

## Electronic Supplementary Information

### A Carbon-Silica-Zirconia Ceramic Membrane with CO<sub>2</sub> Flow-Switching Behavior Promising Versatile High-Temperature H<sub>2</sub>/CO<sub>2</sub> Separation

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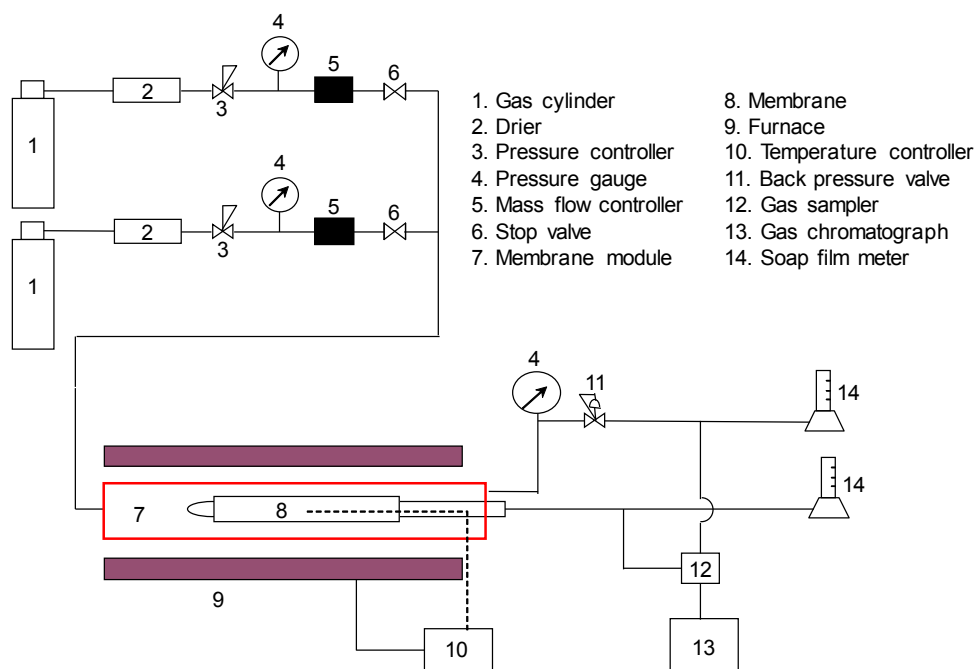


Fig. S1. Schematic flow diagram of the gas permeation testing setup (Test pressures:  $P_u = 200\text{--}500$  kPa,  $P_d = 100$  kPa)

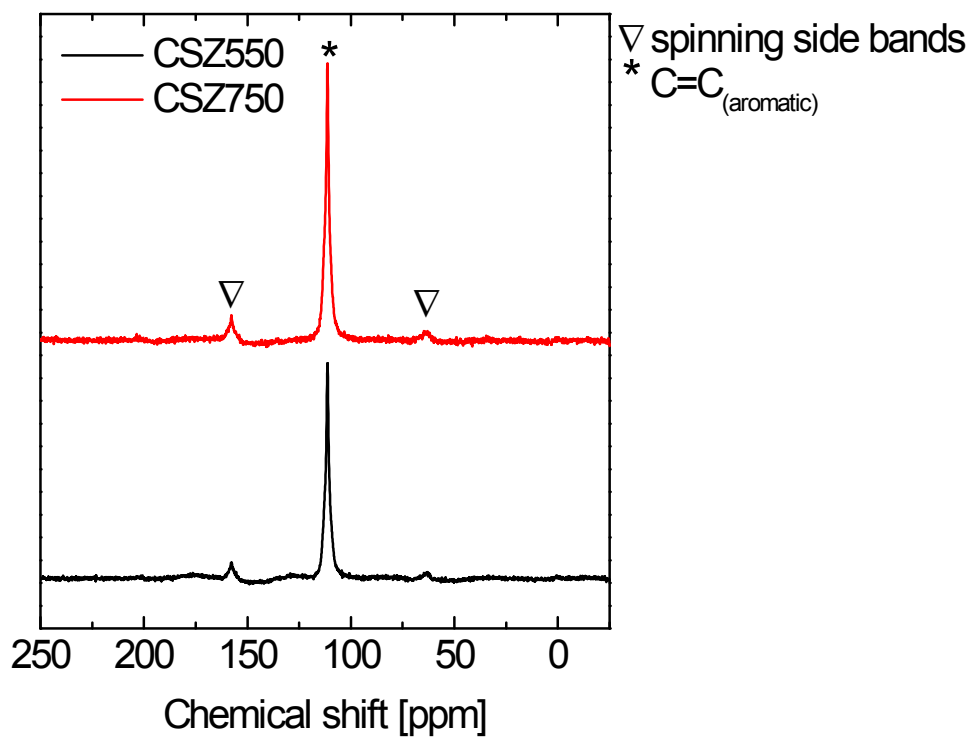


Figure S2. DD-MAS-<sup>13</sup>C-NMR spectra of C-SiO<sub>2</sub>-ZrO<sub>2</sub> prepared at 550 and 750 °C under N<sub>2</sub>

