

Supporting Information for

An Interlocked DNA Cascade System for Universal Probe-based Melting Curve Analysis

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Theoretical calculation model

During the initial stage, three main reactions happened in the system:

1. probe + bridge →probe/bridge;
2. bridge + target →bridge/target;
3. probe + bridge + target →probe/bridge/ target.

Since the initial concentration of probe, bridge and target were 100 nM, thus

$$[\text{target}] + [\text{bridge} / \text{target}] + [\text{probe} / \text{bridge} / \text{target}] = 100 \text{ nM} \quad (1.1)$$

$$[\text{probe}] + [\text{probe} / \text{bridge}] + [\text{probe} / \text{bridge} / \text{target}] = 100 \text{ nM} \quad (1.2)$$

$$[\text{bridge}] + [\text{probe} / \text{bridge}] + [\text{probe} / \text{bridge} / \text{target}] = 100 \text{ nM} \quad (1.3)*$$

MERGEFORMAT

Here for presentation simplicity, we set the [probe/bridge], [probe/target], [probe/bridge/ target] to

be x, y, z. Thus:

$$[\text{probe}] = 100 \text{ nM} - x - z \quad (1.4)$$

$$[WT] = 100 \text{ nM} - y - z \quad (1.5)$$

$$[\text{bridge}] = 100 \text{ nM} - x - y - z \quad (1.6)$$

Since

$$\left\{ \begin{array}{l} x = k_1 \cdot [\text{probe}] \cdot [\text{bridge}] = e^{\frac{-\Delta G_1}{R \cdot T}} \cdot (100 \text{ nM} - x - z) \cdot (100 \text{ nM} - x - y - z) \\ y = k_2 \cdot [\text{target}] \cdot [\text{bridge}] = e^{\frac{-\Delta G_2}{R \cdot T}} \cdot (100 \text{ nM} - y - z) \cdot (100 \text{ nM} - x - y - z) \\ z = k_3 \cdot [\text{target}] \cdot [\text{bridge}] \cdot [\text{probe}] = e^{\frac{-\Delta G_3}{R \cdot T}} \cdot (100 \text{ nM} - x - z) \cdot (100 \text{ nM} - y - z) \cdot (100 \text{ nM} - x - y - z) \end{array} \right. \quad (1.7)$$

Where k_1, k_2, k_3 were the equilibrium constants for reaction 1, 2, 3 and $\Delta G_1, \Delta G_2, \Delta G_3$ were the free

energy change of reaction 1, 2, 3.

The analytical solution of equation (1.7) is complex. For convenience of the subsequent description, we simply set the solution of equation (1.7) to be (x_1, y_1, z_1) .

When no substrate was added to the system, only one main reaction happened:

1. probe + bridge \rightarrow probe/bridge;

Since

$$[\text{probe}] + [\text{probe / bridge}] = 100 \text{ nM} \quad (2.1)$$

$$[\text{bridge}] + [\text{probe / bridge}] = 100 \text{ nM} \quad (2.2)$$

we set the $[\text{probe/bridge}]$ to be x , thus

$$[\text{probe}] = [\text{bridge}] = 100 \text{ nM} - x \quad (2.3)$$

$$x = k_1 \cdot [\text{probe}] \cdot [\text{bridge}] = e^{\frac{-\Delta G_1}{R \cdot T}} \cdot (100 \text{ nM} - x)^2 \quad (2.4)$$

Similarly, we set the solution of equation (2.4) to be x_2 .

Thus

$$\frac{[\text{probe / bridge / target}]}{[\text{probe / bridge}]} = \frac{z_1}{x_2} \quad (2.5)$$

Next, we used a computer program to solve equations (1.7 and 2.4) numerically. The programs were written in MATLAB:

```
function L=calculate(z1,z2,z3)%z1, z3, z3 refers to ΔG1, ΔG2, ΔG3;
```

```
r=8.314;
```

```
t=310.15;
```

```
y1=exp(-z1/(r*t));
```

```
y2=exp(-z2/(r*t));
```

```
y3=exp(-z3/(r*t));
```

```

syms x1 x2 x3 p;

[solp0,solp1,solp2] = solve (y1*(10^-7-x1-x3)*(10^-7-x1-x2-x3)-x1==0,y2*(10^-7-x2-x3)*(10^-
7-x1-x2-x3)-x2==0,y3*(10^-7-x1-x3)*(10^-7-x2-x3)*(10^-7-x1-x2-x3)-x3==0,x1,x2,x3);

a1=double(solp0);

a2=double(solp1);

a3=double(solp2);

A=[a1,a2,a3];

n=size(A);

for i=1:n(1)

if isreal(A(i,1))==1

if A(i,1)>0&&A(i,1)<10^-7

if isreal(A(i,2))==1

if A(i,2)>0&&A(i,2)<10^-7

if isreal(A(i,3))==1

if A(i,3)>0&&A(i,3)<10^-7

y=A(i,:);

break

end

end

end

end

