 300 $^{\circ}\text{C}$, CH_3OH production below 300 $^{\circ}\text{C}$ occurred in the kinetic regime. At 300 $^{\circ}\text{C}$, CH_3OH yield (1.27 %) approaches theoretical equilibrium (1.45 %).² However, above 300 $^{\circ}\text{C}$ CH_3OH production is limited by thermodynamic equilibrium, as observed by the drop in CH_3OH productivity. DME and CH_4 selectivity remained below 1 % in the temperature range studied.

Table S2. Catalytic data for the CO₂ hydrogenation (20 bar, CO₂/H₂/N₂ = 1/3/1, 30 ml·min⁻¹) on 0.25 g PdZn/TiO₂ + 0.25 g SiC. Reaction was equilibrated for 6 hours at each temperature. Selectivity are expressed as %, while productivities are in mmol kg_{cat} h⁻¹.

Temp / °C	X CO ₂ / %	CH ₃ OH sel. / prod.	DME sel. / prod.	CO sel. / prod.	CH ₄ sel. / prod.
240	6.8	24.3 / 340	0.8 / 6	74.6 / 1043	0.3 / 5
270	13.1	15.4 / 486	1.0 / 17	82.6 / 2654	0.5 / 15
300	19.4	9.1 / 518	0.7 / 19	89.6 / 5056	0.6 / 34
320	24.0	4.7 / 333	0.3 / 9	94.4 / 6668	0.6 / 43
340	28.1	2.5 / 207	0.1 / 3	96.7 / 7903	0.7 / 56
360	31.2	1.3 / 115	0.0 / 0	97.9 / 8858	0.8 / 76

2.3 CO₂ hydrogenation over PdZn/TiO₂-ZSM-5 hybrid catalysts

PdZn/TiO₂-ZSM-5 hybrid catalysts, with Si/Al ratios of 80, 50 and 23 were employed to produce hydrocarbons *via* CO₂ hydrogenation, CH₃OH dehydration to DME and consecutive MTH-DMTH. At the studied temperatures range, no significant differences in the CO₂ conversion or CO productivity were observed for PdZn/TiO₂-ZSM-5 hybrid catalysts compared to PdZn/TiO₂. Suggesting that CO was produced *via* RGWS over PdZn/TiO₂ catalyst, and that the activity of the CH₃OH synthesis catalyst was not altered by the proximity of solid acid ZSM-5 zeolites. To confirm that ZSM-5 is not active to convert CO₂ to either CO or CH₃OH a blank reaction up to 270 °C test was performed on ZSM-5 (23:1). As observed in Table S3, no CO₂ conversion was observed at 240 °C, whilst marginal CO₂ conversion to CO was detected at 270 °C.

Table S3. CO₂ hydrogenation (20 bar, CO₂/H₂/N₂ = 1/3/1, 30 ml·min⁻¹) for ZSM-5 (Si/Al = 23/1) (0.5 g, 425 - 625 µm pellet).

Temp / °C	X CO ₂ / %	CO sel. / %	CH ₃ OH sel. / %	CH ₄ sel. / %
240	n/d	n/d	n/d	n/d
270	0.2	100	0	0

DME was the main oxygenate product on PdZn/TiO₂-ZSM-5 hybrid catalysts, indicating that CH₃OH was being effectively dehydrated at solid acid ZSM-5 zeolites. A part of DME, other hydrocarbons product of MTH and DMTH were detected (Table S4). Higher hydrocarbons productivity was observed with increasing the aluminium concentration on ZSM-5 zeolites.

Table S4. Hydrocarbons and oxygenates productivities (mmol kg_{cat} h⁻¹) from CO₂/H₂/N₂ = 1/3/1 feed over PdZn/TiO₂-ZSM-5 hybrid catalysts (20 bar, 30 ml min⁻¹, 0.5 g_{cat}, 2240-360 °C). The subscript (sat) and = stand for saturated and olefin products: C_{2(sat)}, C_{3(sat)}, and C_{4(sat)} correspond to ethane, propane and n-butane respectively; c/t C₄ =, c/t C₅ = and n C₅ = correspond to cis/trans-butene, 2-cis/trans-pentene and 1-pentene respectively.