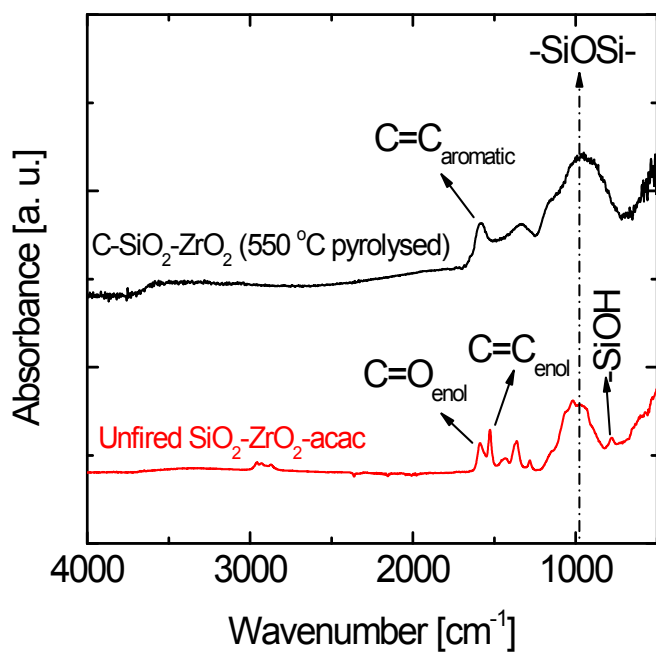


Figure S3. FT-IR spectra of SiO<sub>2</sub>-ZrO<sub>2</sub>-acac powder before and after pyrolysis at 550 °C under N<sub>2</sub>

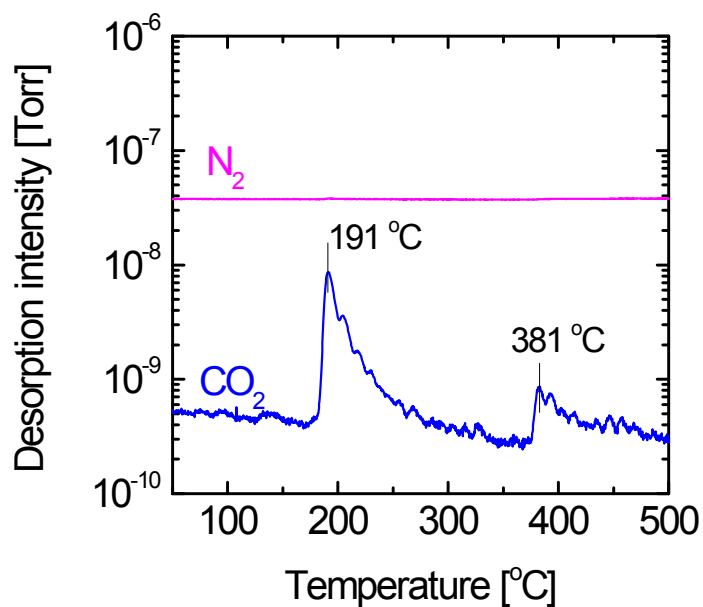


Figure S4.  $\text{N}_2/\text{CO}_2$  mixture temperature programmed desorption in C- $\text{SiO}_2$ - $\text{ZrO}_2$  powder prepared at  $550^{\circ}\text{C}$  under  $\text{N}_2$

