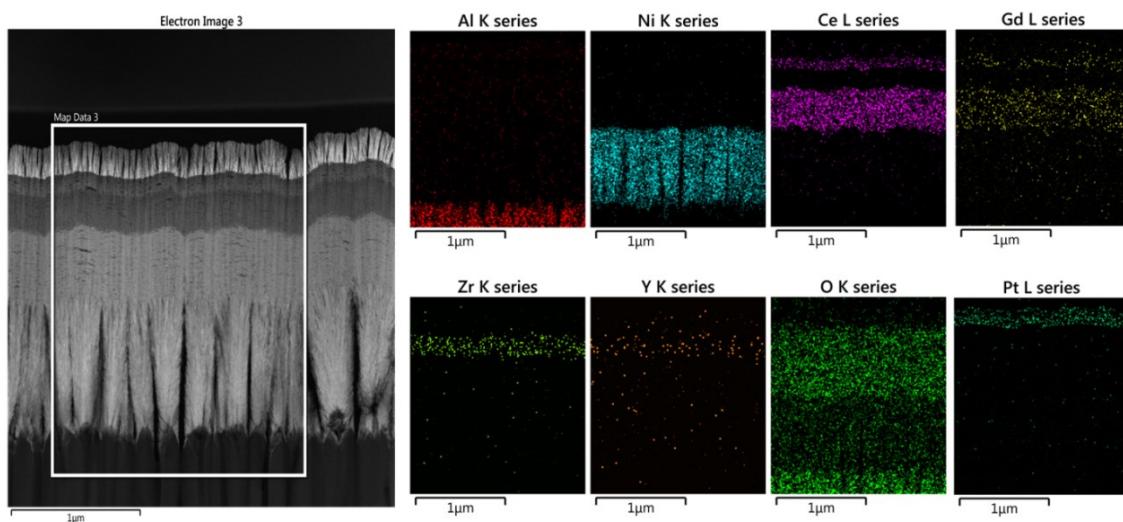


## Supporting Information

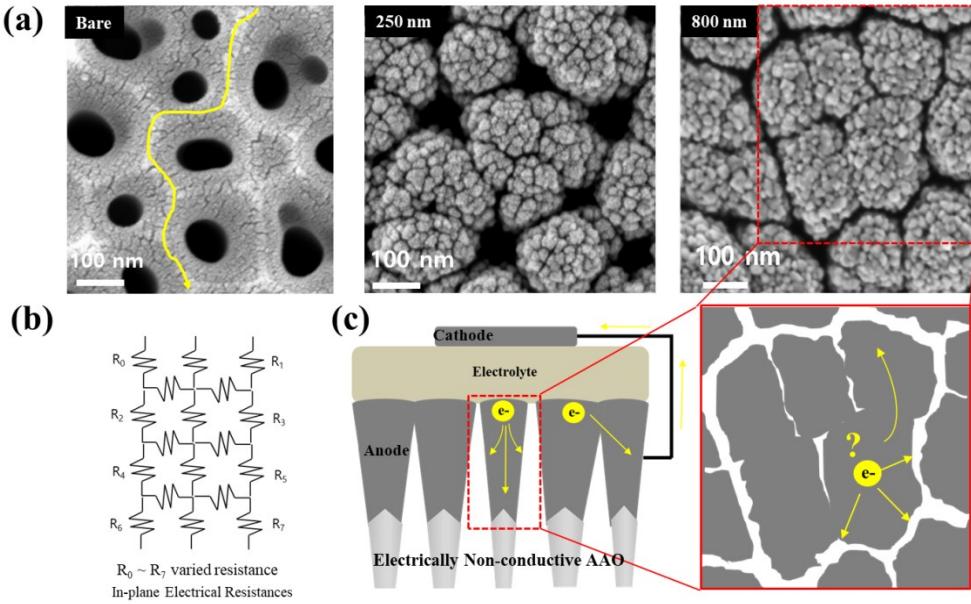
### Low-Temperature, High-Performance Thin-Film Solid Oxide Fuel Cells with Tailored Nano-Column Structures of a Sputtered Ni Anode

