

Supporting Information

Comparative Life Cycle Assessment of Electrochemical Upgrading of CO₂ to Fuels and Feedstocks

Shariful Kibria Nabil, Sean McCoy, Md Golam Kibria*

Department of Chemical and Petroleum Engineering, University of Calgary, 2500 University Drive, NW
Calgary, Alberta, Canada, T2N 1N4

*Correspondance email: md.kibria@ucalgary.ca

Thermochemical CO₂ Utilization Process

For thermochemical processes, hydrogen is considered to be supplied by water electrolysis (50 kWh/kg H₂).¹

Table S1: Thermochemical processes for the CO₂-derived products

Product	System Description	References
Syngas (CO+H ₂)	Process 1: Reverse water-gas shift reaction (rWGS) $\text{CO}_2 + \text{H}_2 \rightarrow \text{CO} + \text{H}_2\text{O}$, at 200-600°C, 30 bar Process 2: Dry reforming of methane (DRM) $\text{CO}_2 + \text{CH}_4 \rightarrow 2\text{CO} + 2\text{H}_2$, at 750°C,	2,3
Formic Acid	Process 1: Equimolar hydrogenation: at 140°C, 30 bar $\text{CO}_2 + \text{H}_2 \rightarrow \text{HCOOH}$ Process 2: rWGS followed by carbonylation $\text{CO}_2 + \text{H}_2 \rightarrow \text{CO} + \text{H}_2\text{O}$, : at 650-1100°C, 30 bar $\text{CO} \rightarrow \text{HCOOH}$	4
Methane	Sabatier reaction: at 280-300°C, 5-8 bar $\text{CO}_2 + 4\text{H}_2 \rightarrow \text{CH}_4 + 2\text{H}_2\text{O}$	5,6
Methanol	Process 1: CO ₂ hydrogenation $\text{CO}_2 + 3\text{H}_2 \rightarrow \text{CH}_3\text{OH} + \text{H}_2\text{O}$, at 210-250°C, 50-75 bar Process 2: CO ₂ -based Syngas route $\text{CO}_2 + \text{H}_2 \rightarrow \text{CO} + \text{H}_2\text{O}$, at 200-600°C, 30 bar $\text{CO} + 2\text{H}_2 \rightarrow \text{CH}_3\text{OH}$	4,7,8
Ethylene	CO ₂ hydrogenation: at 400°C, 15 bar $2\text{CO}_2 + 6\text{H}_2 \rightarrow \text{C}_2\text{H}_4 + \text{H}_2\text{O}$	9

Table S2: Incumbent/commercial production processes for the eight products of interest

Product	System Description	References
Syngas (CO+H ₂)	<p>Process 1: Steam-methane-reforming (SMR): at 850-900 °C, 10-30 bar, with nickel as catalyst</p> $\text{CH}_4 + \text{H}_2\text{O} \rightarrow \text{CO} + 3\text{H}_2$ <p>Process 2: Gasification of coal: 600-1900 °C, 80 atm</p> $3\text{C} + \text{O}_2 + \text{H}_2\text{O} \rightarrow 3\text{CO} + \text{H}_2$	10,11
Formic Acid	<p>Step 1 – CO production via SMR</p> <p>Step 1 – methanol carbonylation: at 80°C, 45 bar</p> $\text{CH}_3\text{OH} + \text{CO} \rightarrow \text{HCOOCH}_3$ <p>Step 2 – hydrolysis of methyl formate</p> $\text{HCOOCH}_3 + \text{H}_2\text{O} \rightarrow \text{CH}_3\text{OH} + \text{HCOOH}$	12
Methane	<p>Process 1: Natural gas (75-99 vol% methane) as fossil equivalent</p> <p>Process 2: Sabatier reaction: at 300-400°C, 5-8 bar, with nickel as catalyst</p> $\text{CO}_2 + 4\text{H}_2 \rightarrow \text{CH}_4 + 2\text{H}_2\text{O}$	13,14
Methanol	<p>Step 1 – syngas production via SMR</p> <p>Step 2 – syngas conversion: at 200-300 °C, 50-100 bar</p> $\text{CO} + 2\text{H}_2 \rightarrow \text{CH}_3\text{OH}$	15
Ethylene	<p>Pyrolysis of hydrocarbons: at 600-900°C</p> $\text{C}_a\text{H}_b \rightarrow \text{C}_2\text{H}_4 + \text{H}_2 + \text{C}_x\text{H}_y$	16
Ethanol	<p>Process 1: Fermentation of Corn:</p> $\text{C}_6\text{H}_{12}\text{O}_6 \rightarrow 2\text{C}_2\text{H}_5\text{OH} + 2\text{CO}_2$ <p>Process 2: Hydration of ethylene: at 260-315°C, 55-75 bar, with phosphoric acid (V) as catalyst</p> $\text{C}_2\text{H}_4 + \text{H}_2\text{O} \rightarrow \text{C}_2\text{H}_5\text{OH}$	17,18
Acetic Acid	<p>Carbonylation of methanol with carbon monoxide: at 190°C, 9 atm, with iridium/ruthenium as catalyst</p> $\text{CH}_3\text{OH} + \text{CO} \rightarrow \text{CH}_3\text{COOH}$	19
n-Propanol	<p>Hydroformylation of ethylene: at 80-150°C, 12-50 bar, with rhodium as catalyst</p> $\text{C}_2\text{H}_4 + \text{CO} + 2\text{H}_2 \rightarrow \text{C}_3\text{H}_7\text{OH}$	20