```

```

end

end

q=y1*(10^-7-p)^2;

r=double(solve(q==p));

if r(1)>0&&r(1)<10^-7

R=r(1);

if r(2)>0&&r(2)<10^-7

R=r(2);

end

end

L=y(3)/R;

```

With this program, we could directly predict the ratio by inputting the values of ΔG_1 , ΔG_2 , ΔG_3 . The results were shown as follows:

Table S1. The calculation results of different reaction systems used in this work

Probe	Bridge	Target	ΔG_1 (j/mol)	ΔG_2 (j/mol)	ΔG_3 (j/mol)	Triplex/ duplex
Probe	bridge-1	wt-1	-57027.92	-53931.76	-132298.08	1.0483
Probe	bridge-2	wt-1	-48618.08	-78450.00	-131754.16	1.163
Probe	bridge-3	wt-1	-54015.44	-56776.88	-135477.92	1.0918
Probe	bridge-4	wt-1	-45270.88	-27070.48	-99118.96	1.3721
Probe	bridge-5	wt-1	-53806.24	-50333.52	-129034.56	1.0939
Probe	bridge-6	wt-2	-49162.00	-58743.36	-130331.60	1.2518

Probe	bridge-7	wt-2	-47195.52	-31631.04	-110081.04	1.347
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Probe	Bridge	Target	ΔG_1 (j/mol)	ΔG_2 (j/mol)	ΔG_3 (j/mol)	Triplex/ duplex
Probe	bridge-8	wt-3	-52467.36	-48157.84	-130540.80	1.1254
Probe	bridge-9	wt-3	-51212.16	-44685.12	-127068.08	1.1619
Probe	bridge-10	wt-4	-61462.96	-59747.52	-140289.52	1.0201
Probe	bridge-11	wt-4	-56986.08	-42634.96	-123135.12	1.1667
Probe	bridge-12	wt-5	-55103.28	-64182.56	-135896.32	1.0713
Probe	bridge-13	wt-5	-52425.52	-57822.88	-129578.48	1.2225
Probe	bridge-14	wt-6	-53178.64	-40961.36	-123344.32	1.1030
Probe	bridge-15	wt-6	-41045.04	-26275.52	-99336.48	1.5126

In order to compare with experimental results in a better way, we modified the mathematical model to calculate the sum of the concentration of triplex and duplex after adding target over the concentration of duplex without adding target.

Thus

$$\frac{[probe / bridge / target] + [probe / bridge]}{[probe / bridge]} = \frac{x_1 + z_1}{x_2} \quad (3.1)$$

Next, we changed the last line of the previous program to “L=(y(1)+y(3))/R” to calculate the ratio.

The results were shown as follows:

Table S2. The calculation results of different reaction systems used in this work

Probe	Bridge	Target	ΔG_1 (j/mol)	ΔG_2 (j/mol)	ΔG_3 (j/mol)	Triplex/ duplex
Probe	bridge-1	wt-1	-57027.92	-53931.76	-132298.08	1.0487
Probe	bridge-2	wt-1	-48618.08	-78450.00	-131754.16	1.1635
Probe	bridge-3	wt-1	-54015.44	-56776.88	-135477.92	1.0924
Probe	bridge-4	wt-1	-45270.88	-27070.48	-99118.96	1.3727
Probe	bridge-5	wt-1	-53806.24	-50333.52	-129034.56	1.0946
Probe	bridge-6	wt-2	-49162.00	-58743.36	-130331.60	1.2529
Probe	bridge-7	wt-2	-47195.52	-31631.04	-110081.04	1.3481
Probe	Bridge	Target	ΔG_1 (j/mol)	ΔG_2 (j/mol)	ΔG_3 (j/mol)	Triplex/ duplex
Probe	bridge-8	wt-3	-52467.36	-48157.84	-130540.80	1.1258
Probe	bridge-9	wt-3	-51212.16	-44685.12	-127068.08	1.1624
Probe	bridge-10	wt-4	-61462.96	-59747.52	-140289.52	1.0209
Probe	bridge-11	wt-4	-56986.08	-42634.96	-123135.12	1.1675
Probe	bridge-12	wt-5	-55103.28	-64182.56	-135896.32	1.0720
Probe	bridge-13	wt-5	-52425.52	-57822.88	-129578.48	1.2231
Probe	bridge-14	wt-6	-53178.64	-40961.36	-123344.32	1.1040
Probe	bridge-15	wt-6	-41045.04	-26275.52	-99336.48	1.5132

Table S3. DNA sequences used in this work.

