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2	Supplementary Materials
3	for
4	A dual-trigger mode ionic hydrogel sensor for contact or
5	contactless motions recognition
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12 Theoretical study of sandwich structure hydrogel with regular concavo-convex pattern

By modeling the regular concavo-convex pattern on the surface of P(AA-co-DMC), a larger 13 14 capacitance of dielectric interlayer was formed caused by more contact area between P(AA-co-DMC) and P(AM-co-HEMAA) hydrogels. Importantly, compared with the conventional 15 sandwich structure, the structured interface has advantages on the pressure sensitivity when 16 samples are suffered the same external loads, including improving the friction between two 17 layers and increasing the total deformation. As shown in Fig. S1, we separate a hexahedral 18 differential element of sample to analyze the stress and strain. By applied the external vertically 19 20 distributed loading, the body forces of the sample are expressed in Equation S1 (ρ is the density of hydrogel (~1kg/m³), g=9.8N/kg). In this loading condition, we assume that the 21 sensor only deforms along the z axis, as defined in Equation S2, where u, v, w are the 22 23 deformation along the x, y, z axis, respectively.





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(S2)

$$u=0, v=0, w=w(z)$$



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Figure S1. Theoretical analysis on the effect of regular concavo-convex pattern in sandwich structure. (A) Stress analysis of hexahedral differential element in hydrogel-based sensor. (B) Illustration of the sandwich structure with or without regular concavo-convex pattern at interface which suffers the external load. (a) Illustration of MOMS structure section. (b) Illustration of comment sandwich structure section. (C) The morphology of regular concavoconvex pattern on the surface of P(AA-*co*-DMC) hydrogel.

The relationship between stress and strain components along three axes can be expressed in **Equation S3**, where $\sigma_{x'} \sigma_{y'} \sigma_z$ are the components of the normal stress, $\tau_{yz'} \tau_{zx'} \tau_{xy}$ are the components of the shear stress, $\varepsilon_{x'} \varepsilon_{y'} \varepsilon_z$ are the components of the normal strain, $\gamma_{yz'} \gamma_{zx'} \gamma_{xy}$ are the shearing strains, E is the elastic modulus, μ is Poisson's ratio of hydrogel ($\mu \approx 0.46^{[1]}$). Heanwhile, **Equation S4** shows the correlation of the strains and displacements. Then, the relationship between stress and deformation (**Equation S5**) can be derived by substituting the **Equation S4** into **Equation S3**.

 $\begin{aligned} \varepsilon_{x} &= \frac{\partial u}{\partial x}, \varepsilon_{y} = \frac{\partial v}{\partial y}, \varepsilon_{z} = \frac{\partial w}{\partial z} \\ \gamma_{yz} &= \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z}, \gamma_{zx} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x}, \\ \gamma_{xy} &= \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \end{aligned}$

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$$\varepsilon_{x} = \frac{1}{E} \left[\sigma_{x} - \mu(\sigma_{y} + \sigma_{z}) \right]$$

$$\varepsilon_{y} = \frac{1}{E} \left[\sigma_{y} - \mu(\sigma_{x} + \sigma_{z}) \right]$$

$$\varepsilon_{z} = \frac{1}{E} \left[\sigma_{z} - \mu(\sigma_{x} + \sigma_{y}) \right]$$

$$\gamma_{yz} = \frac{2(1 + \mu)}{E} \tau_{yz}$$

$$\gamma_{zx} = \frac{2(1 + \mu)}{E} \tau_{zx}$$

$$\gamma_{xy} = \frac{2(1 + \mu)}{E} \tau_{xy}$$
(S3)

(S4)

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$$\sigma_{x} = \frac{E}{1+\mu} \left(\frac{\mu}{1-2\mu} \theta + \frac{\partial u}{\partial x} \right),$$

$$\sigma_{y} = \frac{E}{1+\mu} \left(\frac{\mu}{1-2\mu} \theta + \frac{\partial v}{\partial y} \right),$$

$$\sigma_{z} = \frac{E}{1+\mu} \left(\frac{\mu}{1-2\mu} \theta + \frac{\partial w}{\partial z} \right),$$

$$\tau_{yz} = \frac{E}{2(1+\mu)} \left(\frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right),$$

$$\tau_{zx} = \frac{E}{2(1+\mu)} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right),$$

$$\tau_{xy} = \frac{E}{2(1+\mu)} \left(\frac{\partial v}{\partial z} + \frac{\partial u}{\partial y} \right),$$

