

Unravelling thermal stress due to thermal expansion mismatch in metal-organic frameworks for methane storage

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S1 Materials

System-specific force fields were derived for various MOFs as listed in Tables S1, S2, S3 and S4.

Table S1: Al-based metal-organic frameworks under study.

MOF	ρ ($\text{kg}\cdot\text{m}^{-3}$)	ASA ($\text{m}^2\cdot\text{g}^{-1}$)	Void fraction (%)	LCD (\AA)	α_0 (MK^{-1})	β_0 (GPa)	γ ($\text{MPa}\cdot\text{K}^{-1}$)
Al-soc-MOF-1 ¹	343	5010	79	15.9	-13.3	8.9	-0.118
MOF-519 ²	894	1163	32	8.7	-14.9	10.2	-0.152
MOF-520 ²	529	3793	69	10.1	-12.8	7.8	-0.100
MOF-520-BPDC ³	605	3158	62	10.4	-10.3	13.0	-0.133

Table S2: Zn-based metal-organic frameworks under study.

MOF	ρ ($\text{kg}\cdot\text{m}^{-3}$)	ASA ($\text{m}^2\cdot\text{g}^{-1}$)	Void fraction (%)	LCD (\AA)	α_0 (MK^{-1})	β_0 (GPa)	γ ($\text{MPa}\cdot\text{K}^{-1}$)
IRMOF-8 ⁴	424	4662	81	17.7	-40.3	4.9	-0.196
IRMOF-10 ⁴	304	5244	86	21.5	-47.6	4.9	-0.233
MOF-5 (IRMOF-1) ⁵	555	3993	77	15.5	-36.7	11.1	-0.408
MOF-177 ⁶	406	4895	80	11.9	-30.3	6.2	-0.187
MOF-180 ⁷	242	6358	87	16.5	-131.4	1.4	-0.179
MOF-200 ⁷	204	6335	89	17.9	-39.1	3.7	-0.145
MOF-205 (DUT-6) ^{7,8}	361	5211	83	23.1	-29.3	7.4	-0.218
MOF-210 ⁷	223	6028	88	31.6	-96.6	1.6	-0.155
MOF-905 ⁹	500	4024	79	19.8	-106.9	3.9	-0.415
MOF-950 ⁹	550	4155	76	9.8	-26.0	9.2	-0.239
MUF-7 ¹⁰	364	4863	81	22.0	-25.2	6.8	-0.171
UMCM-1 ¹¹	366	4587	83	25.2	-40.9	5.9	-0.240
UMCM-8 ¹²	490	4337	79	16.2	-26.3	6.3	-0.166
UMCM-9 ¹²	362	5009	83	19.1	-37.5	4.7	-0.175

Table S3: Zr-based metal-organic frameworks under study.

MOF	ρ ($\text{kg}\cdot\text{m}^{-3}$)	ASA ($\text{m}^2\cdot\text{g}^{-1}$)	Void fraction (%)	LCD (\AA)	α_0 (MK^{-1})	β_0 (GPa)	γ ($\text{MPa}\cdot\text{K}^{-1}$)
NU-800 ¹³	567	4458	75	13.9	-80.6	4.1	-0.331
pbz-MOF-1 ¹⁴	630	3360	66	14.6	-10.6	10.8	-0.114

Table S4: Cu-based metal-organic frameworks under study.

