

Supplementary information for

Catalytic exchange of hydrogen isotopes intensified by two-phase stratified flow in wettability designable microchannels

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S1. Preparation of Pt/AC/PDMS coating on the walls of the microchannel reactor

The Pt/AC/PDMS coatings were prepared on the channel walls according to a “glue + powder” approach described by Li et al.^[S1] using the commercial PDMS (Sylgard 184) as the “glue” and the Pt/AC catalyst as the “powder”. The diluted PDMS solution (10% w/v in *n*-hexane) was prepared by dissolving PDMS base and curing agent (a 10:1 w/w ratio) in *n*-hexane. The Pt/AC catalyst was ground and then sieved by a 200-mesh sieve prior to preparing the coatings. The procedure is specified as follows:

- (1) The channel substrate was sealed with a silicone sheet.
- (2) The diluted PDMS solution was injected into the microchannel.
- (3) A thin liquid film would be deposited on the channel walls while the excess solution was withdrawn.
- (4) The silicone sheet was opened to let hexane evaporate.
- (5) After the most of hexane was evaporated, the uncured adhesive surface was covered by the Pt/AC powder for 5 minute.
- (6) After removing the excess powder, the prepared coating was cured under 80 °C for 2 hours. The top surface of the channel substrate was cleaned so that the channel substrate could bond with the cover plate successfully.

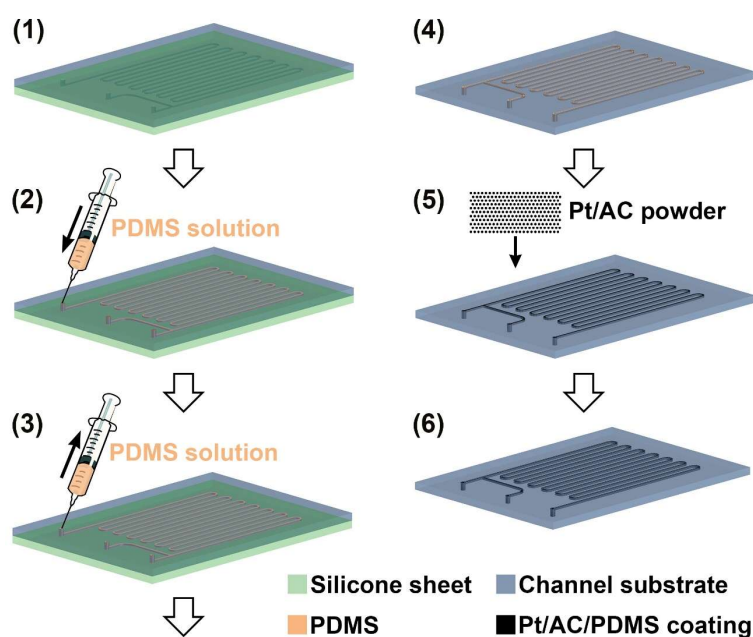


Fig. S1. Schematic of the process for preparing Pt/AC/PDMS coating on the walls of the microchannel reactor.

S2. Calculation of the y_{HD1}^*

Rolston et al.^[S2] measured the overall deuterium (D) isotope separation factor between hydrogen and liquid water, α , at 280–370 K. The α is defined as eqn (S1). The correlation between α and temperature (T , K) is presented as eqn (S2). Based on the mass balance of D, the D abundance in the liquid water at outlet of the microchannel reactor (x_{D1}) is calculated by eqn (S3). The equilibrium D abundance in hydrogen at the outlet (y_{D1}^*) can be calculated by eqn (S4) transformed from eqn (S1). The equilibrium molar fraction of HD in hydrogen at the outlet (y_{HD1}^*) is twice the y_{D1}^* calculated as eqn (S5).