Cat.	Temp / °C	CH ₄	C ₂ (sat)	C ₃ (sat)	CH ₃ OH	DME	C ₄ (sat)	c/t C ₄ =	n C ₅ =	c/t C ₅ =	C _(tot)
PdZn/TiO ₂	240	5	-	-	340	6	-	-	-	-	356
	270	15	-	-	486	17	-	-	-	-	535
	300	34	-	-	518	19	-	-	-	-	589
	320	43	-	-	333	9	-	-	-	-	394
	340	46	-	-	207	3	-	-	-	-	270
	360	76	-	-	115	-	-	-	-	-	191
+ZSM5(80:1)	240	11	-	-	61	306	-	-	-	-	691
	270	39	3	-	80	415	-	-	-	-	954
	300	79	36	47	106	110	13	6	10	1	744
	320	95	48	55	104	40	18	8	13	2	714
	340	115	51	21	100	18	5	4	6	1	484
	360	138	53	2	93	8	0.4	-	0.1	-	362
+ZSM5(50:1)	240	12	0.4	-	73	316	-	-	-	-	719
	270	39	5	-	117	420	-	-	-	-	1006
	300	85	38	14	129	117	7	2	3	-	616
	320	95	51	20	117	71	8	2	4	0.2	576
	340	104	62	24	114	36	9	3	6	0.6	566
	360	125	65	7	95	15	2	0.6	1	-	416
+ZSM5(23:1)	240	20	1	-	79	213	-	-	-	-	526
	270	69	26	17	27	288	5	2	4	-	824
	300	139	94	58	32	94	21	7	13	1	904
	320	174	93	45	44	41	15	6	9	1	753
	340	219	86	22	28	16	4	2	3	0.5	559
	360	249	75	12	49	6	1	1	0.6	-	508

Hydrocarbons selectivity was calculated considering that synthesised hydrocarbons originate from MTH and DMTH (Table S5). Note that CH₄ is also produced as by-product from CH₃OH decomposition over TiO₂, since CH₄ was detected for PdZn/TiO₂, and hence real selectivity towards CH₄ through MTH and DMTH is lower than reported values. Higher aluminium concentration on the ZSM-5 zeolites resulted in an increase in the selectivity towards higher hydrocarbons.

Table S5. Hydrocarbons selectivity based on MTO and DMTO over PdZn/TiO₂-ZSM-5 hybrid catalysts (20 bar, CO₂/H₂/N₂ = 1/3/1, 30 ml min⁻¹). C_{2(sat)}, C_{3(sat)}, and C_{4(sat)} correspond to ethane, propane and n-butane respectively; c/t C₄ =, c/t C₅ = and n C₅ = correspond to cis/trans-butene, 2-cis/trans-pentene and 1-pentene respectively.

PdZn/TiO ₂	Temp. / °C	CH ₄ sel. / %	C _{2(sat)} sel. / %	C _{3(sat)} sel. / %	C _{4(sat)} sel. / %	c/t C ₄ = sel. / %	n C ₅ = sel. / %	c/t C ₅ = sel. / %
+ZSM-5 (80:1)	240	100	0	-	-	-	-	-
	270	87	13	-	-	-	-	-
	300	24	19	36	15	7	-	-
	320	21	21	37	14	7	-	-
	340	36	32	21	7	4	-	-
	360	55	42	2	1	-	-	-
+ZSM-5 (50:1)	240	88	12	-	-	-	-	-
	270	79	21	-	-	-	-	-
	300	37	31	14	11	2	7	-
	320	31	30	20	12	3	4	-
	340	28	33	19	10	3	8	0.7
	360	42	44	7	3	1	3	-
+ZSM-5 (23:1)	240	89	11	-	-	-	-	-
	270	32	24	23	9	4	9	-

300	20	27	26	12	4	10	0.7
320	28	30	22	9	4	7	0.9
340	44	35	13	3	2	3	0.5
360	56	34	8	1	1	1	-