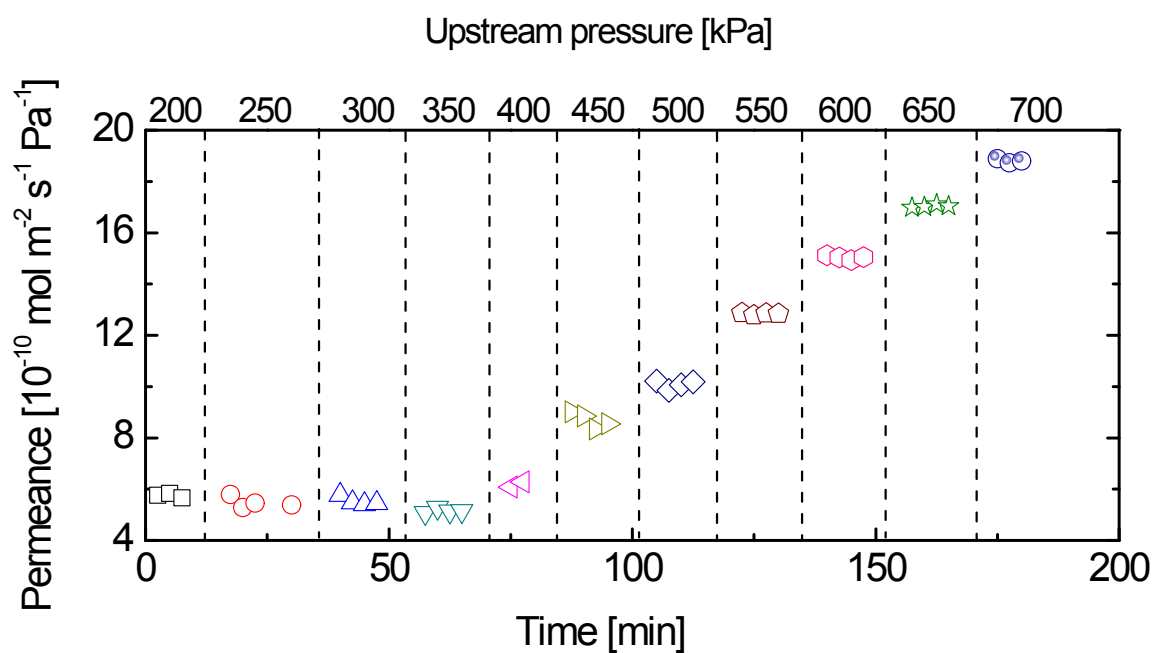


Figure S5. Detailed time course of single  $\text{CO}_2$  permeance at pressures ranging from 200 to 700 kPa

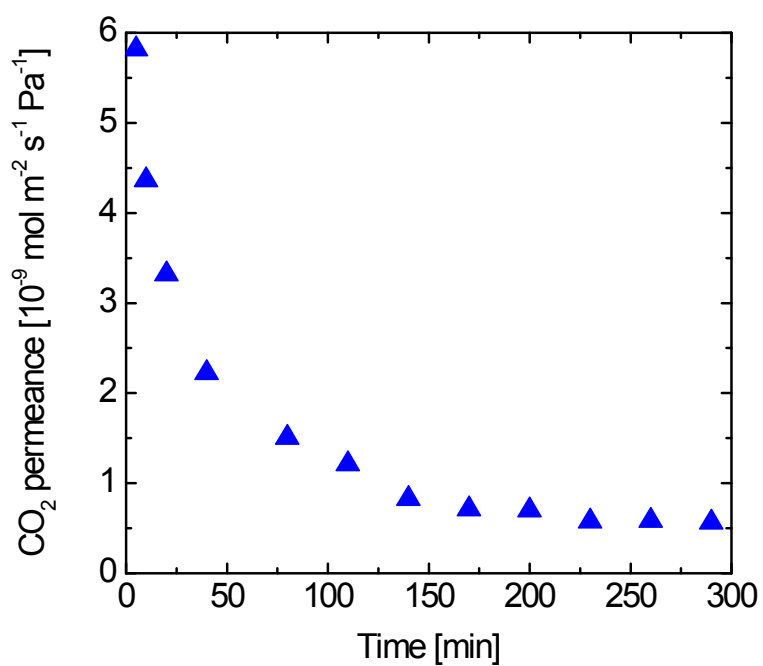


Figure S6. Initial transient CO<sub>2</sub> permeance at 200 kPa and 300 °C before steady state