Table S3: Gibb's free energy of formation (ΔG_f^0)^{21,22}

Component	Molecular Formula	ΔG^0_f (kJ / mol)
Water	H ₂ O	-237.1
Oxygen	O ₂	0
Carbon dioxide	CO ₂	-394.4
Carbon monoxide	CO	-137.2
Formic acid	HCOOH	-361.4
Methane	CH ₄	-50.5
Methanol	CH ₃ OH	-166.6
Ethylene	C ₂ H ₄	68.4
Ethanol	C ₂ H ₅ OH	-174.8
Acetic acid	CH ₃ COOH	-389.9
n-Propanol	C ₃ H ₇ OH	-171.3

All in standard conditions (1 bar, 298K)

Table S4: Higher heating value of products^{23,24}

Products	Higher Hating Value (MJ/kg)
Hydrogen	141.88
Carbon monoxide	10.1
Formic acid	5.52
Methane	55.6
Methanol	22.88
Ethylene	50.3
Ethanol	29.84
Acetic Acid	14.55
n-propanol	33.62

Table S5: PSA separation energy for gaseous products (per kg product)

Products		Single Pass Conversion (%)	CO ₂ Conversion (%) ²⁵	Actual CO ₂ Required (kg)	HCO ₃ ⁻ Formation (%) ²⁵	HCO ₃ ⁻ Formation(kg)	Cathodic Gas Volume and PSA Energy								Anodic Gas Volume and PSA Energy					CO ₂ to CO Separation (kWh/kg)	Overall PSA Energy (kWh)		
							Outlet CO ₂ /CO (kg)	Outlet CO ₂ /CO (m ₃)	Outlet Product (kg)	Outlet Product (m ₃)	Outlet H ₂ (kg)	Outlet H ₂ (m ₃)	Total Volume (m ₃)	1 st PSA Energy (kWh)	2 nd PSA Energy (kWh)	Outlet CO ₂ /CO (kg)	Outlet CO ₂ /CO (m ₃)	Outlet O ₂ (kg)	Outlet O ₂ (m ₃)			Total Volume (m ₃)	3 rd PSA Energy (kWh)
Formic Acid	One-step	50	50	1.91	50	0.96	0.96	0.48	1	-	0.005	0.05	0.54	0.13	-	0.96	0.48	0.35	0.24	0.73	0.18	-	0.32
Syngas (CO+H ₂)	One-step	50	100 [#]	3.14	0	-	1.57	1.37	1	0.87	0.008	0.09	2.34	0.59	0.37	-	-	0.57	0.39	0.39	-	-	0.95
Methane	One-step	50	20	13.7	80	10.96	2.74	1.38	1	1.52	0.06	0.62	3.52	0.88	0.50	10.96	5.54	3.99	2.79	8.33	2.08	-	3.46
	Two-step	50	-	2.74	-	-	1.75	1.54	1	1.52	0.04	0.47	3.52	0.88	0.50	-	-	2.99	2.09	2.09	-	1.67	3.05
Methanol	One-step	50	25	5.48	75	4.11	1.37	0.69	1	-	0.02	0.23	0.93	0.23	-	4.11	2.08	1.50	1.05	3.12	0.78	-	1.01
	Two-step	50	-	1.37	-	-	0.874	0.76	1	-	0.01	0.16	0.92	0.23	-	-	-	0.99	0.69	0.69	-	0.83	1.06
Ethylene	One-step	50	25	12.52	75	9.42	3.14	1.59	1	0.85	0.05	0.53	2.97	0.74	0.53	9.42	4.76	3.42	2.39	7.15	1.79	-	3.06
	Two-step	50	-	3.14	-	-	2	1.75	1	0.85	0.03	0.36	2.96	0.74	0.53	-	-	2.28	1.59	1.60	-	1.90	3.17
Ethanol	One-step	50	25	7.64	75	5.73	1.91	0.96	1	-	0.03	0.32	1.29	0.32	-	5.73	2.89	2.08	1.46	4.35	1.09	-	1.41
	Two-step	50	-	1.92	-	-	1.22	1.07	1	-	0.02	0.21	1.28	0.32	-	-	-	1.39	0.97	0.97	-	1.16	1.48
Acetic Acid	One-step	50	33.5	4.45	67.5	2.98	1.47	0.74	1	-	0.01	0.17	0.91	0.23	-	2.98	1.51	1.07	0.75	2.25	0.56	-	0.79
	Two-step	50	-	1.46	-	-	0.93	0.82	1	-	0.01	0.08	0.89	0.22	-	-	-	0.53	0.37	0.37	-	0.89	1.11
n-Propanol	One-step	50	25	8.76	75	6.57	2.19	1.11	1	-	0.03	0.37	1.48	0.37	-	6.57	3.32	2.39	1.68	4.99	1.25	-	1.62
	Two-step	50	-	2.19	-	-	1.4	1.23	1	-	0.02	0.24	1.48	0.37	-	-	-	1.59	1.12	1.12	-	1.33	1.70

*Assumed basis for PSA separation – **0.25 kWh/Nm³** for all gaseous products²⁶

*Density of gases: H₂ = 0.089 kg/m³, CO = 1.14 kg/m³, CO₂ = 1.98 kg/m³, O₂ = 1.429 kg/m³, CH₄ = 0.657 kg/m³, C₂H₄ = 1.18 kg/m³

*Outlet gas = CO₂ (one-step), CO (two-step)

*No HCO₃⁻ formation has been considered in two-step process

Based on solid-oxide electrolysis cell (SOEC) for CO₂→CO and considering no HCO₃⁻ formation