3. *PdZn/TiO₂ spent reaction characterisation*

3.1 *EXAFS fitting parameters for PdZn/TiO₂ before and after CO₂ hydrogenation*

X-ray absorption spectroscopy (XAS) at Pd K edge was employed to study bulk structural and electronic changes on the PdZn alloy phase after reaction (20 bar, CO₂/N₂/H₂ = 1/1/3, 30 ml·min⁻¹, 240-360 °C, 6 h dwell, 36 h reaction). Measurements were obtained at B18 Diamond light source at Harwell, Oxford. 100 mg of PdZn/TiO₂ after reduction and after reaction were pelleted into an 8 mm diameter disk without diluent. Samples were measured in transmission, a Pd foil was analysed simultaneously and used as a reference. Three scans per sample were averaged before EXAFS analysis, Athena and Artemis software package were used for data interpretation.³ First and second coordination shell Pd paths were fitted at all *k*-weighted χ data using a *k* space window of 3-12 and a *R* window of 1.15-3.5.

76148 and 09157 crystallographic information files (cif) obtained from the Inorganic Crystal Structure Database (ICSD) were used as references to obtain the respective Pd and PdO crystallographic structures. No suitable cif files of PdZn were obtained to calculate Pd scattering paths. Nevertheless, a suitable PdZn structure was obtained by modifying an isostructural AuCu⁴ cif file(reference 180144 from ICSD). Restrictions and parameters employed for EXAFS fitting of the Pd K-edge using Artemis are described in Table S6.

Table S6. Parameters defined and restrictions employed to obtain the coordination number and bond distances for PdZn/TiO₂ catalyst after reduction (5% H₂, 400 °C, 5 °C min⁻¹, 1 h) and after reaction (20 bar, CO₂/H₂/N₂ = 1/3/1, 240-360 °C, 36 h) using Artemis software. *Pd_(a) and Pd_(met) corresponds to Pd within the alloy and Pd within metallic palladium respectively. The term “amp” corresponds to the S₀² obtained from fitting the palladium foil and was fixed at 0.85.

Path	N / S ₀ ²	ΔR	σ ²	restrictions
Pd _(a) -Zn	1 / amp*CN _{Zn}	ΔR _{Zn}	σ ² _{Zn}	CN _{Zn} =14-CN _{Pd1} -CN _{Pd2}
Pd _(a) -Zn-Pd ₁	1 / amp*CN _{Pd1}	ΔR _{Pd1}	σ ² _{Pd1}	CN _{Pd1} =CN _{Pd2} *2
Pd _(a) -Zn-Pd ₂	1 / amp*CN _{Pd2}	ΔR _{Pd2}	σ ² _{Pd2}	
Pd _(met) -Pd _(met)	12 / 0.85	ΔR _{Pd(met)}	σ ² _{Pd(met)}	

3.2 XRD patterns for PdZn/TiO₂ before and after CO₂ hydrogenation

EXAFS analysis of PdZn/TiO₂ after reduction (400 °C, 5% H₂/Ar, 5 °C·min⁻¹) and after reaction (20 bar, CO₂/N₂/H₂ = 1/1/3, 30 ml·min⁻¹, 240-360 °C, 6 h dwell, 36 h reaction) confirmed the stability of the catalytically active PdZn phase (Figure 5). No differences in the first coordination shell (bond distances or coordination number) were observed between catalysts. The presence of metallic Pd and PdZn was detected by EXAFS analysis. In accordance with the PdZn alloy formation mechanism, the formation of a PdZn layer is formed over a Pd nanoparticle *via* hydrogen spill over.^{5,6} The presence of PdZn and Pd after reduction was confirmed by XRD. No changes in peak intensity or broadening on (111) Pd or (111) and (200) PdZn reflection at 40.1°, 41.2° and 44.1° respectively were observed after reaction. The presence of ZnO was also observed at 31.7°, 34.4° and 36.3°. ZnO is formed from the 1:5 excess of Zn(acac)₂ to Pd(acac)₂ used for the synthesis of the PdZn/TiO₂ catalyst. No appreciable differences were observed after reaction on the ZnO reflection. However, a clear intensity rises on rutile TiO₂ and anatase TiO₂ reflections was observed (Figure S2), which could suggest TiO₂ particles agglomeration.