(S5)
and

$$\theta = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = \frac{\partial w}{\partial z}.$$

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52 By incorporation of the **Equation S5** and differential equations of mechanics equilibrium theory, 53 **Equation S6** can be further established. Subsequently, according to the boundary conditions 54 including $(-\sigma_z)_{z=0} = q$ and $(w)_{z=h} = 0$, we could get the total deformation along the vertical 55 section (Δ), as shown in **Equation S7** and **S8**. Compared with the comment sandwich structure, due 56 to the difference of *E* between different material layers, the Δ value of MOMS is larger under the 57 same loading condition, thereby generating more intense capacitive variation and achieving better 58 sensitivity.

and

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$$\frac{E}{2(1+\mu)} \left(\frac{1}{1-2\mu\partial x} + \nabla^{2}u \right) + f_{x} = 0,$$

$$\frac{E}{2(1+\mu)} \left(\frac{1}{1-2\mu\partial y} + \nabla^{2}v \right) + f_{y} = 0,$$

$$\frac{E}{2(1+\mu)} \left(\frac{1}{1-2\mu\partial z} + \nabla^{2}w \right) + f_{z} = 0,$$

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$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^{2'}}, \ \frac{\partial\theta}{\partial x} = 0, \ \frac{\partial\theta}{\partial y} = 0, \ \frac{\partial\theta}{\partial z} = \frac{d^2w}{dz^2}.$$

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$$w = \frac{(1+\mu)(1-2\mu)}{E(1-\mu)} [q(h-z) + \frac{\rho g}{2} (h^2 - z^2)]$$
(S7)

$$\Delta = \int_{z} (w) \, dz \tag{S8}$$

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65 The characterization and mechanical properties of the P(AA-*co*-DMC) hydrogel and P(AM-66 *co*-HEMAA)

The zwitterionic hydrogel exhibited the typical porous three-dimensional network, which has 67 advantage on the transport of the mobile ions (Fig. S2A). As shown in Fig. S2B, the FTIR 68 spectrum of PAA hydrogel exhibited characteristic peaks at 3345, 1550, 1450, and 1405 cm⁻ 69 ¹corresponded to -OH stretching, C=O stretching of -COONa, and C=O deformation vibration 70 of -COOH, respectively. By contrast, the spectrum of PDMC had five main characteristic 71 absorption bands including the peaks at 1713, 1643, 1485, 1299, and 960 cm⁻¹ corresponded to 72 73 C-O γ absorption band, C=C γ absorption band, (CH₂)₂ δ absorption band, quaternary 74 ammonium N⁺(CH₃)₃ absorption band, and C-O δ absorption band. All these characteristic 75 absorption bands were performed in the P(AA-co-DMC) hydrogel spectrum, which determined the copolymer had a DMC and AA block structure. 76



Figure S2. The morphology and composition analysis of P(AA-*co*-DMC) hydrogel (mole ratio=1). (A) The typical
SEM images of the freeze-dried xerogels for the zwitterionic hydrogel. (B) The composition analysis of polyacrylic
acid (PAA), Polymethyl propylene oxyethyl trimethylammonium chloride (PDMC), and P(AA-*co*-DMC) hydrogel.

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82 As for the electric conductivity of the zwitterionic hydrogel and P(AM-co-HEMAA) hydrogel synthesized in this work, the resistance of the sample with a size of 10*8*1.03 mm³ is 4.33 Ω and 83 64.2Ω , respectively. Based on the following equation, the conductivity of P(AA-co-DMC) hydrogel 84 85 and P(AM-co-HEMAA) hydrogel are equal to 2.97 S/m and 0.20 S/m, respectively . 86

$$\sigma = \frac{1}{R_b} \cdot \frac{d}{S} \tag{S9}$$

Where σ is the conductivity of the sample, R_b is the resistance, d is the thickness, and S is the 88 89 effective area.