Table S6: Energy breakdown for electrochemical conversion (one-step vs two-step)

Products		Capture Energy (kWh/kg)*	Conversion Energy (kWh/kg)	Separation Energy (kWh/kg)	10% BoP (kWh / kg)	Total (kWh/kg)
Formic Acid	One-step	0.34	3.62	22.04	0.36	26.36
	Two-step		-	-	-	-
Syngas (CO+H ₂)	One-step	0.56	15.11 [#]	0.95	1.51	18.13
	Two-step		-	-	-	-
Methane	One-step	0.97	36.54	3.46	3.65	44.63
	Two-step		25.00	3.04	2.50	31.51
Methanol	One-step	0.48	14.57	27.44	1.46	43.96
	Two-step		10.28	27.49	1.03	39.29
Ethylene	One-step	1.11	32.49	3.06	3.25	39.91
	Two-step		22.69	3.17	2.27	29.24
Ethanol	One-step	0.68	19.74	17.26	1.97	39.65
	Two-step		13.78	17.33	1.38	33.17
Acetic Acid	One-step	0.52	10.04	25.31	1.00	36.87
	Two-step		7.05	25.63	0.71	33.90
n-Propanol	One-step	0.77	22.56	10.22	2.26	35.81
	Two-step		15.70	10.30	1.57	28.35

[#]CO is commercially available as syngas (CO+H₂). Functional unit has been taken as 1 kg CO+0.216 kg H₂ for consistent comparison with incumbent and thermochemical processes.²⁷ Thus, conversion energy of CO contains energy for 1 kg CO and 0.216 kg H₂ from water electrolysis (50 kWh/kg H₂²⁸).

*Capture energy is calculated based on CO₂ requirement per kg product, average capture energy for a power plant (3vol% CO₂) = **0.354 kWh/kg CO₂**²⁹

*Assumed basis for PSA separation – **0.25 kWh/Nm³** for all gaseous products²⁶

* 95% energy conversion efficiency (thermal to electrical) for distillation have been assumed.³⁰

Table S7: Global warming impact (GWI) for eight electrochemical CO₂ reduction products

CO ₂ derived products via one or two step electrochemical conversion routes		Capture emissions* (kg CO ₂ e/kg product)	Capture emissions# (kg CO ₂ e/kg product)	Carbon credit for H ₂ (kg CO ₂ e/kg product)	Conversion emissions (kg CO ₂ e/kg product)	Separation emissions (kg CO ₂ e/kg product)	Emissions from BOP (kg CO ₂ e/kg product)	Net GWI* (kg CO ₂ e/kg product)	Net GWI# (kg CO ₂ e/kg product)
Formic acid	One-step	-0.76	-0.48	-0.04	0.62	3.74	0.06	3.62	3.91
Syngas (CO+H ₂)	One-step	-1.25	-0.78	-0.07	2.57	0.16	0.27	1.66	2.13
Methane	One-step	-2.19	-1.37	-0.47	6.21	0.59	0.62	4.76	5.58
	Two-step			-0.35	4.25	0.52	0.43	2.65	3.47
Methanol	One-step	-1.09	-0.69	-0.17	2.48	4.66	0.25	6.11	6.53
	Two-step			-0.12	1.75	4.67	0.17	5.38	5.79
Ethylene	One-step	-2.51	-1.57	-0.40	5.52	0.52	0.55	3.68	4.63
	Two-step			-0.27	3.86	0.53	0.39	2.00	2.94
Ethanol	One-step	-1.53	-0.96	-0.25	3.36	2.93	0.34	4.85	5.42
	Two-step			-0.16	2.34	2.95	0.23	3.84	4.41
Acetic acid	One-step	-1.18	-0.74	-0.13	1.71	4.30	0.17	4.87	5.31
	Two-step			-0.06	1.19	4.36	0.12	4.44	4.88
n-Propanol	One-step	-1.75	-1.1	-0.28	3.84	1.74	0.38	3.92	4.58
	Two-step			-0.19	2.67	1.75	0.27	2.75	3.40

EEF = 0.17 kg CO₂e/kWh (see details in Table S6)

*Assumed footprint for carbon feedstock is -0.8 kg CO₂e/kg CO₂ capture³¹

Assumed footprint for carbon feedstock is -0.5 kg CO₂e/kg CO₂ capture³¹

Electricity emission factor, EEF has been taken as **0.17 kg CO₂e/kWh** (representing average carbon intensity for present-day electricity generation in Canada).

Table S8: EEF based on percentage calculation for renewable share for Canadian electricity generation³²

Renewable Share	EEF (kg CO₂e/kWh)
50%	0.17
66%	0.12
80%	0.07
90%	0.035

GWI of O₂, H₂ and H₂O (One-step Methanol as Reference)

a) For O₂:³³

Based on cryogenic super critical air separation,

Specific energy demand for O₂ supply = 200 kWh/tonne O₂

$$\text{Overall CO}_2 \text{ emission} = 0.17 \frac{\text{kg}}{\text{kWh}} * 200 \frac{\text{kWh}}{\text{t O}_2} * \frac{1 \text{ t}}{1000 \text{ kg}} = \mathbf{0.034 \text{ kg/kg O}_2}$$

For methanol, 1.66 kg O₂ is produced per kg methanol.

$$\text{Thus, environmental burden from O}_2 \text{ production} = \frac{0.034 \text{ kg CO}_2\text{e}}{\text{kg O}_2} * \frac{1.66 \text{ kg O}_2}{\text{kg methanol}} = \mathbf{0.06 \text{ kg CO}_2\text{e/kg methanol}}$$

b) For H₂:¹

H₂ supply has been considered by polymer electrolyte membrane-based water electrolysis.