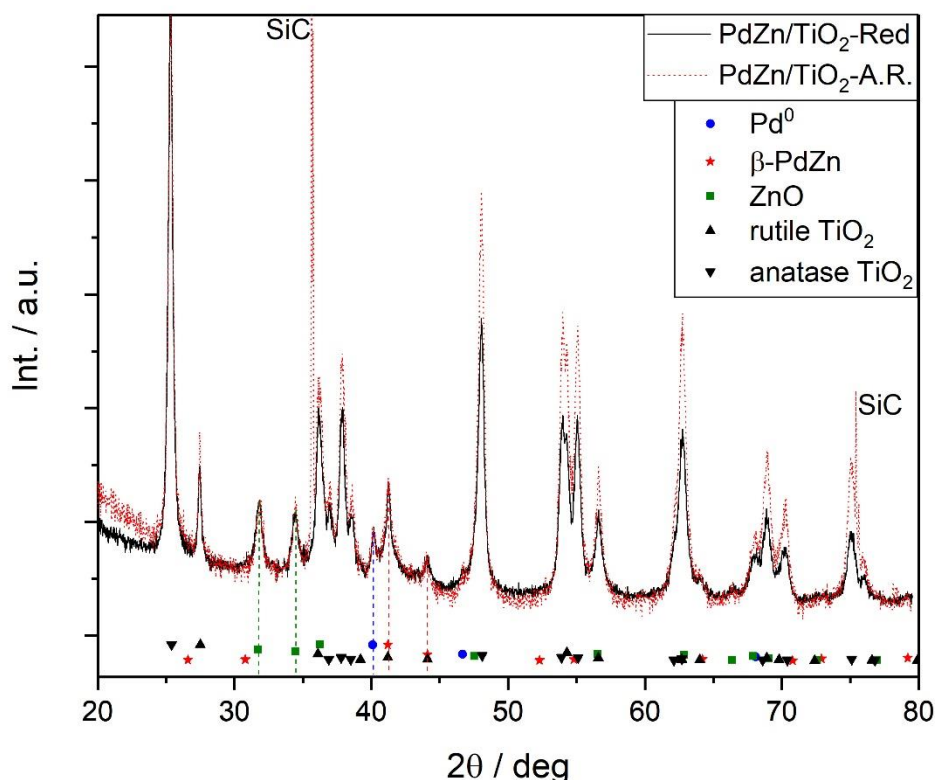


Figure S2. XRD patterns for PdZn/TiO₂ recorded after reduction (400 °C, 5 °C min⁻¹, 1 h) and after reaction (20 bar, CO₂/H₂/N₂ = 1/3/1, 240 - 360 °C, 36 h).

3.3 XPS characterisation for PdZn/TiO₂ before and after CO₂ hydrogenation

To monitor surface changes of the reduced PdZn/TiO₂ (400 °C, 5 °C min⁻¹, 1 h) catalyst during reaction (20 bar, CO₂/H₂/N₂ = 1/3/1, 240 - 360 °C, 36 h) Pd(3d) and Zn(LM₂) orbitals were analysed by XPS. Due to the low sensitivity towards chemical changes of Zn(2p), Pd(3d) and Zn(LM₂) peaks were calibrated against the Zn(2p) orbital at 1020 eV.⁷ The Pd(3d) for PdZn/TiO₂ before and after reaction was centred at 335.6 eV, in between reported values for Pd⁸⁻¹⁰ and PdZn.^{4,10,11} Peak fitting using Finite-Lorentzian line shapes for Pd and PdZn (including satellites) and Gaussian line shapes for PdO peaks and its satellites with Shirley background¹² confirmed the presence of Pd, PdZn and PdO at 335.0, 335.9 and 337.2 eV respectively (Figure S3a). The Zn(LM₂) main peak for PdZn/TiO₂ prior and post reaction was centred 998 eV, a lower intensity satellite contribution was observed at 991 eV, indicating the presence of ZnO (Figure S3b).