Name	Sequences (5'→3')
Probe	FAM-GGCGCGGGCCCAGCCCTACCGCGCC-BHQ1
WT-1	GTAAAAGACATGACAGCGATACTTCCCAGAGC
MT-1	GTAAAAGACATGACAG T GATACTTCCCAGAGC
WT-2	TTTGCTGAGAATAAACAGCTTCTAGCTCCATC
MT-2	TTTGCTGAGAATAACA A CTTCTAGCTCCATC
WT-3	GCAATACCATTAGGACATAGGCATGGCAA
MT-3	GCAATACCATTAGGA T ATAGGCATGGCAA
WT-4	GGACATTACCACAGATCCTACAGGCATTAAA
MT-4	GGACATTACCACAGA C CCTACAGGCATTAAA
WT-5	ATGCACCTGTAACAATAGCTGAGTCTTGG
MT-5	ATGCACCTGTAACA A CAGCTGAGTCTTGG
WT-6	TGGTGTTCATCAAATGAGTGATC
MT-6	TGGTGTTCATCAA G TGAGTGATC
WT-1-L	GCAACTGGAGCCAAGAAGAGTAACAAGCCAATGAACAGACAAGTA AAGACATGACAGCGATACTTCCCAGAGCTGAAGTTAACAAATGCACC TGGTTC
MT-1-L	CCTGCAACTGGAGCCAAGAAGAGTAACAAGCCAATGAACAGACAAG TAAAAGACATGACAG T GATACTTCCCAGAGCTGAAGTTAACAAATGC ACCTGGTTC

Name	Sequences (5'→3')
WT-4-L	CACACAAATTACTAGCATCAGGAATGAAGGAGAGGACATTACCA CAGA TCCTACAGGCATTTAAAAGAGAACAGGCAAATTATCATGAAC TACTTA TGCTAATAAAC
MT-4-L	CACACAAATTACTAGCATCAGGAATGAAGGAGAGGACATTACCA CAGA CCCTACAGGCATTTAAAAGAGAACAGGCAAATTATCATGAAC TACTTA TGCTAATAAAC
Bridge-1	GCGCGACGGAAAGTATCACTGTCATGTCGCGCGTAGGGCTGGC
Bridge-2	CCGCGCTGAGGGAAAGTATCACTGTCATGTCAGCCGGTAGGGCTGG C
Bridge-3	CCGCGCATGGGAAAGTATCACTGTCATGTCATGCGCGTAGGGCTG G GC
Bridge-4	CCGCGCGACAAAGTATCACTGTCATGTCGCGCGTAGGGCTGGC
Bridge-5	CCGCGCATGGAAAGTATCACTGTCATGTCATGCGCGTAGGGCTGGC
Bridge-6	CCGCGCTGAGGAGCTAGAAGTTATTCTAGCGCGTAGGGCTGC
Bridge-7	CCGCGCGAGGCTAGAAGTTATTCTAGCGCGTAGGGCTGGC
Bridge-8	CCGCGCCCACCATGCCTATATCCTGAATGGCGCGTAGGGCTGGC
Bridge-9	CCGCGCCAATGCCTATATCCTGAATGGCGCGTAGGGCTGGC
Bridge-10	CCGCGCTACGCCGTAGGGCTGTGGTAGCGCGTAGGGCTGGC
Bridge-11	CCGCGCTACCCGTAGGGCTGTGGTAGCGCGTAGGGCTGGC
Bridge-12	CCGCGCACCGACTCAGCTGTTACAGGTGCGCGTAGGGCTGGC

Name	Sequences (5'→3')
Bridge-13	CCCGCGACCACTCAGCTGTTACAGGTGCGCGTAGGGGCTGGC
Bridge-14	CCCGCGGGTCACTCACTGATGAACACCGCGCGTAGGGGCTGGC
Bridge-15	CCCGCGGGTACTCACTGATGAACACCGCGCGTAGGGGCTGGC
FP-1	GCAACTGGAGCCAAGAAGA
RP-1	GAACCAGGTGCATTGTTAAC
FP-2	CACACAAATTACTAGCATCAG
RP-2	GTTTATTAGCATAAGTAGTTCAT
ssDNA-1	TTTTACTTGTCTGTCATTGGCTGTTACTCTTCTGGCTCCAGTGCA GG
ssDNA-2	CTGGTATTGAACACTTAGTAAAAGAACCGAGGTGCATTGTTAACTCA GCTCTGGG
ssDNA-3	GTCCTCTCCTCATTCCGTGATGCTAGTAATTGTGTGTTCTCT TTG TTC TTA ATC AAT ATA GC
ssDNA-4	GATATAGTTGTGTTATTAGCATAAGTAGTCATGATAATTGCCGTT CTCTT TTTAA

The point mutations in the sequences are indicated in red.