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#### 1. STEM-EDX analysis of TF-SOFCs



**Fig. S1.** STEM-EDX images of TF-SOFCs. The distribution of elements is analyzed by mapping the white line box region.



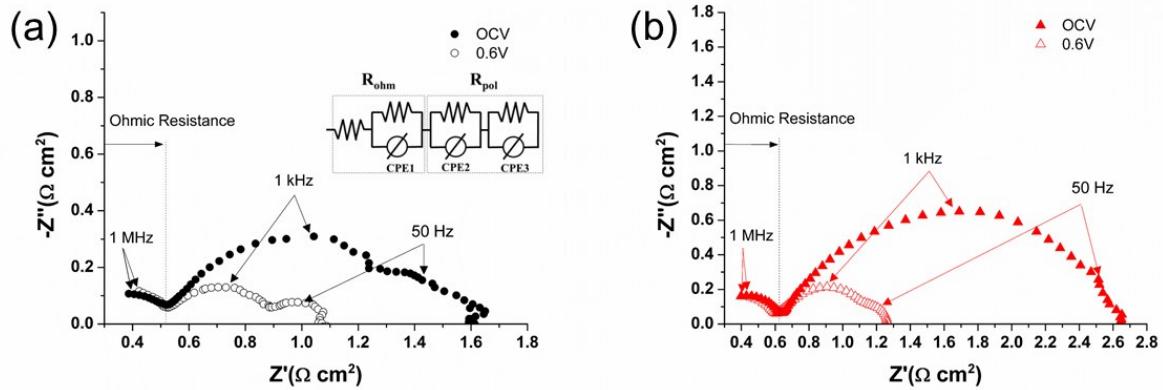
**Fig. S2.** (a) Surface FESEM views of bare AAO substrate, 250 nm-thick, and 800 nm-thick sputtered anodes. (b) Conceptual equivalent-circuit for current collecting in sputtered Ni anode deposited on nanoporous AAO substrate. (c) A schematic illustration of an electron pathway produced from the electrolyte/electrode interface in AAO supported TF-SOFCs architecture.

## 2. XRD analysis for the sputtered anodes.

**Table S1.** Texture coefficient (TC) calculated for the sputtered Ni anodes on amorphous quartz wafer.

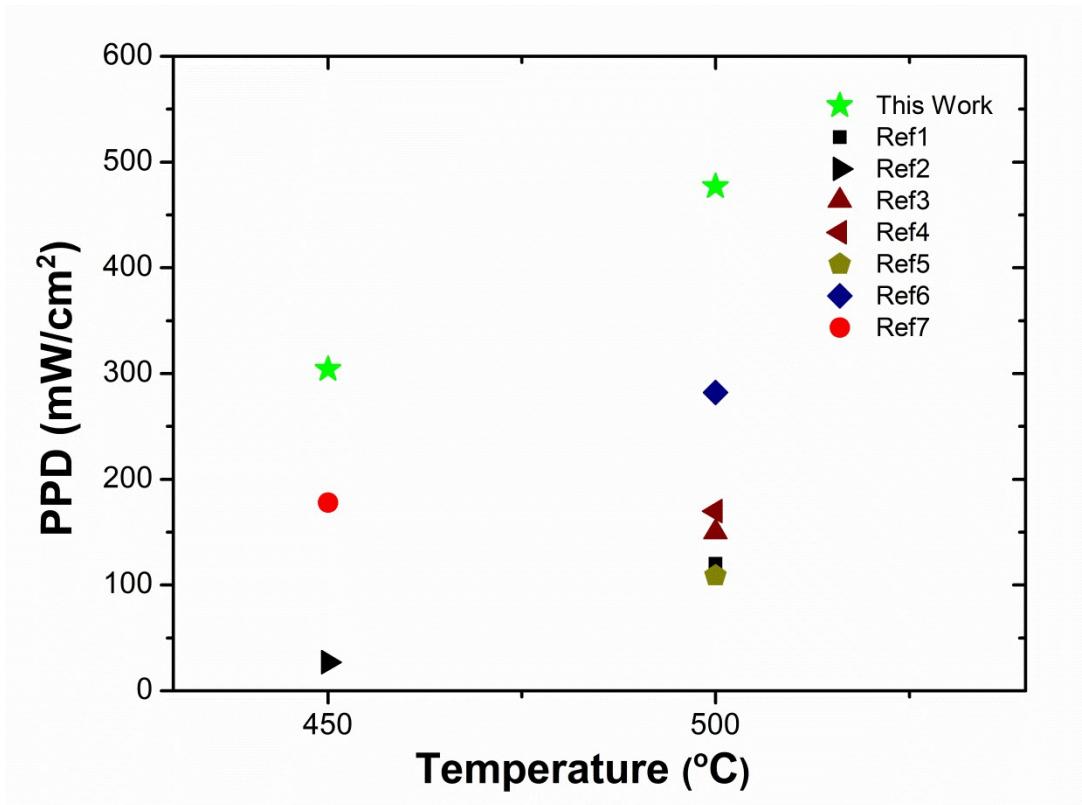
<i>Sample Detail</i>	<i>(111)</i>	<i>(200)</i>	<i>(220)</i>
ROT1( $45^\circ$ )	1.38	0.78	0.82
ROT3( $45^\circ$ )	1.45	0.97	0.55
ROT2( $45^\circ$ )	1.46	0.76	0.76
ROT1( $75^\circ$ )	1.48	0.88	0.63