$$\text{GWI of H}_2 \text{ via water electrolysis} = 0.17 \frac{\text{kg}}{\text{kWh}} * 50 \frac{\text{kWh}}{\text{kg H}_2} = \mathbf{8.50 \text{ kg CO}_2\text{e/kg H}_2}$$

For methanol, 0.02 kg H₂ is produced (10% selectivity) per kg methanol.

$$\text{Thus, environmental burden from H}_2 \text{ production} = \frac{8.5 \text{ kg CO}_2\text{e}}{\text{kg H}_2} * \frac{0.02 \text{ kg H}_2}{\text{kg methanol}} = \mathbf{0.17 \text{ kg CO}_2\text{e/kg methanol}}$$

c) For H₂O:³⁴

Underground water pumping energy = 0.45 kWh/m³

Average treatment energy before supply = 0.327 kWh/m³

$$\text{Total energy} = 0.78 \text{ kWh/m}^3 = (0.78/1000) = \frac{0.78 \text{ kWh}}{\text{m}^3} * \frac{\text{m}^3}{1000 \text{ kg}} = 7.8 \times 10^{-4} \text{ kWh/kg}$$

EEF = 0.17 kg CO₂e/kWh

$$\text{GWI for water treatment and supply} = \frac{0.00078 \text{ kWh}}{\text{kg}} * \frac{0.17 \text{ kg CO}_2\text{e}}{\text{kWh}} = \mathbf{1.326 \times 10^{-4} \text{ kg CO}_2\text{e/kg H}_2\text{O}}$$

For methanol, 0.94 kg water is required per kg methanol.

$$\text{Thus, GWI} = \frac{0.000133 \text{ kg CO}_2\text{e}}{\text{kg H}_2\text{O}} * \frac{0.94 \text{ kg H}_2\text{O}}{\text{kg methanol}} = \mathbf{0.00012 \text{ kg CO}_2\text{e/kg methanol}}$$

Table S9: Comparison between electrochemical and thermochemical CO₂ conversion as compared to incumbent routes

Products	Incumbent		Electrochemical CO ₂ conversion (with -0.8 kg CO ₂ e/kg CO ₂ as capture footprint)		Thermochemical CO ₂ conversion
	Industrial Production Process	GWI (kg CO ₂ e/kg)	One-step, GWI (kg CO ₂ e/kg)	Two-step GWI (kg CO ₂ e/kg)	GWI (kg CO ₂ e/kg)#
Formic acid	Methyl formate hydrolysis	1.1-1.5 ²⁷	3.62	-	0.54-1.58 ²⁷
Syngas (CO+ H₂)	- Steam-methane-reforming - Coal gasification	1.74 ²⁷	1.66	-	1.92-2.51 ²⁷
Methanol	Reforming of syngas	0.68-1.08 ²⁷	6.11	5.38	1.21-1.44 ²⁷
Methane	- Natural gas (75-99 vol% methane) - Sabatier reaction	0.66 ²⁸ 0.46 ³⁵ 0.5 ²⁷	4.76	2.65	3.0-5.0 ²⁷
Ethylene	Steam cracking of naptha	1.9 ^{36,77}	3.68	2.00	3.30 ³⁷
Ethanol	- Corn fermentation - Ethylene hydration	0.00 ³⁸ -0.5 ^{39,40}	4.85	3.84	N/A
Acetic Acid	Methanol carbonylation with CO	1.75 ³⁶	4.87	4.44	N/A
n-Propanol	Hydroformylation of ethylene	4.44 ^{***}	3.92	2.75	N/A

*EEF = 0.17 kg CO₂e/kWh (see details in Table S6)

***ecoinvent V3.5 (IPCC GWP100a), #We assumed similar environmental impact (GWI) of steam-methane-reforming and water electrolysis for H₂ supply at 0.17 kg CO₂e/kWh.

Calculation for EE (with One-step Methanol as Reference)

Assuming 1000 kg/day basis of methanol,

Calculated thermodynamic voltage = 1.21 V

Assumed anodic overpotential = 0.8 V

Assumed cathodic overpotential = 0.6 V

Total voltage = 1.21 + 0.6 + 0.8 V = 2.61 V

Assumed faradaic efficiency = 90%

Number of electrons per mole = 6

Molar mass = 32.04

$$\text{Calculated current} = \frac{1000 \text{ kg} \cdot 1 \text{ day} \cdot 1000 \text{ g} \cdot \text{mol}}{\text{day} \cdot 86400 \text{ s} \cdot 1 \text{ kg} \cdot 32.04 \text{ g}} * 6e^- * \frac{96485 \text{ C}}{\text{mol}} = 209124.45 \text{ A} = 209.12 \text{ A/kg}$$

$$\text{Total current} = \frac{209.12 \text{ A}}{0.9} = 232.36 \text{ A}$$

$$\text{Electrochemical conversion energy} = 232.36 \text{ A} * 2.61 \text{ V} * 24 \text{ h} * \frac{1 \text{ kWh}}{1000 \text{ Wh}} = 14.55 \text{ kWh}$$