1. Optimization of the bridge design of five other mutation points

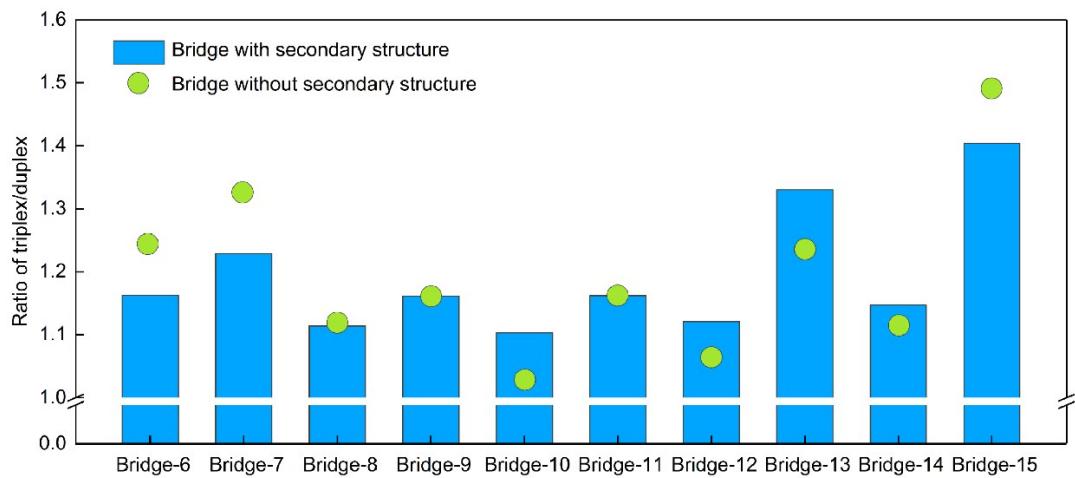


Figure S1. Choose the best Bridge strands of *BRCA1*/c.5152+66G>A, *RCA1*/c.2612C>T, *BRCA2*/c.7397T>C, *BRCA2*/c.8755-66T>C, *BRCA2*/c.2971A>G mutation points by comparing the calculated values with the experimental values.