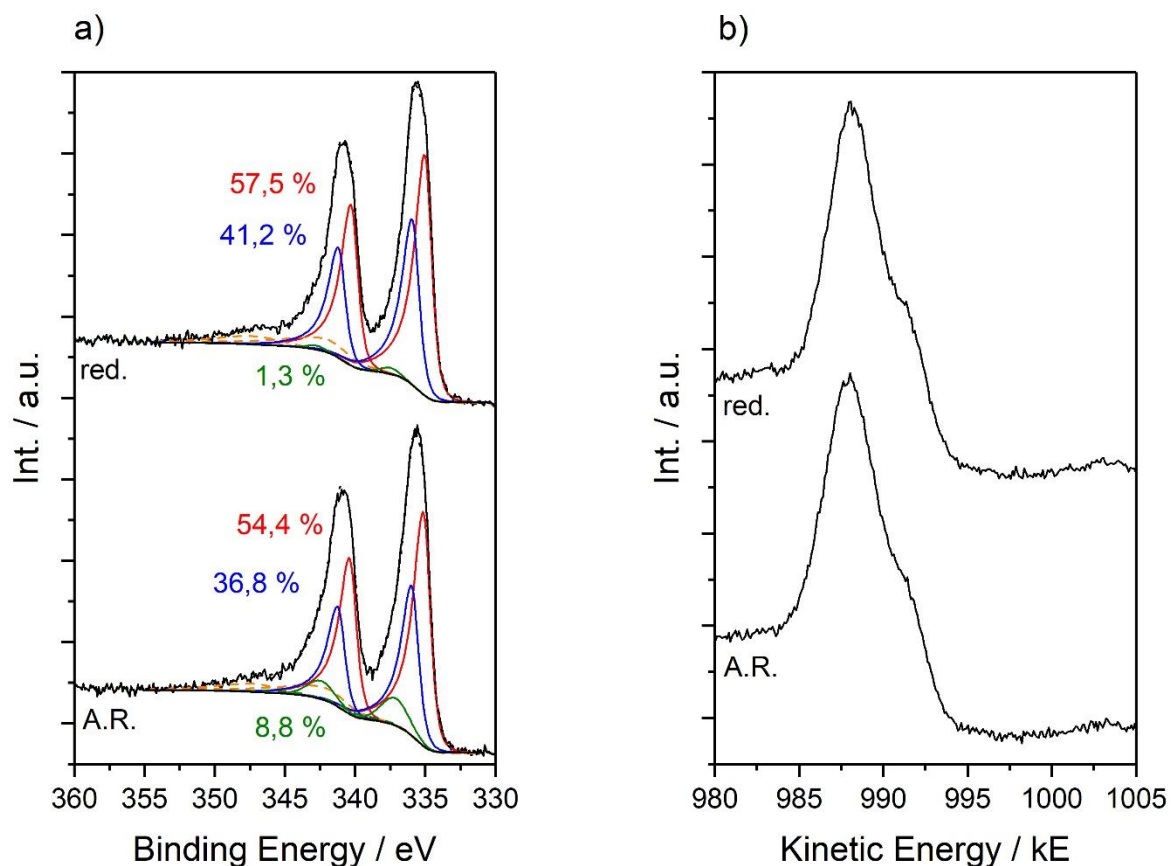


Figure S3. a) Pd(3d) and b) Zn(LM₂) XPS analysis of PdZn/TiO₂ catalyst after reduction (red.) in 5% H₂/Ar (400 °C, 5 °C·min⁻¹, 1 h) and after CO₂ hydrogenation (A.R.) (240-360 °C, 36 h, 20 bar, CO₂/N₂/H₂ = 1/1/3, 30 ml·min⁻¹). On the Pd(3d) peak, metallic Pd, PdZn and PdO are represented in red, blue and green respectively, Pd and PdZn satellites contributions are represented by an orange dashed line, peak fitting is represented by a dotted line.

3.4 Coke deposition determination by TGA-MS over PdZn/TiO₂-ZSM-5 hybrid catalysts during CO₂ hydrogenation

The main deactivation mechanism of zeolites during the conversion of methanol to olefins (MTO) or hydrocarbons (MTH) processes is by coke deposition. Coke can deposit over acid sites, block internal zeolite cavities, and block the zeolite surface limiting CH₃OH diffusion.¹³ To determine the extent of coke deposition over PdZn/TiO₂-ZSM-5 hybrid catalysts during reaction (240-360 °C, 36 h, 20 bar, CO₂/N₂/H₂ = 1/1/3, 30 ml·min⁻¹) fresh and spent samples were analysed by TGA-MS (Figure S4). A steady mass loss was observed under 200 °C which can be attributed to physisorbed and chemisorbed water. No clear mass loss above 200 °C was detected for PdZn/TiO₂-ZSM-5(23) catalyst (Figure S4a). However, a clear 1wt. % mass loss at c.a. 200 °C was observed for PdZn/TiO₂-ZSM-5(50 and 80) compared to the fresh samples (Figure S4b and S4c, respectively). This loss in weight was accompanied by the release of CO₂ (figure S4e and Figure S4f), the detection of CO₂ at this temperature can be