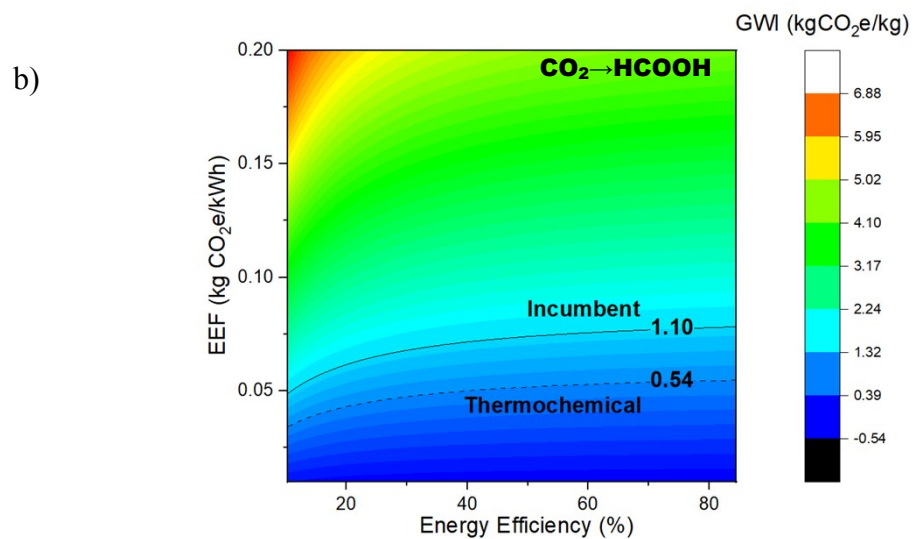
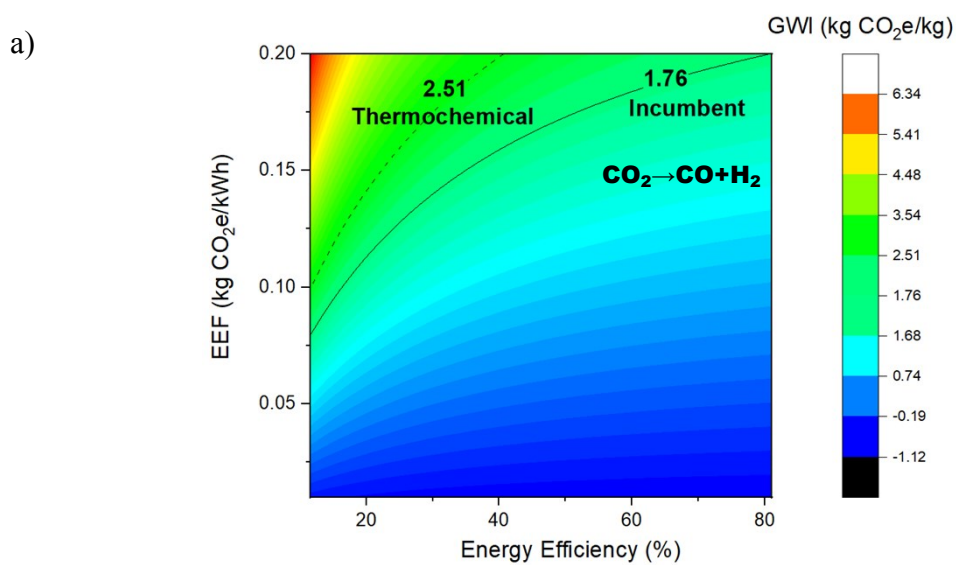
$$\text{Higher heating value} = 22.88 \text{ MJ} * \frac{.277 \text{ kWh}}{1 \text{ MJ}} = 6.36 \text{ kWh}$$

$$\text{Thus, energy efficiency} = \frac{6.36 \text{ kWh}}{14.55 \text{ kWh}} = 43.7\%$$

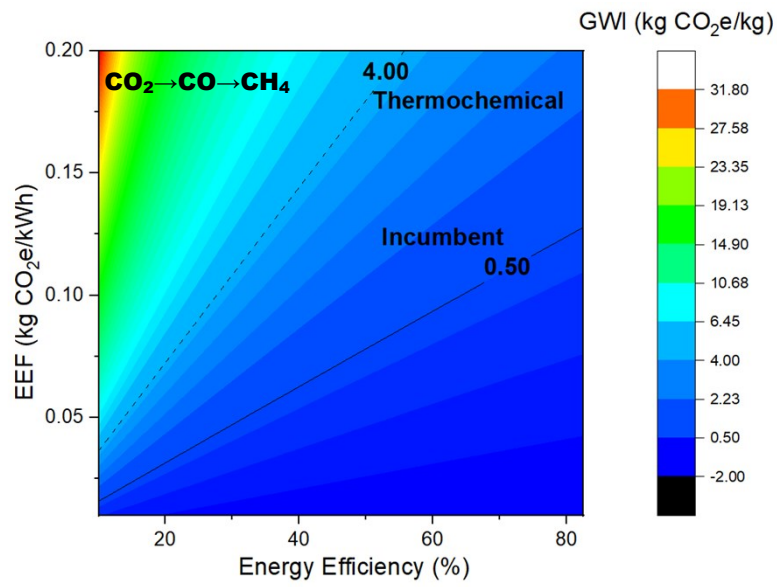
Table S10: Future projections for electricity emission factor (EEF) for US grid mix⁴¹

Year	Projected Renewable Share (%)	Projected EEF (kg CO ₂ e/kWh)
2020	20	0.430
2030	33	0.317
2040	41	0.297
2050	51	0.256

