Silicone dielectric elastomers optimized by crosslinking pattern - a simple approach to high-performance actuators.

Codrin Tuguia*, George-Theodor Stiubianua, Manole-Stelian Serbulea^{b,c}, Maria Cazacua

^aInorganic Polymers Department, Petru Poni Institute of Macromolecular Chemistry, Aleea Grigore Ghica Voda 41A, 700487, Iasi, Romania

^bTechnical University of Civil Engineering Bucharest, Soil Mechanics and Foundation Engineering Department, bd. Lacul Tei 122, sector 2, 022396, Bucharest, Romania ^cGeotechnical Expert S.R.L., str. Fabrica de Gheață 16-18, ap. 55, sector 2, 022540, Bucharest, Romania

Email: tugui.codrin@icmpp.ro



Figure S1. Molecular weight of A1, A2 and A3 determined by GPC.







Figure S3. GPC data and NMR spectrum of polymer B2.



Figure S4. GPC data and NMR spectrum of polymer B3.



Figure S5. NMR spectrum of polymer C1.



Figure S6. NMR spectrum of polymer C2.



Figure S7. GPC data and NMR spectrum of polymer X1.



Figure S8. GPC data and NMR spectrum of polymer X3.



Figure S9. GPC data and NMR spectrum of polymer X2.



Figure S10. The actuator configuration for lateral strain measurements.



Figure S11. The amount of soluble fraction extracted from films.



Figure S12. The average molecular weight of polymer chains between two consecutive junctions.



Figure S13. Cyclic stress-strain curves (top) and the corresponding stress relaxation (bottom) for Series R1.



Figure S14. Cyclic stress-strain curves (top) and the corresponding stress relaxation (bottom) for Series R2.



Figure S15. Cyclic stress-strain curves (top) and the corresponding stress relaxation (bottom) for Series R3.



Figure S16. Cyclic stress-strain curves (top) and the corresponding stress relaxation (bottom) for Series R4.

In actuation mode, when an electric field is applied on film made of dielectric material, the Maxwell pressure generated between the two electrodes is given by:

$$\boldsymbol{p} = \boldsymbol{\varepsilon} \boldsymbol{\varepsilon}_0 \boldsymbol{E}^2 \tag{1}$$

where p is the electrostatic pressure across the electrodes, ε is the relative permittivity, ε_0 is the permittivity of the free space and E^2 represents the electric fields applied on electrodes. If we use the linear-elasticity and boundary approximations, the actuation strain in z direction (thickness) is given by:

$$s_z = -\frac{p}{Y} \tag{2}$$

where *Y* represents the Young's modulus.

Considering the elastomers are incompressible At=const, where A represents the area of the electrodes, t is the thickness of the dielectric film placed between electrodes, thereby it is possible to determine the actuated thickness of the elastomer t_1 :

$$\boldsymbol{t}_1 = \boldsymbol{t}_0 - (\boldsymbol{s}_z \cdot \boldsymbol{t}_0) \tag{3}$$

where t_0 is the thickness of initial unactuated elastomer.

The actuated diameter of the electrodes will be:

$$\boldsymbol{d}_1 = \sqrt{\frac{\boldsymbol{d}_0^2 \cdot \boldsymbol{t}_0}{\boldsymbol{t}_1}} \tag{4}$$

where d_0 and d_1 are the initial and the final diameter of the circular electrode.

The theoretical in plane actuation (lateral actuation) s_x was calculated with the formula:

$$s_x = \frac{d_1 - d_0}{d_0} \cdot 100 \tag{5}$$

We substitute equation (1) in equation (2), then substitute equation (2) in (3), then we substitute (4) in equation (5) and we obtain the equation mentioned in the paper (numbered as equation 6):

$$s_{x} = \frac{\sqrt{\frac{d_{0}^{2} \cdot t_{0}}{t_{0} - \left(\frac{\boldsymbol{\varepsilon} \cdot \boldsymbol{\varepsilon}_{0} \cdot \boldsymbol{E}^{2}}{\boldsymbol{Y} \cdot \boldsymbol{t}_{0}\right)}} - d_{0}}{d_{0}} \cdot 100$$



Figure S17. Young's modulus values of R1-1, R2-1, R3-1 and R4-3 determined from stress-strain curves within 0 - 20% and 20 - 35%, strain, respectively.