$$\alpha = \frac{x_{\text{D}}^*(1 - y_{\text{D}}^*)}{y_{\text{D}}^*(1 - x_{\text{D}}^*)} \quad (\text{S1})$$

$$\ln \alpha = -0.2143 + \frac{368.9}{T} + \frac{27870}{T^2} \quad (\text{S2})^{[\text{S2}]}$$

$$x_{\text{D1}} = \frac{2x_{\text{D0}}F_{\text{H}_2\text{O}} - (y_{\text{HD1}} - y_{\text{HD0}})F_{\text{H}_2}}{2F_{\text{H}_2\text{O}}} \quad (\text{S3})$$

$$y_{\text{D1}}^* = \frac{1}{1 - \alpha + \alpha / x_{\text{D1}}} \quad (\text{S4})$$

$$y_{\text{HD1}}^* = 2y_{\text{D1}}^* \quad (\text{S5})$$

where x_{D}^* and y_{D}^* are the equilibrium D abundances in liquid water and hydrogen, respectively; x_{D0} is the D abundance in liquid water at inlet of the microchannel reactor; $F_{\text{H}_2\text{O}}$ and F_{H_2} are the feeding molar flow rates of water and hydrogen, respectively; y_{HD0} and y_{HD1} are the molar fractions of HD in hydrogen at inlet and outlet of the microchannel reactor, respectively.

