

Supplementary Materials for  
**Mixed Conductive Composites for ‘Low-Temperature’ Thermochemical CO<sub>2</sub>  
Splitting and Syngas Generation**

The PDF file includes:

**Fig. S1** XRD patterns of CGCO/LNF at different ratios 20/80; 46/60; 80/20.

**Fig. S2** Weight loss of mixed conductive composites CGCO/LNF 60/40 in (a) CH<sub>4</sub> TPR and (b) H<sub>2</sub> TPR.

**Fig. S3** Kinetics TA- DTG Redox Material mass change in the 5% CH<sub>4</sub>/Ar for reduction step for cycled CGCO (100/0), CGCO/LNF (80/20, 60/40, 40/60, 20/80), LNF (0/100), at the temperature of 750°C, 700 °C, 650 °C, 600 °C. (a) redox cycle (b) reduction, and (c) oxidation step.

**Fig. S4** Apparent activation energies of methane-POx for CGCO, LNF, and CGCO/LNF 60/40.

**Fig. S5** Effect of temperature on the reactivity of (a)CGCO and (b)LNF.

**Fig. S6** Effect of (a) temperature and (b) different ratios of CGCO and LNF on the coke formation of CGCO/LNF (H<sub>2</sub>/CO ratio).

**Fig. S7** *In-situ* XRD patterns of (a) CGCO and (b) LNF during the three redox cycles at 750°C.

**Table S1** Quantification from Rietveld refinement on standalone CGCO, LNF and CGCO/LNF with CGCO/LNF = 60/40 weight ratio (equal to 67.6/32.4 molar ratio)

**Fig. S8** The intensity ratio of La<sub>2</sub>O<sub>3</sub> at peak 29 and LNF at peak 32.

**Fig. S9** STEM and EDX mappings of (a) fresh and (b) reduced CGCO/LNF 60/40.

**Fig. S10** SEM images of the CGCO/LNF 60/40 fresh and cycled.

**Fig. S11** The absorption signal in six CO pulses.

**Table S2** CO chemisorption for CGCO, LNF, CGCO/LNF 60/40 (sample=0.3 g)

**Table S3** The specific surface areas of CGCO, LNF, and CGCO/LNF 60/40 by BET test.

**Fig. S12** N<sub>2</sub> adsorption/desorption isotherms of CGCO, LNF, CGCO/LNF 60/40.

**Fig. S13** The *in-situ* XRD patterns of CGCO/LNF 60/40 for different redox cycles.

**Fig. S14** The XRD patterns of LNF (fresh and reduced).

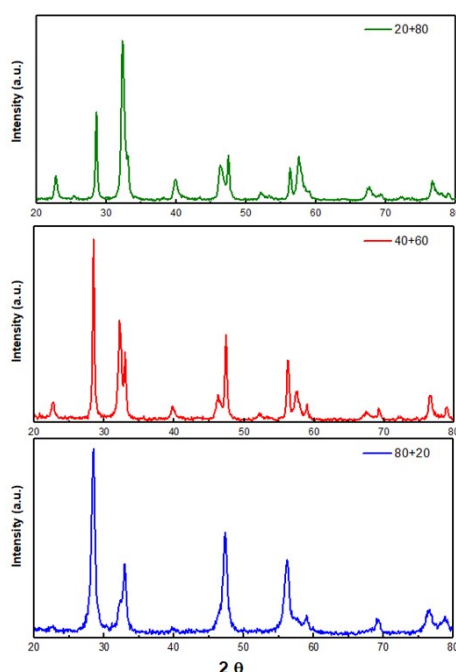
**Fig. S15** Oxygen capacity tested in the TGA reactor (750°C, 700°C, 650°C, 600°C).

**Fig. S16** XRD patterns of the fresh and cycled CGCO/LNF 60/40 after 50 redox cycles.

**Table S4** Performance comparisons of the redox catalyst in this study versus the

recently published redox catalysts on methane POx and CO<sub>2</sub> splitting

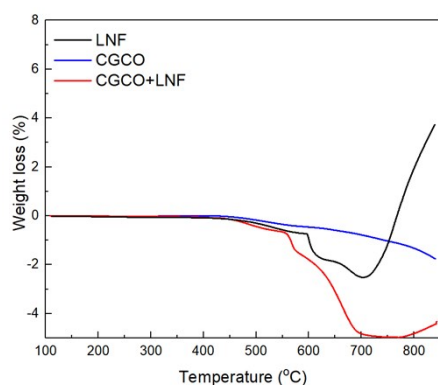
### XRD characterization



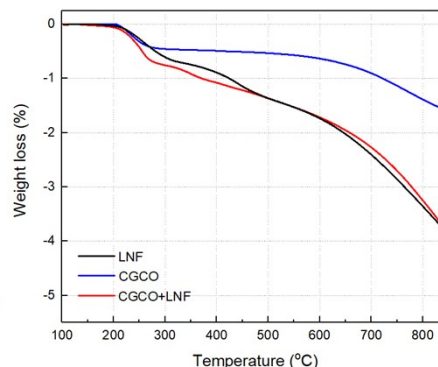
**Fig. S1** XRD patterns of CGCO/LNF at different ratios 20/80; 40/60; 80/20.

TPR demonstrated that the weight loss of CGCO, LNF and CGCO/LNF 60/40 during CH<sub>4</sub>-TPR and H<sub>2</sub>-TPR. It was evident that the weight of LNF in **Fig.S2 (a)** was increased rapidly after 700 °C, indicating the pure LNF was prone to coke in the reducing gas of methane. In compare, the weight of CGCO/LNF 60/40 in the methane atmosphere did not show the apparent weight gain until 800 °C.

To eliminate the influence of coke, the H<sub>2</sub>-TPR experiments were tested to see the weight loss at the temperature range of 100 °C to 850 °C shown in **Fig. S2(b)**. It was observed that the weight loss of CGCO/LNF 60/40 was almost the same as the LNF. Because the weight loss of standalone CGCO is only 1.5%, about 4% weight loss of CGCO/LNF 60/40 might come from the extra oxygen removal of CGCO and LNF in the mixed conductive composites. It indicated that the synergistic effect of the mixed conductive composites could facilitate 1.4% more oxygen removal from the two oxygen suppliers considering the weight ratio of CGCO and LNF.



(a) CH<sub>4</sub>-TPR



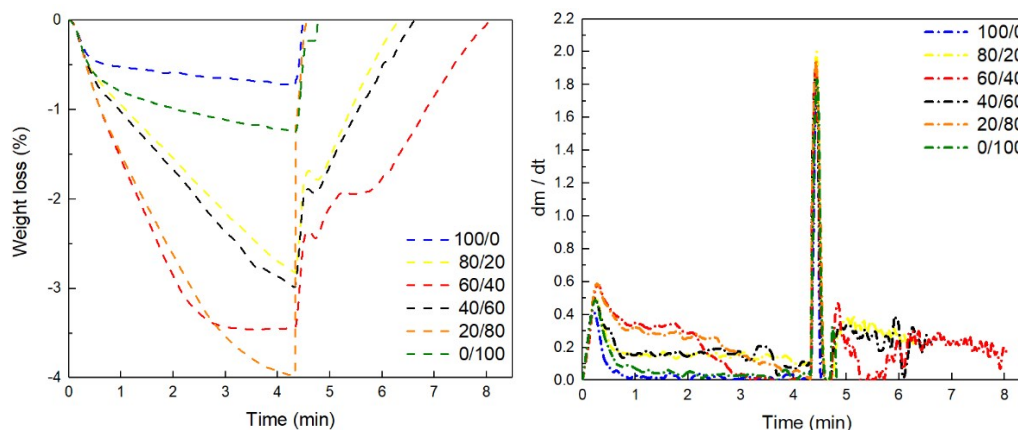
(b) H<sub>2</sub>-TPR

**Fig. S2** Weight loss of mixed conductive composites CGCO/LNF 60/40 in (a) CH<sub>4</sub> TPR and (b) H<sub>2</sub> TPR.