### 3. Electrochemical performance of TF-SOFCs with nanostructured Ni anode.

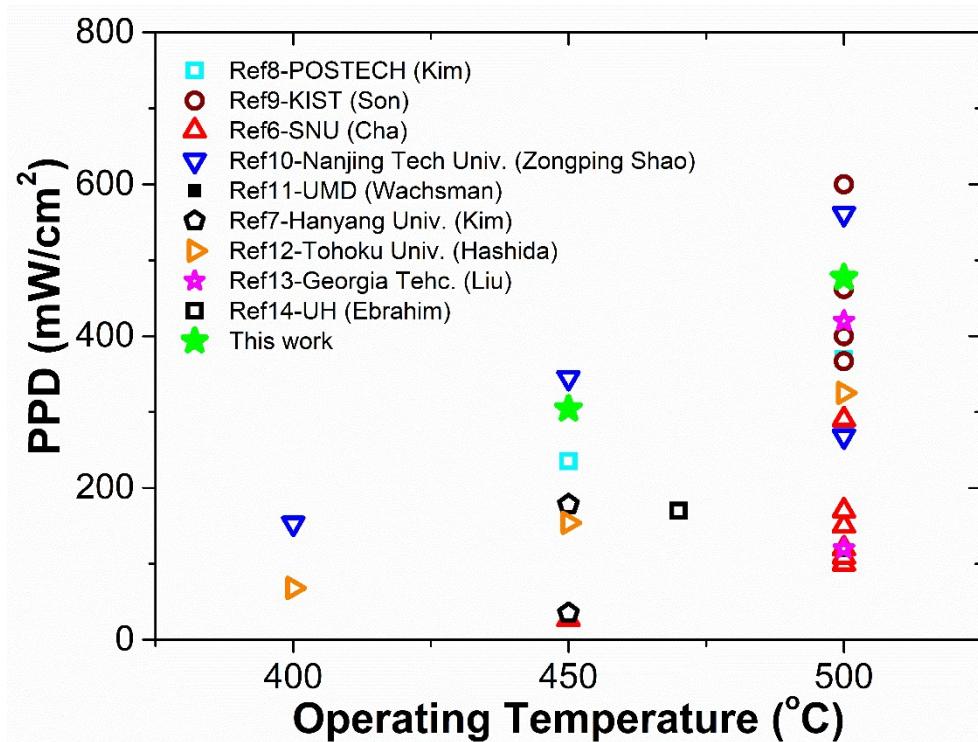


**Fig. S3.** Electrochemical impedance spectroscopy (EIS) analysis of (a) ROT1( $75^\circ$ ) and (b) ROT1( $45^\circ$ ) cells measured at 0.6 and OCV.