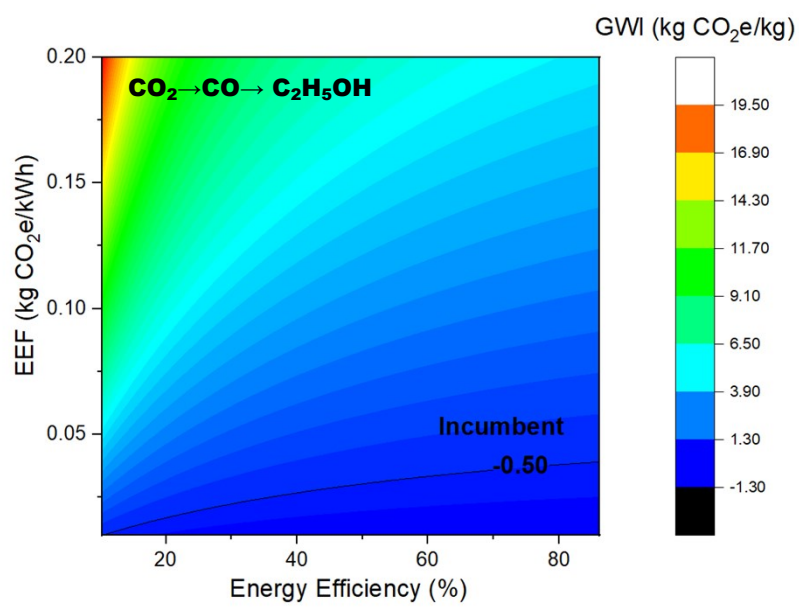
Contour Plots for Electrochemical CO₂- Derived Products



c)



d)



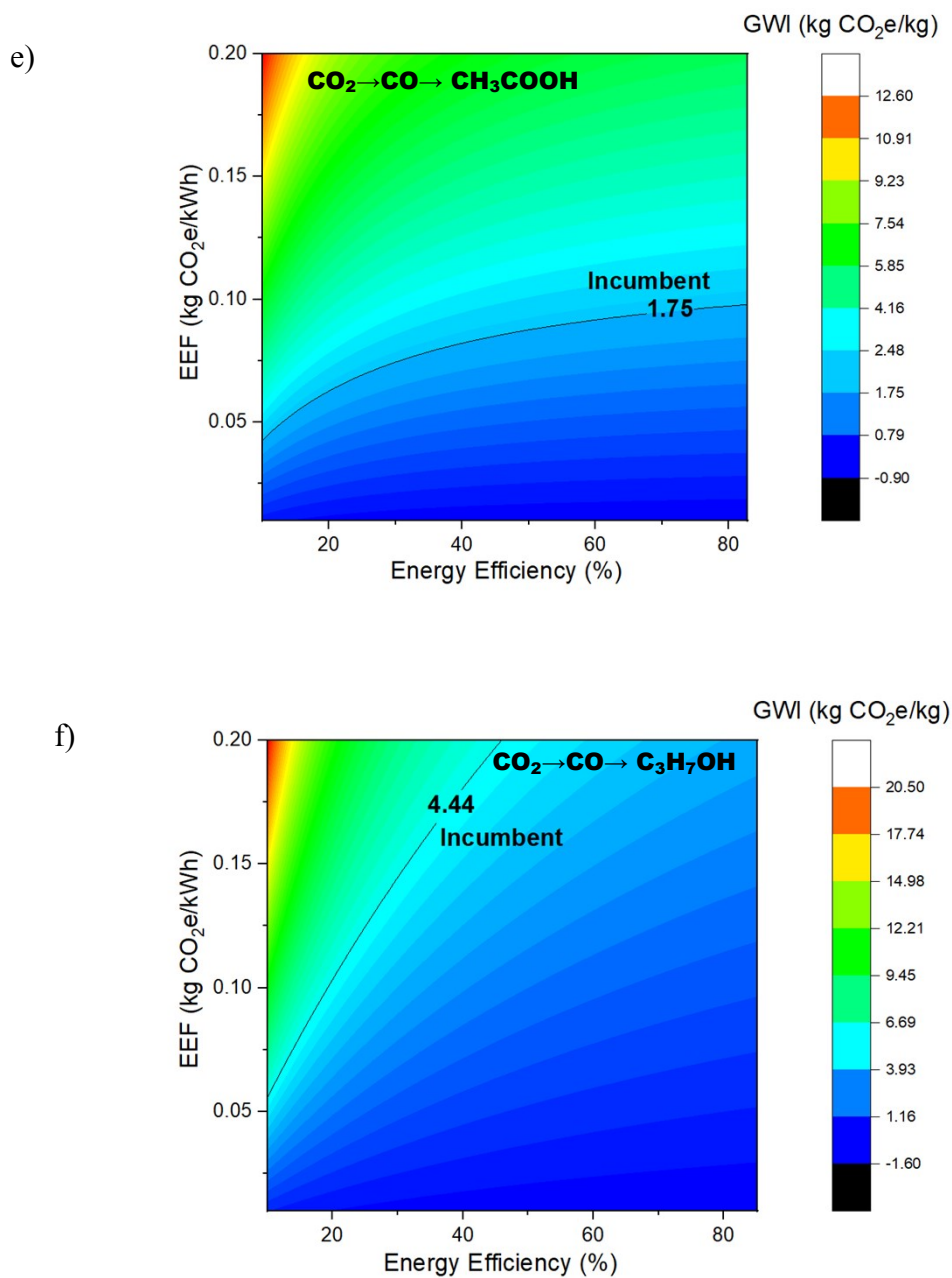


Figure S1: Effect of EEF and EE on GWI for electrosynthesis products. a) Syngas, b) Formic acid, c) Methane, d) Ethanol, e) Acetic acid, f) n-Propanol. 10wt% feed concentration has been considered for liquid products. CO_2 capture footprint has been considered as $-0.8 \text{ kg CO}_2\text{e/kg CO}_2$ captured.