MOF	ρ ($\text{kg}\cdot\text{m}^{-3}$)	ASA ($\text{m}^2\cdot\text{g}^{-1}$)	Void fraction (%)	LCD (\AA)	α_0 (MK^{-1})	β_0 (GPa)	γ ($\text{MPa}\cdot\text{K}^{-1}$)
FJI-H5 ¹⁵	415	4385	80	22.1	-18.9	1.7	-0.031
HKUST-1 ¹⁶	851	2229	66	13.5	-9.7	20.7	-0.199
HNUST-2 ¹⁷	555	4604	73	11.5	-32.5	4.7	-0.152
MFM-112 ¹⁸	475	4200	77	22.7	-14.4	11.6	-0.167
MOF-505 (NOTT-100) ^{19,20}	888	2422	64	10.2	-10.8	20.2	-0.219
NJU-Bai 10 ²¹	652	3404	71	12.9	-13.5	6.3	-0.085
NJU-Bai 17 ²²	789	2942	67	10.2	-12.1	15.5	-0.187
NJU-Bai 19 ²³	680	3293	68	11.2	-9.7	13.9	-0.135
NJU-Bai 41 ²⁴	708	2902	65	11.9	-9.6	9.9	-0.095
NJU-Bai 42 ²⁴	664	3483	71	11.8	-7.5	11.1	-0.083
NOTT-101 ²⁵	657	3384	71	11.7	-10.1	14.3	-0.145
NOTT-108 ²⁵	749	2730	66	11.6	-7.7	15.4	-0.117
NU-111 ²⁶	390	4704	80	23.4	-58.1	5.7	-0.330
NU-125 ²⁷	550	3795	74	19.9	-11.8	6.4	-0.075
NU-135 ²⁸	721	2803	62	11.8	-9.2	13.3	-0.122
NU-140 ²⁹	367	4979	81	25.0	-17.1	2.0	-0.035
PCN-11 ³⁰	714	3112	70	10.7	-17.8	18.0	-0.320
PCN-14 ³¹	786	2353	56	11.7	-4.8	14.5	-0.070
PCN-61 ³²	537	3795	74	20.2	-37.0	10.6	-0.392
PCN-66 ³²	413	4726	80	22.9	-50.9	5.4	-0.274
PCN-68 (NOTT-116) ^{33,34}	355	5113	81	25.7	-42.0	6.6	-0.276
PCN-610 (NU-100) ^{33,35}	274	5876	86	28.9	-107.4	1.6	-0.171
UTSA-20 ³⁶	885	2085	58	10.4	-9.7	8.0	-0.078
UTSA-61 ³⁷	690	2834	68	17.5	-17.7	17.9	-0.318
UTSA-76 ³⁸	669	3288	71	11.5	-7.8	13.5	-0.106
UTSA-80 ³⁹	676	2837	64	13.7	-17.2	8.6	-0.147
UTSA-88 ⁴⁰	831	2412	62	11.6	-9.9	13.8	-0.137
UTSA-110 ⁴¹	571	4021	74	12.8	-15.8	7.5	-0.119
ZJU-5 ⁴²	664	3309	71	11.6	-11.5	14.6	-0.167
ZJU-32 ⁴³	420	4759	80	16.2	-23.0	6.3	-0.146
ZJU-35 ⁴⁴	630	3190	74	15.0	-13.5	12.8	-0.173
ZJU-36 ⁴⁴	489	3948	78	17.5	-38.6	3.0	-0.146

S2 Extra figures and tables

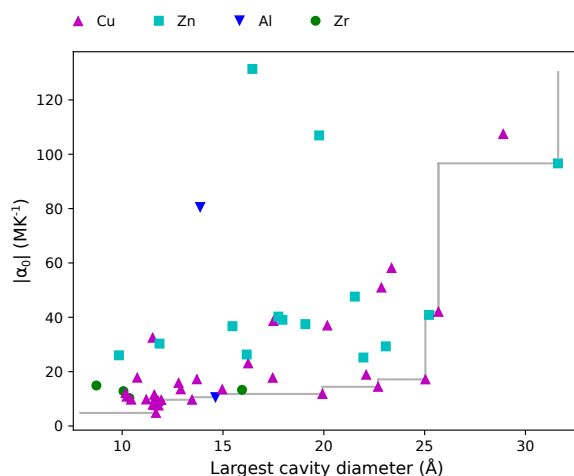


Figure S1: The magnitude of the thermal expansion coefficient as a function of the largest cavity diameter. A Pareto front where the thermal expansion coefficient is minimized and the largest cavity diameter is maximised is shown.