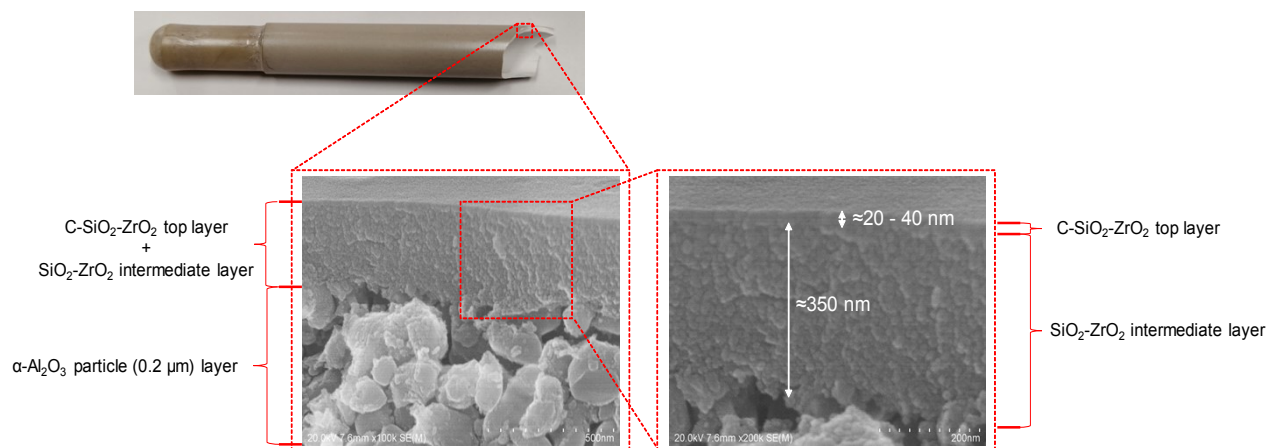


Fig. S7 FE-SEM images of the cross-section profile of a C-SiO<sub>2</sub>-ZrO<sub>2</sub> membrane.

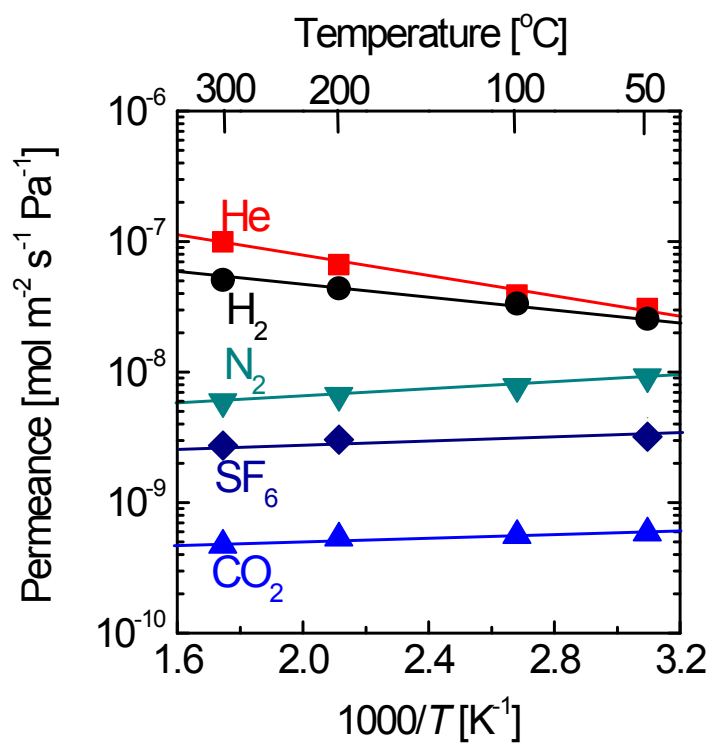


Figure S8. Temperature dependence of single-gas permeance and permeance ratios at temperatures ranging from 50 to 300 °C for a C-SiO<sub>2</sub>-ZrO<sub>2</sub> membrane prepared at 550 °C