Relation Between Distillation Feed Concentration with Energy for Separation

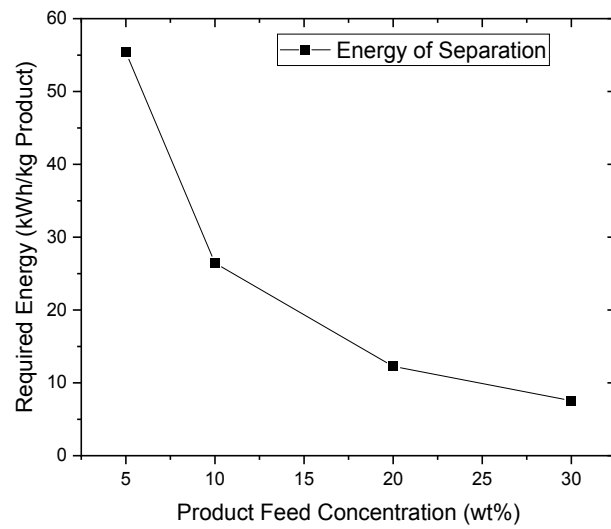


Figure S2: Relation between feed concentration in distillation and required energy for separation (with methanol as reference)

Sensitivity Analysis for Electrosynthesis of Two-step Methanol

Table S11: Performance metrics for sensitivity analysis

	Scenario 1	Base case	Scenario 2
Faradaic Efficiency (%)	45	90	100
Overpotential (V)	0.3	0.6	0.9
PSA Energy (kWh/kg)	0.125	0.25	0.375
CO ₂ Capture Footprint (kg CO ₂ e/kg CO ₂)	-0.4	-0.8	-1.2
Product Feed Concentration (wt%)	5	10	15

*EEF = 0.17 kg CO₂e/kWh

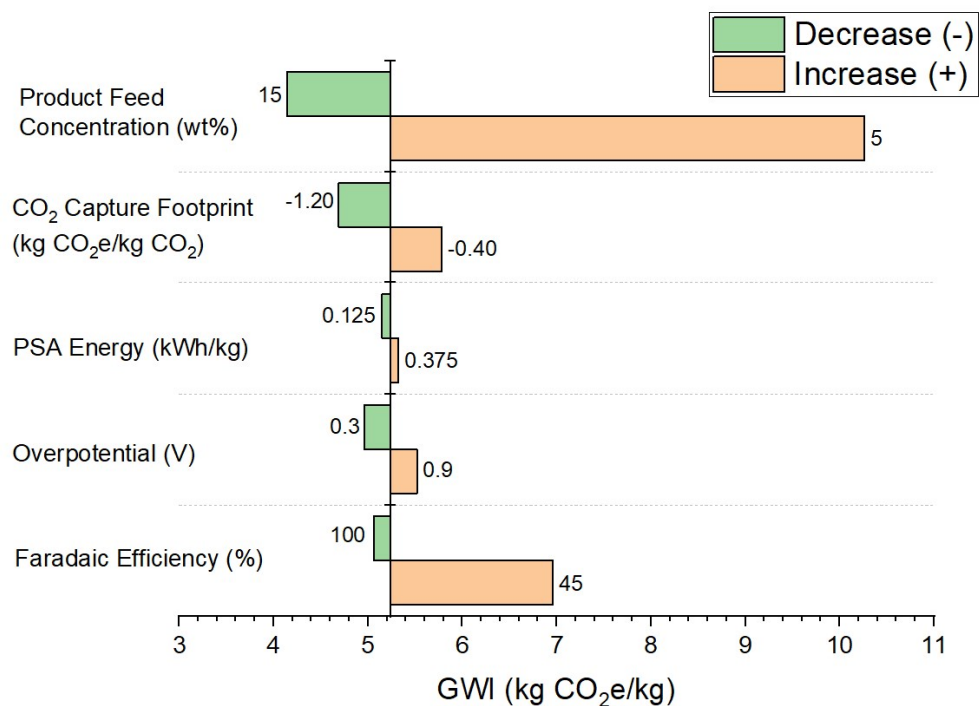


Figure S3: Sensitivity analysis for two-step methanol based on performance metrics

