

Supplementary Information

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The carbon balance was calculated according to equation S1†.

$$C - \text{balance} = \frac{\dot{n}_{CO,in} + \dot{n}_{CO_2,in} - (\dot{n}_{MeOH,out} + 2 * \dot{n}_{DME,out} + \dot{n}_{CO,out} + \dot{n}_{CO_2,out} + v_x \dot{n}_{C_xH_y})}{\dot{n}_{CO,in} + \dot{n}_{CO_2,in}} \quad (\text{S1})$$

The measuring procedure with purging and reference point repetition is shown in Fig. S1†.

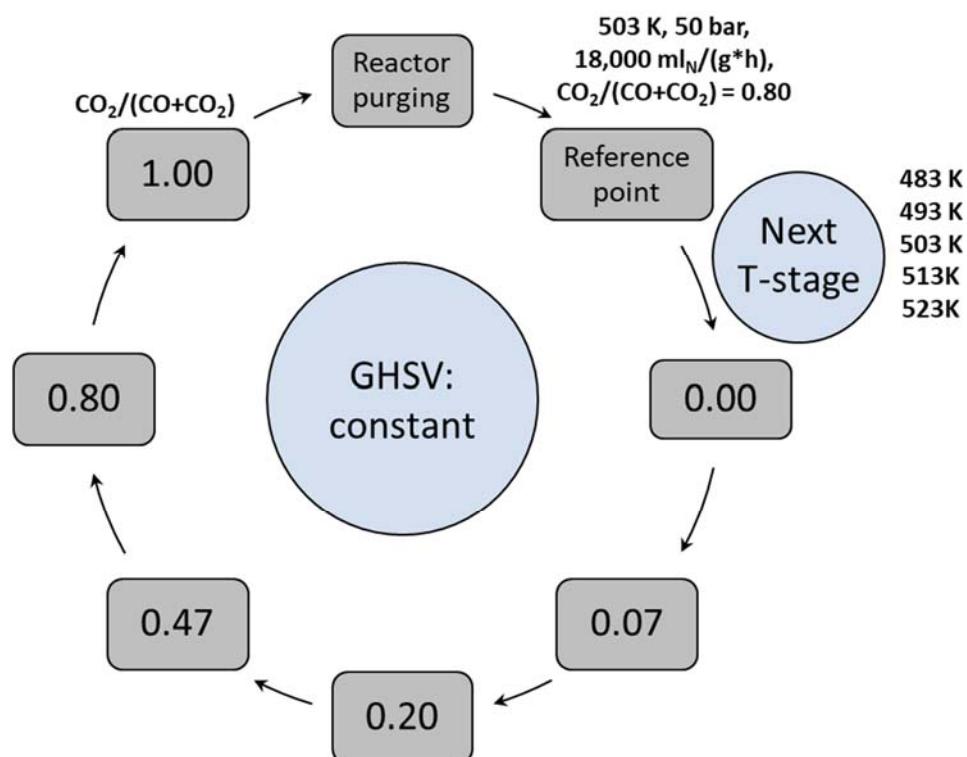


Fig. S1: Schematic illustration of the procedure of varying reaction conditions at a constant GHSV with recurring reference point at 50 bar.

All reaction conditions in this work were strongly, kinetically controlled due to the large distance to equilibrium (Fig S2†), exemplified by the CO_x conversion at the reaction conditions shown in main manuscript (Figure 2 a).

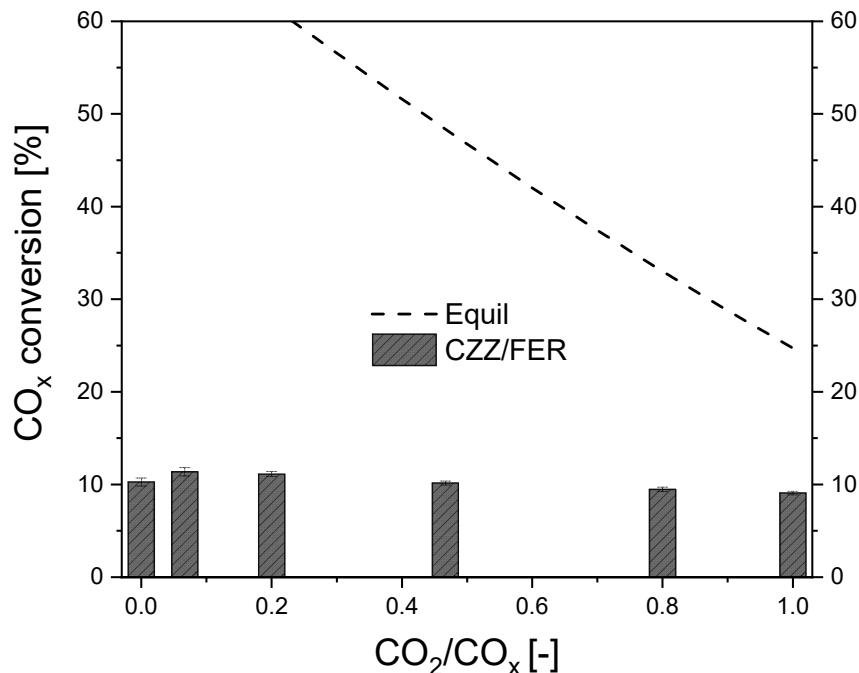


Fig. S2: CO_x conversion with CZZ/FER (1:1 wt%) (black bars) under variation of the CO₂/CO_x inlet ratio at 50 bar, 523 K and 36 000 mLN/(g·h).and the respective equilibrium curve calculated via ASPEN PLUS.

An overview of the influence of the CO₂/CO_x inlet-ratio on selectivity, CO/CO₂ conversion and MeOH/DME productivity can be found in Table S1†.

Table S1: Effect of CO₂/CO_x inlet-ratio with the use of CZZ/FER 1:1 wt% on the CO₂ and CO conversion, the DME, MeOH, CO₂ and CO selectivity, and the DME and MeOH productivity. Measurement conditions: GHSV: 18 000 mL_N/(g*h), 50 bar and 523 K.

Inlet-ratio/-	Conversion/ %				Selectivity/ %			Productivity/ g _i /(kg _{Cu} *h)	
	CO ₂ /CO _x	CO ₂	CO	DME	MeOH	CO ₂	CO	DME	MeOH
0.00	<0	25.2	58.6 ^b	1.4	32.9	<0	643.1	21.3	
0.07	<0	26.9	64.3 ^b	1.9	28.6	<0	684.1	28.1	
0.20	<0	27.9	69.8 ^b	3.4	23.3	<0	659.7	44.5	
0.47	<0	30.0	88.3 ^b	7.6	2.3	<0	586.2	69.8	
0.80	13.2	15.4	85.8 ^a	13.6	<0	<0	468.1	103.6	
1.00	20.9	<0	42.3 ^c	8.5	<0	49.1	364.0	101.3	

a: Eq 5, b: Eq 6, c: Eq 7