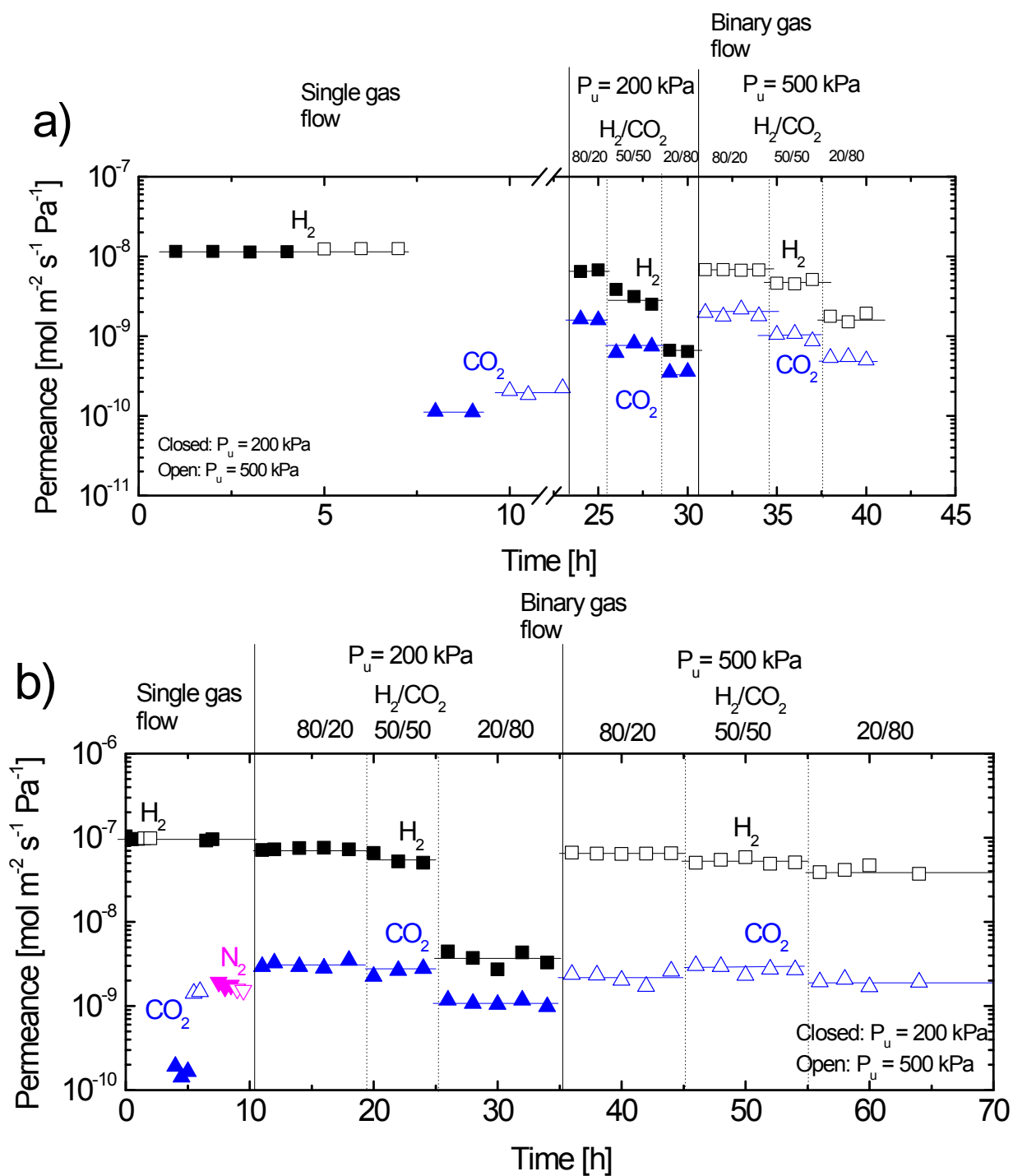


Figure S9. Detailed time courses for the permeance of single-gas and a binary-gas mixture at 50 (a) and 300 °C (b)

As presented by Kamaruddin and Koros [1], the mass flux of a species, A, that is the result of the bulk motion of a mixture of gases, A and B, can be written as follows:

$$n_A^{bulk} = (n_A + n_B)\omega_A \quad (S1)$$

Where  $n_A$ ,  $n_B$  and  $\omega_A$  are the total mass flux of components A and B and the concentration of component A, respectively. Equation S1 for the mass flux of CO<sub>2</sub> caused by the bulk motion of a mixture of CO<sub>2</sub> and H<sub>2</sub> could be written as follows:

$$n_{CO_2}^{bulk} = (n_{H_2} + n_{CO_2})\omega_{CO_2} \quad (S2)$$

The fraction of the bulk-flow contribution that a component makes to the total mass flux in a gaseous mixture is defined as the ratio of the bulk mass flux of the component to the total mass flux. For the CO<sub>2</sub> component in a H<sub>2</sub>/CO<sub>2</sub> mixture, equation S3 gives the fraction of the H<sub>2</sub>-CO<sub>2</sub> bulk flux contributed by the CO<sub>2</sub> flow [1].

$$\prod_{CO_2}^{bulk} = \frac{n_{CO_2}^{bulk}}{n_{CO_2}} = \frac{(n_{H_2} + n_{CO_2})\omega_{CO_2}}{n_{CO_2}} = (1 + r)\omega_{CO_2}^{avg} \quad (S3)$$