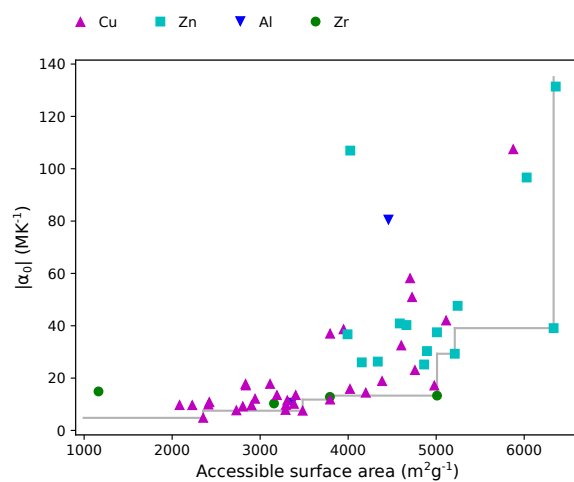


Figure S2: The magnitude of the thermal expansion coefficient as a function of the accessible surface area. A Pareto front where the thermal expansion coefficient is minimized and the accessible surface area is maximised is shown.

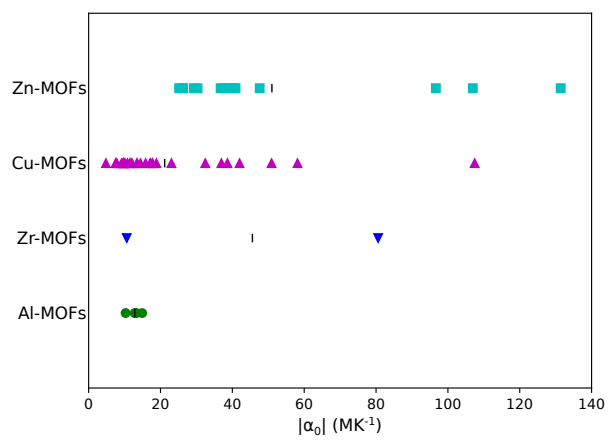


Figure S3: Influence of the inorganic building block on the thermal expansion coefficient. The vertical black line indicates the average per inorganic building block.