Bibliography

- 1 L. Bertuccioli, A. Chan, D. Hart, F. Lehner, B. Madden and E. Standen, *Study on development of water electrolysis in the EU, Fuel Cells and hydrogen Joint Undertaking*, 2014.
- 2 R. H. Elder, A. Azapagic and R. W. K. Allen, *Energy Environ. Sci.*, 2015, **8**, 1775–1789.
- 3 C. S. Chen, J. H. Wu and T. W. Lai, *J. Phys. Chem. C*, 2010, **114**, 15021–15028.
- 4 C. Chiang, K. Lin and H. Chuang, *J. Clean. Prod.*, , DOI:10.1016/j.jclepro.2017.11.229.
- 5 M. De Saint, P. Baurens and C. Bouallou, *Int. J. Hydrogen Energy*, 2014, **39**, 17024–17039.
- 6 B. Müller, K. Müller and D. Teichmann, 2013, 2002–2013.
- 7 A. A. Kiss, J. J. Pragt, H. J. Vos, G. Bargeman and M. T. De Groot, *Chem. Eng. J.*, 2016, **284**, 260–269.
- 8 L. K. Rihko-struckmann, A. Peschel, R. Hanke-rauschenbach and K. Sundmacher, *Ind. Eng. Chem. Res.*, 2010, 11073–11078.
- 9 J. Gao, J. Chunmiao and Bi. Liu, *Catal. Sci. Technol.*, 2017, **7**, 5602–5607.
- 10 J. Bierhals and M. Griesheim, *Ullman's Encycl. Ind. Chem.*, , DOI:10.1002/14356007.a05.
- 11 C. M. Kalamaras and A. M. Efstathiou, in *Conference Papers in Energy*, Hindawi Publishing Corporation, 2013, vol. 2013.
- 12 J. Hietala, A. Vuori, P. Johnsson, I. Pollari, W. Reutemann and H. Kieczka, *Ullman's Encycl. Ind. Chem.*
- 13 S. Rönsch, J. Schneider, S. Matthischke, M. Schlüter, M. Götz, J. Lefebvre, P. Prabhakaran and S. Bajohr, *Fuel*, 2016, **166**, 276–296.
- 14 G. Hammer, T. Lubcke, R. Kettner, M. R. Pillarella, H. Recknagel, A. Commichau, H.-J. Neumann and B. Paczynska-Lahme, *Ullman's Encycl. Ind. Chem.*, , DOI:10.1002/14356007.a17.
- 15 E. Fiedler, G. Grossmann, D. B. Kersebohm, G. Weiss and C. Witte, *Ullman's Encycl. Ind. Chem.*, , DOI:10.1002/14356007.a16.
- 16 H. Zimmermann and R. Walzi, *Ullman's Encycl. Ind. Chem.*, , DOI:10.1002/14356007.a10.
- 17 N. Kosaric, Z. Duvnjak, A. Farkas, H. Sahm, S. Bringer-Meyer, O. Goebel and D. Mayer, *Ullman's Encycl. Ind. Chem.*
- 18 U.S. Patent US 3686334 A, 1972, 1–4.
- 19 C. Le Berre, P. Serp, P. Kalek and G. P. Torrence, *Ullman's Encycl. Ind. Chem.*
- 20 A. J. Papa, *Ullman's Encycl. Ind. Chem.*, , DOI:10.1002/14356007.a22.
- 21 Organic Compounds: Physical and Thermochemical Data, http://www2.ucdsb.on.ca/tiss/stretton/database/organic_thermo.htm, (accessed 4 July 2020).
- 22 D. R. Lide, *CRC handbook of chemistry and physics*, CRC press, 2004, vol. 85.
- 23 Hydrogen Tools, Lower-and-higher-heating-values-fuels, <https://h2tools.org/hyarc/calculator-tools/lower-and-higher-heating-values-fuels>, (accessed 5 July 2020).

- 24 The Engineering ToolBox, Heat of Combustion, https://www.engineeringtoolbox.com/standard-heat-of-combustion-energy-content-d_1987.html, (accessed 5 July 2020).
- 25 E. Jeng and F. Jiao, *React. Chem. Eng.*, DOI:10.1039/D0RE00261E.
- 26 A. Paturska, M. Repele and G. Bazbauers, *Energy Procedia*, 2015, **72**, 71–78.
- 27 J. Artz, T. E. Müller, K. Thenert, J. Kleinekorte, R. Meys, A. Sternberg, A. Bardow and W. Leitner, *Chem. Rev.*, 2018, **118**, 434–504.
- 28 A. Sternberg, C. M. Jens and A. Bardow, *Green Chem.*, 2017, **19**, 2244–2259.
- 29 J. David and H. Herzog, *Energy*, 2000, 13–16.
- 30 C. M. Summers, *Sci. Am.*, 1971, **225**, 148–160.
- 31 L. J. Müller, A. Kätelhön, S. Bringezu, S. McCoy, S. Suh, R. Edwards, V. Sick, S. Kaiser, R. Cuéllar-Franca, A. El Khamlichi, J. H. Lee, N. von der Assen and A. Bardow, *Energy Environ. Sci.*, 2020, **13**, 2979–2992.
- 32 Canada Energy Regulator, Canada’s Renewable Power Landscape 2017 – Energy Market Analysis, <https://www.cer-rec.gc.ca/nrg/sttstc/lctret/rprt/2017cndrnwblpwr/index-eng.html>, (accessed 15 July 2020).
- 33 P. Markewitz, J. Marx, A. Schreiber and P. Zapp, *Energy Procedia*, 2013, **37**, 2864–2876.
- 34 A. K. Plappally and J. H. Lienhard V, *Renew. Sustain. Energy Rev.*, 2012, **16**, 4818–4848.
- 35 W. Hoppe, N. Thonemann and S. Bringezu, *J. Ind. Ecol.*, 2018, **22**, 327–340.
- 36 M. Jouny, G. S. Hutchings and F. Jiao, *Nat. Catal.*, 2019, **2**, 1062–1070.
- 37 S. J. Bennett, D. J. Schroeder and S. T. McCoy, *Energy Procedia*, 2014, **63**, 7976–7992.
- 38 M. Jouny, W. Luc and F. Jiao, *Ind. Eng. Chem. Res.*, 2018, **57**, 2165–2177.
- 39 N. Thonemann and M. Pizzol, *Energy Environ. Sci.*, 2019, **12**, 2253–2263.
- 40 P. De Luna, C. Hahn, D. Higgins, S. A. Jaffer, T. F. Jaramillo and E. H. Sargent, *Science (80-.)*, DOI:10.1126/science.aav3506.
- 41 U.S Energy Information Administration, *Annual Energy Outlook 2020*, 2020.