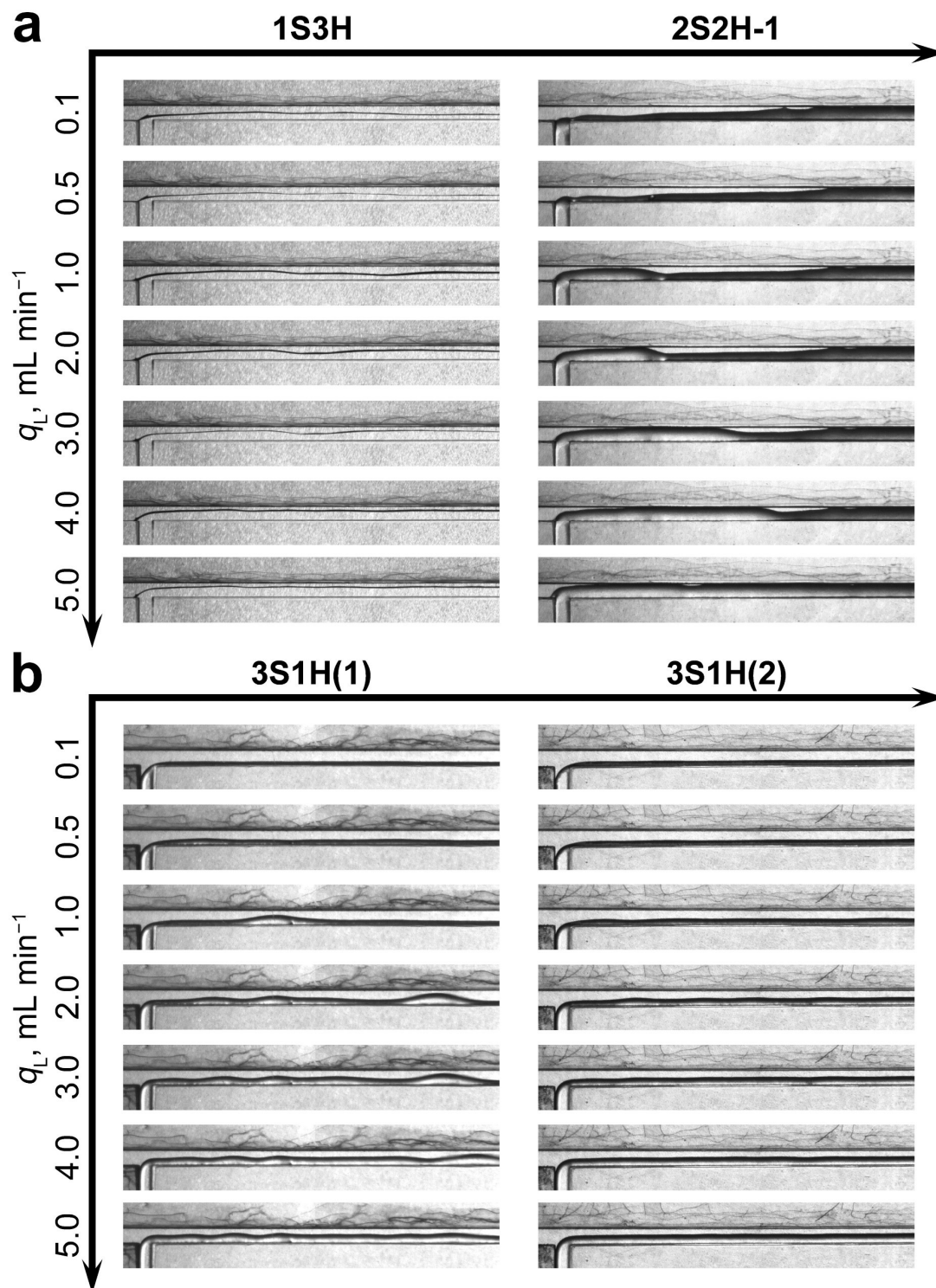


Fig. S2. Effects of liquid flow rate (q_L) on flow patterns at a given gas flow rate ($q_G = 15.0 \text{ mL min}^{-1}$) in the 1S3H, 2S2H-1, 3S1H(1) and 3S1H(2) microchannels.

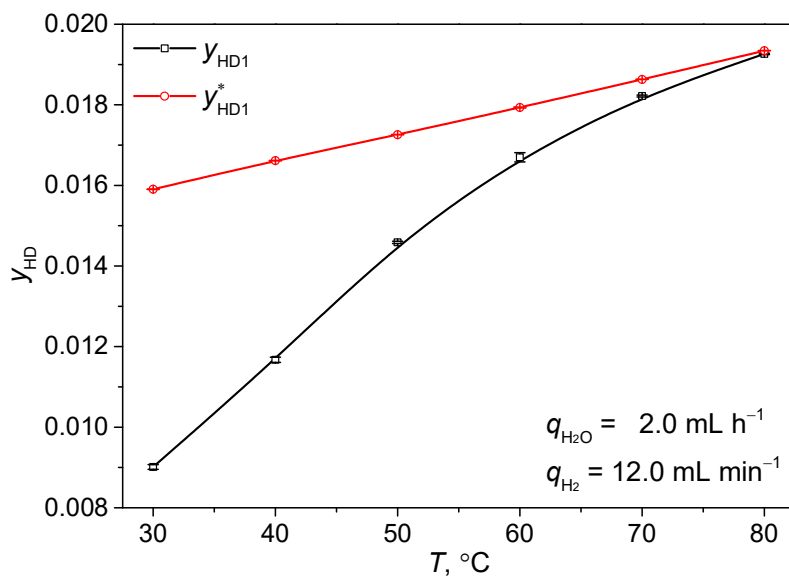


Fig. S3. Effects of temperature (T) on molar fraction (y_{HD1}) and equilibrium molar fraction (y_{HD1}^*) of HD in hydrogen at outlet of the microchannel reactor at $x_{D0} = 0.03$, $q_{H_2O} = 2.0 \text{ mL h}^{-1}$ and $q_{H_2} = 12.0 \text{ mL min}^{-1}$.

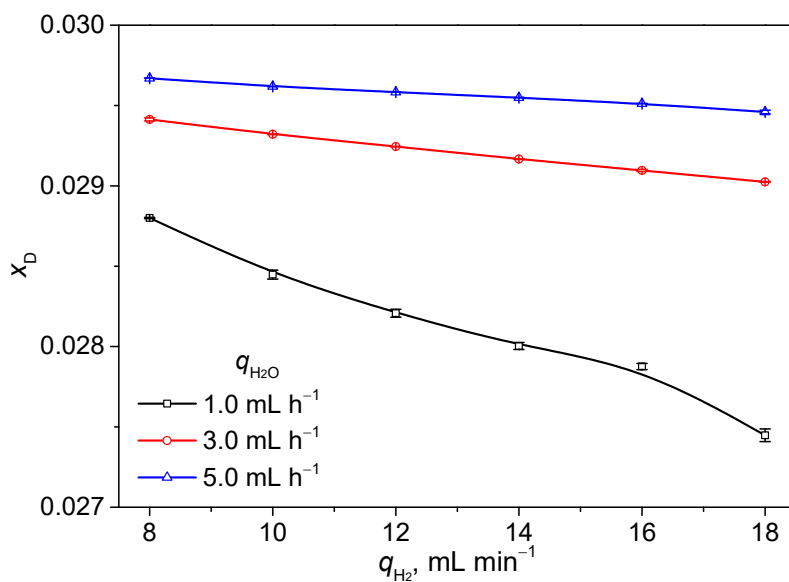


Fig. S4. Effects of hydrogen (q_{H_2}) and water (q_{H_2O}) flow rates on average D abundance in the water flow ($x_D = (x_{D0} + x_{D1})/2$) of the microchannel reactor at $x_{D0} = 0.03$ and $T = 60 \text{ }^\circ\text{C}$.