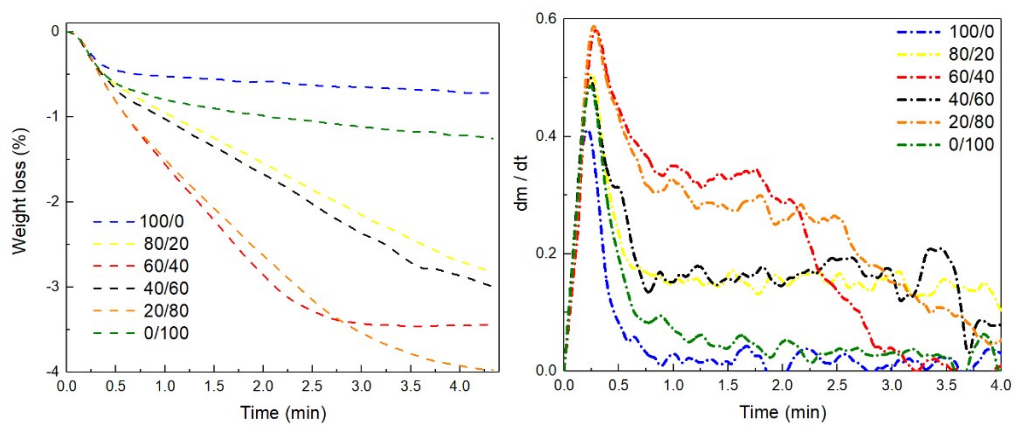
### Isothermal Redox cycles

It showed that the mixed conductive material CGCO/LNF exhibited good kinetics with a higher oxygen migration rate both in reduction and oxidation steps. It was observed that both standalone CGCO and LNF exhibited a single lattice oxygen extraction peak within the first half-minute of methane-PO<sub>x</sub> step (**Fig. S3 750°C**). As a comparison, CGCO/LNF composites exhibited both the lattice oxygen extraction peak at 0.5 min and a “plateau-like” lattice oxygen extraction curve from t = 0.5 min to t = 2.0–4.0 min. This might indicate that the CGCO/LNF composite was “activated” at the beginning of the methane-PO<sub>x</sub> step, following with steady lattice oxygen extraction afterward.

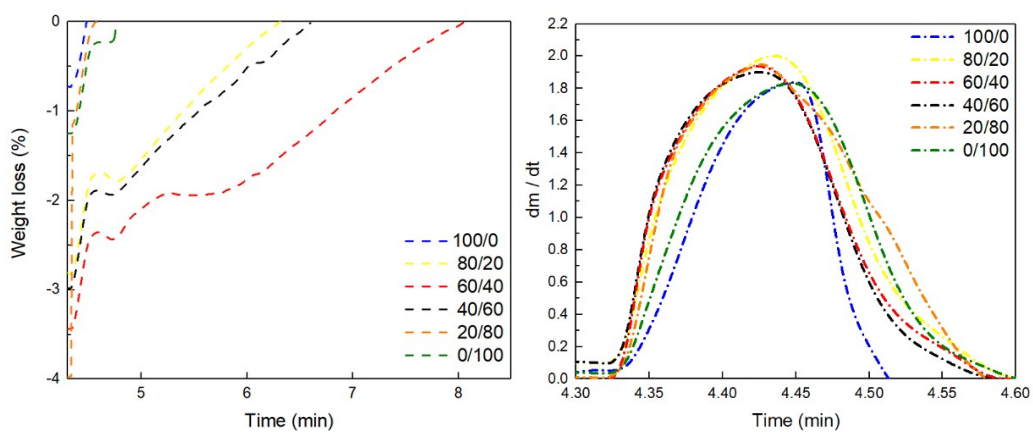
### The kinetics of Reduction and oxidation



(a)

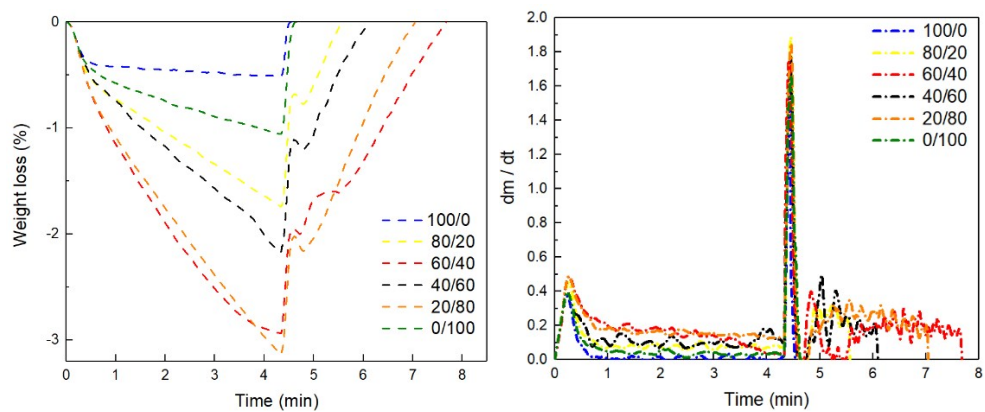


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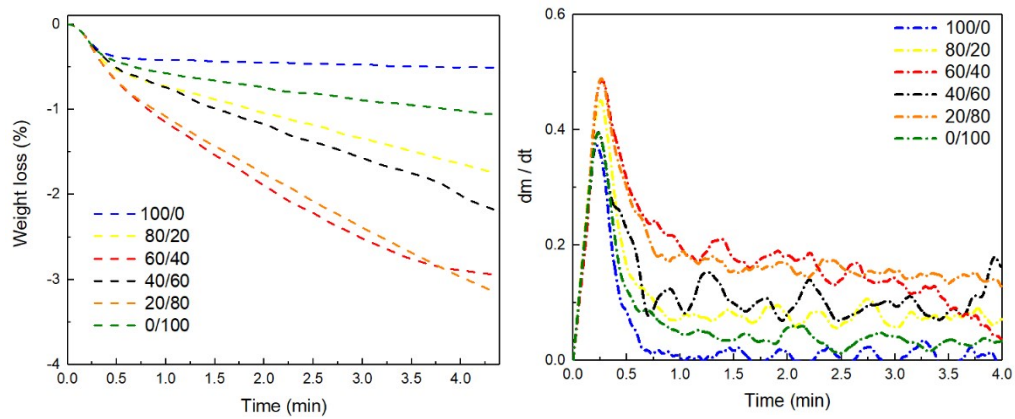


(c)

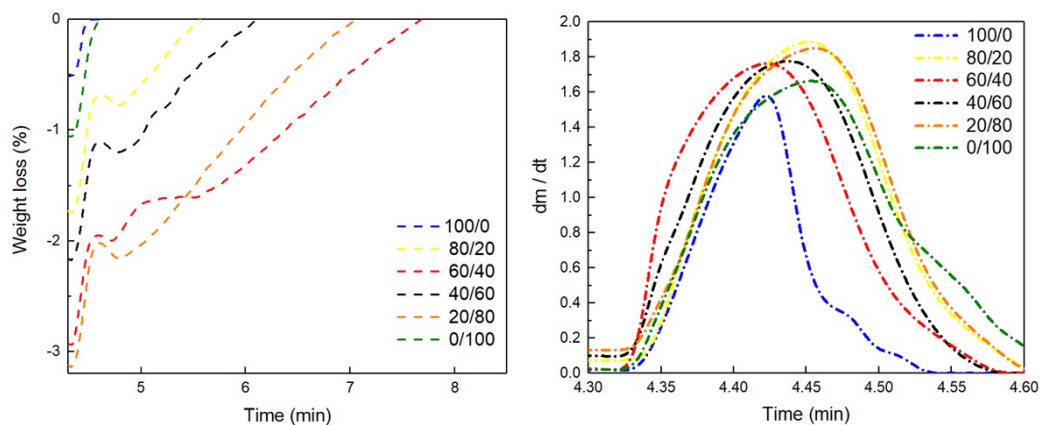
750°C



(a)

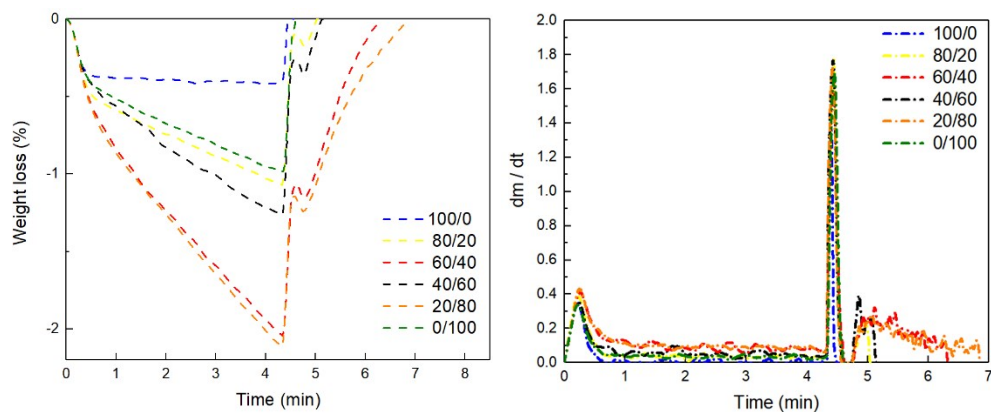


(b)