Moreover, we further tested the dielectric property of the P(AM-co-HEMAA) hydrogel. It performs 90 91 the satisfying permittivity under the frequency with a range of 200 kHz-20 MHz, which is a guarantee for the sensing performance of this kind of capacitive hydrogel system. 92 93



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96 Figure S3. Electrochemical Impedance Spectroscopy of the hydrogels with 5 mV amplitude and 0.01-10⁵ Hz 97 frequency. (A) Electrochemical Impedance Spectroscopy of the P(AA-co-DMC) hydrogel (mole ratio=1). The upper 98 left image inset is the enlargement, and the bottom right is the equivalent circuit. (B) Electrochemical Impedance 99 Spectroscopy of the P(AM-co-HEMAA) hydrogels. The upper left image inset is the enlargement, and the bottom

100 right is the equivalent circuit. (C) The permittivity of P(AM-co-HEMAA) hydrogel from 200 kHz to 20 MHz.





Figure S4. Mechanical Properties of P(AA-*co*-DMC) hydrogels with different proportion and
components of MOMS. (A, B) Tension and compression tests for (AA-*co*-DMC) hydrogels with
different mole ratio at room temperature. (C) Comparation of each components and MOMS elastic
modulus. (D) The compression tests for P(AA-co-DMC) and P(AM-co-HEMAA) hydrogel. (E,F)
Cyclic elongation tests for P(AA-*co*-DMC) and P(AM-*co*-HEMAA) hydrogel at 3-fold tensile



Figure S5. The stability and durability of MOMS suffering cyclic loading. (A)The 500 cyclic tension experiment with 20% elongation under the speed of 10 mm/s. (B, C, D) The enlargement of the figure A during 100-260 s, 1640-1800 s, and 3340-3500 s sections.

117 Theoretical analysis of the capacitance changes of MOMS in touch-free mode

Based on the Equation 1 & 2, the capacitance variations generated by the changes of distance and effective overlap area between finger and MOMS surface can be got in the Equation S10. Therefore, by detecting the variation values, the recognition of diverse noncontact gestures and monitor on hands remote motions can be achieved accurately. As a result, the more satisfying and freedom human–machine interfaces experience for screen sensors, wearable devices, intelligent robots, and home automation will be achieved.

$$\frac{\Delta C}{C_0} = \frac{C_{EDL} + C_D}{C_{EDL} + 2C_D} \left(\frac{1}{C_{finger}} \frac{C_{EDL} + C_D}{C_D C_{EDL}} - 1 \right),$$
(S10)
and
$$C_{finger} = \frac{\varepsilon S_{finger}}{4\pi k' d_{finger}}.$$

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126 Where C_{EDL} is the capacitance of the EDL, C_D is the capacitance of the dielectric hydrogel, C_{finger} 127 is the capacitance formed between finger and electrolyte hydrogel, ε is the dielectric constant of the 128 dielectric layer, S is the effective area of the conducting layer, k' is the electrostatic constant, and d 129 is the thickness of the dielectric.



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132 **Figure S6.** The schematics of fabrication process of a 4×4 array sensors with two-step method. 133



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135 Figure S7. Capacitance variation signals of the sensor with various cover materials (2 mm

136 thickness) to a palm at the same working distance (3 mm).

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Monomer	Chemical structure
Acroleic acid (AA)	O OH
[2-(Methacryloyloxy)ethyl] trimethylammonium chloride (DMC)	
Acrylamide (AM)	H ₂ N O
N-(2-Hydroxyethyl)acrylamide (HEMAA)	O H H O H

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Table S1. The chemical structure of monomers used in this work

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141 Movie S1

142 The performance on wrist pulse detection.

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144 Movie S2

145 The performance on the remote gesture movements detection of MOMS.

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147 Movie S3

148 The performance on the remote gesture movements detection of MOMS covered by different 149 materials.

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152 **Reference**

153 [S1] U. Chippada, B. Yurke, N. A. Langrana. Simultaneous determination of Young's modulus,

154 shear modulus, and Poisson's ratio of soft hydrogels. Journal of Materials Research, 2010, 25, 3,

155 545-555.