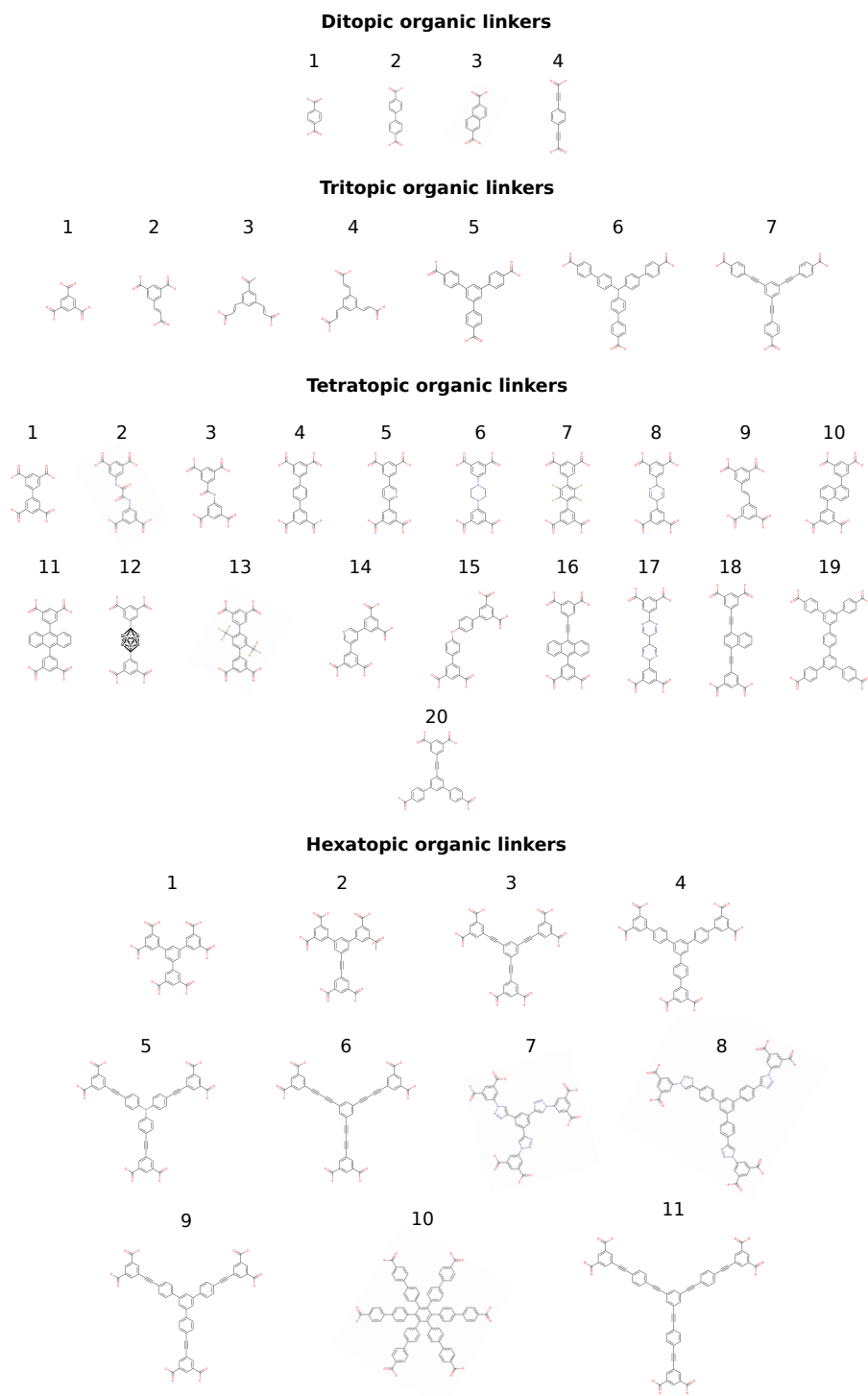


Figure S4: Overview of the organic linkers used in this work. The hydrogens are implicit.

Table S5: Organic linkers of the Al-based metal-organic frameworks under study (Figure S4).

MOF	Ditopic	Tritopic	Tetratopic	Hexatopic
Al-soc-MOF-1 ¹	-	-	19	-
MOF-519 ²	-	5	-	-
MOF-520 ²	-	5	-	-
MOF-520-BPDC ³	2	5	-	-

Table S6: Organic linkers of the Zn-based metal-organic frameworks under study (Figure S4).

MOF	Ditopic	Tritopic	Tetratopic	Hexatopic
IRMOF-8 ⁴	3	-	-	-
IRMOF-10 ⁴	2	-	-	-
MOF-5 (IRMOF-1) ⁵	1	-	-	-
MOF-177 ⁶	-	5	-	-
MOF-180 ⁷	-	7	-	-
MOF-200 ⁷	-	6	-	-
MOF-205 (DUT-6) ^{7,8}	3	5	-	-
MOF-210 ⁷	2	7	-	-
MOF-905 ⁹	1	4	-	-
MOF-950 ⁹	-	4	-	-
MUF-7 ¹⁰	1, 2	5	-	-
UMCM-1 ¹¹	1	5	-	-
UMCM-8 ¹²	1, 3	-	-	-
UMCM-9 ¹²	2, 3	-	-	-

Table S7: Organic linkers of the Zr-based metal-organic frameworks under study (Figure S4).

MOF	Ditopic	Tritopic	Tetratopic	Hexatopic
NU-800 ¹³	4	-	-	-
pbz-MOF-1 ¹⁴	-	-	-	10

Table S8: Organic linkers of the Cu-based metal-organic frameworks under study (Figure S4).