### 5. Performance comparison of low temperature solid oxide fuels (LT-SOFCs)



**Fig. S4.** Performance comparison with reported literature data related to AAO supported thin-film SOFCs. All of the references use Ni-based anode fabricated by sputtering. Hydrogen gas is used for the anode side, and the cathode is exposed to an ambient atmosphere. (PPD: peak power density)(Ref number refers to the supplementary references listed in the last section.)<sup>[1-7]</sup>



**Fig. S5.** Performance comparison with reported literature data related to other cell configurations.<sup>[8-14]</sup>

### 3. Surface FESEM analysis and image processing for TPBs length calculation.

In accordance with the model suggested by Bouvard *et al.*, the average coordination number of the electronic and ionic phases can be expressed as

$$Z_{el} = \frac{Z - 3}{3 + \frac{n_{el}}{n_{el} + (1 - n_{el})P^2}} \quad (7)$$

$$Z_{io} = \frac{(Z - 3)P^2}{3 + \frac{\varphi_{el}P^3}{n_{el} + (1 - n_{el})P^2}} \quad (8)$$

$$n_{el} = \frac{\varphi_{el}P^3}{1 - \varphi_{el} + \varphi_{el}P^3}$$

(9)

where  $P$  ( $\equiv r_{io}/r_{el}$ ) is the size ratio of ionic particles to electronic particles;  $n_{el}$  is the number fraction of the electronic phase;  $\varphi_{el}$  is the number fraction of the ionic phase; and  $Z$  is the average coordination number, typically assumed to be 6. The coordination number between electronic-phase (i) and ionic-phase (j) is given as

$$Z_{i-j} = n_j \frac{Z_i Z_j}{Z} \quad (10)$$

The probability that an i-phase particle in the percolated cluster connects the two ends of the composite;

$$P_i = \left\{ 1 - \left[ \frac{(4.236 - Z_{i-j})}{2.472} \right]^{2.5} \right\}^{0.4} \quad (11)$$

The threshold used in this formula, introduced by Suzuki *et al.*, means that  $Z_{i-j}$  value cannot be greater than 4.236.<sup>48</sup> The length of a neck formed between Ni and GDC particles is considered the TPB length, and neck radius is denoted as  $r_c$ .

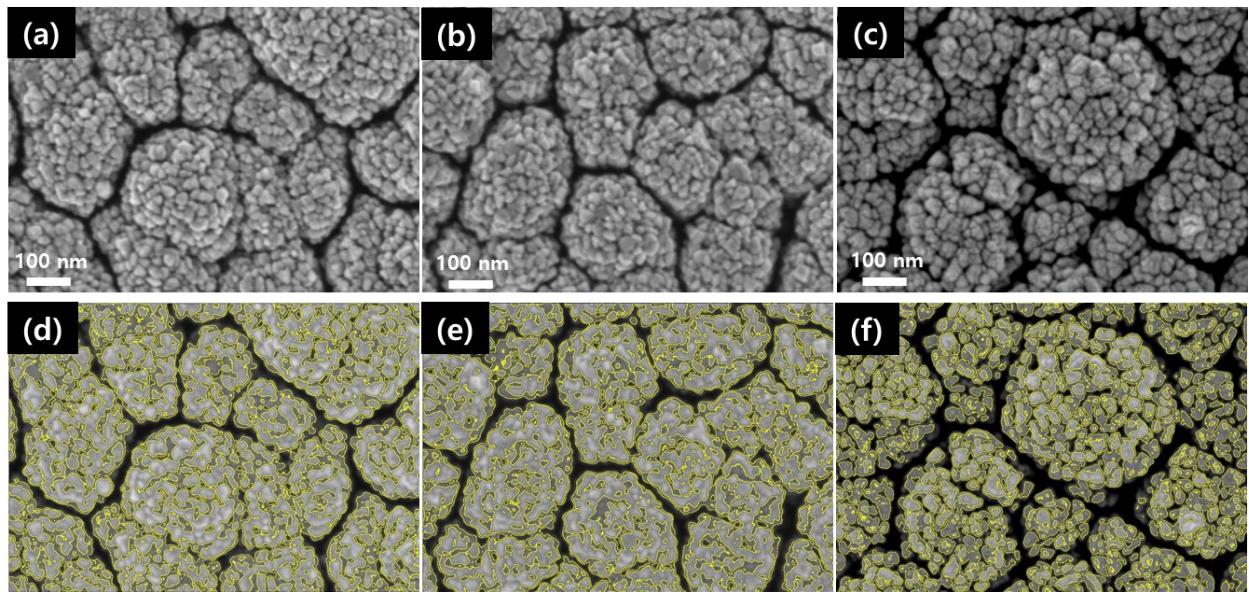
$$r_c = \sin \theta_c \cdot \min(r_{el}, r_{io}) \quad (12)$$