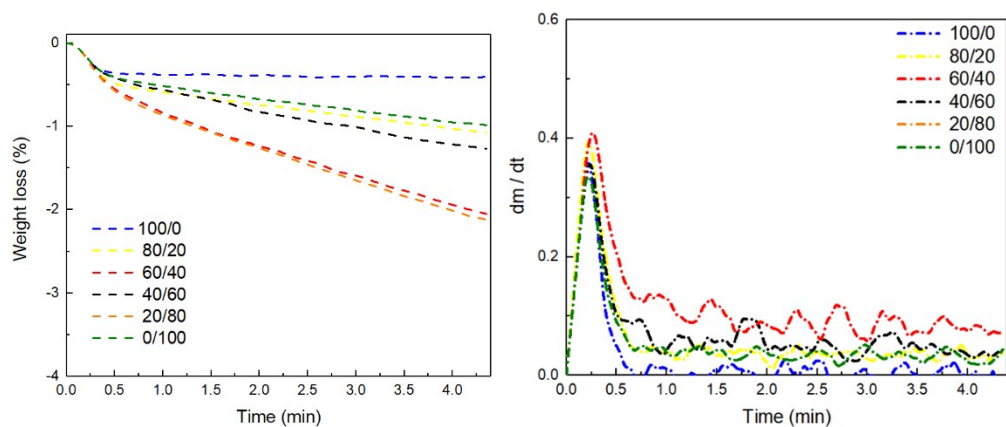


(c)

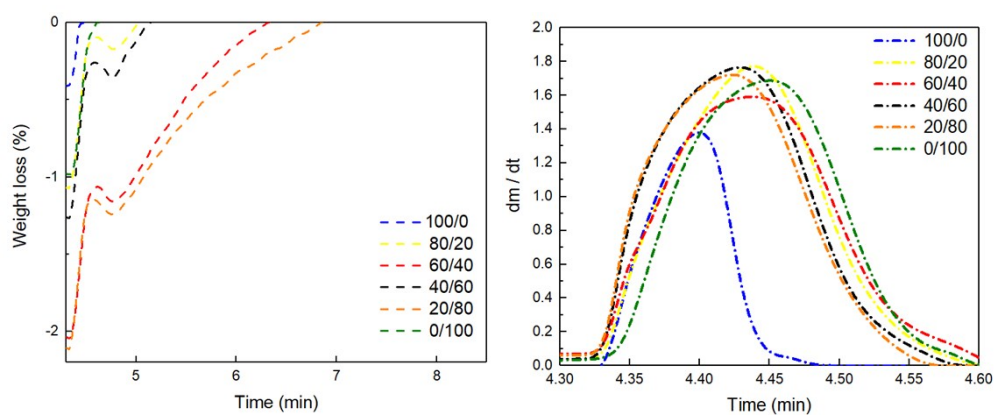
700°C



(a)

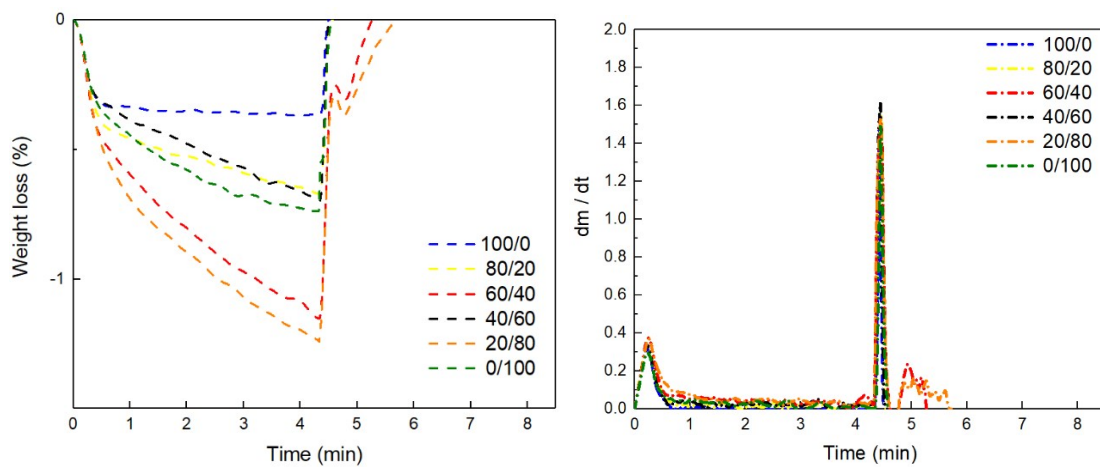


(b)



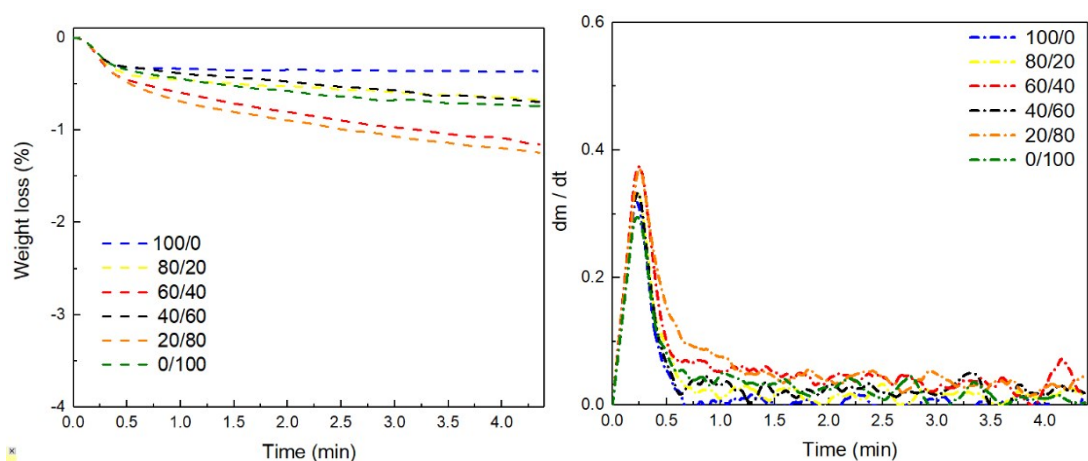
(c)

650°C

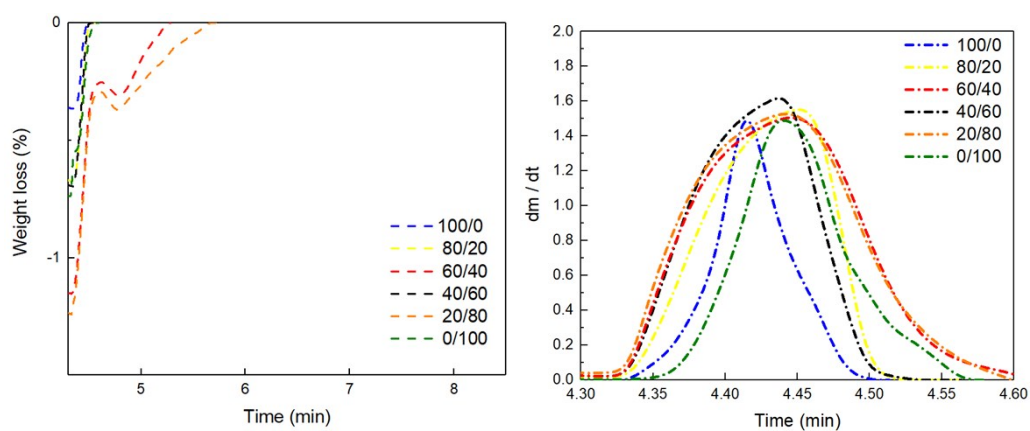


(a)





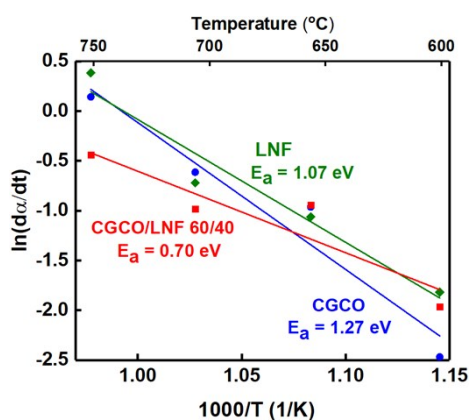
(b)



(c)

600°C

**Fig. S3** Kinetics TA- DTG Redox Material mass change in the 5% CH<sub>4</sub>/Ar for reduction step for cycled CGCO (100/0), CGCO/LNF (80/20, 60/40, 40/60, 20/80), LNF (0/100), at the temperature of 750°C, 700 °C, 650 °C, 600 °C. (a) redox cycle and (b) reduction, and (c) oxidation step.