Where  $\prod^{bulk}$  is the fraction of the bulk flux contribution,  $r$  is the permeance ratio of H<sub>2</sub> to CO<sub>2</sub> and  $\omega^{avg}$  is the average CO<sub>2</sub> concentration across the membrane thickness. Applying the log mean difference of CO<sub>2</sub> concentration across the membrane thickness, equation S3 becomes

$$\prod_{CO_2}^{bulk} = (1 + r) \frac{(\omega_{CO_2}^f - \omega_{CO_2}^r)}{\ln \left( \frac{\omega_{CO_2}^f - \omega_{CO_2}^p}{\omega_{CO_2}^r - \omega_{CO_2}^p} \right)} \quad (S4)$$

For a single CO<sub>2</sub> flow, while adopting a single H<sub>2</sub> flow as the frame of reference with a linear CO<sub>2</sub> concentration gradient, equation S3 can be written as follows:

$$\prod_{CO_2}^{bulk} = \left(1 + \frac{1}{r}\right) \left( \frac{\omega_{CO_2}^f + \omega_{CO_2}^p}{2} \right) \quad (S5)$$

Where  $\omega^f$ ,  $\omega^r$  and  $\omega^p$  are the concentrations of CO<sub>2</sub> in the feed, retentate and permeate, respectively, and  $r$  becomes the ideal selectivity of H<sub>2</sub> over CO<sub>2</sub>. Equations S4 and S5 can thus be plotted against the CO<sub>2</sub> feed-side pressure, as shown in Figure S8. Clearly, the bulk phase flow contribution of CO<sub>2</sub> is much higher in the binary mixture than in pure CO<sub>2</sub> flow and increases as the CO<sub>2</sub> feed pressure increases.

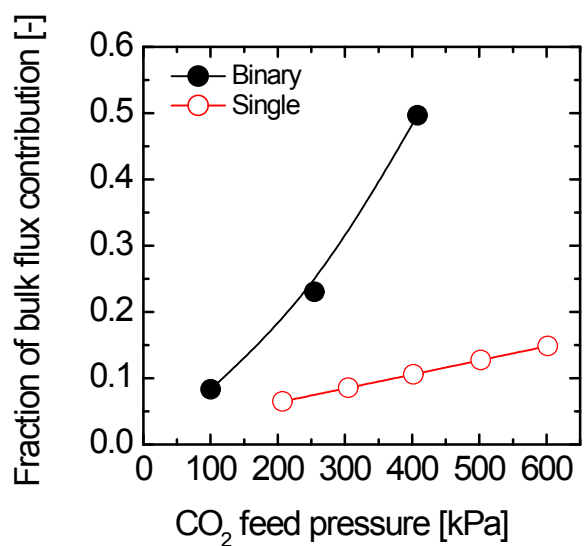


Figure S10. Calculated fraction of the CO<sub>2</sub> bulk flux contribution at 300 °C as a function of the CO<sub>2</sub> feed pressure in single and binary systems (at total  $P_u = 500$  kPa)



Table S1. Comparison of H<sub>2</sub> permeance-H<sub>2</sub>/CO<sub>2</sub> mixture selectivity trade-off of high-temperature H<sub>2</sub>/CO<sub>2</sub> separation membranes

No.	Membrane type	Separation mechanism	H <sub>2</sub> permeance x 10 <sup>-8</sup> [mol m <sup>-2</sup> s <sup>-1</sup> Pa <sup>-1</sup> ]	H <sub>2</sub> /CO <sub>2</sub> selectivity [-]	Reference
200-300 °C					
1	Zeolite (SAPO-34)	Size exclusion	7	23	[2]
2	ZIF-7	Size exclusion	4.5	13.6	[3]
3	Zeolite (B-ZSM-5)	Size exclusion	0.6	33	[4]
4	SiC	Size exclusion	0.89	49	[5]
5	Si	Size exclusion	50	6.8	[6]
6	Pd-organosilica	H <sub>2</sub> flow enhancement	5.8	33.5	[7]
>300 °C					
7	SiO <sub>2</sub> -TiO <sub>2</sub>	Size exclusion	24.2	13.6	[8]
8	MFI-type Zeolite	Size exclusion	39.6	141	[9]
9	Zeolite (B-ZSM-5)	Size exclusion	10	47	[4]
300 °C, 500 kPa					
	C-SiO <sub>2</sub> -ZrO <sub>2</sub>	Flow transition H <sub>2</sub> enhancement	7	20-30	This work

#### Supplementary references

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