where  $\theta_c$  is generally considered to be 15°. By combining all of these variables, the length of TPBs can be calculated as;

$$l_{tpb} = 2\pi r_c N_t n_{el} n_{io} P_{el} P_{io} \frac{Z_{el} Z_{io}}{Z} \quad (13)$$

$$N_t = \frac{1 - \varepsilon_{pore}}{\frac{4}{3}\pi r_{el}^3 [n_{el} + (1 - n_{el})P^3]} \quad (14)$$

where  $\varepsilon_{pore}$  is the volume fraction of the pore, which is measured from HR-TEM images.



**Fig. S6.** Surface FESEM analysis for sputtered Ni anode varied with (a) ROT1( $45^\circ$ ), (b) ROT2( $45^\circ$ ), (c) ROT3( $45^\circ$ ). Image processing for calculating TPBs length by applying volume expansion method of (d) ROT1( $45^\circ$ ), (e) ROT2( $45^\circ$ ), and (f) ROT3( $45^\circ$ ). The yellow line shown in the images represents an overlapping region between Ni and pore phases that expanded to an infinitely small area.

**Table S2.** Comparison of TPBs density calculated by using binary-random sphere model and volume expansion method.

	TPB density $L_{\text{tpb}}$ [ $\mu\text{m}/\mu\text{m}^3$ ]		
Method	ROT3( $45^\circ$ )	ROT2( $45^\circ$ )	ROT1( $45^\circ$ )
<b>Binary-Random Sphere Model</b>	66.21	84.63	91.26
<b>Volume Expansion Method</b>	65.26	75.83	79.08

#### 4. Dusty gas model (DGM) applied for nanostructured anode and cathode

*Mass transport equations*

$$\frac{\varepsilon}{RT} \frac{\partial(y_i P)}{\partial t} = -\nabla \cdot N_i + r_i \text{ (mol/m}^{-3}\text{s}^{-1})$$

$\varepsilon$ : the porosity,  $N_i$ : the rate of mass transport,

$r_i$ : the rate of reaction inside the porous medium.

Assumption: the diffusion process is at steady-state, and the electrochemical reactions take place at the boundary of the electrode-electrolyte interface rather than throughout the porous medium.

$$\nabla \cdot N_i = 0$$

The dusty-gas model (DGM)

$$\frac{N_i}{D_{i,k}^{eff}} + \sum_{j=1, j \neq i}^n \frac{X_j N_i - X_i N_j}{D_{ij}^{eff}} = -\frac{P}{RT} \frac{dX_i}{dz} - \frac{X_i}{RT} \left( 1 + \frac{K P_t}{\mu D_{i,K}^{eff}} \right) \nabla P_i$$

$X_i$ : molar fraction,  $P_i$ : partial pressure,  $N_i$ : molar flux of gas species  $i$ .

$P_t$ : total pressure,  $\mu$  and  $K$ : mixture viscosity and permeability.

$$D_{i,K}^{eff} \text{ and } D_{ij}^{eff}$$

: effective Knudsen diffusion coefficients and effective binary diffusivities

Assumption: Pressure is uniform

$$\frac{N_i}{D_{i,k}^{eff}} + \sum_{j=1, j \neq i}^n \frac{X_j N_i - X_i N_j}{D_{ij}^{eff}} = -\frac{P}{RT} \frac{dX_i}{dz}$$

For diffusion with heterogeneous chemical reaction, the flux ratios are governed by reaction stoichiometry—Graham's law of diffusion in gaseous mixtures.

$$\sum_{i=1}^n N_i \sqrt{M_i}$$

$M_i$ : the molecular weight of component  $i$ .