**Fig. S4** Apparent activation energies of methane POx for CGCO, LNF, and CGCO/LNF 60/40.

**Analysis** of the apparent activation energy of the methane POx process.

The methane reduction kinetics of CGCO, LNF and CGCO/LNF 60/40 can be compared in terms of dimensionless conversion ( $\alpha$  vs.  $t$ ) and its derivative ( $d\alpha/dt$  vs.  $\alpha$ ). A model-free (isoconversional) kinetics method<sup>1</sup> were used on the processed TGA data in order to obtain approximate activation energy and qualitative insights for the reduction of CGCO, LNF and CGCO/LNF 60/40 by methane. According to the

equation: 
$$\left[ \frac{\partial \ln \left( \frac{d\alpha}{dt} \right)}{\partial T^{-1}} \right]_{\alpha} = - \frac{E_a}{R} \quad (\alpha = \text{const}),$$
 the temperature dependence of the isoconversional reaction rate can be used to evaluate isoconversional values of the activation energy. We determined the activation energies at several fixed conversion numbers between 20% and 50% (the rates at initial and final reaction stages are less reliable). Similar apparent activation energies were obtained at different conversion numbers selected. In **Fig. S4**, we illustrated 40% conversion as the calculation standard, where the activation energy was best approximated by the average value. Finally, the activation energy of methane reduction on standalone CGCO, LNF and the mixed composite CGCO/LNF 60/40 were calculated by the isoconversional method over the temperature range from 600 °C to 750 °C.

### Definition of reactivity parameters

The results of partial oxidation of methane and CO<sub>2</sub> splitting at 750 °C are shown in **Fig. 4** by using CH<sub>4</sub> conversion, CO selectivity, CO<sub>2</sub> conversion, and O extracted. For the experiments, the methane and CO<sub>2</sub> conversion are defined as:

$$CH_4 \text{ conversion } \% = \frac{\text{Moles of } CH_4 \text{ consumed}}{\text{Moles of } CH_4 \text{ introduced}} * 100\% \quad (1)$$

$$CO_2 \text{ conversion } \% = \frac{\text{Moles of } CO_2 \text{ consumed}}{\text{Moles of } CO_2 \text{ introduced}} * 100\% \quad (2)$$

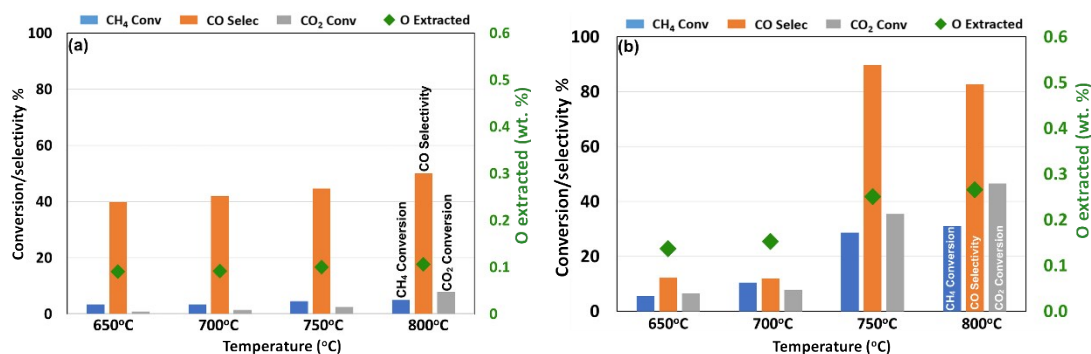
The CO selectivity is defined as:

$$CO \text{ selectivity } \% = \frac{\text{Moles of } CO \text{ produced}}{\text{Moles of } CO \text{ and } CO_2 \text{ produced}} * 100\% \quad (3)$$

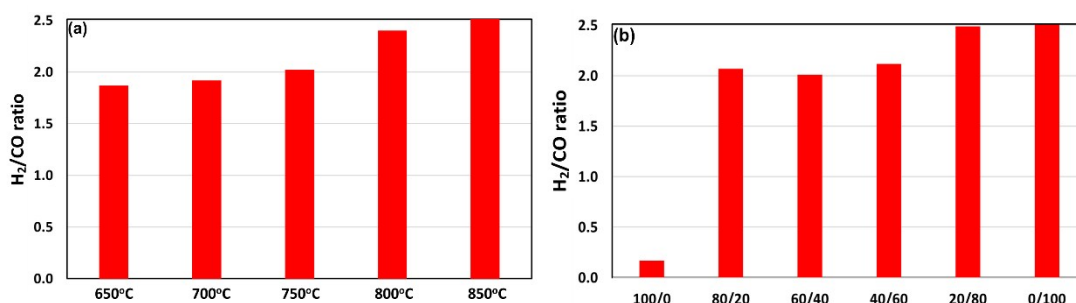
The O extracted wt. % is defined as:

$$O \text{ extracted } \% = \frac{\text{Moles of } CO \text{ produced} + 4 * \text{Moles of } CO_2 \text{ produced}}{\text{Total moles of O}} * 100\% \quad (4)$$

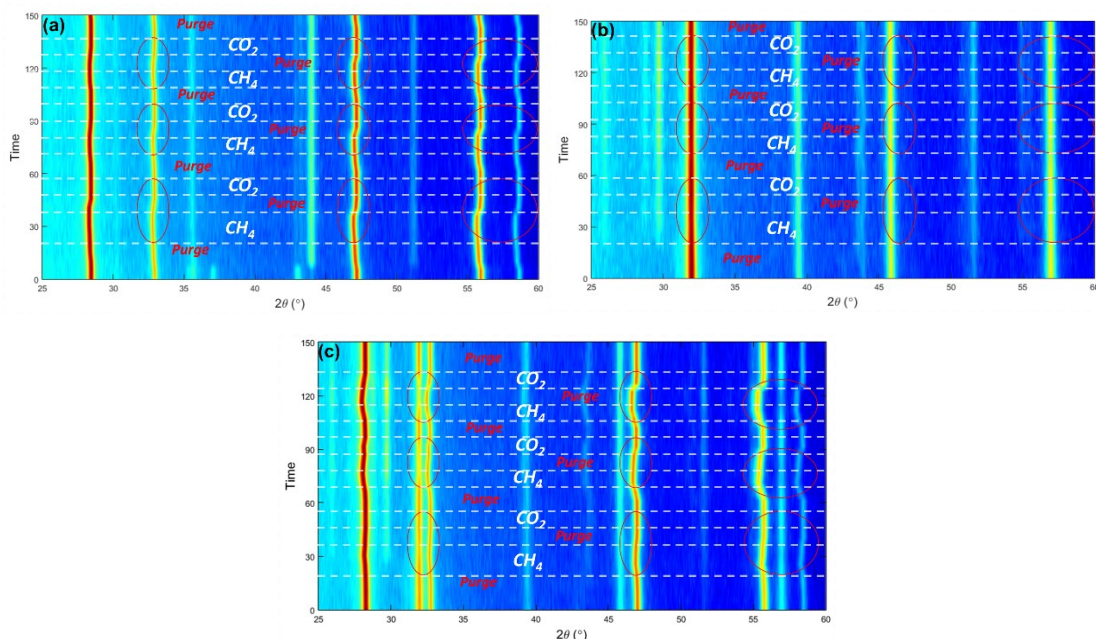




**Fig. S5** Effect of temperature on the reactivity of (a) CGCO and (b) LNF.



**Fig. S6** Effect of (a) temperature and (b) different ratios of CGCO and LNF on the coke formation of CGCO/LNF (H<sub>2</sub>/CO ratio).