2. Schematic illustration of the ssDNA strand strategy

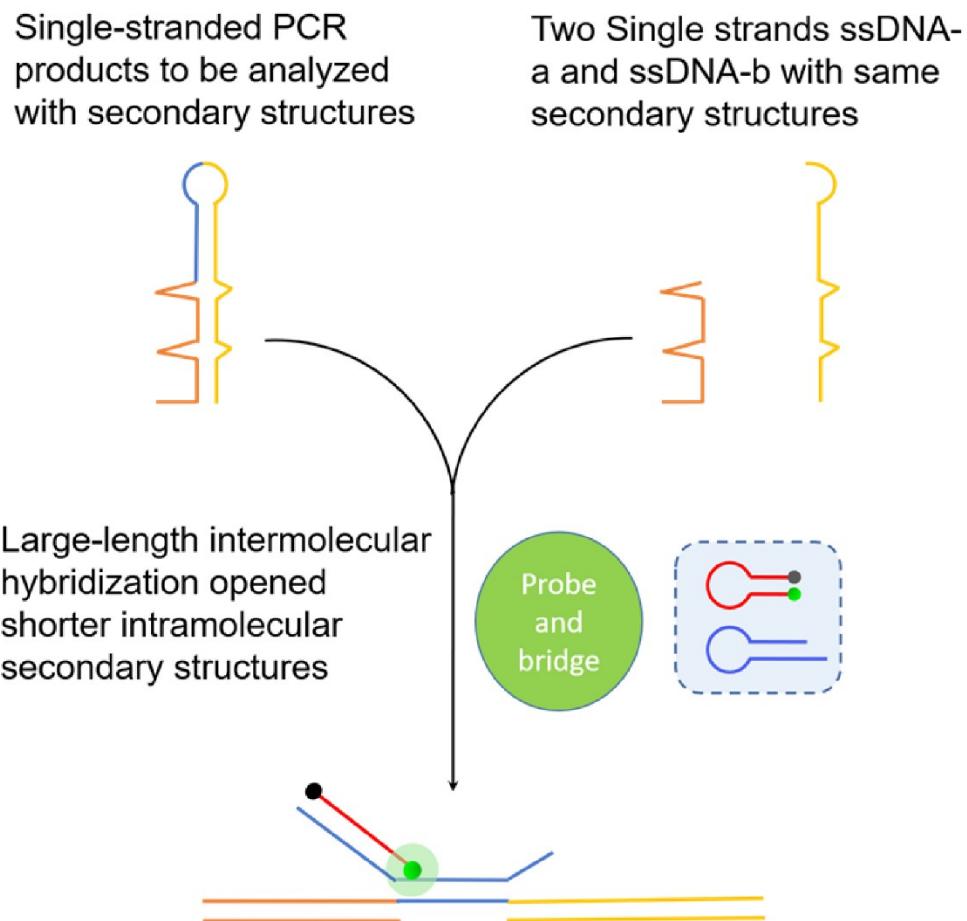


Figure S2. two single-stranded strands ssDNA-a and ssDNA-b were designed to eliminate the influence of the secondary structure on the detection performance. After asymmetric PCR of genomic DNA, ssDNA-a and ssDNA-b were added at 1, 2, 4, and 8 times the bridge concentration. The results showed 4 times the concentration of ssDNA-a and ssDNA-b can get a better discrimination effect.

3. Sanger sequencing of mutations from genomic DNA of ovarian cancer patient and normal genomic DNA from normal after asymmetric PCR.

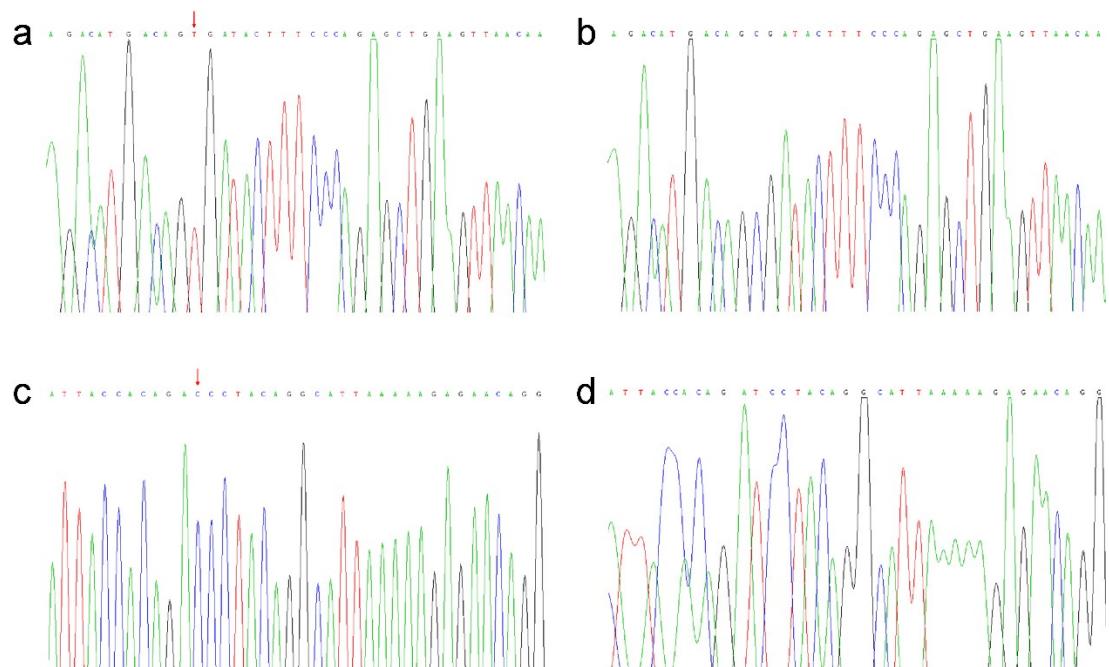


Figure S3. (a) *BRCA1*/c.2082C>T mutation from genomic DNA of ovarian cancer patient 1. (b) *BRCA1*/c.2082C>T of normal genomic DNA from normal people. (c) *BRCA2*/c.7397T>C mutation from genomic DNA of ovarian cancer patient 2. (d) *BRCA2*/c.7397T>C of normal genomic DNA from normal people. (Mutated bases are marked with red arrows).