For binary component systems.

$$\frac{N_1}{D_{1,k}^{eff}} + \frac{X_2 N_1 - X_1 N_2}{D_{12}^{eff}} = - \frac{P}{RT} \frac{dX_1}{dz}$$

$$N_1 \left( \frac{1}{D_{1,k}^{eff}} + \frac{X_2 - X_1 N_2 / N_1}{D_{12}^{eff}} \right) = - \frac{P}{RT} \frac{dX_1}{dz}$$

$$y_2 = 1 - y_1, N_2 / N_1 = - \sqrt{M_1 / M_2} \text{ (Gram's law)}$$

$$N_1 = - \frac{P}{RT} \left[ \frac{1}{D_{1,k}^{eff}} + \frac{1 - \alpha X_1}{D_{12}^{eff}} \right] - 1 \frac{dX_1}{dz}$$

$$\alpha = 1 - \left( \frac{M_1}{M_2} \right)^{1/2}$$

$$\frac{d^2 X_1}{dz^2} + \frac{\alpha}{D_{12}^{eff}} \left[ \frac{1}{D_{1,k}^{eff}} + \frac{1 - \alpha X_1}{D_{12}^{eff}} \right] - 1 \left( \frac{dX_1}{dz} \right)^2 = 0$$

Initial conditions:

$$X_{1,z=0} = X_{1,bulk}$$

$$\left( \frac{dX_1}{dz} \right)_{z=0} = - \frac{JRT}{2PF} \left[ \frac{1}{D_{1,k}^{eff}} + \frac{1 - \alpha X_1}{D_{12}^{eff}} \right]$$

$$D_{i,K}^{eff} = D_{i,K} \frac{\varepsilon_{pore}}{\tau_{pore}}, D_{ij}^{eff} = D_{i,K} \frac{\varepsilon_{pore}}{\tau_{pore}}$$

$\tau_{pore}$ : tortuosity of the pore

$$D_{i,K} = \frac{d_p}{2} \sqrt{\frac{8RT}{\pi M_i}}$$

$d_p$ : the mean pore diameter

$$d_p \approx d_h = \frac{4}{(S/\varepsilon)_{pore}}$$

$d_h$ : the hydraulic diameter,  $S$ : surface area of the pore

$$\frac{1}{D_a^{eff}} = \frac{\tau_{pore}}{\varepsilon_{pore}} \left( \frac{1}{D_{H_2-H_2O}} + \frac{1}{D_{H_2K}} \right), \quad \frac{1}{D_c^{eff}} = \frac{\tau_{pore}}{\varepsilon_{pore}} \left( \frac{1}{D_{O_2-N_2}} + \frac{1}{D_{N_2K}} \right)$$

For the binary diffusion coefficients, Fuller-Schettler-Giddings' equation is adopted.

$$D_{ij} = \frac{0.01013T^{1.75}((1/M_i \times 10^3) + (1/M_j \times 10^3))^{1/2}}{P[(\sum v_i \times 10^6)^{1/3} + (\sum v_j \times 10^6)^{1/3}]^2}$$

$\sum v_i$ : the diffusion volume of the molecules of species  $i$ .

The equations given above are solved by the Runge-Kutta method with Matlab.

**Table S3.** Geometrical Variables for 1D simulation.

Variables	Notation	Value	Unit
Anode grain size	$d_a$	3.3x10-8	[m]
Cathode grain size	$d_c$	2.3x10-8	[m]
Electrolyte grain size	$d_e$	2.2x10-8	[m]
Electrode probability	$\varphi_{el}$	0.42	
Anode tortuosity	$\tau_{pore,a}$	1.3	
Cathode tortuosity	$\tau_{pore,c}$	1.3	

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