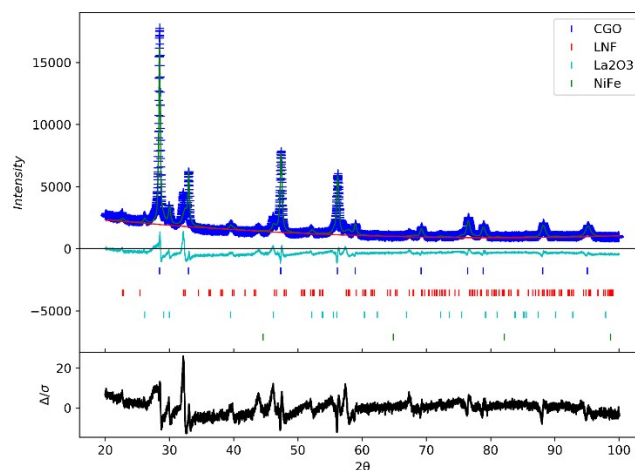


**Fig. S7** *In-situ* XRD patterns of (a) CGCO and (b) LNF during the three redox cycles at 750°C; (c) CGCO/LNF 60/40 for three redox cycles.

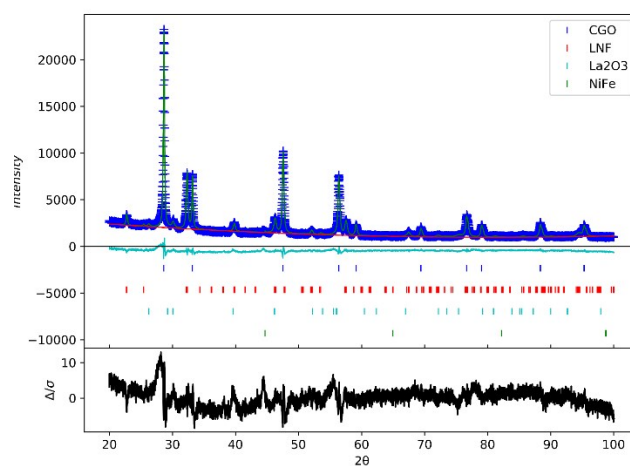
**Table S1.** Quantification from Rietveld refinement on standalone CGCO, LNF and CGCO/LNF with CGCO/LNF = 60/40 weight ratio (equal to 67.6/32.4 molar ratio)

Oxygen extraction from the oxygen recourse			
Standalone CGCO	Standalone LNF	CGCO in CGCO/LNF	LNF in CGCO/LNF

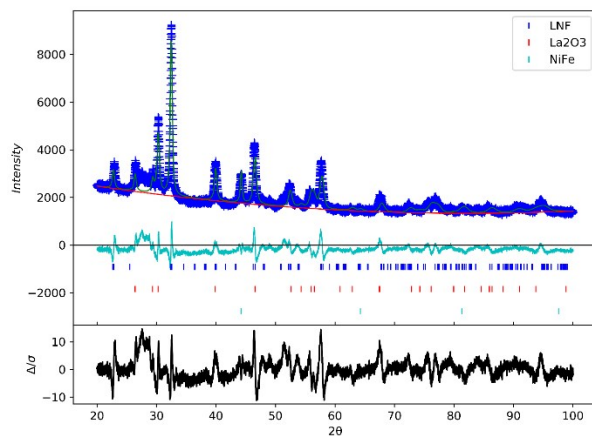
Rietveld refinement	0.86 wt.%	0.86 wt.%	3.81 wt.%	1.88 wt.%
Experimental (TGA)	0.65 wt.%	1.03 wt.%	NA	NA
<b>Total oxygen extraction from CGCO/LNF 60/40</b>				
Rietveld refinement	0.68*3.81 wt.% + 0.32*1.88 wt.%		3.18 wt.%	
Experimental (TGA)	NA		3.4 wt.%	