MOF	Ditopic	Tritopic	Tetratopic	Hexatopic
FJI-H5 ¹⁵	-	-	15	-
HKUST-1 ¹⁶	-	1	-	-
HNUST-2 ¹⁷	-	-	18	-
MFM-112 ¹⁸	-	-	-	4
MOF-505 (NOTT-100) ^{19,20}	-	-	1	-
NJU-Bai 10 ²¹	-	-	14	-
NJU-Bai 17 ²²	-	-	3	-
NJU-Bai 19 ²³	-	-	6	-
NJU-Bai 41 ²⁴	-	-	10	-
NJU-Bai 42 ²⁴	-	-	2	-
NOTT-101 ²⁵	-	-	4	-
NOTT-108 ²⁵	-	-	7	-
NU-111 ²⁶	-	-	-	6
NU-125 ²⁷	-	-	-	7
NU-135 ²⁸	-	-	12	-
NU-140 ²⁹	-	-	-	8
PCN-11 ³⁰	-	-	9	-
PCN-14 ³¹	-	-	11	-
PCN-61 ³²	-	-	-	3
PCN-66 ³²	-	-	-	5
PCN-68 (NOTT-116) ^{33,34}	-	-	-	9
PCN-610 (NU-100) ^{33,35}	-	-	-	11
UTSA-20 ³⁶	-	-	-	1
UTSA-61 ³⁷	-	-	-	2
UTSA-76 ³⁸	-	-	8	-
UTSA-80 ³⁹	-	-	16	-
UTSA-88 ⁴⁰	-	-	13	-
UTSA-110 ⁴¹	-	-	17	-
ZJU-5 ⁴²	-	-	5	-
ZJU-32 ⁴³	-	-	20	-
ZJU-35 ⁴⁴	-	2	-	-
ZJU-36 ⁴⁴	-	3	-	-

S3 Force field simulations

The first-principles force fields used to model the systems under study are derived using QuickFF.^{45,46} Within this protocol, the quantum mechanical potential energy surface (PES) is approximated by a sum of analytical functions of the nuclear coordinates that describe the covalent (cov) and noncovalent (noncov) interactions. The latter are composed of electrostatic and van der Waals interactions. The force field and a structure are added for every MOF in Yaff-format as supplementary information.

$$V^{FF} = \underbrace{V_{bond} + V_{bend} + V_{oopd} + V_{torsion} + V_{cross}}_{V_{cov}} + \underbrace{V_{ei} + V_{vdW}}_{V_{noncov}}. \quad (\text{S3.1})$$

S3.1 First-principles cluster data

The required first-principles cluster data for the determination of the covalent terms in the force field are generated with Gaussian 16⁴⁷ using the B3LYP⁴⁸ exchange-correlation functional. A 6-311G(*d,p*) basis set⁴⁹ is used for all row 1, row 2 and row 3 atoms, together with the LanL2DZ basis set for Zn and Zr.⁵⁰ The atomic charges are derived with the Minimal Basis Iterative Stockholder (MBIS) partitioning scheme⁵¹ from the all-electron density obtained with Gaussian 16. The atomic charges of the Zn- and Zr-clusters are obtained from the PBE⁵² all-electron density computed with GPAW⁵³. The force field parameters for the atom types overlapping in the organic linker and the inorganic brick cluster models were averaged.

S3.2 Covalent interactions

The covalent interactions – which mimic the chemical bonds between the atoms – are approximated by different terms as a function of the internal coordinates (bonds, bends, out-of-plane distances, and dihedrals). The unknown force field parameters are fitted following the QuickFF procedure.⁴⁵ We use an extended version⁴⁶ to include anharmonic bond and bend terms,⁵⁴ which are important when modeling nuclear quantum effects and the thermal expansion of MOFs.^{55,56} The anharmonic bond and bend terms are given by:

$$V_{\text{bond}}^{ij} = \frac{K_{ij}}{2} (r_{ij} - r_{0,ij})^2 \left[1 - \alpha (r_{ij} - r_{0,ij}) + \frac{7}{12} \cdot \alpha^2 \cdot (r_{ij} - r_{0,ij})^2 \right], \quad (\text{S3.2})$$

$$V_{\text{bend}}^{ijk} = \frac{K_{ijk}}{2} (\theta_{ijk} - \theta_{0,ijk})^2 \left[1 - a_1 (\theta_{ijk} - \theta_{0,ijk}) + a_2 \cdot (\theta_{ijk} - \theta_{0,ijk})^2 - a_3 \cdot (\theta_{ijk} - \theta_{0,ijk})^3 + a_4 (\theta_{ijk} - \theta_{0,ijk})^4 \right], \quad (\text{S3.3})$$

with $\alpha = 2.55 \text{ \AA}^{-1}$, $a_1 = 0.014 \text{ deg}^{-1}$, $a_2 = 5.6 \cdot 10^{-5} \text{ deg}^{-2}$, $a_3 = 7 \cdot 10^{-7} \text{ deg}^{-3}$, and $a_4 = 2.2 \cdot 10^{-8} \text{ deg}^{-4}$. We also add cross terms between the bonds and bends to improve the correspondence with the first-principles data.⁵⁵ The included cross terms are:

- angle stretch-stretch terms (ASS) between neighboring bonds, i.e. part of the same angle
- angle stretch-angle terms (ASA).

The mathematical expression of these terms is given by

$$V_{\text{ASS}}^{ijk} = K_{ijk}^{\text{ASS}} (r_{ij} - r_{0,ij}) (r_{jk} - r_{0,jk}) \quad (\text{S3.4})$$

$$V_{\text{ASA}}^{ijk} = \left[K_{ijk}^{\text{ASA1}} (r_{ij} - r_{0,ij}) + K_{ijk}^{\text{ASA2}} (r_{jk} - r_{0,jk}) \right] (\theta_{ijk} - \theta_{0,ijk}). \quad (\text{S3.5})$$

The out-of-plane distances are described using a harmonic potential:

$$V_{\text{oopd}}^{ijkl} = \frac{K_{ijkl}}{2} (d_{ijkl} - d_{0,ijkl})^2. \quad (\text{S3.6})$$

This is a four-atom interaction, in which the internal coordinate is the distance between the central atom and the plane determined by its three neighbors. The fourth covalent

term is the dihedral energy term. Here, a cosine term is used as a function of the dihedral angle, including the multiplicity m_ϕ of the dihedral angle:

$$V_{torsion}^{ijkl} = \frac{K_{ijkl}}{2} [1 - \cos(m_\phi(\phi_{ijkl} - \phi_{0,ijkl}))]. \quad (\text{S3.7})$$

The unknown parameters in all terms (force constants, rest values, and multiplicities) in the covalent energy expression can be estimated directly with QuickFF.

S3.3 Electrostatic interactions

The electrostatic interactions are modeled by a Coulomb interaction between Gaussian charge distributions,⁵⁷ which allows to include all pairwise interactions. The atomic charges q_i are derived with the Minimal Basis Iterative Stockholder (MBIS) partitioning scheme.⁵¹

$$V_{ei} = \frac{1}{2} \sum_{\substack{i,j=1 \\ (i \neq j)}} \frac{q_i q_j}{4\pi\epsilon_0 r_{ij}} \operatorname{erf}\left(\frac{r_{ij}}{d_{ij}}\right) \quad (\text{S3.8})$$

Gaussian charge distributions are used with a total charge q_i and radius d_i , centered on atom i . The mixed radius of the Gaussian charges,⁵⁷ d_{ij} , is given by $\sqrt{d_i^2 + d_j^2}$. The interaction depends on the distance r_{ij} between the two atoms.

S3.4 Van der Waals interactions

The van der Waals interactions are described by the MM3-Buckingham model^{58,59} up to a finite cutoff (12 Å) and are supplemented with tail corrections.⁶⁰

$$V_{vdW} = \epsilon_{ij} \left[1.84 \cdot 10^5 \exp\left(-12 \frac{r}{\sigma_{ij}}\right) - 2.25 \left(\frac{\sigma_{ij}}{r}\right)^6 \right] \quad (\text{S3.9})$$

The two parameters σ_{ij} and ϵ_{ij} are the equilibrium distance and the well depth of the potential. These parameters are typically determined with empirical mixing rules for the interaction between atom i and atom j :

$$\sigma_{ij} = \sigma_i + \sigma_j \quad \text{and} \quad \epsilon_{ij} = \sqrt{\epsilon_i \epsilon_j} \quad (\text{S3.10})$$

and these parameters were taken from the MM3 force field for every atom and are tabulated in Ref. 59. In MM3, the 1-2 and 1-3 interactions are discarded to avoid a strong overestimation of the repulsion terms.

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