assigned to coke formation with a high content of oxygen. No coke formation in the form of aromatics was detected at higher temperature.¹⁴

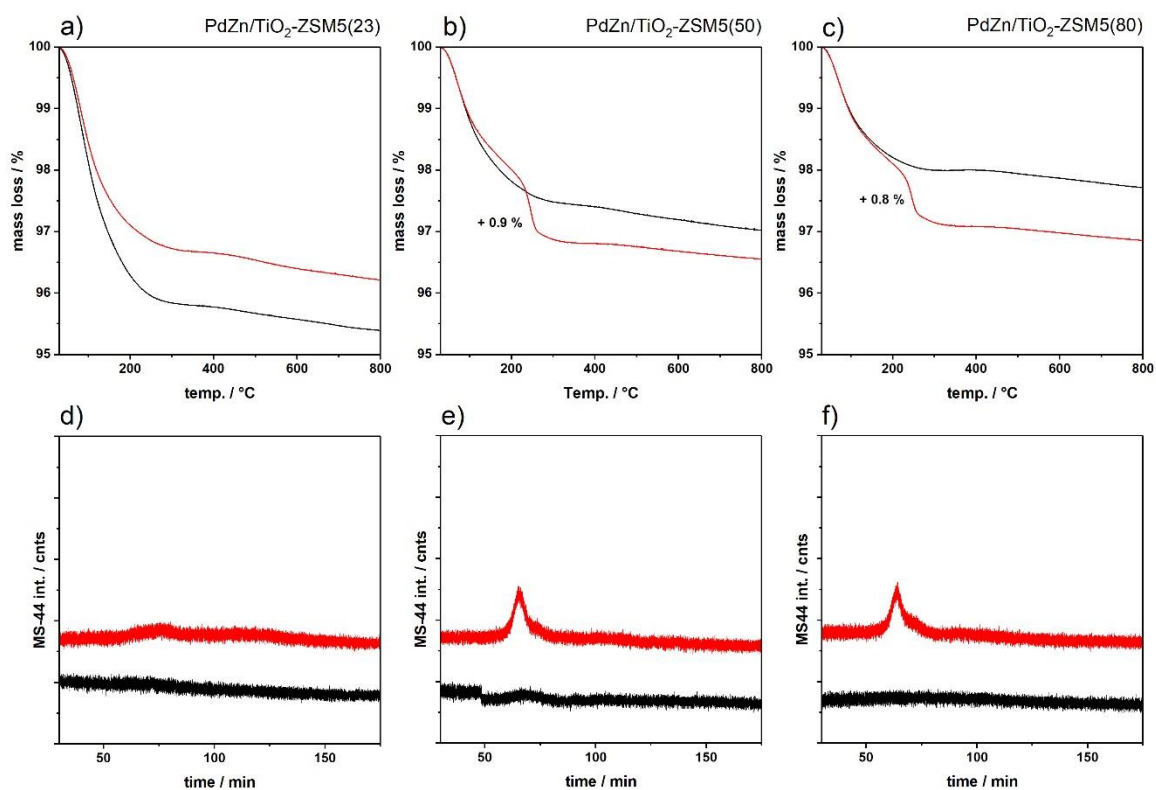


Figure S4. TGA analysis on PdZn/TiO₂-ZSM-5 hybrid catalysts with a Si/Al ratio of a) 23, b) 50 and c) 80 with its respective d), e) and f) mass spectra below. Black and red lines corresponds to fresh and spent (240-360 °C, 36 h, 20 bar, CO₂/N₂/H₂ = 1/1/3, 30 ml·min⁻¹) samples, respectively.

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