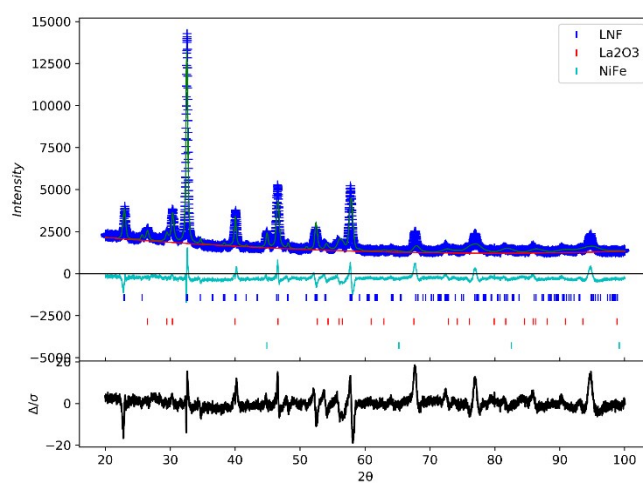
CGCO-LNF reduced



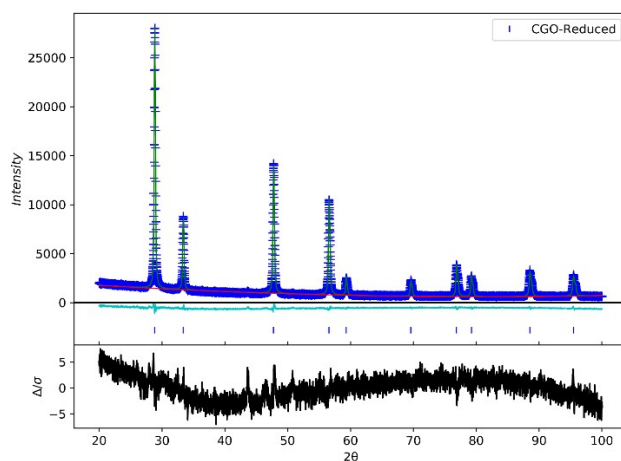
CGCO-LNF oxidized



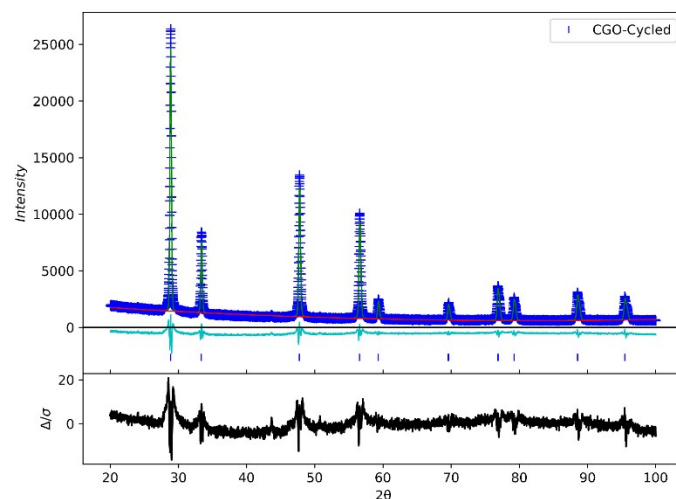
LNF reduced



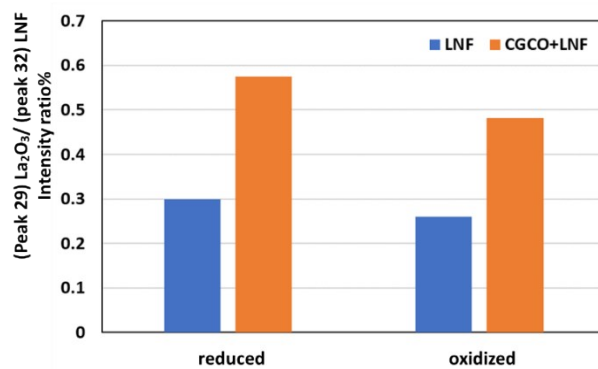
LNF oxidized



CGCO reduced

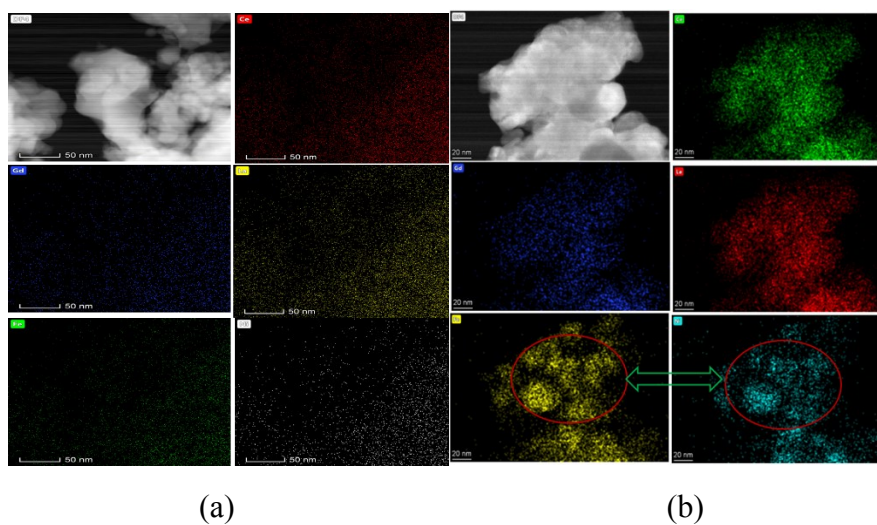


CGCO oxidized



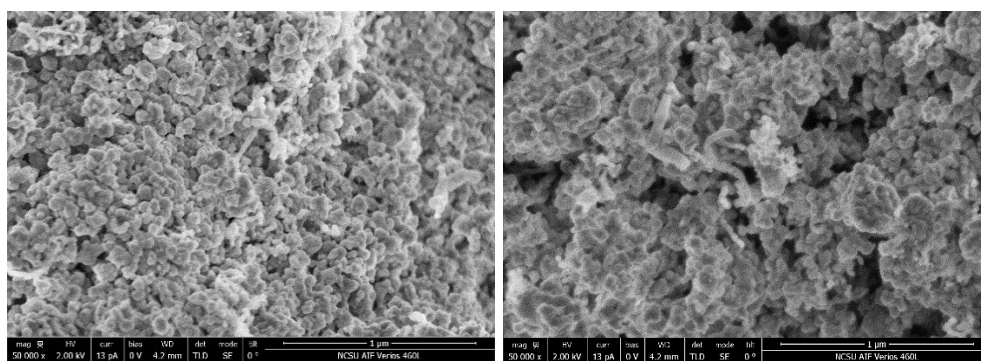
**Fig. S8** The intensity ratio of  $\text{La}_2\text{O}_3$  at peak 29 and LNF at peak 32.

## TEM

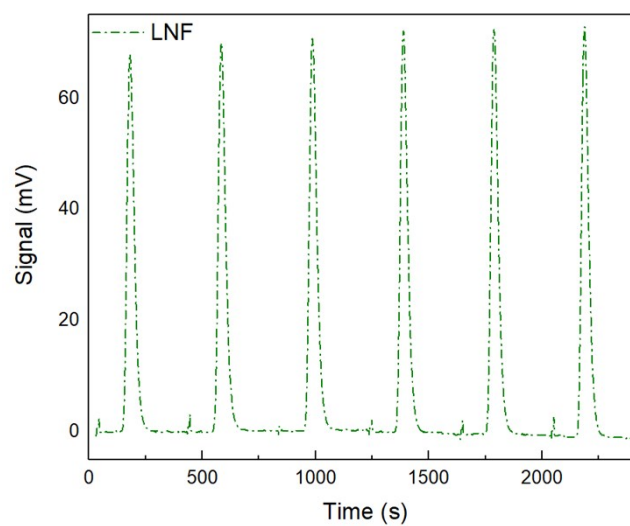
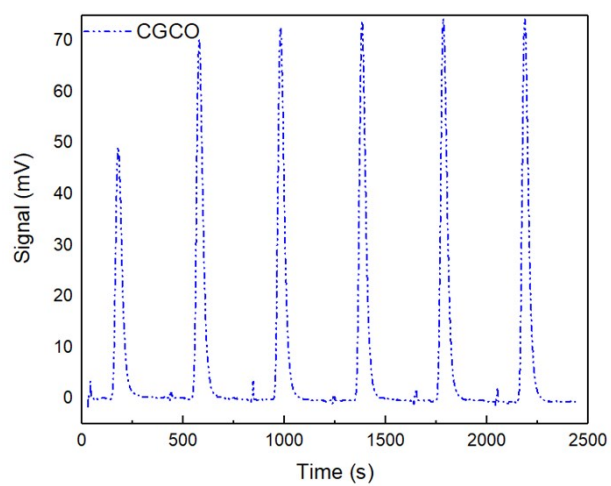


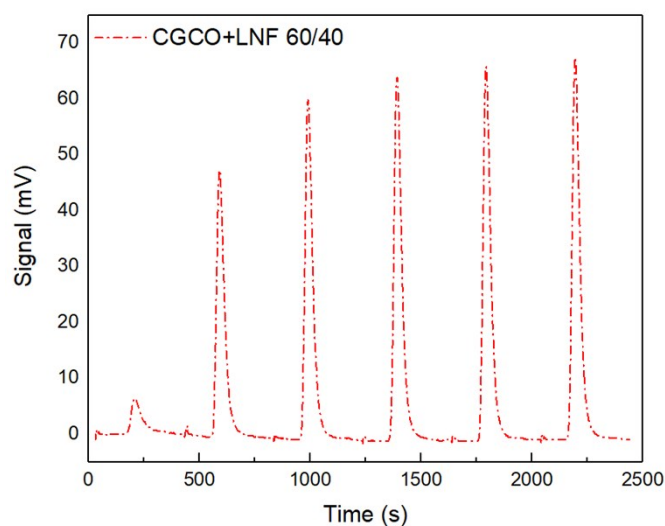
**Fig. S9** The STEM and EDX mappings of (a) fresh and (b) reduced CGCO/LNF 60/40.

## SEM



**Fig. S10** SEM images of the CGCO/LNF 60/40 fresh and cycled.





**Fig. S11** The absorption signal in six CO pulses.

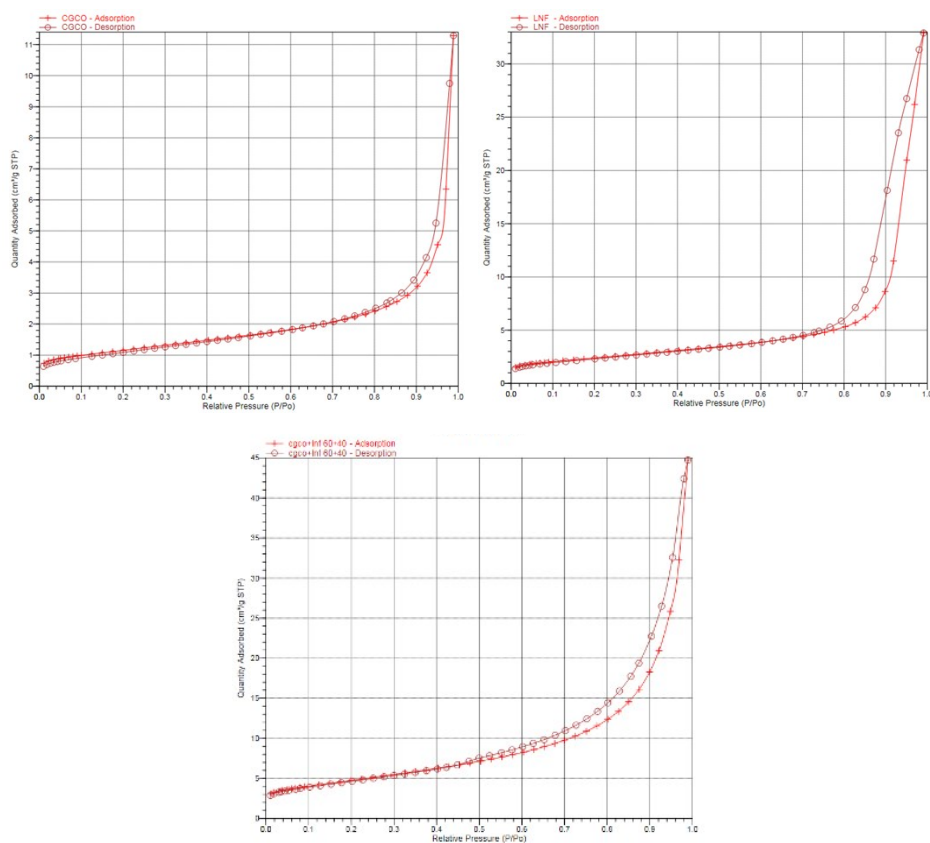
**Table S2.** CO chemisorption for CGCO, LNF, CGCO/LNF 60/40 (sample=0.3 g)

	CO adsorption (mol)			Total CO adsorption (mol g <sup>-1</sup> )
	1 <sup>st</sup> pulse	2 <sup>nd</sup> pulse	3 <sup>rd</sup> pulse	
CGCO	$9.99 \times 10^{-7}$	$1.58 \times 10^{-7}$	$4.52 \times 10^{-8}$	$4.01 \times 10^{-6}$
LNF	$2.46 \times 10^{-7}$	$9.14 \times 10^{-8}$	$7.10 \times 10^{-9}$	$1.10 \times 10^{-6}$
CGCO/LNF 60/40	$2.57 \times 10^{-6}$	$7.83 \times 10^{-7}$	$2.65 \times 10^{-7}$	$1.21 \times 10^{-5}$