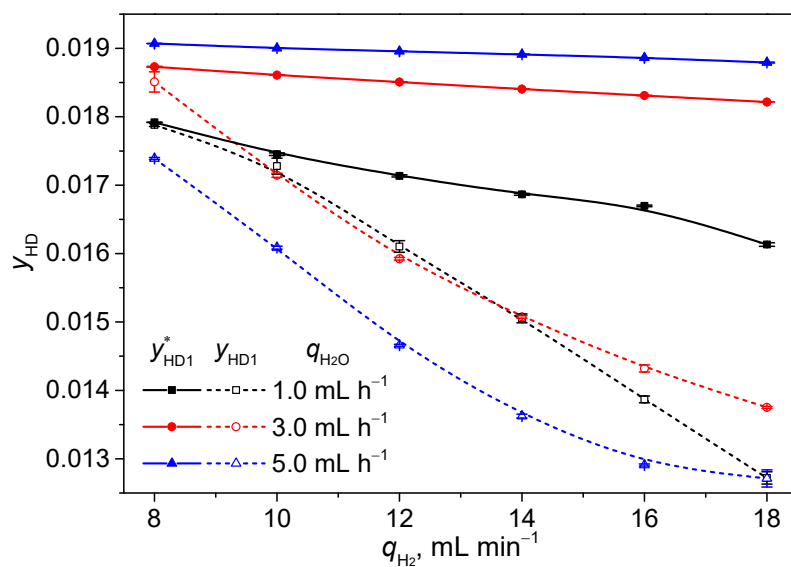


Fig. S5. Effects of hydrogen (q_{H_2}) and water (q_{H_2O}) flow rates on molar fraction (y_{HD1}) and equilibrium molar fraction (y_{HD1}^*) of HD in hydrogen at outlet of the microchannel reactor at $x_{D0} = 0.03$ and $T = 60$ °C.

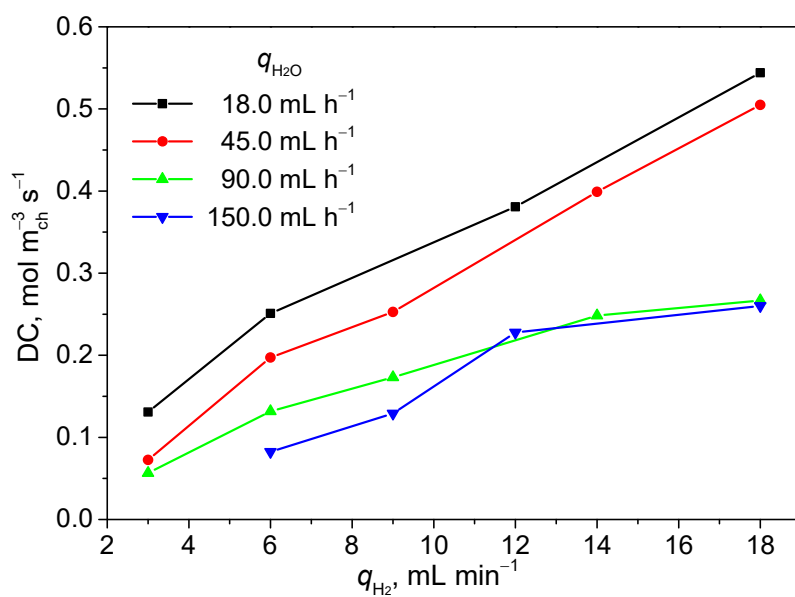


Fig. S6. Effects of hydrogen (q_{H_2}) and water (q_{H_2O}) flow rates on deuterium removal capacity (DC) in the microchannel reactor at $x_{D0} = 0.03$ and $T = 60$ °C.

References

- [S1] Z. Li, M. Cao, P. Li, Y. Zhao, H. Bai, Y. Wu and L. Jiang, *Matter*, 2019, **1**, 661–673.
[S2] J. H. Rolston, J. Den Hartog and J. P. Butler, *J. Phys. Chem.*, 1976, **80**, 1064–1067.