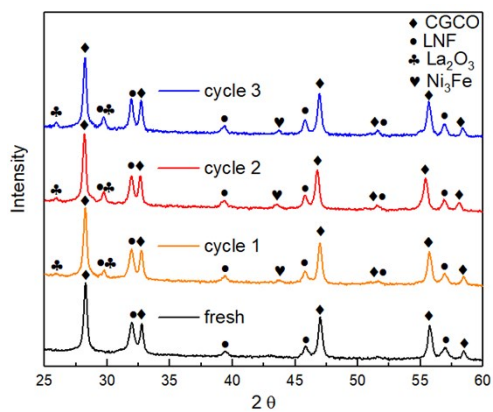
**Table S3.** The specific surface areas of CGCO, LNF, and CGCO/LNF 60/40 by BET test

	BET surface area (m <sup>2</sup> /g)
CGCO	4.02
LNF	8.35
CGCO/LNF 60/40	17.09



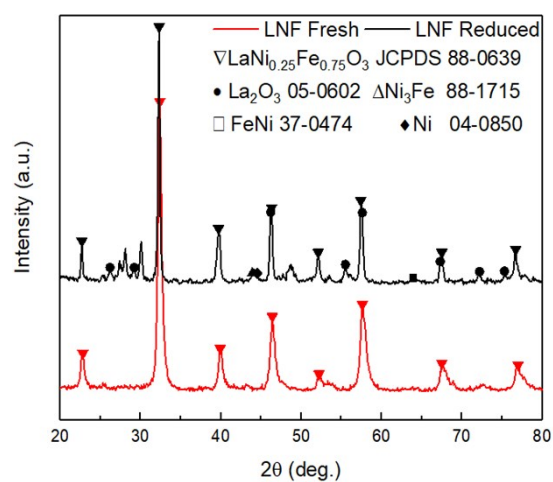


**Fig. S12** N<sub>2</sub> adsorption/desorption isotherms of CGCO, LNF, CGCO/LNF 60/40.

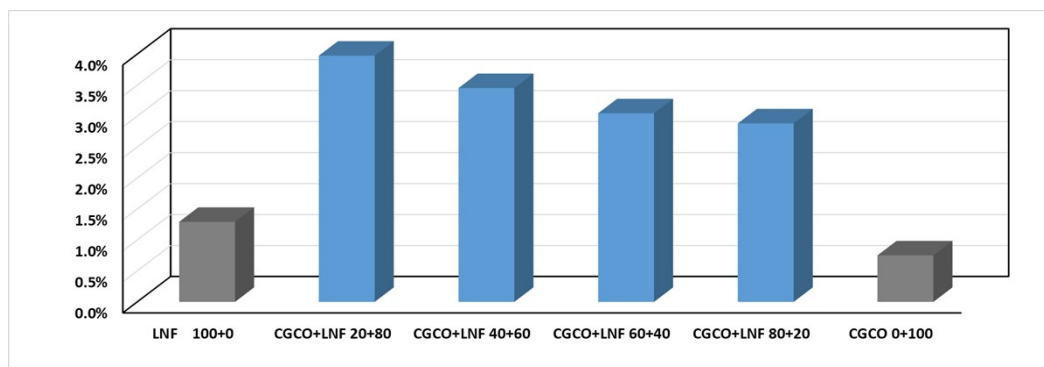
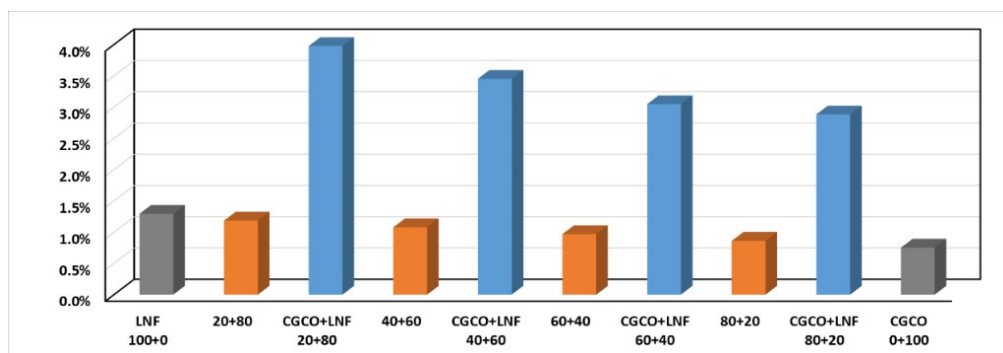


**Fig. S13** *In-situ* XRD patterns of CGCO/LNF 60/40 for different redox cycles.

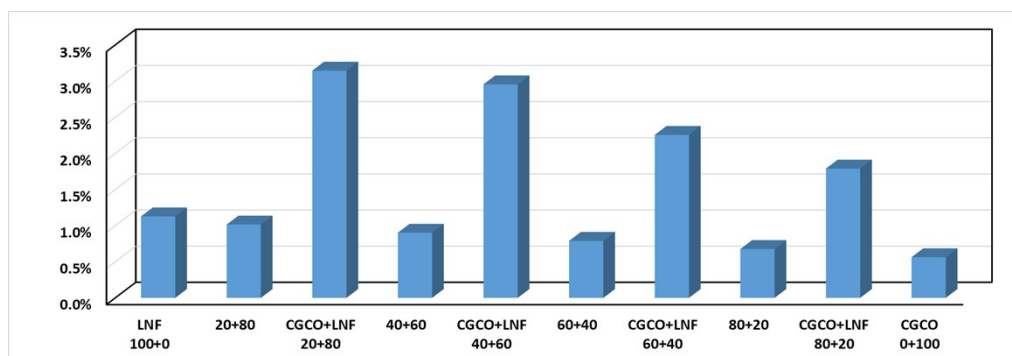


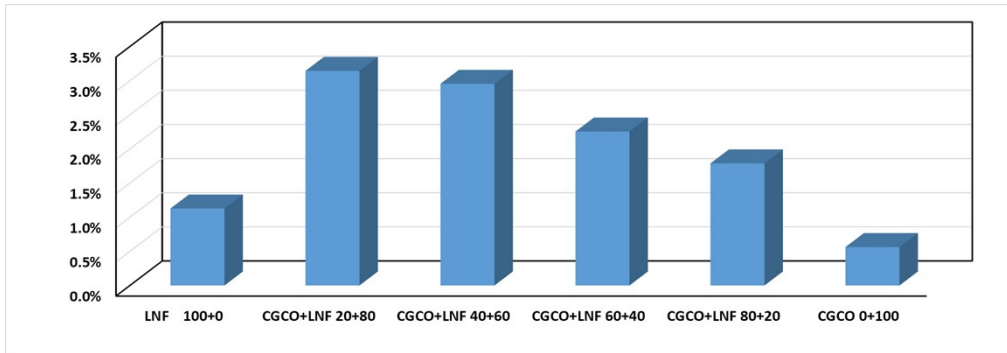


**Fig. S14** XRD patterns of LNF (fresh and reduced).

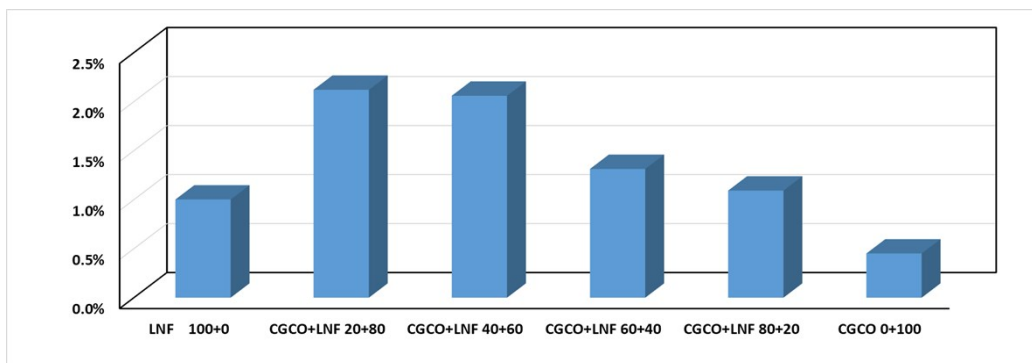
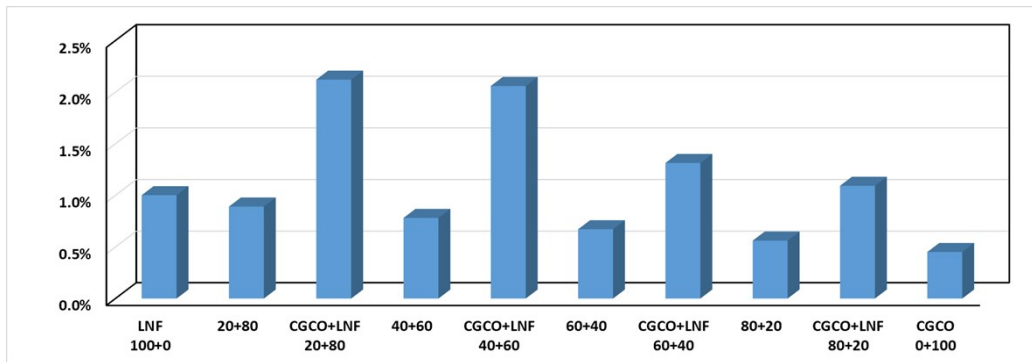


750 °C

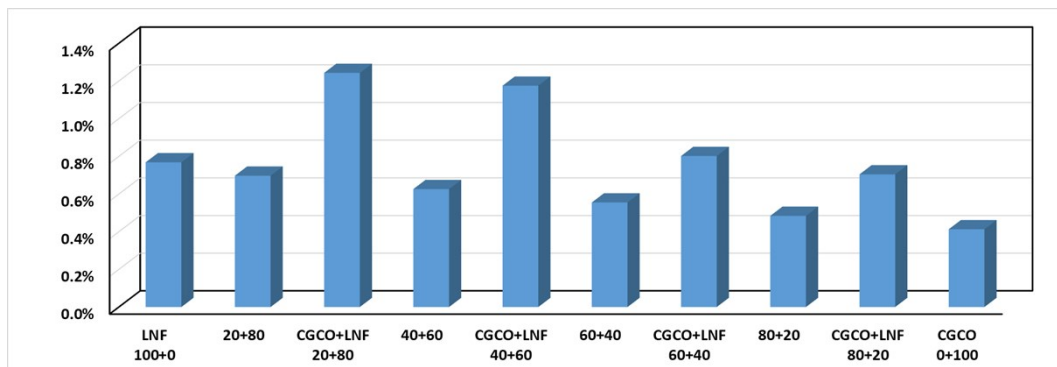


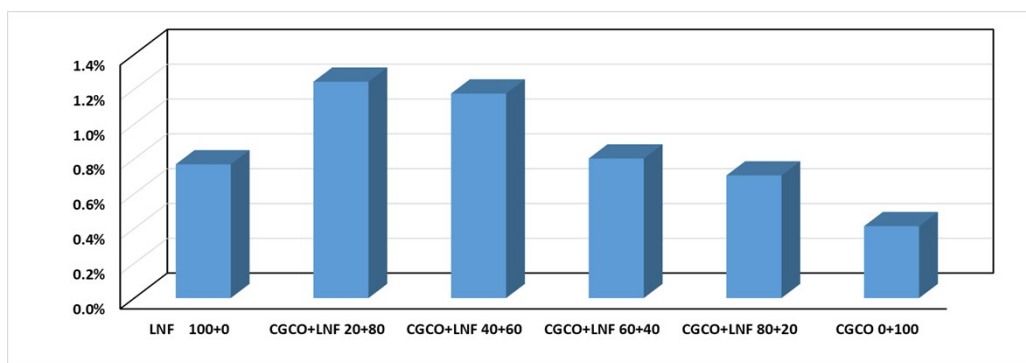


700 °C



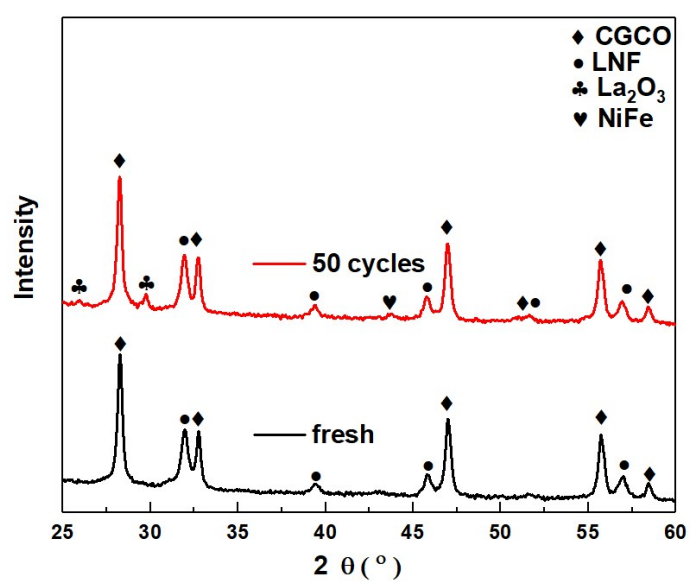
650 °C





600 °C

**Fig. S15** Oxygen capacity tested in the TGA reactor (750°C, 700°C, 650°C, 600°C).



**Fig. S16** XRD patterns of the fresh and cycled CGCO/LNF 60/40 after 50 redox cycles.

**Table S4.** Performance comparisons of the redox catalyst in this study versus the recently published redox catalysts on methane POx and CO<sub>2</sub> splitting

Redox catalyst composition	PGM type, content and cost (\$/kg catalyst)	Optimal reaction temperature (°C)	CO <sub>2</sub> conversion	Average CO <sub>2</sub> conv. rate (mmol kg <sub>cat</sub> <sup>-1</sup> s <sup>-1</sup> )	Methane conversion	Syngas selectivity	Average methane utilization rate (mmol kg <sub>cat</sub> <sup>-1</sup> s <sup>-1</sup> )	H <sub>2</sub> /CO Ratio (or coking)	Ref
<i>LaNi<sub>0.35</sub>Fe<sub>0.65</sub>O<sub>3</sub>-Ce<sub>0.85</sub>Gd<sub>0.1</sub>Cu<sub>0.05</sub>O<sub>2</sub></i>	N/A	750 °C (600 – 750 °C)*	91%	1.36	91%	96%	3.79	2 (this study)	
Rh-LaCeO <sub>4-x</sub>	0.5wt% Rh ~ \$650	650 °C	95%	0.71	90%	89%	3.75	5.5% coke	2
Fe/CeO <sub>2</sub> -IMP	N/A	800 °C	10%	1.86	2%	~2%	0.37	4.8	
Ni/CeO <sub>2</sub> -COM	N/A	800 °C	15%	2.79	12%	70%	2.23	1.8	
CeNi <sub>0.3</sub> O <sub>3</sub> -CP	N/A	800 °C	65%	12.09	60%	95%	11.16	1.9	
CeNi <sub>0.5</sub> Zr <sub>0.5</sub> O <sub>y</sub> -CP	N/A	800 °C	80%	14.88	78%	87%	14.51	3.5	3
Co/CeO <sub>2</sub> -IMP	N/A	800 °C	80%	14.88	80%	90%	14.88	2	
Ni/CeO <sub>2</sub> -IMP	N/A	800 °C	86%	15.9	88%	98%	16.3	~2.2 ~4% coke	
NiFe <sub>2</sub> O <sub>4</sub>	N/A	900 °C	19.86% for 1 <sup>st</sup> cycle 16.38% after 3 cycles	7.39 for 1 <sup>st</sup> cycle 6.09 after 3 cycles	90% 1 <sup>st</sup> cycle 75% after 3 cycles	Not detected	33.48 1 <sup>st</sup> cycle 27.90 after 3 cycles	2.5	4
Sr <sub>3</sub> Fe <sub>2</sub> O <sub>7-δ</sub> -Ca <sub>0.5</sub> Mn <sub>0.5</sub> O <sub>2</sub>	N/A	900 °C	90%	11.96	95%	95%	12.62	1.96	5
Fe <sub>0.88</sub> Ni <sub>0.12</sub> O <sub>x</sub> on ceria	N/A	1000 °C	90%	6.70	90%	90%	5.58	2	6
La <sub>0.6</sub> Sr <sub>0.4</sub> Co <sub>0.2</sub> Fe <sub>0.8</sub> O <sub>3-δ</sub>	N/A	1030 °C	8%	3.77	17%	50%	1.27	n/a	7

\* the redox catalyst in this study is highly active within this temperature range.

## References Cited.

1. Vyazovkin, S.; Burnham, A. K.; Criado, J. M.; Pérez-Maqueda, L. A.; Popescu, C.; Sbirrazzuoli, N., ICTAC Kinetics Committee recommendations for performing kinetic computations on thermal analysis data. *Thermochimica Acta* **2011**, 520 (1), 1-19.
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